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Revision 0

KEY WORDS:

Saltstone Disposal Facility

Performance Assessment

Closure Cap

**SALTSTONE DISPOSAL FACILITY
MECHANICALLY STABILIZED EARTH VAULT
CLOSURE CAP DEGRADATION BASE CASE:
INSTITUTIONAL CONTROL TO PINE FOREST SCENARIO (U)**

DECEMBER 18, 2003

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LIST OF ACRONYMS AND ABBREVIATIONS

ACRONYMS

CN	Curve Number
FC	field capacity
FML	flexible membrane liner
GCL	geosynthetic clay liner
GSE	GSE Lining Technology, Inc.
HELP	Hydrologic Evaluation of Landfill Performance
MMES	Martin Marietta Energy Systems, Inc.
PA	Performance Assessment
SCS	Soil Conservation Service
SDF	Saltstone Disposal Facility
SRP	Savannah River Plant
SRS	Savannah River Site
U.S.	United States
USCS	Unified Soil Classification System
USLE	Universal Soil Loss Equation
USDA	United States Department of Agriculture
USEPA	United States Environmental Protection Agency
WP	wilting point
WSRC	Westinghouse Savannah River Company

LIST OF ACRONYMS AND ABBREVIATIONS

ABBREVIATIONS

A	Area
A	Universal Soil Loss Equation soil loss
C	Universal Soil Loss Equation vegetative cover factor
cm	centimeter
cm ²	square centimeter
cm ³	cubic centimeter
cu	cubic
d	thickness or depth
D	diameter
F	fraction
ft	feet
ft ²	square feet
ft ³	cubic feet
ft-msl	feet above mean sea level
g	gram
hr	hour
in	inch
Instal.	installation
K	saturated hydraulic conductivity
K	Universal Soil Loss Equation soil erodibility factor
L	liter
lbs	pounds
LS	Universal Soil Loss Equation slope length and steepness factor
m	meter
m ³	cubic meter
mg	milligram
mil	thousandth of an inch
mph	miles per hour

LIST OF ACRONYMS AND ABBREVIATIONS**ABBREVIATIONS (continued)**

n	porosity
N	no
P	Universal Soil Loss Equation erosion control practice factor
R	Universal Soil Loss Equation rainfall erosion index
Recirc.	Recirculation
s	second
Sat. Hyd. Cond.	saturated hydraulic conductivity
sec	second
STD.	Standard
VEG.	vegetative
Vol	volume
Y	yes
yr	year
ρ_b	bulk density
ρ_p	particle density
'	foot
"	inch
%	percent
#	number
/	per

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1.0 EXECUTIVE SUMMARY

As part of the current Saltstone Disposal Facility (SDF) Performance Assessment (PA) revision, the closure cap configuration was reevaluated and closure cap degradation mechanisms and their impact upon infiltration through the closure cap was evaluated for the existing SDF concrete vaults (i.e. vaults 1 and 4) for the base case land use scenario (i.e. institutional control to pine forest scenario) and documented in Phifer and Nelson (2003). The closure cap configuration was modified from a compacted kaolin barrier layer concept to a geosynthetic clay layer (GCL) barrier layer concept. The degradation mechanisms developed included pine forest succession, erosion, and colloidal clay migration. These degradation mechanisms resulted in changes in the hydraulic properties of the closure cap layers and resulting increases in infiltration through the closure cap over time.

Subsequently, Winship (2003) recommended that future SDF vaults be based upon Mechanically Stabilized Earth (MSE) technology rather than poured in place concrete technology. Due to these recommended SDF vault changes, the closure cap degradation mechanisms and their impact upon infiltration through the closure cap has been reevaluated for the proposed MSE vaults for the base case land use scenario (i.e. institutional control to pine forest scenario). This has been conducted as part of the PA revision and as documented herein. This land use scenario assumes a 100-year institutional control period following final SDF closure during which the closure cap is maintained. At the end of institutional control, it is assumed that a pine forest succeeds the cap's original bamboo cover. Infiltration through the upper hydraulic barrier layer of the closure cap as determined by this evaluation will be utilized as the infiltration input to subsequent PORFLOW vadose zone contaminant transport modeling, which will also be performed as part of the PA revision.

The impact of pine forest succession, erosion, and colloidal clay migration as degradation mechanisms on the hydraulic properties of the closure cap layers over time has been estimated and the resulting infiltration through the MSE vault closure cap has been evaluated. The primary changes caused by the degradation mechanisms that result in increased infiltration are the formation of holes in the upper GCL by pine forest succession and the reduction in the saturated hydraulic conductivity of the drainage layers due to colloidal clay migration into the layers. Erosion can also result in significant increases in infiltration if it causes the removal of soil layers, which provide water storage for the promotion of evapotranspiration.

For the institutional control to pine forest, land use scenario, infiltration through the upper GCL was estimated at approximately 0.36 inches/year under initial intact conditions. Such infiltration increased from approximately 0.41 inches/year at the end of institutional control (i.e. year 100) to approximately 12.0 inches/year at year 1000 in nearly a linear fashion. From year 1800 to year 10,000 the infiltration approaches 14.1 inches/year. At year 1800 approximately 0.3 percent of the GCL area had holes due to root penetration resulting in an infiltration near that of typical background infiltration (i.e. as though the GCL were not there at all). A very small area of holes essentially controlled the hydraulic performance of the GCL. It is assumed that the infiltration remains at 14.1 inches/year until approximately year 97,000, at which point the thickness of the upper backfill above the erosion barrier is equal to the assumed evapotranspiration zone depth of 22 inches (Phifer and Nelson 2003). After year 97,000 it is assumed that infiltration through the upper GCL increases linearly from 14.1 inches/year to a maximum of 18.1 inches/year in year 280,000. As the thickness of the upper backfill layer decreases below 22 inches the evapotranspiration zone extends into the erosion barrier, which provides inadequate water storage for the promotion of evapotranspiration. This results in the infiltration increase over 14.1 inches/year after year 97,000.

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2.0 INTRODUCTION

The existing Saltstone Disposal Facility (SDF) vaults (i.e. vaults 1 and 4) are above grade, roofed, reinforced concrete vaults into which Saltstone is poured. Saltstone is a grout consisting of low-level radioactive salt solution mixed with blast furnace slag, flyash, and cement, which solidifies to form a dense, microporous, monolithic, low-level radioactive waste. It is anticipated that active Saltstone disposal operations will last for approximately 30 years. During the operations period the roofed, Saltstone-filled vaults remain above grade (interim closure). Final closure of all the filled vaults is not anticipated until near or at the end of the operational period and will consist of the placement of a closure cap over the vaults. (MMES 1992; Cook et al. 2000; Cook et al. 2002)

As part of the current SDF Performance Assessment (PA) revision, the closure cap configuration was reevaluated and closure cap degradation mechanisms and their impact upon infiltration through the closure cap was evaluated for the existing SDF concrete vaults for the base case land use scenario (i.e. institutional control to pine forest scenario) and documented in Phifer and Nelson (2003). The degradation mechanisms developed included pine forest succession, erosion, and colloidal clay migration. These degradation mechanisms resulted in changes in the hydraulic properties of the closure cap layers and resulting increases in infiltration through the closure cap over time. Phifer and Nelson (2003) additionally recommended that the SDF closure cap barrier layer be changed from a compacted kaolin layer to a geosynthetic clay layer (GCL). It was recommended that the revised SDF closure cap consist of the following major components from the ground surface to the top of the vault roof (i.e., top to bottom), as shown in Figure 2.0-1 (Phifer and Nelson 2003):

- Bamboo vegetative cover to promote evapotranspiration,
- 0.15 m (6 inch) vegetative soil (i.e., topsoil) at a three percent slope,
- 0.76 m (30 inch) upper backfill layer (i.e., structural fill),
- 0.3 m (12 inch) erosion barrier consisting of 2-inch to 6-inch granite stone with a d_{50} (i.e. median size) of 4 inches,
- 0.3 m (12 inch) middle backfill layer to provide additional water storage for the promotion of evapotranspiration in case the topsoil and upper backfill are eroded away,
- A geotextile filter fabric to minimize the migration of fines into the underlying drainage layer,
- 0.3 m (12 inch) upper drainage layer with an initial saturated hydraulic conductivity of 0.1 cm/s and a slope of three percent,
- 0.0051 m (0.2 inch) geosynthetic clay liner (GCL),
- A minimum 1.49 m (58.57 inch) lower backfill (this layer will vary in thickness) which is used to change the direction of slope by 90 degrees and increase the slope to three percent,
- A geotextile filter fabric to minimize the migration of fines into the underlying drainage layer,
- 0.61 m (24 inch) lower drainage layer with an initial saturated hydraulic conductivity of 0.1 cm/s and conforming to vault roof slope, and
- 0.0051 m (0.2 inch) GCL.

Subsequently, Winship (2003) recommended that future SDF vaults be based upon Mechanically Stabilized Earth (MSE) technology and consist of the following major components from the roof to the floor of the vault, as shown in Figure 2.0-2:

- 60 mil High Density Polyethylene (HDPE) membrane,

- 21 inch concrete roof at an 11.4 percent slope,
- 35 feet of Saltstone,
- 12 inch drainage layer with a saturated hydraulic conductivity of 0.1 cm/s and a slope of two percent,
- 0.0051 m (0.2 inch) geosynthetic clay liner (GCL),
- 60 mil HDPE membrane, and
- 12 inch concrete floor slab.

Due to these recommended SDF vault changes, the closure cap degradation mechanisms and their impact upon infiltration through the closure cap has been reevaluated for the proposed MSE vaults for the base case land use scenario (i.e. institutional control to pine forest scenario). This has been conducted as part of the PA revision and as documented herein. This land use scenario assumes a 100-year institutional control period following final SDF closure during which the closure cap is maintained. At the end of institutional control, it is assumed that a pine forest succeeds the cap's original bamboo cover. Infiltration through the upper hydraulic barrier layer of the closure cap as determined by this evaluation will be utilized as the infiltration input to subsequent PORFLOW vadose zone contaminant transport modeling, which will also be performed as part of the PA revision.

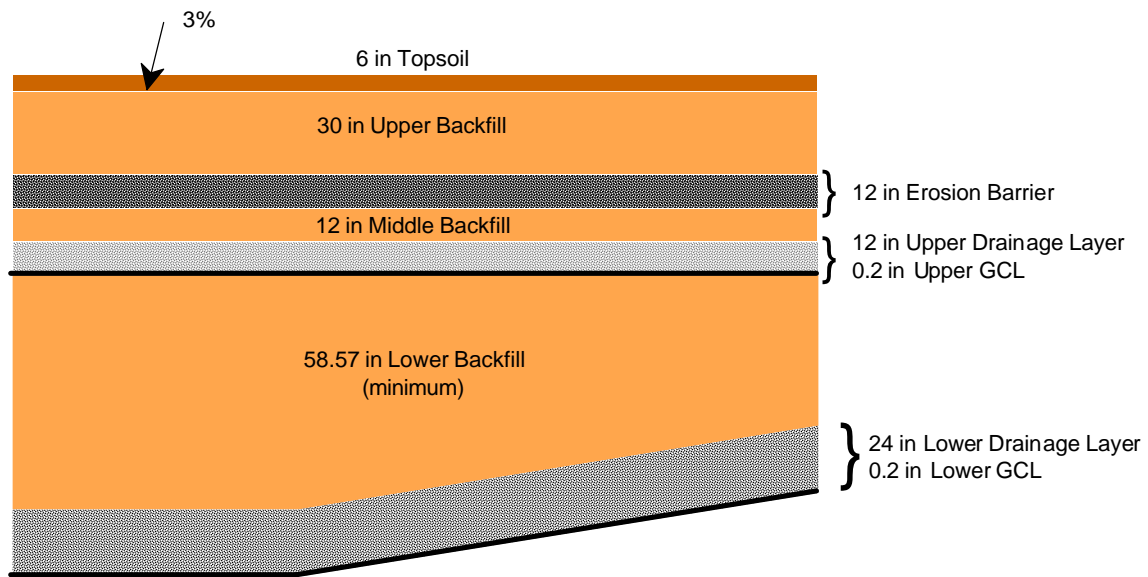


Figure 2.0-1. Saltstone Disposal Facility Closure Cap

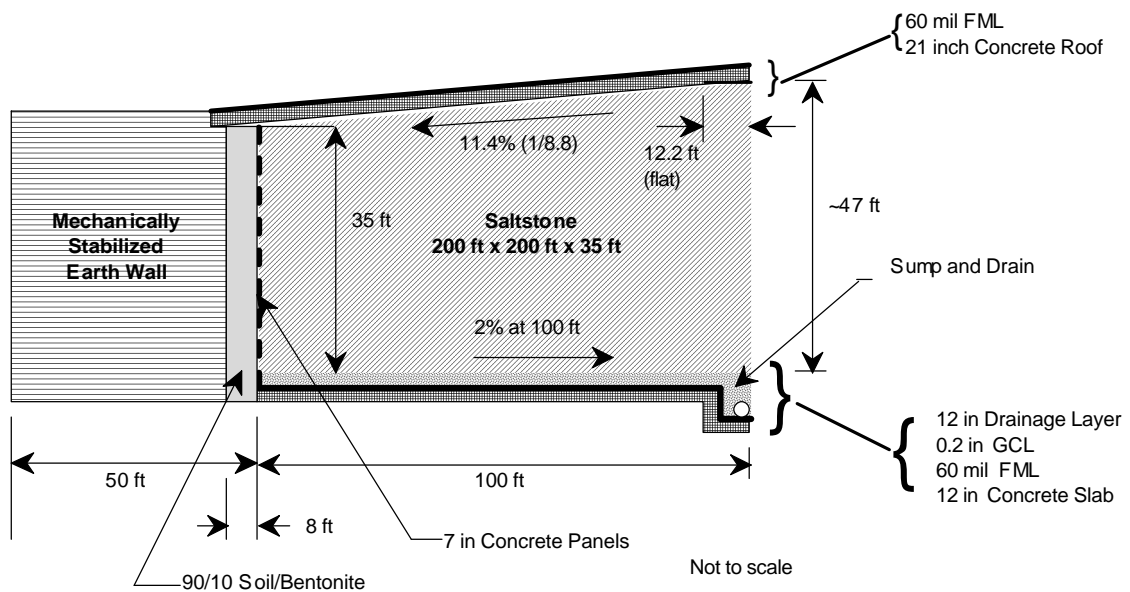


Figure 2.0-2. Saltstone Disposal Facility MSE Vault

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3.0 INTACT CLOSURE CAP INFILTRATION

3.1 Intact SDF GCL Closure Cap Footprint, Configuration, and Properties

The MSE vault layout presented in Figure 3.1-1 has been utilized for the evaluation presented herein. This layout assumes that three 200-foot by 200-foot MSE vaults are placed between existing vaults 1 and 4. The layout is based upon the following:

- The recommendations outlined within Appendix 7.5 of Winship 2003, and
- The Saltstone Project preference to initially locate MSE vaults between existing vaults 1 and 4.

Based upon this layout, a closure cap footprint and drainage system configuration (Figure 3.1-2) has been developed. The drainage system configuration is also based upon the drainage system previously selected by Phifer and Nelson (2003) for the existing vault design and layout (i.e. the concrete vaults). Figure 3.1-3 presents the MSE vault and closure cap cross-section as previously described in Section 2.0. The assumption has been made that the lower GCL only covers the MSE vault roof whereas the upper GCL is continuous over the entire closure cap footprint presented in Figure 3.1-2. Table 3.1-1 presents the intact SDF GCL closure cap configuration and soil properties as developed by Phifer and Nelson (2003).

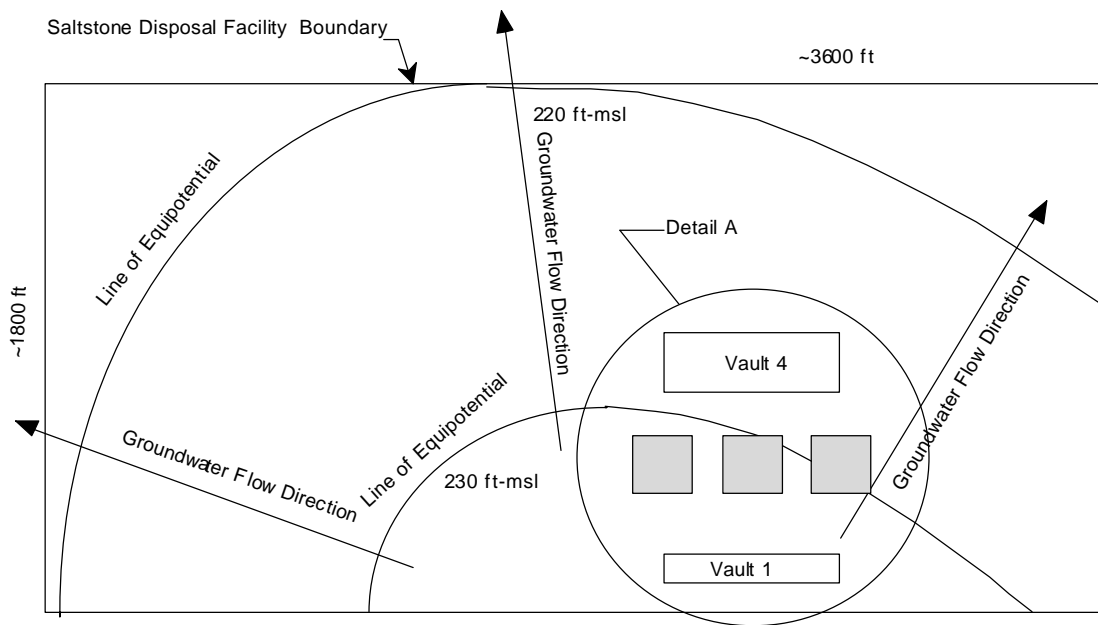


Figure 3.1-1. MSE Vault Layout

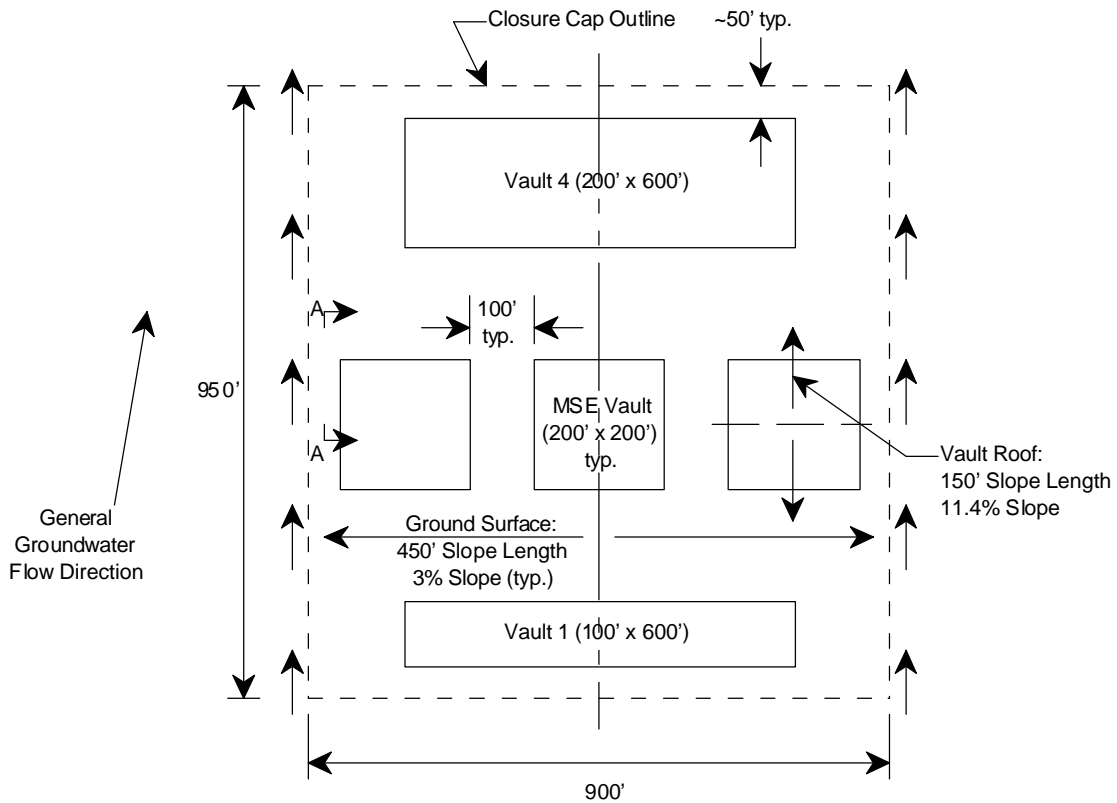


Figure 3.1-2. Closure Cap Footprint and Drainage System (Detail A)

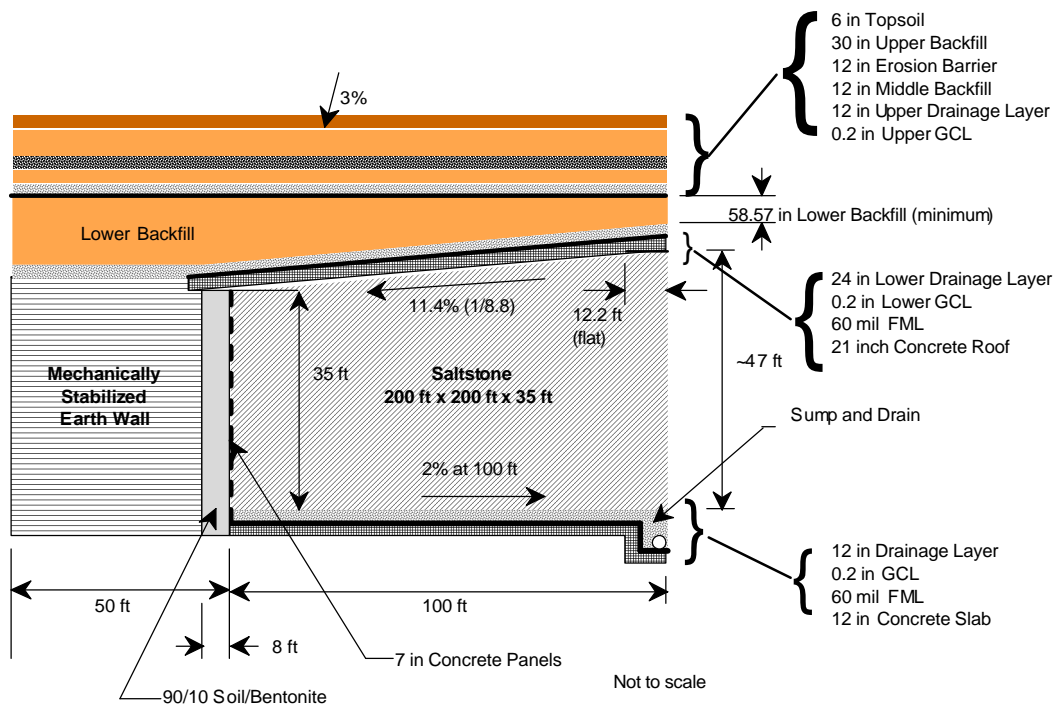


Figure 3.1-3. MSE Vault and Closure Cap Cross-Section (Section A-A)

Table 3.1-1. Intact SDF GCL Closure Cap Configuration and Properties (Phifer and Nelson 2003)

Layer	Thickness (inches)	Saturated Hydraulic Conductivity (cm/sec)	Total Porosity (Vol/Vol)	Field Capacity (Vol/Vol)	Wilting Point (Vol/Vol)
Topsoil ¹	6	1.00E-03	0.4	0.11	0.058
Upper Backfill ¹	30	1.00E-04	0.37	0.24	0.136
Erosion Barrier ²	12	3.97E-04	0.06	0.056	0.052
Middle Backfill ¹	12	1.00E-04	0.37	0.24	0.136
Geotextile Filter Fabric ³	-	-	-	-	-
Upper Drainage Layer ¹	12	1.00E-01	0.38	0.08	0.013
Upper GCL	0.2 ⁴	5.00E-09 ⁵	0.75 ⁶	0.747 ⁶	0.40 ⁶
Lower Backfill ¹	58.57 (minimum)	1.00E-04	0.37	0.24	0.136
Geotextile Filter Fabric ⁵	-	-	-	-	-
Lower Drainage Layer ¹	24	1.00E-01	0.38	0.08	0.013
Lower GCL	0.2 ⁴	5.00E-09 ⁵	0.75 ⁶	0.747 ⁶	0.40 ⁶

¹ WSRC 2002a² Phifer and Nelson 2003³ It is assumed that a geotextile filter fabric will be placed above the drainage layers to minimize the infiltration of fines from the overlying layers into the drainage layer. However it is not necessary to include the filter fabric in the HELP models.⁴ USEPA 2001⁵ GSE 2002⁶ USEPA 1994a and USEPA 1994b

3.2 HELP Model and Generic Input Data

The Hydrologic Evaluation of Landfill Performance (HELP) model has been utilized to conduct the evaluation of the impact of closure cap degradation upon infiltration for the closure cap described in Section 3.1. The HELP model is a quasi-two-dimensional water balance model designed to conduct landfill water balance analyses. The model requires the input of weather, soil, and design data. It provides estimates of runoff, evapotranspiration, lateral drainage, vertical percolation (infiltration), hydraulic head, and water storage for the evaluation of various landfill designs. Personnel at the U.S. Army Engineer Waterways Experiment Station in Vicksburg, Mississippi developed the HELP model, under an interagency agreement with the U.S. Environmental Protection Agency (USEPA). HELP model version 3.07, issued on November 1, 1997, is the latest version of the model available from the Waterways Experiment Station (USEPA 1994a and USEPA 1994b). (WSRC 2002a)

The HELP model requires the input of evapotranspiration, precipitation, temperature, and solar radiation data. Phifer and Nelson (2003) developed the weather data utilized to conduct this

evaluation. The HELP model weather data input files, which were utilized for all HELP model runs, are provided in the following appendices:

- Appendix A, Augusta Synthetic Precipitation Modified with SRS Specific Average Monthly Precipitation Data over 100 Years (file name: Zprec.d4),
- Appendix B, Augusta Synthetic Temperature Modified with SRS Specific Average Monthly Temperature Data over 100 Years (file name: Ztemp.d7),
- Appendix C, Augusta Synthetic Solar Radiation Data over 100 Years (file name: Zsolar.d13), and
- Appendix D, Augusta Evapotranspiration Data (file name: Zevap.d11).

Table 3.2-1 provides a listing of generic input parameters (i.e., HELP model query) and the associated values selected. Use of selected fixed values for these HELP model queries provides compatibility between the different HELP model runs. The landfill area is based upon the Figure 3.1-2 length (950 feet) and width (900 feet), which results in a surface area of 760,000 feet squared or 19.6 acres. It has been assumed that the final covers are appropriately sloped so that 100 percent of the covers allow runoff to occur (i.e., there are no depressions). A yes response has been provided to the HELP model query, which asks, “Do you want to specify initial moisture storage? (Y/N).” The amount of water or snow on the surface of the covers was assumed to be zero as the initial model condition.

Table 3.2-1. Generic Input Parameter Values – Area and Initial Moisture

Input Parameter (HELP Model Query)	Generic Input Parameter Value
Landfill area	19.63 acres
Percent of area where runoff is possible	100%
Do you want to specify initial moisture storage? (Y/N)	Y
Amount of water or snow on surface	0 in.

As stated the initial moisture storage has been specified for all soil layers. While the initial moisture storage is not a fixed value for all runs, a fixed method of selecting the initial moisture storage value has been utilized for consistency. The initial, soil moisture storage value has been selected as follows:

- The initial moisture storage of soil layers designated as either a vertical percolation layer or a lateral drainage layer was set at the field capacity of the soil.
- The initial moisture storage of soil layers designated as a barrier soil liner was set at the porosity of the soil.

The Soil Conservation Service (SCS) runoff curve number (CN) is another required HELP model input parameter that has been made consistent. The HELP model provides three options to specify the CN. The option that produces a HELP model computed curve number, based on surface slope and slope length, soil texture of the top layer, and vegetation, was utilized. Table 3.2-2 provides the input values of surface slope and slope length, soil texture of the top layer, and vegetation that were utilized to produce the HELP model computed curve number. The 3 percent slope is that specified for the top surface of the Saltstone final cover within the Saltstone closure plan (Cook et al. 2000). The 450-foot slope length is based upon Figure 3.1-2. The soil texture selected as an input for calculation of the CN is a loamy fine sand per the United States Department of Agriculture (USDA) and a silty sand per Unified Soil Classification System (USCS), since it closely represents the typical vegetative soil layers utilized at the Savannah River Site (SRS). The corresponding number in the HELP default soil texture list is 5. Based upon these input parameter values the HELP model computed a CN of 54.4.

Table 3.2-2. Generic Input Parameter Values – Curve Number (CN)

CN Input Parameter (HELP Model Query)	CN Input Parameter Value
Slope	3%
Slope length	450 ft
Soil Texture	5 (HELP model default soil texture)
Vegetation	4 (i.e., a good stand of grass)
HELP Model Computed Curve Number	54.4

3.3 Intact Closure Cap Infiltration

HELP modeling of the Table 3.1-1 intact SDF MSE vault closure cap configuration has been performed utilizing the Section 3.2 generic input data. As documented in Phifer and Nelson (2003), the HELP model does not need to include the vault in order to obtain an appropriate infiltration through the upper GCL. Therefore the vault has not been included in any of the HELP modeling presented herein. Based upon this modeling the infiltration through the upper GCL has been estimated to be 0.36 inches per year for intact conditions. The following appendix provides the detailed HELP model, input data and output file for the intact condition:

- Appendix E, Intact SDF MSE Vault Closure Cap (0 Years): HELP Model Input Data and Output File (output file name: ZMSEIout.OUT)

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4.0 CLOSURE CAP DEGRADATION

The following three primary closure cap degradation mechanisms have been assumed to significantly impact the infiltration through the closure cap over time:

- Pine forest succession
- Erosion
- Colloidal clay migration

Phifer and Nelson (2003) discussed each of these degradation mechanisms in detail.

4.1 Pine Forest Succession

According to the PA and Closure Plan the SDF closure cap will be vegetated with bamboo. Bamboo is a shallow-rooted species that quickly establishes a dense ground cover and evapotranspires year-round in the SRS climate. Pine trees are the most deeply rooted naturally occurring plants at SRS. (MMES 1992; Cook et al. 2000). The institutional control to pine forest, land use scenario evaluated herein assumes a 100-year institutional control period following final SDF closure during which the closure cap is maintained. It is assumed that a pine forest begins to encroach upon the bamboo at the end of institutional control, when the closure cap is no longer maintained.

The following assumptions, which were made relative to the succession of bamboo by a pine forest by Phifer and Nelson (2003), have also been utilized for this evaluation:

- 200 years after the end of institutional control it is assumed that the entire cap is dominated by pine.
- Complete turnover of the 400 mature trees per acre occurs every 100 years (in a staggered manner).
- There are 400 mature trees per acre with 4 roots to 6 feet and 1 root to 12 feet. The roots are 3 inches in diameter at a depth of 1 foot and 0.25 inches in diameter at either 6 or 12 feet, whichever is applicable.

4.2 Erosion

The topsoil and upper backfill layers, which are located above the erosion barrier, are subject to erosion. For the institutional control to pine forest land use scenario, it is assumed that the closure cap will be vegetated with bamboo during the institutional control period, with a combination of bamboo and pine trees for 200 years immediately following the institutional control period, and with a pine forest thereafter. The projected erosion rate for both the topsoil and upper backfill layers has been determined utilizing the Universal Soil Loss Equation (Horton and Wilhite 1978; Goldman et al. 1986). The Universal Soil Loss Equation (USLE) is expressed as:

$$A = R \times K \times LS \times C \times P \quad (\text{Eq. 5.2-1})$$

where

A = soil loss (tons/acre/year)

R = rainfall erosion index (100 ft-ton/acre per in/hr)

K = soil erodibility factor, tons/acre per unit of R

LS = slope length and steepness factor, dimensionless

C = vegetative cover factor, dimensionless

P = erosion control practice factor, dimensionless

Table 4.2-1 presents the USLE parameter values utilized and the source of the values for both the topsoil and backfill.

Table 4.2-1. USLE Parameter Values

USLE Parameter	Value Utilized	Source
R for SRS location	260	Horton and Wilhite 1978
K for topsoil	0.28	Phifer and Nelson 2003 and Goldman et al. 1986 Figure 5.6
K for backfill	0.20	Phifer and Nelson 2003 and Goldman et al. 1986 Figure 5.6
LS for 450-foot 3% slope (see Figure 3.1-2)	0.45	Goldman et al. 1986 Table 5.5
C for both bamboo and pine forest	0.001	Horton and Wilhite 1978
P for no supporting practices	1	Not applicable

Based upon the Universal Soil Loss Equation and the Table 4.2-1 parameter values the following soil losses were estimated:

- Topsoil with a natural successional forest has an estimated soil loss of 0.0328 tons/acre/year ($A = 260 \times 0.28 \times 0.45 \times 0.001 \times 1$). Based upon the dry bulk density the estimated soil loss can be converted to a loss in terms of depth of loss per year. From Jones and Phifer (2002), the dry bulk density of topsoil was taken as 90 lbs/ft³. Topsoil with a natural successional forest has an estimated depth of soil loss of approximately 2.0E-04 inches/year.

$$(Loss = \frac{0.0328 \text{ tons / acre / year} \times 2000 \text{ lbs / ton} \times 12 \text{ inches / foot}}{43560 \text{ ft}^2 / \text{acre} \times 90 \text{ lbs / ft}^3}).$$

- Backfill with a natural successional forest has an estimated soil loss of 0.0234 tons/acre/year ($A = 260 \times 0.20 \times 0.45 \times 0.001 \times 1$). Based upon the dry bulk density the estimated soil loss can be converted to a loss in terms of depth of loss per year. From Jones and Phifer (2002), the dry bulk density of backfill was taken as 104 lbs/ft³. Backfill with a natural successional forest has an estimated depth of soil loss of approximately 1.2E-04 inches/year.

$$(Loss = \frac{0.0234 \text{ tons / acre / year} \times 2000 \text{ lbs / ton} \times 12 \text{ inches / foot}}{43560 \text{ ft}^2 / \text{acre} \times 104 \text{ lbs / ft}^3}).$$

4.3 Colloidal Clay Migration

It is assumed that colloidal clay migrates from overlying backfill layers and accumulates in the drainage layers reducing the saturated hydraulic conductivity of the drainage layers over time. As previously documented in Phifer and Nelson (2003), it will be assumed that water-flux driven colloidal clay migration at a concentration of 63 mg/L occurs from overlying backfill layers to the drainage layers. It will be further assumed that the colloidal clay accumulates in the drainage layer from the bottom up filling the void space of the drainage layer with clay at a density of 1.1 g/cm³ (Hillel 1982).

4.4 Closure Cap Degradation Summary

Based upon the assumed closure cap degradation mechanisms, pine forest succession, erosion, and colloidal clay migration, a degradation scenario has been assumed for each layer as outlined in Table 4.4-1. These degradation scenarios form the basis for modifying the thickness and hydraulic properties of each layer over time. This information has been utilized in Section 5.0 to determine infiltration through the upper GCL over time.

Table 4.4-1. SDF GCL Closure Cap Layer Degradation Scenarios (Phifer and Nelson 2003)

Layer	Degradation Scenario
Vegetation	Bamboo is maintained during the 100-year institutional control period, pine trees begin to encroach upon the bamboo at the end of institutional control, and a pine forest covers the cap 200 years after the end of institutional control.
Topsoil	Topsoil erosion occurs at 2.0E-04 inches per year.
Upper Backfill	Backfill erosion occurs at 1.2E-04 inches per year, after the topsoil layer has been depleted.
Erosion Control Barrier	Maintenance during institutional control period prevents degradation of the erosion control barrier. However pine forest succession and associated root penetration results in holes through the erosion control barrier. This does not impact its ability to function as an erosion barrier, however it allows the overlying backfill to fill the holes left after the roots decompose. Since degradation of the erosion barrier is assumed to be caused by intrusion of the overlying backfill following root decomposition, erosion barrier degradation will be assumed to cease once the upper backfill is eroded to three inches thick.
Middle Backfill	Colloidal clay migration from the 1-foot-thick middle backfill to the underlying 1-foot-thick upper drainage layer causes the saturated hydraulic conductivity to increase over time.
Geotextile Filter Fabric	For purposes of colloidal clay migration into the underlying drainage layer the geotextile filter fabric is assumed to be ineffective over the time period under consideration.
Upper Drainage Layer	Colloidal clay migration from the overlying 1-foot-thick backfill into the 1-foot-thick upper drainage layer causes the saturated hydraulic conductivity to decrease over time.
Upper GCL	Maintenance during institutional control period prevents degradation of the upper GCL. However pine forest succession and associated root penetration results in holes through the GCL. This allows the overlying drainage layer to fill the holes after the roots decompose.
Lower Backfill	None. While it is assumed that colloidal clay migration from this layer to the underlying lower drainage layer occurs, it is also assumed that the thickness of the lower backfill layer (minimum 5-foot) relative to the lower drainage layer (2-foot) prevents the quantity of clay loss necessary to change the hydraulic properties of the lower backfill.
Geotextile Filter Fabric	For purposes of colloidal clay migration into the underlying drainage layer the geotextile filter fabric is assumed to be ineffective over the time period under consideration.
Lower Drainage Layer	Colloidal clay migration from the overlying minimum 5-foot-thick lower backfill into the 1-foot-thick lower drainage layer reduces its saturated hydraulic conductivity over time.
Lower GCL	None. Pine tree roots do not penetrate to sufficient depth to impact this layer. Additionally, the underlying concrete vault roof along with the GCL produces a hard layer and continuous water saturation within and above these layers so that root elongation is stopped.

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5.0 CLOSURE CAP INFILTRATION

5.1 Degraded Layer Properties over Time

The SDF GCL closure cap initial (0 year) intact layer thickness and hydraulic property values from top to bottom are provided in Table 3.1-1. The degradation scenarios for each layer are provided in Table 4.4-1. Based upon the Table 4.4-1 degradation scenarios, the Table 3.3-1 initial SDF closure cap layer thickness and hydraulic property values have been modified to account for degradation at 100, 300, 550, 1,000, 1,800, 3,400, 5,600 and 10,000 years after closure of the SDF. The following discussions provide additional detail associated with determination of the degraded properties for the erosion barrier, upper GCL, middle backfill, upper drainage layer, and lower drainage layer as originally presented by Phifer and Nelson (2003).

5.1.1 Erosion Barrier

Maintenance during the institutional control period prevents degradation of the erosion barrier. However pine forest succession and associated root penetration results in holes through the erosion control barrier. This does not impact its ability to function as an erosion barrier, however it allows the overlying backfill to fill the holes after the roots decompose. It is assumed that the hydraulic conductivity of the infiltrating backfill increases one order of magnitude (i.e. from $1.0\text{E-}04$ to $1.0\text{E-}03$ cm/s) when it fills the hole since it will not be mechanically compacted at that time. The equivalent hydraulic properties of the overall erosion barrier change as the area of holes filled with backfill material increases with time. The equivalent hydraulic properties have been estimated over time by area proportioning the properties between that of the intact erosion barrier and infiltrating backfill.

5.1.2 Upper GCL

Maintenance during the institutional control period prevents degradation of the upper GCL. However pine forest succession and associated root penetration results in holes through the erosion barrier. This allows the overlying drainage layer to fill the holes after the roots decompose. The holes in the GCL essentially act as direct conduits from the upper drainage layer to the lower backfill layer. When saturated conditions occur in the drainage layer after major precipitation events, cones of depression are created around the holes in the GCL with a radius of influence much greater than the radius of the hole. This means that a small area of GCL holes can greatly reduce the lateral flow of water in the drainage layer and increase the vertical flow into the lower backfill. Due to the significant influence of holes in the GCL to the quantity of infiltration, the use of equivalent hydraulic properties is not appropriate, since it does not consider the radius of influence associated with holes. Therefore, within the HELP model the degraded GCL has been modeled as a geomembrane liner with leakage through holes. The HELP model considers both water flux through intact portions of the geomembrane using an “equivalent geomembrane hydraulic conductivity” and water flux through holes in the geomembrane. The HELP model does not assign a porosity, field capacity, or wilting point to geomembranes, however this is not considered essential to the GCL, since it is assumed that the GCL will remain fully saturated and it is below the depth where evapotranspiration is assumed to occur. The HELP model allows the input of up to 999,999 one square centimeter installation defects for a geomembrane liner. Therefore the calculated area of holes created by root penetration has been converted into an equivalent number of one square centimeter installation defects for input to the HELP model. Excellent contact is assumed between the GCL and underlying backfill layer as a HELP model input, since the GCL is put in dry and swells into the surrounding soil as it hydrates.

5.1.3 Middle Backfill and Upper Drainage Layer

It is assumed that water-flux driven colloidal-clay migration from the 1-foot-thick middle backfill to the underlying 1-foot-thick upper drainage layer causes the middle backfill saturated hydraulic conductivity to increase over time and that of the upper drainage layer to decrease over time. It has been assumed that clay migration occurs out of the backfill into the drainage layer with the water flux containing 63 mg/L of colloidal clay. Since both layers are of the same thickness and the middle backfill layer has limited clay content, it has been assumed that half the clay content of the backfill will migrate into the drainage layer. At which point the two layers essentially become the same material and material property changes cease. Based upon this it will be assumed that the endpoint saturated hydraulic conductivity of the layers will become that of the log mid-point between the initial backfill and upper drainage layer conditions. It will also be assumed that the endpoint porosity, field capacity, and wilting point will become the arithmetic average of the backfill and upper drainage layer. The hydraulic properties at times prior to the endpoint have been proportioned between that of the endpoint properties and the initial properties based upon the fraction of clay that has migrated out of the backfill.

5.1.4 Lower Drainage Layer

It is assumed that colloidal clay migration from the minimum 5-foot-thick overlying backfill into the 2-foot-thick lower drainage layer is driven by the water flux through the upper GCL. This water flux driven clay migration enters into the lower drainage layer and fills the lower drainage layer from the bottom up. This reduces the saturated hydraulic conductivity of the clay-filled portion from 1.0E-01 to 1.0E-04 cm/s (i.e. to the saturated hydraulic conductivity of the overlying backfill), while the conductivity of the clean portion remains at 1.0E-01 cm/s. As the thickness of the lower drainage layer filled with clay increases, the equivalent hydraulic conductivity of the entire layer decreases. The equivalent horizontal hydraulic conductivity for this layer has been determined from the following equation (Freeze and Cherry 1979):

$$K_h = \sum_{i=1}^n \frac{K_i d_i}{d} \quad (\text{Eq. 6.1-1})$$

where

K_h = equivalent horizontal saturated hydraulic conductivity,

K_i = horizontal saturated hydraulic conductivity of i^{th} layer,

d_i = thickness of i^{th} layer,

d = total thickness

This is different from that assumed for the upper drainage layer, since the lower drainage layer has significantly more backfill overlying it.

5.1.5 Summary Material Properties over Time

The calculations associated with determination of the layer thicknesses and hydraulic property values over time are provided in Appendix F. Table 5.1-1 provides the primary Appendix F, material property results (thickness, saturated hydraulic conductivity, and holes in the upper GCL), for layers which change with time and were utilized in subsequent HELP modeling. The porosity, field capacity, and wilting points are not provided in Table 5.1-1. Values for these parameters are provided in Appendix F.

Table 5.1-1. Material Property Summary Results for HELP Modeling from Appendix F

Year	Vegetation	Topsoil Layer Thickness (inches)	Erosion Barrier Saturated Hydraulic Conductivity (cm/s)	Middle Backfill Layer Saturated Hydraulic Conductivity (cm/s)
0	Bamboo	6	3.97E-04	1.00E-04
100	Bamboo	5.980	3.97E-04	1.20E-04
300	Pine Forest	5.940	3.98E-04	1.60E-04
550	Pine Forest	5.890	3.99E-04	2.30E-04
1,000	Pine Forest	5.800	4.01E-04	4.60E-04
1,800	Pine Forest	5.640	4.06E-04	1.60E-03
3,400	Pine Forest	5.320	4.15E-04	3.20E-03
5,600	Pine Forest	4.880	4.27E-04	3.20E-03
10,000	Pine Forest	4.0	4.51E-04	3.20E-03
Year	Upper Drainage Layer Saturated Hydraulic Conductivity (cm/s)	One Square Centimeter Holes in Upper GCL ¹ (#/acre)	Lower Drainage Layer Saturated Hydraulic Conductivity (cm/s)	
0	1.00E-01	0	1.00E-01	
100	8.60E-02	0	1.00E-01	
300	6.30E-02	7,432	9.98E-02	
550	4.30E-02	26,013	9.89E-02	
1,000	2.10E-02	59,458	9.61E-02	
1,800	6.30E-03	118,916	8.96E-02	
3,400	3.20E-03	237,832	7.56E-02	
5,600	3.20E-03	401,341	5.62E-02	
10,000	3.20E-03	728,360	1.74E-02	

¹ Number of HELP model installation defects

5.2 Degraded Closure Cap Infiltration over Time

Table 5.1-1 and Appendix F data were utilized as input to the HELP model (USEPA 1994a and USEPA 1994b) in order to determine infiltration through the upper GCL at each degraded time step. The following appendices provide the detailed HELP model, input data and output files for each time step:

- Appendix G, Degraded SDF MSE Vault Closure Cap (100 Years): HELP Model Input Data and Output File (output file name: ZMSED1ou.OUT)
- Appendix H, Degraded SDF MSE Vault Closure Cap (300 Years): HELP Model Input Data and Output File (output file name: ZMSED2ou.OUT)
- Appendix I, Degraded SDF MSE Vault Closure Cap (550 Years): HELP Model Input Data and Output File (output file name: ZMSED3ou.OUT)
- Appendix J, Degraded SDF MSE Vault Closure Cap (1,000 Years): HELP Model Input Data and Output File (output file name: ZMSED4ou.OUT)

- Appendix K, Degraded SDF MSE Vault Closure Cap (1,800 Years): HELP Model Input Data and Output File (output file name: ZMSED5ou.OUT)
- Appendix L, Degraded SDF MSE Vault Closure Cap (3,400 Years): HELP Model Input Data and Output File (output file name: ZMSED6ou.OUT)
- Appendix M, Degraded SDF MSE Vault Closure Cap (5,600 Years): HELP Model Input Data and Output File (output file name: ZMSED7ou.OUT)
- Appendix N, Degraded SDF MSE Vault Closure Cap (10,000 Years): HELP Model Input Data and Output File (output file name: ZMSED8ou.OUT)

The following outputs from this evaluation are necessary inputs to the subsequent PORFLOW vadose zone modeling:

- Infiltration through the upper GCL
- Saturated hydraulic conductivity of the 2-foot-thick lower Drainage Layer

Table 5.2-1 provides a summary of these parameter values. Figure 5.2-1 additionally provides the infiltration through the upper GCL over time in graphical format.

Table 5.2-1. Inputs for PORFLOW Vadose Zone Modeling

Year	Infiltration through Upper GCL (in/yr)	Lower Drainage Layer Saturated Hydraulic Conductivity (cm/s)
0	0.36	1.00E-01
100	0.41	1.00E-01
300	3.05	9.98E-02
550	7.90	9.89E-02
1,000	12.04	9.61E-02
1,800	13.76	8.96E-02
3,400	14.03	7.56E-02
5,600	14.08	5.62E-02
10,000	14.09	1.74E-02
11,953	NA	1.00E-04
280,000	18.12	NA

NA = not applicable

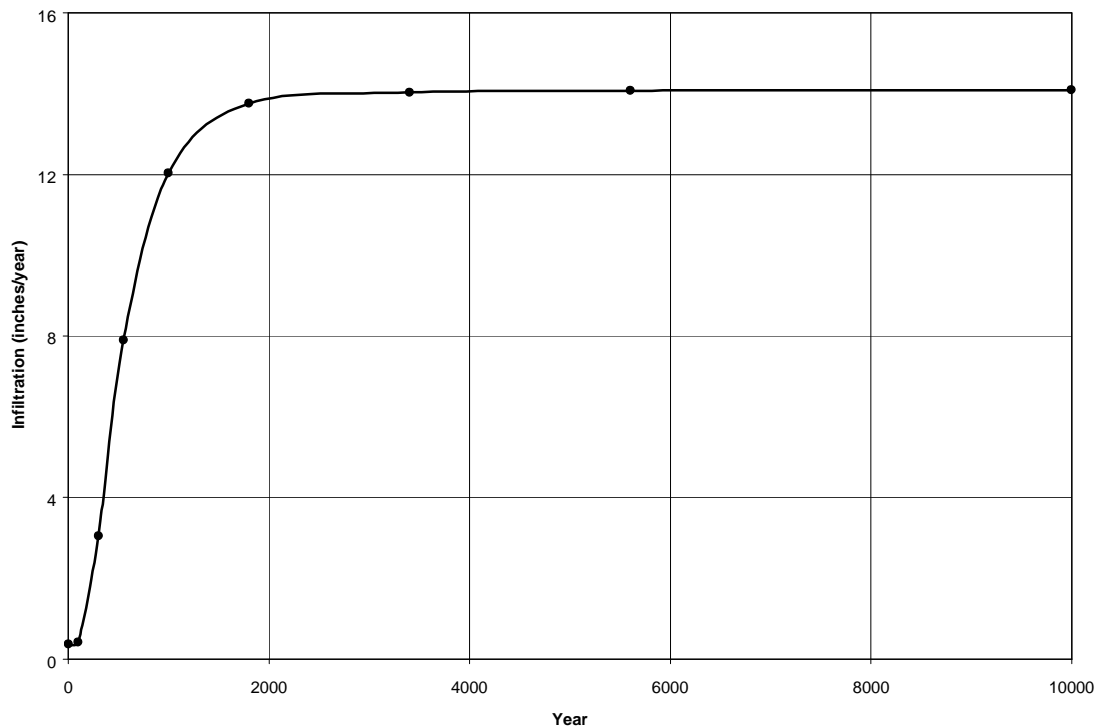


Figure 5.2-1. Infiltration through Upper GCL

5.3 Worse Case Infiltration

The worse case infiltration through the upper GCL and the associated time of occurrence have been determined based upon the following:

- As documented in Phifer and Nelson (2003), worse case infiltration occurs when both the topsoil and upper backfill have eroded away, since the underlying erosion barrier does not provide as efficient water storage for the promotion of evapotranspiration as the topsoil and upper backfill.
- Since degradation of the erosion barrier is assumed to be caused by intrusion of the overlying backfill following root decomposition, erosion barrier degradation will be assumed to cease once the upper backfill is eroded to three inches thick. Therefore erosion barrier properties will be taken as those at complete erosion of the topsoil and upper backfill for determination of the worse case infiltration through the upper GCL. (see Table 4.4-1)
- As outlined in Appendix F, it is assumed that the material properties of the middle backfill and upper drainage layer become the same at year 2246 and remain constant thereafter. Therefore the middle backfill and upper drainage layer material properties will be taken as those determined at year 2246 for determination of the worse case infiltration through the upper GCL.
- The upper GCL becomes ineffective as a barrier layer at year 1800 when holes comprise 0.29 percent of the layer's area (see Appendix F). Therefore for determination of the worse case infiltration the GCL will be assigned as a barrier soil liner with the same material properties as the overlying middle backfill and upper drainage layer at year 2246.

- As previously demonstrated in Appendix F, the material properties of the lower drainage layer do not impact infiltration through the upper GCL. Completely silted in conditions will be assumed for the lower drainage layer for determination of the worse case infiltration.

Appendix F provides the material property calculations based upon the above assumptions and the detailed HELP model input data and output file associated with this worse case infiltration through the upper GCL. The worse case infiltration through the upper GCL was determined to be 18.1 inches/year in year 280,000. This worse case infiltration has been included in Table 5.2-1 for comparison purposes. As seen the infiltration has been estimated at approximately 14.1 inches per year in year 10,000 and 18.1 inches per year in year 280,000. It is assumed that after the topsoil completely erodes and the upper backfill erodes to 22 inches thick in approximately year 97,000 (see Appendix F) that infiltration through the upper GCL would increase linearly from approximately 14.1 inches/year to approximately 18.1 inches/year in year 280,000. This is assumed since the evapotranspiration zone depth utilized in the HELP modeling is 22 inches (Phifer and Nelson 2003).

In addition to the worse case infiltration, the time that the lower drainage layer completely silts in and assumes the properties of the overlying backfill has been estimated to occur in approximately year 12,000 (see Appendix F). This has also been included in Table 5.2-1 as input to the PORFLOW modeling.

6.0 SUMMARY AND CONCLUSIONS

The impact of pine forest succession, erosion, and colloidal clay migration as degradation mechanisms on the hydraulic properties of the closure cap layers over time has been estimated and the resulting infiltration through the MSE vault closure cap has been evaluated. The primary changes caused by the degradation mechanisms that result in increased infiltration are the formation of holes in the upper GCL by pine forest succession and the reduction in the saturated hydraulic conductivity of the drainage layers due to colloidal clay migration into the layers. Erosion can also result in significant increases in infiltration if it causes the removal of soil layers, which provide water storage for the promotion of evapotranspiration.

For the institutional control to pine forest, land use scenario, infiltration through the upper GCL was estimated at approximately 0.36 inches/year under initial intact conditions. Such infiltration increased from approximately 0.41 inches/year at the end of institutional control (i.e. year 100) to approximately 12.0 inches/year at year 1000 in nearly a linear fashion. From year 1800 to year 10,000 the infiltration approaches 14.1 inches/year. At year 1800 approximately 0.3 percent of the GCL area had holes due to root penetration resulting in an infiltration near that of typical background infiltration (i.e. as though the GCL were not there at all). A very small area of holes essentially controlled the hydraulic performance of the GCL. It is assumed that the infiltration remains at 14.1 inches/year until approximately year 97,000, at which point the thickness of the upper backfill above the erosion barrier is equal to the assumed evapotranspiration zone depth of 22 inches (Phifer and Nelson 2003). After year 97,000 it is assumed that infiltration through the upper GCL increases linearly from 14.1 inches/year to a maximum of 18.1 inches/year in year 280,000. As the thickness of the upper backfill layer decreases below 22 inches the evapotranspiration zone extends into the erosion barrier, which provides inadequate water storage for the promotion of evapotranspiration. This results in the infiltration increase over 14.1 inches/year after year 97,000.

Table 5.2-1 provides a summary of the necessary inputs to the subsequent PORFLOW vadose zone modeling including infiltration through the upper GCL and the saturated hydraulic conductivity of the lower drainage layer, side vertical drainage layer, and vault base drainage layer.

Performance of the closure cap relative to infiltration through the upper GCL could be further improved, if necessary, as follows:

- Increasing the depth of the GCL, which would result in smaller diameter root penetrations.
- Placing a suitable biobarrier above the GCL to prevent root penetration into the GCL.

Optimization of layers within the evapotranspiration zone for water storage to promote subsequent evapotranspiration could also possibly be a means of increasing the performance of the closure cap.

A technical report design check of this report and associated calculations has been performed per WSRC (2002b) and documented in Appendix O.

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8.0 APPENDICES

Appendix A	Augusta Synthetic Precipitation Modified with SRS Specific Average Monthly Precipitation Data over 100 Years (file name: Zprec.d4)	A-1
Appendix B	Augusta Synthetic Temperature Modified with SRS Specific Average Monthly Temperature Data over 100 Years (file name: Ztemp.d7)	B-1
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Appendix O	Technical Report Design Checklist	O-1

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Appendix A, Augusta Synthetic Precipitation Modified with SRS Specific Average Monthly Precipitation Data over 100 Years (file name: Zprec.d4)

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Appendix B, Augusta Synthetic Temperature Modified with SRS Specific Average Monthly Temperature Data over 100 Years (file name: Ztemp.d7)

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Appendix C, Augusta Synthetic Solar Radiation Data over 100 Years (file name: Zsolar.d13)

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Appendix D, Augusta Evapotranspiration Data (file name: Zevap.d11)

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Appendix E, Intact SDF MSE Vault Closure Cap (0 Years): HELP Model Input Data and Output File (output file name: ZMSEIout.OUT)

Input Data:

Input Parameter (HELP Model Query)				Generic Input Parameter Value			
Landfill area =				19.63 acres			
Percent of area where runoff is possible =				100%			
Do you want to specify initial moisture storage? (Y/N)				Y			
Amount of water or snow on surface =				0 inches			
CN Input Parameter (HELP Model Query)				CN Input Parameter Value			
Slope =				3 %			
Slope length =				450 ft			
Soil Texture =				5 (HELP model default soil texture)			
Vegetation =				4 (i.e., a good stand of grass)			
HELP Model Computed Curve Number = 54.4							
Layer			Layer Number		Layer Type		
Topsoil			1		1 (vertical percolation layer)		
Upper Backfill			2		1 (vertical percolation layer)		
Erosion Barrier			3		1 (vertical percolation layer)		
Middle Backfill			4		1 (vertical percolation layer)		
Upper Drainage Layer			5		2 (lateral drainage layer)		
Upper GCL			6		3 (barrier soil liner)		
Lower Backfill			7		1 (vertical percolation layer)		
Lower Drainage Layer			8		2 (lateral drainage layer)		
Lower GCL			9		3 (barrier soil liner)		
	Layer Type	Layer Thickness (in)	Soil Texture No.	Total Porosity (Vol/Vol)	Field Capacity (Vol/Vol)	Wilting Point (Vol/Vol)	Initial Moisture (Vol/Vol)
1	1	6		0.4	0.11	0.058	0.11
2	1	30		0.37	0.24	0.136	0.24
3	1	12		0.06	0.056	0.052	0.056
4	1	12		0.37	0.24	0.136	0.24
5	2	12		0.38	0.08	0.013	0.08
6	3	0.2		0.75	0.747	0.40	0.75
7	1	58.57		0.37	0.24	0.136	0.24
8	2	24		0.38	0.08	0.013	0.08
9	3	0.2		0.75	0.747	0.40	0.75

Input Data (continued):

	Layer Type	Sat. Hyd. Conductivity * (cm/sec)	Drainage Length (ft)	Drain Slope (%)	Leachate Recirc. (%)	Recirc. to Layer (#)	Subsurface Inflow (in/yr)
1	1	1.00E-03					
2	1	1.00E-04					
3	1	3.97E-04					
4	1	1.00E-04					
5	2	1.00E-01	450	3			
6	3	5.00E-09					
7	1	1.00E-04					
8	2	1.00E-01	150	11.4			
9	3	5.00E-09					
	Layer Type	Geomembrane Pinhole Density (#/acre)	Geomembrane Instal. Defects (#/acre)	Geomembrane Placement Quality	Geotextile Transmissivity (cm ² /sec)		
1	1						
2	1						
3	1						
4	1						
5	2						
6	3						
7	1						
8	2						
9	3						

The lack of values in the table for particular parameters in particular layers denotes that no HELP model input was required for that parameter in that layer. No data are missing from the table.

* The HELP model output often produces an increased number of significant digits for the Effective Saturated Hydraulic Conductivity over that of the actual input.

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**
**      HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE
**      HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)
**      DEVELOPED BY ENVIRONMENTAL LABORATORY
**      USAE WATERWAYS EXPERIMENT STATION
**      FOR USEPA RISK REDUCTION ENGINEERING LABORATORY
**
**
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*****

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PRECIPITATION DATA FILE:  D:\HELP3\Hweather\ZPREC.D4
TEMPERATURE DATA FILE:   D:\HELP3\Hweather\ZTEMP.D7
SOLAR RADIATION DATA FILE: D:\HELP3\Hweather\ZSOLAR.D13
EVAPOTRANSPIRATION DATA:  D:\HELP3\Hweather\ZEVAP.D11
SOIL AND DESIGN DATA FILE: D:\HELP3\Hsdfmse\ZMSEI.D10
OUTPUT DATA FILE:         D:\HELP3\Hsdfmse\ZMSEIout.OUT

```

TIME: 14:56 DATE: 11/13/2003

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*****

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TITLE: Intact SDF MSE Vault Closure Cap - 0 years

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NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER
WERE SPECIFIED BY THE USER.

LAYER 1

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

```

THICKNESS           =      6.00  INCHES
POROSITY             =      0.4000 VOL/VOL
FIELD CAPACITY       =      0.1100 VOL/VOL
WILTING POINT        =      0.0580 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.1100 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.100000005000E-02 CM/SEC

```

LAYER 2

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

```

THICKNESS           =     30.00  INCHES
POROSITY             =      0.3700 VOL/VOL
FIELD CAPACITY       =      0.2400 VOL/VOL
WILTING POINT        =      0.1360 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.2400 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.999999975000E-04 CM/SEC

```

LAYER 3

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.0600	VOL/VOL
FIELD CAPACITY	=	0.0560	VOL/VOL
WILTING POINT	=	0.0520	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0560	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.396999996000E-03	CM/SEC

LAYER 4

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC

LAYER 5

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3800	VOL/VOL
FIELD CAPACITY	=	0.0800	VOL/VOL
WILTING POINT	=	0.0130	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0800	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.100000001000	CM/SEC
SLOPE	=	3.00	PERCENT
DRAINAGE LENGTH	=	450.0	FEET

LAYER 6

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.7500	VOL/VOL
FIELD CAPACITY	=	0.7470	VOL/VOL
WILTING POINT	=	0.4000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.7500	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC

LAYER 7

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	58.57	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC

LAYER 8

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	24.00	INCHES
POROSITY	=	0.3800	VOL/VOL
FIELD CAPACITY	=	0.0800	VOL/VOL
WILTING POINT	=	0.0130	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0800	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.100000001000	CM/SEC
SLOPE	=	11.40	PERCENT
DRAINAGE LENGTH	=	150.0	FEET

LAYER 9

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.7500	VOL/VOL
FIELD CAPACITY	=	0.7470	VOL/VOL
WILTING POINT	=	0.4000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.7500	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT
SOIL DATA BASE USING SOIL TEXTURE # 5 WITH A
GOOD STAND OF GRASS, A SURFACE SLOPE OF 3. %
AND A SLOPE LENGTH OF 450. FEET.

SCS RUNOFF CURVE NUMBER	=	54.40	
FRACTION OF AREA ALLOWING RUNOFF	=	100.0	PERCENT
AREA PROJECTED ON HORIZONTAL PLANE	=	19.630	ACRES
EVAPORATIVE ZONE DEPTH	=	22.0	INCHES
INITIAL WATER IN EVAPORATIVE ZONE	=	4.500	INCHES
UPPER LIMIT OF EVAPORATIVE STORAGE	=	8.320	INCHES
LOWER LIMIT OF EVAPORATIVE STORAGE	=	2.524	INCHES
INITIAL SNOW WATER	=	0.000	INCHES
INITIAL WATER IN LAYER MATERIALS	=	28.649	INCHES
TOTAL INITIAL WATER	=	28.649	INCHES
TOTAL SUBSURFACE INFLOW	=	0.00	INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM
AUGUSTA GEORGIA

STATION LATITUDE = 33.22 DEGREES
 MAXIMUM LEAF AREA INDEX = 3.50
 START OF GROWING SEASON (JULIAN DATE) = 68
 END OF GROWING SEASON (JULIAN DATE) = 323
 EVAPORATIVE ZONE DEPTH = 22.0 INCHES
 AVERAGE ANNUAL WIND SPEED = 6.50 MPH
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 68.00 %
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 70.00 %
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 77.00 %
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 73.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
4.38	3.95	4.68	2.91	3.56	4.99
5.43	5.41	3.93	3.12	2.96	3.45

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
46.30	50.00	57.20	64.30	72.10	78.40
81.60	80.30	75.20	65.10	56.70	48.80

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA
AND STATION LATITUDE = 33.30 DEGREES

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 100

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	4.56	3.57	4.76	2.74	3.60	4.97
	5.81	5.32	4.41	2.99	2.75	3.41
STD. DEVIATIONS	2.44	1.60	2.47	1.31	2.12	2.60
	2.83	2.95	2.54	2.28	1.72	1.90

RUNOFF

TOTALS	0.004	0.000	0.004	0.000	0.000	0.002
	0.027	0.091	0.016	0.006	0.002	0.001

STD. DEVIATIONS	0.020	0.000	0.027	0.000	0.002	0.015
	0.092	0.404	0.086	0.058	0.015	0.004

EVAPOTRANSPIRATION

TOTALS	1.577	2.093	3.072	3.553	3.661	4.141
	4.897	4.522	3.384	1.619	0.948	1.114

STD. DEVIATIONS	0.221	0.236	0.582	0.760	1.525	1.546
	1.588	1.378	1.039	0.606	0.207	0.206

LATERAL DRAINAGE COLLECTED FROM LAYER 5

TOTALS	2.5102	2.0619	1.9352	1.2047	0.4142	0.3121
	0.5589	0.8185	0.7450	0.7795	0.9036	1.5056

STD. DEVIATIONS	1.8312	1.5189	1.4896	1.0415	0.4532	0.5842
	0.8112	1.0393	1.0279	1.0745	1.2152	1.3333

PERCOLATION/LEAKAGE THROUGH LAYER 6

TOTALS	0.0617	0.0514	0.0488	0.0322	0.0142	0.0105
	0.0162	0.0224	0.0208	0.0213	0.0239	0.0381

STD. DEVIATIONS	0.0421	0.0351	0.0336	0.0239	0.0106	0.0141
	0.0193	0.0244	0.0241	0.0253	0.0284	0.0312

LATERAL DRAINAGE COLLECTED FROM LAYER 8

TOTALS	0.0511	0.0483	0.0446	0.0307	0.0106	0.0070
	0.0123	0.0180	0.0165	0.0174	0.0205	0.0327

STD. DEVIATIONS	0.0320	0.0336	0.0343	0.0278	0.0152	0.0131
	0.0178	0.0224	0.0227	0.0238	0.0276	0.0281

PERCOLATION/LEAKAGE THROUGH LAYER 9

TOTALS	0.0051	0.0049	0.0053	0.0051	0.0049	0.0035
	0.0036	0.0040	0.0040	0.0038	0.0036	0.0043

STD. DEVIATIONS	0.0009	0.0001	0.0003	0.0005	0.0011	0.0019
	0.0021	0.0020	0.0019	0.0021	0.0021	0.0019

 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 6

AVERAGES	2.1516	1.9398	1.6538	1.0666	0.3539	0.2755
	0.4775	0.6992	0.6594	0.6660	0.7977	1.2862
STD. DEVIATIONS	1.5865	1.4607	1.2739	0.9329	0.3872	0.5157
	0.6930	0.8878	0.9127	0.9179	1.0727	1.1390

DAILY AVERAGE HEAD ON TOP OF LAYER 9

AVERAGES	0.0039	0.0040	0.0034	0.0024	0.0008	0.0005
	0.0009	0.0014	0.0013	0.0013	0.0016	0.0025
STD. DEVIATIONS	0.0024	0.0028	0.0026	0.0022	0.0012	0.0010
	0.0013	0.0017	0.0018	0.0018	0.0022	0.0021

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 100

	INCHES		CU. FEET	PERCENT
	-----	-----	-----	-----
PRECIPITATION	48.90	(7.734)	3484469.2	100.00
RUNOFF	0.154	(0.4340)	10947.61	0.314
EVAPOTRANSPIRATION	34.582	(3.6251)	2464196.75	70.719
LATERAL DRAINAGE COLLECTED FROM LAYER 5	13.74952	(5.50704)	979748.062	28.11757
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.36170	(0.12899)	25773.611	0.73967
AVERAGE HEAD ON TOP OF LAYER 6	1.002	(0.403)		
LATERAL DRAINAGE COLLECTED FROM LAYER 8	0.30966	(0.12406)	22065.420	0.63325
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.05203	(0.00803)	3707.190	0.10639
AVERAGE HEAD ON TOP OF LAYER 9	0.002	(0.001)		
CHANGE IN WATER STORAGE	0.053	(1.9051)	3804.31	0.109

PEAK DAILY VALUES FOR YEARS 1 THROUGH 100		
	(INCHES)	(CU. FT.)
PRECIPITATION	6.87	489534.875
RUNOFF	2.647	188618.8120
DRAINAGE COLLECTED FROM LAYER 5	0.45348	32313.73240
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.018346	1307.25354
AVERAGE HEAD ON TOP OF LAYER 6	21.373	
MAXIMUM HEAD ON TOP OF LAYER 6	31.170	
LOCATION OF MAXIMUM HEAD IN LAYER 5 (DISTANCE FROM DRAIN)	121.6 FEET	
DRAINAGE COLLECTED FROM LAYER 8	0.01253	892.95929
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.000195	13.90441
AVERAGE HEAD ON TOP OF LAYER 9	0.029	
MAXIMUM HEAD ON TOP OF LAYER 9	0.055	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	9.4 FEET	
SNOW WATER	2.36	168188.7190
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3692
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.1147

*** Maximum heads are computed using McEnroe's equations. ***

Reference: Maximum Saturated Depth over Landfill Liner
by Bruce M. McEnroe, University of Kansas
ASCE Journal of Environmental Engineering
Vol. 119, No. 2, March 1993, pp. 262-270.

FINAL WATER STORAGE AT END OF YEAR 100

LAYER	(INCHES)	(VOL/VOL)
1	1.6120	0.2687
2	9.2097	0.3070
3	0.7200	0.0600
4	4.1112	0.3426
5	2.0564	0.1714
6	0.1500	0.7500
7	14.0568	0.2400
8	1.9214	0.0801
9	0.1500	0.7500
SNOW WATER	0.000	

Appendix F, SDF GCL Closure Cap Degraded Property Value Calculations

The SDF GCL closure cap initial (0 year) layer thickness and hydraulic property values from top to bottom are provided in Table 3.1-1. The degradation scenarios for each layer are provided in Table 4.4-1. Based upon the Table 4.4-1 degradation scenarios, the Table 3.1-1 initial SDF closure cap layer thickness and hydraulic property values have been modified to account for degradation at 100, 300, 550, 1,000, 1,800, 3,400, 5,600 and 10,000 years after closure of the SDF.

Topsoil and Upper Backfill Layer Thickness:

From Section 4.2 the soil loss in terms of depth of loss per year for the topsoil and upper backfill was estimated to be 2.0E-04 inches/year and 1.2E-04 inches/year, respectively.

Topsoil Thickness Over Time Calculation:

Year	Thickness
0	6" – (0 years × 2.0E-04 inches/year) = 6"
100	6" – (100 years × 2.0E-04 inches/year) = 5.980"
300	6" – (300 years × 2.0E-04 inches/year) = 5.940"
550	6" – (550 years × 2.0E-04 inches/year) = 5.890"
1,000	6" – (1000 years × 2.0E-04 inches/year) = 5.800"
1,800	6" – (1800 years × 2.0E-04 inches/year) = 5.640"
3,400	6" – (3400 years × 2.0E-04 inches/year) = 5.320"
5,600	6" – (5600 years × 2.0E-04 inches/year) = 4.880"
10,000	6" – (10000 years × 2.0E-04 inches/year) = 4.0"

Since the topsoil does not completely erode away within the 10,000 years of interest, no reduction in the upper backfill layer occurs.

Erosion Barrier Hydraulic Properties:

Maintenance during institutional control period prevents degradation of the erosion control barrier. Subsequent to the institutional control period, pine forest succession will result in root penetration through the erosion control barrier. This does not impact its ability to function as an erosion barrier, however it allows the overlying backfill to fill the holes after the roots decompose. It is assumed that the hydraulic conductivity of the infiltrating backfill increases one order of magnitude (i.e. from 1.0E-04 to 1.0E-03 cm/s) when it falls into the hole since it will not be mechanically compacted at that time. The hydraulic properties of the erosion barrier as a whole change as the backfill material fills the root penetration holes.

From Section 4.1 the following assumptions relative to the succession of bamboo by a pine forest that impact the erosion barrier hydraulic properties were made:

- 200 years after the end of institutional control it is assumed that the entire cap is covered with pine (i.e. 400 mature trees per acre).
- Complete turnover of the 400 mature trees per acre occurs every 100 years (in a staggered manner).
- There are 400 mature trees per acre with 4 roots to 6 feet and 1 root to 12 feet. The roots are 3 inches in diameter at a depth of 1 foot and 0.25 inches in diameter at either 6 or 12 feet, whichever is applicable.

Very little erosion of the topsoil is estimated for the institutional control to pine forest, land use scenario, within the 10,000 years of interest. Therefore the estimated thickness of the topsoil layer at 10,000 years (i.e. 4 inches) has been utilized to determine the area of the holes in the erosion barrier created by root penetration. This is a conservative assumption.

Area of holes in erosion barrier due to root penetration:

Average Erosion Barrier Depth (see Table 3.1-1) = $4'' + 30'' + \frac{1}{2}(12'') = 40'' \approx 3.3'$

Root Diameter for 4-6' roots at 3.3':

3'' diameter at 1' depth and 0.25'' at 6'

$$(3'' - 0.25'') / (6' - 1') = 0.55'' / ft$$

$$\text{Diameter} = 0.25'' + [(6' - 3.3') \times 0.55'' / ft] = 1.74''$$

Area of for 4-6' roots at 3.3':

$$\text{Area} = 4 \times \frac{1}{4}\pi D^2 = \pi D^2 = \pi (1.74'')^2 = 9.5 \text{ in}^2$$

Root Diameter for 1-12' root at 3.3':

3'' diameter at 1' depth and 0.25'' at 12'

$$(3'' - 0.25'') / (12' - 1') = 0.25'' / ft$$

$$\text{Diameter} = 0.25'' + [(12' - 3.3') \times 0.25'' / ft] = 2.4''$$

Area of for 1-12' roots at 3.3':

$$\text{Area} = \frac{1}{4}\pi D^2 = \frac{1}{4}\pi (2.4'')^2 = 4.5 \text{ in}^2$$

Total area of holes in erosion barrier per tree:

$$\text{Total area} = 9.5 \text{ in}^2 + 4.5 \text{ in}^2 = 14 \text{ in}^2 \times ft^2 / 144 \text{ in}^2 \approx 0.1 \text{ ft}^2 / \text{tree}$$

Total area of holes per acre per 100 years:

400 trees/acre/100 years

$$\text{Total area} = 0.1 \text{ ft}^2 / \text{tree} \times 400 \text{ trees/acre/100 years} = 40 \text{ ft}^2 / \text{acre/100 years}$$

Year	Area of holes in erosion barrier / acre
0	0
100	0
300 ¹	40 ft ² / acre
550	40 ft ² / acre + [(550 yrs – 300 yrs) × 40 ft ² / acre/100 years = 140 ft ² / acre
1,000	40 ft ² / acre + [(1000 yrs – 300 yrs) × 40 ft ² / acre/100 years = 320 ft ² / acre
1,800	40 ft ² / acre + [(1800 yrs – 300 yrs) × 40 ft ² / acre/100 years = 640 ft ² / acre
3,400	40 ft ² / acre + [(3400 yrs – 300 yrs) × 40 ft ² / acre/100 years = 1280 ft ² / acre
5,600	40 ft ² / acre + [(5600 yrs – 300 yrs) × 40 ft ² / acre/100 years = 2160 ft ² / acre
10,000	40 ft ² / acre + [(10000 yrs – 300 yrs) × 40 ft ² / acre/100 years = 3920 ft ² / acre

¹ 200 years after the end of institutional control (i.e. at year 300) it is assumed that the entire cap is covered with pine (i.e. 400 mature trees per acre). It is assumed that each “generation” of roots becomes instantaneous voids at the 100-year turnover period.

Year	Fraction (f) of erosion barrier area comprising holes
0	$0 \div 43560 \text{ ft}^2/\text{acre} = 0$
100	$0 \div 43560 \text{ ft}^2/\text{acre} = 0$
300	$40 \text{ ft}^2/\text{acre} \div 43560 \text{ ft}^2/\text{acre} = 0.00092$
550	$140 \text{ ft}^2/\text{acre} \div 43560 \text{ ft}^2/\text{acre} = 0.00321$
1,000	$320 \text{ ft}^2/\text{acre} \div 43560 \text{ ft}^2/\text{acre} = 0.00735$
1,800	$640 \text{ ft}^2/\text{acre} \div 43560 \text{ ft}^2/\text{acre} = 0.0147$
3,400	$1280 \text{ ft}^2/\text{acre} \div 43560 \text{ ft}^2/\text{acre} = 0.0294$
5,600	$2160 \text{ ft}^2/\text{acre} \div 43560 \text{ ft}^2/\text{acre} = 0.0496$
10,000	$3920 \text{ ft}^2/\text{acre} \div 43560 \text{ ft}^2/\text{acre} = 0.08999$

The equivalent horizontal hydraulic conductivity for horizontal flow in a series of horizontal layers with different saturated hydraulic conductivities can be determined from the following equation (Freeze and Cherry 1979):

$$K_h = \sum_{i=1}^n \frac{K_i d_i}{d}, \text{ where } K_h = \text{equivalent horizontal saturated hydraulic conductivity, } K_i = \text{horizontal saturated hydraulic conductivity of } i^{\text{th}} \text{ layer, } d_i = \text{thickness of } i^{\text{th}} \text{ layer, } d = \text{total thickness}$$

In a similar manner the equivalent vertical hydraulic conductivity for vertical flow in a horizontal zone containing areas of materials with different saturated hydraulic conductivities can be determined based upon an area proportionality as follows:

$$K_v = \sum_{i=1}^n \frac{K_i A_i}{A}, \text{ where } K_v = \text{equivalent vertical saturated hydraulic conductivity, } K_i = \text{vertical saturated hydraulic conductivity of } i^{\text{th}} \text{ layer, } A_i = \text{Area of } i^{\text{th}} \text{ layer, } A = \text{total area}$$

The following are the input saturated hydraulic conductivities:

For backfill that drops into holes in the erosion barrier = $1.0\text{E-}03 \text{ cm/s}$

Intact erosion barrier = $3.97\text{E-}04 \text{ cm/s}$

The fraction (F) provided above is equivalent to A_i/A for the backfill that drops into holes in the erosion barrier and one minus the fraction ($1 - F$) is equivalent to A_i/A for the intact erosion barrier, making the equation:

$$K_v = (1.0\text{E-}03 \times F) + (3.97\text{E-}04 \times (1 - F))$$

Year	K_v
0	$(1.0\text{E-}03 \text{ cm/s} \times 0) + (3.97\text{E-}04 \text{ cm/s} \times (1 - 0)) = 3.97\text{E-}04 \text{ cm/s}$
100	$(1.0\text{E-}03 \text{ cm/s} \times 0) + (3.97\text{E-}04 \text{ cm/s} \times (1 - 0)) = 3.97\text{E-}04 \text{ cm/s}$
300	$(1.0\text{E-}03 \text{ cm/s} \times 0.00092) + (3.97\text{E-}04 \text{ cm/s} \times (1 - 0.00092)) = 3.98 \text{E-}04 \text{ cm/s}$
550	$(1.0\text{E-}03 \text{ cm/s} \times 0.00321) + (3.97\text{E-}04 \text{ cm/s} \times (1 - 0.00321)) = 3.99\text{E-}04 \text{ cm/s}$
1,000	$(1.0\text{E-}03 \text{ cm/s} \times 0.00735) + (3.97\text{E-}04 \text{ cm/s} \times (1 - 0.00735)) = 4.01\text{E-}04 \text{ cm/s}$
1,800	$(1.0\text{E-}03 \text{ cm/s} \times 0.0147) + (3.97\text{E-}04 \text{ cm/s} \times (1 - 0.0147)) = 4.06\text{E-}04 \text{ cm/s}$
3,400	$(1.0\text{E-}03 \text{ cm/s} \times 0.0294) + (3.97\text{E-}04 \text{ cm/s} \times (1 - 0.0294)) = 4.15\text{E-}04 \text{ cm/s}$
5,600	$(1.0\text{E-}03 \text{ cm/s} \times 0.0496) + (3.97\text{E-}04 \text{ cm/s} \times (1 - 0.0496)) = 4.27\text{E-}04 \text{ cm/s}$
10,000	$(1.0\text{E-}03 \text{ cm/s} \times 0.08999) + (3.97\text{E-}04 \text{ cm/s} \times (1 - 0.08999)) = 4.51\text{E-}04 \text{ cm/s}$

In an analogous manner the equivalent porosity (n), field capacity (FC), and wilting point (WP) can be determined based upon an area proportionality as follows:

$$n = \sum_{i=1}^n n_i A_i$$

$$FC = \sum_{i=1}^n FC_i A_i$$

$$WP = \sum_{i=1}^n WP_i A_i$$

The following are the input properties:

Material	Porosity	Field Capacity	Wilting Point
Backfill	0.37	0.24	0.136
Erosion Barrier	0.06	0.056	0.052

Year	n
0	$(0.37 \times 0) + (0.06 \times (1 - 0)) = 0.06$
100	$(0.37 \times 0) + (0.06 \times (1 - 0)) = 0.06$
300	$(0.37 \times 0.00092) + (0.06 \times (1 - 0.00092)) = 0.06$
550	$(0.37 \times 0.00321) + (0.06 \times (1 - 0.00321)) = 0.061$
1,000	$(0.37 \times 0.00735) + (0.06 \times (1 - 0.00735)) = 0.062$
1,800	$(0.37 \times 0.0147) + (0.06 \times (1 - 0.0147)) = 0.065$
3,400	$(0.37 \times 0.0294) + (0.06 \times (1 - 0.0294)) = 0.069$
5,600	$(0.37 \times 0.0496) + (0.06 \times (1 - 0.0496)) = 0.075$
10,000	$(0.37 \times 0.08999) + (0.06 \times (1 - 0.08999)) = 0.088$

Year	FC
0	$(0.24 \times 0) + (0.056 \times (1 - 0)) = 0.056$
100	$(0.24 \times 0) + (0.056 \times (1 - 0)) = 0.056$
300	$(0.24 \times 0.00092) + (0.056 \times (1 - 0.00092)) = 0.562$
550	$(0.24 \times 0.00321) + (0.056 \times (1 - 0.00321)) = 0.0566$
1,000	$(0.24 \times 0.00735) + (0.056 \times (1 - 0.00735)) = 0.0574$
1,800	$(0.24 \times 0.0147) + (0.056 \times (1 - 0.0147)) = 0.0587$
3,400	$(0.24 \times 0.0294) + (0.056 \times (1 - 0.0294)) = 0.0614$
5,600	$(0.24 \times 0.0496) + (0.056 \times (1 - 0.0496)) = 0.0651$
10,000	$(0.24 \times 0.08999) + (0.056 \times (1 - 0.08999)) = 0.0726$

Year	WP
0	$(0.136 \times 0) + (0.052 \times (1 - 0)) = 0.052$
100	$(0.136 \times 0) + (0.052 \times (1 - 0)) = 0.052$
300	$(0.136 \times 0.00092) + (0.052 \times (1 - 0.00092)) = 0.521$
550	$(0.136 \times 0.00321) + (0.052 \times (1 - 0.00321)) = 0.0523$
1,000	$(0.136 \times 0.00735) + (0.052 \times (1 - 0.00735)) = 0.0526$
1,800	$(0.136 \times 0.0147) + (0.052 \times (1 - 0.0147)) = 0.0532$
3,400	$(0.136 \times 0.0294) + (0.052 \times (1 - 0.0294)) = 0.0545$
5,600	$(0.136 \times 0.0496) + (0.052 \times (1 - 0.0496)) = 0.0562$
10,000	$(0.136 \times 0.08999) + (0.052 \times (1 - 0.08999)) = 0.0596$

Summary Erosion Barrier Hydraulic Properties with Time:

Year	K _v	n	FC	WP
0	3.97E-04 cm/s	0.06	0.056	0.052
100	3.97E-04 cm/s	0.06	0.056	0.052
300	3.98 E-04 cm/s	0.06	0.562	0.521
550	3.99E-04 cm/s	0.061	0.0566	0.0523
1,000	4.01E-04 cm/s	0.062	0.0574	0.0526
1,800	4.06E-04 cm/s	0.065	0.0587	0.0532
3,400	4.15E-04 cm/s	0.069	0.0614	0.0545
5,600	4.27E-04 cm/s	0.075	0.0651	0.0562
10,000	4.51E-04 cm/s	0.088	0.0726	0.0596

Upper GCL Holes:

Maintenance during the institutional control period prevents degradation of the upper GCL. However pine forest succession and associated root penetration results in holes through the erosion barrier. This allows the overlying drainage layer to fill the holes after the roots decompose. The holes in the GCL essentially act as direct conduits from the upper drainage layer to the lower backfill layer. When saturated conditions occur in the drainage layer after major precipitation events, cones of depression are created around the holes in the GCL with a radius of influence much greater than the radius of the hole. This means that a small area of GCL holes can greatly reduce the lateral flow of water in the drainage layer and increase the vertical flow into the lower backfill.

From Section 4.1 the following assumptions were made relative to the succession of bamboo by a pine forest that result in root penetration into the upper GCL:

- 200 years after the end of institutional control it is assumed that the entire cap is covered with pine (i.e. 400 mature trees per acre).
- Complete turnover of the 400 mature trees per acre occurs every 100 years (in a staggered manner).
- There are 400 mature trees per acre with 4 roots to 6 feet and 1 root to 12 feet. The roots are 3 inches in diameter at a depth of 1 foot and 0.25 inches in diameter at either 6 or 12 feet, whichever is applicable.

Very little erosion of the topsoil is estimated for the institutional control to pine forest, land use scenario, within the 10,000 years of interest. Therefore the estimated thickness of the topsoil layer at 10,000 years (~4 inches) has been utilized to determine the area of the holes in the upper GCL created by root penetration. This is a conservative assumption.

Area of holes in upper GCL due to root penetration:

$$\text{Upper GCL Depth (see Table 3.1-1)} = 4'' + 30'' + 12'' + 12'' + 12'' = 70'' \approx 5.8'$$

Root Diameter for 4-6' roots at 5.8':

$$3'' \text{ diameter at } 1' \text{ depth and } 0.25'' \text{ at } 6'$$

$$(3'' - 0.25'') / (6' - 1') = 0.55'' / ft$$

$$\text{Diameter} = 0.25'' + [(6' - 5.8') \times 0.55'' / ft] = 0.36''$$

Area of for 4-6' roots at 5.8':

$$\text{Area} = 4 \times \frac{1}{4}\pi D^2 = \pi D^2 = \pi (0.36'')^2 = 0.41 \text{ in}^2$$

Root Diameter for 1-12' root at 3.3':

$$3'' \text{ diameter at } 1' \text{ depth and } 0.25'' \text{ at } 12'$$

$$(3'' - 0.25'') / (12' - 1') = 0.25'' / ft$$

$$\text{Diameter} = 0.25'' + [(12' - 5.8') \times 0.25''/\text{ft}] = 1.8''$$

Area of for 1-12' roots at 3.3':

$$\text{Area} = \frac{1}{4}\pi D^2 = \frac{1}{4}\pi(1.8'')^2 = 2.54 \text{ in}^2$$

Total area of holes in erosion barrier per tree:

$$\text{Total area} = 0.41 \text{ in}^2 + 2.54 \text{ in}^2 = 2.95 \text{ in}^2 \times \text{ft}^2/144 \text{ in}^2 \approx 0.02 \text{ ft}^2/\text{tree}$$

Total area of holes per acre per 100 years:

$$400 \text{ trees/acre}/100 \text{ years}$$

$$\text{Total area} = 0.02 \text{ ft}^2/\text{tree} \times 400 \text{ trees/acre}/100 \text{ years} = 8 \text{ ft}^2/\text{acre}/100 \text{ years}$$

Year	Area of holes in upper GCL / acre due to root penetration
0	0
100	0
300 ¹	8 ft ² / acre
550	8 ft ² / acre + [(550 yrs – 300 yrs) × 8 ft ² / acre/100 years] = 28 ft ² / acre
1,000	8 ft ² / acre + [(1000 yrs – 300 yrs) × 8 ft ² / acre/100 years] = 64 ft ² / acre
1,800	8 ft ² / acre + [(1800 yrs – 300 yrs) × 8 ft ² / acre/100 years] = 128 ft ² / acre
3,400	8 ft ² / acre + [(3400 yrs – 300 yrs) × 8 ft ² / acre/100 years] = 256 ft ² / acre
5,600	8 ft ² / acre + [(5600 yrs – 300 yrs) × 8 ft ² / acre/100 years] = 432 ft ² / acre
10,000	8 ft ² / acre + [(10000 yrs – 300 yrs) × 8 ft ² / acre/100 years] = 784 ft ² / acre

¹ 200 years after the end of institutional control (i.e. at year 300) it is assumed that the entire cap is covered with pine (i.e. 400 mature trees per acre)

Number of one-square-centimeter holes in upper GCL per acre due to root penetration (each HELP model installation defect for a flexible membrane liner (FML) is assumed to be one square centimeter):

$$1 \text{ cm}^2 = 0.001076391 \text{ ft}^2 \text{ so } 0.001076391 \text{ ft}^2/\text{installation defect}$$

Year	Percent of GCL area degraded due to root penetration
0	0
100	0
300	(8 ft ² / acre ÷ 43560 ft ² / acre) × 100 = 0.018
550	(28 ft ² / acre ÷ 43560 ft ² / acre) × 100 = 0.064
1,000	(64 ft ² / acre ÷ 43560 ft ² / acre) × 100 = 0.15
1,800	(128 ft ² / acre ÷ 43560 ft ² / acre) × 100 = 0.29
3,400	(256 ft ² / acre ÷ 43560 ft ² / acre) × 100 = 0.59
5,600	(432 ft ² / acre ÷ 43560 ft ² / acre) × 100 = 0.99
10,000	(784 ft ² / acre ÷ 43560 ft ² / acre) × 100 = 1.8

Year	# of installation defects in upper GCL / acre due to root penetration
0	0
100	0
300	$8 \text{ ft}^2/\text{acre} \div 0.001076391 \text{ ft}^2/\text{installation defect} = 7,432$
550	$28 \text{ ft}^2/\text{acre} \div 0.001076391 \text{ ft}^2/\text{installation defect} = 26,013$
1,000	$64 \text{ ft}^2/\text{acre} \div 0.001076391 \text{ ft}^2/\text{installation defect} = 59,458$
1,800	$128 \text{ ft}^2/\text{acre} \div 0.001076391 \text{ ft}^2/\text{installation defect} = 118,916$
3,400	$256 \text{ ft}^2/\text{acre} \div 0.001076391 \text{ ft}^2/\text{installation defect} = 237,832$
5,600	$432 \text{ ft}^2/\text{acre} \div 0.001076391 \text{ ft}^2/\text{installation defect} = 401,341$
10,000	$784 \text{ ft}^2/\text{acre} \div 0.001076391 \text{ ft}^2/\text{installation defect} = 728,360$

Middle Backfill Layer and Upper Drainage Layer Hydraulic Properties:

It is assumed that colloidal clay migration from the 1-foot-thick middle backfill to the underlying 1-foot-thick upper drainage layer causes the middle backfill saturated hydraulic conductivity to increase over time and that of the upper drainage layer to decrease over time.

Determine mass of clay to fill upper drainage layer void volume (0.38):

Assume clay bulk density is 1.1 g/cm^3

Look at a 1-ft^2 area of the 1-foot-thick upper drainage layer (i.e. 1 ft^3)

Void volume = $0.38 \times 1 \text{ ft}^3 = 0.38 \text{ ft}^3$

Clay mass per $\text{ft}^3 = 1.1 \text{ g/cm}^3 \times 0.38 \text{ ft}^3 \times 2.831685\text{E-}02 \text{ m}^3/\text{ft}^3 \times 1,000,000 \text{ cm}^3/\text{m}^3 = 11,836.3 \text{ g}$

Determine available clay mass in the middle backfill layer:

Assume that the middle backfill layer consists of 20% clay and 80% sand with a dry bulk density of $104\text{-lbs}/\text{ft}^3$.

Clay mass = $104 \text{ lbs}/\text{ft}^3 \times 0.20 \times 453.59 \text{ g/lbs} = 9,434.7 \text{ g}/\text{ft}^3$

There is not enough clay in the middle backfill layer to fill the upper drainage layer. Therefore it will be assumed that half the clay content of the middle backfill migrates into the upper drainage layer, at which point the two layers essentially become the same material and material property changes cease. Based upon this it will be assumed that the endpoint saturated hydraulic conductivity of the layers will become that of the log mid-point between the initial backfill and upper drainage layer conditions. It will also be assumed that the endpoint porosity, field capacity, and wilting point will become the arithmetic average of the backfill and upper drainage layer.

Endpoint hydraulic properties:

Intact hydraulic properties:

Hydraulic Parameter	Middle Backfill	Upper Drainage Layer
K	$1.0\text{E-}04 \text{ cm/s}$	$1.0\text{E-}01 \text{ cm/s}$
n	0.37	0.38
FC	0.24	0.08
WP	0.136	0.013

Endpoint saturated hydraulic conductivity:

Middle backfill: $K_{\text{MB}} = 0.0001$; $\log K_{\text{MB}} = -4$

Upper drainage layer: $K_{\text{UDL}} = 0.1$; $\log K_{\text{UDL}} = -1$

$$\text{Log mid-point: } \frac{\text{Log } K_{MB} + \text{Log } K_{UDL}}{2} = \frac{-1 + (-4)}{2} = -2.5$$

$$K_E = 10^{-2.5} = 3.2\text{E-}03 \text{ cm/s}$$

Endpoint n, FC, and WP:

$$n = (0.37 + 0.38)/2 = 0.375$$

$$\text{FC} = (0.24 + 0.08)/2 = 0.16$$

$$\text{WP} = (0.136 + 0.013)/2 = 0.0745$$

It will be assumed that the clay migrates out of the middle backfill into the upper drainage layer with the water flux containing 63 mg/L of colloidal clay. It will also be assumed that the time to achieve the endpoint conditions will be based upon the estimated water flux into the upper drainage layer and migration of half the clay content of the middle backfill layer (i.e. $9,434.7 \text{ g/ft}^3 \div 2 = 4717.4 \text{ g/ft}^3$).

Determine flux of water into the upper drainage layer:

Section 3.3 intact SDF closure cap Modeling determined the following average annual flux of water into the upper drainage layer (see Appendix E):

$$\text{Precipitation} = 48.90 \text{ inches/year}$$

$$\text{Runoff} = 0.154 \text{ inches/year}$$

$$\text{Evapotranspiration} = 34.582 \text{ inches/year}$$

$$\text{Flux of water into upper drainage layer} = \text{Precipitation} - (\text{Runoff} + \text{Evapotranspiration})$$

$$\text{Flux of water into upper drainage layer} = 48.90 \text{ in/yr} - (0.154 \text{ in/yr} + 34.582 \text{ in/yr})$$

$$\text{Flux of water into upper drainage layer} = 14.164 \text{ in/yr}$$

The above flux is based upon the best case cap conditions; therefore, will determine the flux based upon the Preliminary 10,000 year conditions as follows:

- 10,000 year eroded topsoil at 4.0 inches (see above)
- 10,000 year erosion barrier conditions with $K = 4.51\text{E-}04 \text{ cm/s}$; $n = 0.088$; $\text{FC} = 0.0726$; $\text{WP} = 0.0596$ (see above)
- Middle backfill and upper drainage layer at end state conditions with $K = 3.2\text{E-}03 \text{ cm/s}$; $n = 0.375$; $\text{FC} = 0.16$; $\text{WP} = 0.0745$ (see above)
- Upper GCL with 728,360 holes
- Lower drainage layer with intact backfill properties (used since 10,000 year conditions for this layer not yet determined)

The detailed HELP model input data and output file associated with the 10,000-year conditions is provided at the end of this appendix. The following are the pertinent values extracted from the output file:

$$\text{Precipitation} = 48.90 \text{ inches/year}$$

$$\text{Runoff} = 0.181 \text{ inches/year}$$

$$\text{Evapotranspiration} = 34.556 \text{ inches/year}$$

$$\text{Flux of water into upper drainage layer} = \text{Precipitation} - (\text{Runoff} + \text{Evapotranspiration})$$

$$\text{Flux of water into upper drainage layer} = 48.90 \text{ in/yr} - (0.181 \text{ in/yr} + 34.556 \text{ in/yr})$$

Flux of water into upper drainage layer = 14.163 in/yr

There is essentially no difference between the flux into the upper drainage layer with either the intact or 10,000-year conditions. Therefore, a water flux into the upper drainage layer of ~14.2 in/yr will be used for determination of the time when the endpoint properties are reached.

Determine yearly clay migration into the upper drainage layer:

Flux into upper drainage layer = 14.2 in/yr

Colloidal clay concentration = 63 mg/L

Flux through a 1 ft² area = 14.2 in/yr \times ft/12 in \times 1 ft² = 1.18 ft²/yr

Clay flux = 1.18 ft²/yr \times 63 mg/L \times 2.831685E-02 m³/ft³ \times 1000L/m³ = 2,105 mg/yr = 2.1 g/yr

Determine time it takes for the 4717.4 g of clay to migrate from the middle backfill layer to the upper drainage layer:

Time = 4717.4 g \div 2.1 g/yr = 2,246 years

Determine middle backfill and upper drainage layer hydraulic property variation with time:

It will be assumed that the K of the middle backfill layer is increasing log linearly with time from 1.0E-04 cm/s to 3.2E-03 cm/s, until year 2,246 at which time the K becomes static. Conversely it will be assumed that the K of the upper drainage layer is decreasing log linearly with time from 1.0E-01 cm/s to 3.2E-03 cm/s, until year 2,246 at which time the K becomes static. Porosity (n), FC, and WP will be assumed to behave similarly but in an arithmetic linear manner.

Initial and End State hydraulic properties:

Hydraulic Parameter	Initial Middle Backfill	Initial Upper Drainage Layer	End State at 2,246 years
K	1.0E-04 cm/s	1.0E-01 cm/s	3.2E-03 cm/s
n	0.37	0.38	0.375
FC	0.24	0.08	0.16
WP	0.136	0.013	0.0745

Determine fraction change for each year:

Year	Fraction
0	0 \div 2246 = 0
100	100 \div 2246 = 0.0445
300	300 \div 2246 = 0.1336
550	550 \div 2246 = 0.2449
1,000	1000 \div 2246 = 0.4452
1,800	1800 \div 2246 = 0.8014
3,400	1.0
5,600	1.0
10,000	1.0

Determine variation in K, n, FC, and WP with time in the middle backfill:

Year	Fraction, F	K^1 (cm/s)	n^2	FC^3	WP^4
0	0	0.0001	0.37	0.24	0.136
100	0.0445	0.00012	0.37	0.236	0.133
300	0.1336	0.00016	0.371	0.229	0.128
550	0.2449	0.00023	0.371	0.220	0.121
1,000	0.4452	0.00046	0.372	0.204	0.109
1,800	0.8014	0.0016	0.374	0.176	0.0867
3,400	1.0	0.0032	0.375	0.16	0.0745
5,600	1.0	0.0032	0.375	0.16	0.0745
10,000	1.0	0.0032	0.375	0.16	0.0745

$$^1 K = 10^{[-4 + ((-2.5 - (-4))F)]} = 10^{(-4 + 1.5F)}$$

$$^2 n = 0.37 + (0.375 - 0.37)F$$

$$^3 FC = 0.24 - (0.24 - 0.16)F$$

$$^4 WP = 0.136 - (0.136 - 0.0745)F$$

Determine variation in K, n, FC, and WP with time in the upper drainage layer:

Year	Fraction, F	K^1 (cm/s)	n^2	FC^3	WP^4
0	0	0.1	0.38	0.08	0.013
100	0.0445	0.086	0.38	0.084	0.016
300	0.1336	0.063	0.379	0.089	0.021
550	0.2449	0.043	0.379	0.10	0.028
1,000	0.4452	0.021	0.378	0.116	0.040
1,800	0.8014	0.0063	0.376	0.144	0.062
3,400	1.0	0.0032	0.375	0.16	0.0745
5,600	1.0	0.0032	0.375	0.16	0.0745
10,000	1.0	0.0032	0.375	0.16	0.0745

$$^1 K = 10^{[-1 + ((-2.5 - (-1))F)]} = 10^{(-1 - 1.5F)}$$

$$^2 n = 0.38 - (0.38 - 0.375)F$$

$$^3 FC = 0.08 - (0.16 - 0.08)F$$

$$^4 WP = 0.013 - (0.0745 - 0.013)F$$

Lower Drainage Layer Hydraulic Properties:

It is assumed that colloidal clay migration from the overlying backfill is driven by the water flux through the upper GCL. This water flux driven clay migration enters into the 2-foot thick lower drainage layer and fills the lower drainage layer from the bottom up. This reduces the saturated hydraulic conductivity of the clay filled portion from 1.0E-01 to 1.0E-04 cm/s (i.e. the saturated hydraulic conductivity of the overlying backfill layer). As the thickness of the lower drainage layer filled with clay increases the overall hydraulic conductivity of the layer decreases. This is different from that assumed for the upper drainage layer since the lower drainage layer has significantly more backfill overlying it. The HELP model was run for each year with all of the previously degraded properties (see above) without degradation of the lower drainage layer in order to determine the infiltration through the upper GCL. The results are as follows:

Year	Infiltration through upper GCL (inches/year)
0	0.36170
100	0.41335
300	3.04724
550	7.89958
1,000	12.03710
1,800	13.76236
3,400	14.03487
5,600	14.07915
10,000	14.09278

It is assumed that there is a linear increase in the infiltration over time between data points.

Determine cumulative volume of water through the lower drainage layer over time:

Year	Infiltration through upper GCL (inches/year)	Time Step Volume ¹ (inches)	Cumulative Volume ² (inches)	Cumulative Volume over one ft ² area ³ (ft ³)
0	0.36170	0	0	0
100	0.41335	38.752	38.752	3.2
300	3.04724	346.059	384.811	32.1
550	7.89958	1368.352	1753.163	146.1
1,000	12.03710	4485.753	6238.916	519.9
1,800	13.76236	10319.784	16558.700	1379.9
3,400	14.03487	22237.784	38796.484	3233.0
5,600	14.07915	30925.422	69721.906	5810.2
10,000	14.09278	61978.246	131700.152	10975.0

¹ $V = [I_1 \times (T_2 - T_1)] + [1/2 \times (I_2 - I_1)(T_2 - T_1)]$, where I = infiltration at time step 1 or 2; T = time at time step 1 or 2

² Cumulative Volume = Previous cumulative volume + Volume at current time step

³ Cumulative Volume over one ft² area = (Cumulative Volume ÷ 12 in/ft) × 1 ft²

Determine mass of clay to fill lower drainage layer void volume (0.38):

Assume clay bulk density is 1.1 g/cm³

Look at a 1-ft² area of the 2-foot-thick upper drainage layer (i.e. 2 ft³)

Void volume = $0.38 \times 2 \text{ ft}^3 = 0.76 \text{ ft}^3$

Clay mass per ft³ = $1.1 \text{ g/cm}^3 \times 0.76 \text{ ft}^3 \times 2.831685\text{E-}02 \text{ m}^3/\text{ft}^3 \times 1,000,000 \text{ cm}^3/\text{m}^3 = 23,672.9 \text{ g}$

Determine total flux of water into the lower drainage layer required to completely fill it with clay:

It will be assumed that the clay migrates out of the lower backfill into the lower drainage layer with the water flux containing 63 mg/L of colloidal clay.

$$V = \frac{23,672.9 \text{ g} \times 1000 \text{ mg/g}}{63 \text{ mg/L} \times 28.31685 \text{ L/ft}^3} = 13,269.8 \text{ ft}^3$$

Determine the mass of clay that has migrated into the lower drainage layer at the end of each time step:

Year	Mass of clay into lower drainage layer
0	0
100	$3.2 \text{ ft}^3 \times 63 \text{ mg/L} \times 28.31685 \text{ L/ft}^3 \times \text{g/1000 mg} = 5.7 \text{ g}$
300	$32.1 \text{ ft}^3 \times 63 \text{ mg/L} \times 28.31685 \text{ L/ft}^3 \times \text{g/1000 mg} = 57.3 \text{ g}$
550	$146.1 \text{ ft}^3 \times 63 \text{ mg/L} \times 28.31685 \text{ L/ft}^3 \times \text{g/1000 mg} = 260.6 \text{ g}$
1,000	$519.9 \text{ ft}^3 \times 63 \text{ mg/L} \times 28.31685 \text{ L/ft}^3 \times \text{g/1000 mg} = 927.5 \text{ g}$
1,800	$1379.9 \text{ ft}^3 \times 63 \text{ mg/L} \times 28.31685 \text{ L/ft}^3 \times \text{g/1000 mg} = 2,461.7 \text{ g}$
3,400	$3233.0 \text{ ft}^3 \times 63 \text{ mg/L} \times 28.31685 \text{ L/ft}^3 \times \text{g/1000 mg} = 5,767.5 \text{ g}$
5,600	$5810.2 \text{ ft}^3 \times 63 \text{ mg/L} \times 28.31685 \text{ L/ft}^3 \times \text{g/1000 mg} = 10,365.2 \text{ g}$
10,000	$10975.0 \text{ ft}^3 \times 63 \text{ mg/L} \times 28.31685 \text{ L/ft}^3 \times \text{g/1000 mg} = 19,579.0 \text{ g}$

Determine the fraction of the lower drainage layer filled at the end of each time step:

Year	Fraction of the lower drainage layer filled
0	0
100	$5.7 \text{ g} \div 23,672.9 \text{ g} = 0.000241$
300	$57.3 \text{ g} \div 23,672.9 \text{ g} = 0.00242$
550	$260.6 \text{ g} \div 23,672.9 \text{ g} = 0.0110$
1,000	$927.5 \text{ g} \div 23,672.9 \text{ g} = 0.0392$
1,800	$2,461.7 \text{ g} \div 23,672.9 \text{ g} = 0.104$
3,400	$5,767.5 \text{ g} \div 23,672.9 \text{ g} = 0.244$
5,600	$10,365.2 \text{ g} \div 23,672.9 \text{ g} = 0.438$
10,000	$19,579.0 \text{ g} \div 23,672.9 \text{ g} = 0.827$

The following are the hydraulic properties of the clean and clay filled portion of the lower drainage layer:

Material	Saturated Hydraulic Conductivity (cm/s)	Porosity	Field Capacity	Wilting Point
Clean	1.0E-01	0.38	0.08	0.013
Clay filled	1.0E-04	0.22 (see below)	0.21 (see below)	0.20 (see below)

Determine the porosity of the clay filled portion of the lower drainage layer:

Porosity of the clay:

Assumed clay bulk density, $\rho_b = 1.1 \text{ g/cm}^3$

Assumed clay particle density, $\rho_p = 2.6 \text{ g/cm}^3$

$$\text{Resulting clay porosity, } n = 1 - \frac{r_b}{r_p} = 1 - \frac{1.1 \text{ g/cm}^3}{2.6 \text{ g/cm}^3} = 0.58$$

Porosity of the clay filled portion = Porosity of clean portion \times porosity of clay

Porosity of the clay filled portion = $0.38 \times 0.58 = 0.22$

Determine the field capacity and wilting point of the clay filled portion of the lower drainage layer:

Will assume that the field capacity and wilting point of the clay fill portion has the same ratio versus its porosity of 0.22 as the equivalent ratio for kaolin clay.

From WSRC 2002a the following kaolin properties are found: $n = 0.56$; $FC = 0.55$; $WP = 0.50$

$FC = 0.22 \times (0.55 \div 0.56) \approx 0.21$

$WP = 0.22 \times (0.50 \div 0.56) \approx 0.20$

Determine the equivalent horizontal hydraulic conductivity of the lower drainage layer over time:

The equivalent horizontal hydraulic conductivity for horizontal flow in a series of horizontal layers with different saturated hydraulic conductivities can be determined from the following equation (Freeze and Cherry 1979):

$$K_h = \sum_{i=1}^n \frac{K_i d_i}{d}, \text{ where } K_h = \text{equivalent horizontal saturated hydraulic conductivity, } K_i = \text{horizontal saturated hydraulic conductivity of } i^{\text{th}} \text{ layer, } d_i = \text{thickness of } i^{\text{th}} \text{ layer, } d = \text{total thickness}$$

The fraction, F , equals d_i/d for the clay filled portion and d_i/d for the clean drainage layer material equals $(1 - F)$, making the equation:

$$K_h = (K_{filled} \times F) + [K_{clean} \times (1 - F)]$$

Year	Equivalent K (cm/s)
0	0.1
100	$(0.0001 \times 0.000241) + [0.1 \times (1 - 0.000241)] = 0.1$
300	$(0.0001 \times 0.00242) + [0.1 \times (1 - 0.00242)] = 0.0998$
550	$(0.0001 \times 0.0110) + [0.1 \times (1 - 0.0110)] = 0.0989$
1,000	$(0.0001 \times 0.0392) + [0.1 \times (1 - 0.0392)] = 0.0961$
1,800	$(0.0001 \times 0.104) + [0.1 \times (1 - 0.104)] = 0.0896$
3,400	$(0.0001 \times 0.244) + [0.1 \times (1 - 0.244)] = 0.0756$
5,600	$(0.0001 \times 0.438) + [0.1 \times (1 - 0.438)] = 0.0562$
10,000	$(0.0001 \times 0.827) + [0.1 \times (1 - 0.827)] = 0.0174$

Determine the equivalent n , FC , and WP for the lower drainage layer over time:

In an analogous manner to that for K , the equivalent n , FC , and WP can be determined based upon the fraction filled as follows:

$$n = (n_{filled} \times F) + [n_{clean} \times (1 - F)]$$

$$FC = (FC_{filled} \times F) + [FC_{clean} \times (1 - F)]$$

$$WP = (WP_{filled} \times F) + [WP_{clean} \times (1 - F)]$$

Year	Equivalent n
0	$(0.22 \times 0) + [0.38 \times (1 - 0)] = 0.38$
100	$(0.22 \times 0.000241) + [0.38 \times (1 - 0.000241)] = 0.38$
300	$(0.22 \times 0.00242) + [0.38 \times (1 - 0.00242)] = 0.38$
550	$(0.22 \times 0.0110) + [0.38 \times (1 - 0.0110)] = 0.378$
1,000	$(0.22 \times 0.0392) + [0.38 \times (1 - 0.0392)] = 0.374$
1,800	$(0.22 \times 0.104) + [0.38 \times (1 - 0.104)] = 0.363$
3,400	$(0.22 \times 0.244) + [0.38 \times (1 - 0.244)] = 0.341$
5,600	$(0.22 \times 0.438) + [0.38 \times (1 - 0.438)] = 0.310$
10,000	$(0.22 \times 0.827) + [0.38 \times (1 - 0.827)] = 0.248$

Year	Equivalent FC
0	$(0.21 \times 0) + [0.08 \times (1 - 0)] = 0.08$
100	$(0.21 \times 0.000241) + [0.08 \times (1 - 0.000241)] = 0.08$
300	$(0.21 \times 0.00242) + [0.08 \times (1 - 0.00242)] = 0.0803$
550	$(0.21 \times 0.0110) + [0.08 \times (1 - 0.0110)] = 0.0814$
1,000	$(0.21 \times 0.0392) + [0.08 \times (1 - 0.0392)] = 0.0851$
1,800	$(0.21 \times 0.104) + [0.08 \times (1 - 0.104)] = 0.0935$
3,400	$(0.21 \times 0.244) + [0.08 \times (1 - 0.244)] = 0.112$
5,600	$(0.21 \times 0.438) + [0.08 \times (1 - 0.438)] = 0.137$
10,000	$(0.21 \times 0.827) + [0.08 \times (1 - 0.827)] = 0.188$

Year	Equivalent WP
0	$(0.20 \times 0) + [0.013 \times (1 - 0)] = 0.013$
100	$(0.20 \times 0.000241) + [0.013 \times (1 - 0.000241)] = 0.013$
300	$(0.20 \times 0.00242) + [0.013 \times (1 - 0.00242)] = 0.0134$
550	$(0.20 \times 0.0110) + [0.013 \times (1 - 0.0110)] = 0.0150$
1,000	$(0.20 \times 0.0392) + [0.013 \times (1 - 0.0392)] = 0.0203$
1,800	$(0.20 \times 0.104) + [0.013 \times (1 - 0.104)] = 0.0324$
3,400	$(0.20 \times 0.244) + [0.013 \times (1 - 0.244)] = 0.0586$
5,600	$(0.20 \times 0.438) + [0.013 \times (1 - 0.438)] = 0.0949$
10,000	$(0.20 \times 0.827) + [0.013 \times (1 - 0.827)] = 0.168$

Summary Lower Drainage Layer Hydraulic Properties with Time:

Year	K (cm/s)	n	FC	WP
0	0.1	0.38	0.08	0.013
100	0.1	0.38	0.08	0.013
300	0.0998	0.38	0.0803	0.0134
550	0.0989	0.378	0.0814	0.0150
1,000	0.0961	0.374	0.0851	0.0203
1,800	0.0896	0.363	0.0935	0.0324
3,400	0.0756	0.341	0.112	0.0586
5,600	0.0562	0.310	0.137	0.0949
10,000	0.0174	0.248	0.188	0.168

The HELP model was rerun for each time step with all of the degraded properties (see above) including that of the lower drainage layer. Infiltration through the upper GCL did not change with the addition of the degraded lower drainage layer properties. Therefore the above estimated lower drainage layer hydraulic properties over time are verified.

Worse Case Infiltration through the Upper GCL

The worse case infiltration through the upper GCL and the associated time of occurrence have been determined based upon the following:

- As documented in Phifer and Nelson (2003), worse case infiltration occurs when both the topsoil and upper backfill have eroded away, since the underlying erosion barrier does not provide as efficient water storage for the promotion of evapotranspiration as the topsoil and upper backfill.
- Since degradation of the erosion barrier is assumed to be caused by intrusion of the overlying backfill following root decomposition, erosion barrier degradation will be assumed to cease once the upper backfill is eroded to three inches thick. Therefore erosion barrier properties will be taken as those at

complete erosion of the topsoil and upper backfill for determination of the worse case infiltration through the upper GCL. (see Table 4.4-1)

- As outlined in Appendix F, it is assumed that the material properties of the middle backfill and upper drainage layer become the same at year 2246 and remain constant thereafter. Therefore the middle backfill and upper drainage layer material properties will be taken as those determined at year 2246 for determination of the worse case infiltration through the upper GCL.
- The upper GCL becomes ineffective as a barrier layer at year 1800 when holes comprise 0.29 percent of the layer's area (see Appendix F). Therefore for determination of the worse case infiltration the GCL will be assigned as a barrier soil liner with the same material properties as the overlying middle backfill and upper drainage layer at year 2246.
- As previously demonstrated in Appendix F, the material properties of the lower drainage layer do not impact infiltration through the upper GCL. Completely silted in conditions will be assumed for the lower drainage layer for determination of the worse case infiltration.

From Section 4.2 the soil loss in terms of depth of loss per year for the topsoil and upper backfill was estimated to be 2.0E-04 inches/year and 1.2E-04 inches/year, respectively.

Determine time required to completely erode the topsoil:

$$6'' \div 2.0\text{E-}04 \text{ inches/year} = 30,000 \text{ years}$$

Determine time required to completely erode the upper backfill:

$$30'' \div 1.2\text{E-}04 \text{ inches/year} = 250,000 \text{ years}$$

Total time required to completely erode both the topsoil and upper backfill:

$$30,000 \text{ years} + 250,000 \text{ years} = 280,000 \text{ years}$$

Determine the hydraulic properties of the erosion barrier when the upper backfill has eroded to three inches thick:

Determine time required to erode the upper backfill to 3 inches thick:

$$((30'' - 3'') \div 1.2\text{E-}04 \text{ inches/year}) + 30,000 \text{ years} = 255,000 \text{ years}$$

Will use the average thickness of the topsoil plus upper backfill over the 225,000 years to determine the average hole penetration size in the erosion barrier over that period:

$$((30'' + 6'') \div 2) = 19.5''$$

Area of holes in erosion barrier due to root penetration:

$$\text{Average Erosion Barrier Depth} = 19.5'' + \frac{1}{2}(12'') = 25.5'' \approx 2.1'$$

Root Diameter for 4-6' roots at 2.1':

$$3'' \text{ diameter at } 1' \text{ depth and } 0.25'' \text{ at } 6'$$

$$(3'' - 0.25'') / (6' - 1') = 0.55'' / \text{ft}$$

$$\text{Diameter} = 0.25'' + [(6' - 2.1') \times 0.55''/\text{ft}] = 2.4''$$

Area for 4-6' roots at 2.1':

$$\text{Area} = 4 \times \frac{1}{4}\pi D^2 = \pi D^2 = \pi(2.4'')^2 = 18.1 \text{ in}^2$$

Root Diameter for 1-12' root at 2.1':

$$3'' \text{ diameter at } 1' \text{ depth and } 0.25'' \text{ at } 12'$$

$$(3''-0.25'')/(12'-1') = 0.25''/ft$$

$$\text{Diameter} = 0.25'' + [(12' - 2.1') \times 0.25''/ft] = 2.73''$$

Area of for 1-12' roots at 3.3':

$$\text{Area} = \frac{1}{4}\pi D^2 = \frac{1}{4}\pi(2.73'')^2 = 5.8 \text{ in}^2$$

Total area of holes in erosion barrier per tree:

$$\text{Total area} = 18.1 \text{ in}^2 + 5.8 \text{ in}^2 = 23.9 \text{ in}^2 \times ft^2/144 \text{ in}^2 \approx 0.17 \text{ ft}^2/\text{tree}$$

Total area of holes per acre per 100 years:

$$400 \text{ trees/acre/100 years}$$

$$\text{Total area} = 0.17 \text{ ft}^2/\text{tree} \times 400 \text{ trees/acre/100 years} = 68 \text{ ft}^2/\text{acre/100 years}$$

Area of holes in erosion barrier at year 255,000:

$$68 \text{ ft}^2/\text{acre} + [(255,000 \text{ yrs} - 300 \text{ yrs}) \times 68 \text{ ft}^2/\text{acre/100 years}] = 173,264 \text{ ft}^2/\text{acre}$$

This means that at 255,000 years the entire erosion barrier has been disturbed and mixed with the upper backfill layer. Therefore we will assume that the erosion barrier properties at this time becomes that of 2-inch to 6-inch granite stone filled with the backfill. This is different from the way the properties were determined for the erosion barrier through 10,000 years, where the area of the erosion barrier impacted by root penetrations and backfill intrusion was less than 10 percent. Consideration of the erosion barrier as stone with backfill fill pores is assumed to provide the properties for the erosion barrier after complete mixing with the backfill. For backfill dropping into hole and mixing with the stone will assume that the saturated hydraulic conductivity of the backfill increases from 1E-04 to 1E-03 cm/s.

Determine the combined soil material properties for the 2-inch to 6-inch granite stone filled with backfill:

The porosity of the 2-inch to 6-inch granite stone with a d_{50} (i.e. median size) of 4 inches is taken as 0.397 based upon the porosity of poorly graded gravel from USEPA 1994a and USEPA 1994b.

From Table 3.1-1 the properties of the backfill are as follows:

Property	Property Value
Saturated Hydraulic Conductivity	1.0E-03 cm/s ¹
Porosity	0.37
Field Capacity ¹	0.24
Wilting Point ¹	0.136

¹ For backfill dropping into hole and mixing with the stone will assume that the saturated hydraulic conductivity of the backfill increases from 1E-04 to 1E-03 cm/s.

The matrix of an individual granite stone itself is considered impermeable and non-porous. The porosity of a layer of granite stone is considered to be 0.397. When the granite stone porosity is filled with backfill, the resultant hydraulic properties, which are area or volume based, become that of the backfill times the granite stone porosity. The resultant hydraulic properties are shown below:

Property	Property Value
Saturated Hydraulic Conductivity	1.0E-03 cm/s \times 0.397 = 3.97E-04 cm/s
Porosity	0.37 \times 0.397 = 0.147
Field Capacity ¹	0.24 \times 0.397 = 0.095
Wilting Point ¹	0.136 \times 0.397 = 0.054

Based upon the above the following are the input properties utilized for the topsoil, upper backfill, erosion barrier, middle backfill, upper drainage layer, upper GCL, and lower drainage layer for determination of the worse case infiltration through the upper GCL.

Summary Hydraulic Properties layer for determination of the worse case infiltration through the upper GCL at 280,000 years:

Layer	Thickness (inches)	K (cm/s)	n	FC	WP
Topsoil	0	NA	NA	NA	NA
Upper Backfill	0	NA	NA	NA	NA
Erosion Barrier	12	3.97E-04	0.147	0.095	0.054
Middle Backfill	12	3.2E-03	0.375	0.16	0.0745
Upper Drainage Layer	12	3.2E-03	0.375	0.16	0.0745
Upper GCL	0.2	3.2E-03	0.375	0.16	0.0745
Lower Drainage Layer	24	1.0E-04	0.37	0.24	0.136

NA = not applicable

To determine the CN number for determination of runoff the HELP model utilizes default soil textures. The HELP model does not include any default soil textures equivalent to the erosion barrier therefore soil texture #5 which has been utilized for all other HELP model runs has also been utilized for this worse case run. This is considered appropriate since on a yearly average basis runoff is a very small percentage of the annual precipitation compared to evapotranspiration, lateral drainage, and infiltration.

The above parameter values were utilized as HELP model input to determine the worse case infiltration through the upper GCL at 280,000 years. The detailed HELP model input data and output file associated with this worse case infiltration are provided at the end of this appendix. The worse case infiltration through the upper GCL at 280,000 years was determined to be 18.118 inches/year.

Determine time required to completely erode the topsoil and erode the upper backfill to 22 inches thick (22 inches is the evapotranspiration zone depth utilized in the HELP modeling (Phifer and Nelson 2003)):

$$(6'' \div 2.0E-04 \text{ inches/year}) + ((30'' - 22'') \div 1.2E-04 \text{ inches/year}) = 96,667 \text{ years}$$

From year 96,667 it is assumed that infiltration through the upper GCL would increase linearly from approximately 14.1 inches/year to approximately 18.1 inches/year in year 280,000.

Year that Lower Drainage Layer Completely Silts In

From year 10,000 to year 96,667 it is assumed that the infiltration through the upper GCL is 14.1 inches per year. From previous calculations above:

- It takes a total of 13,269.8 ft³ of infiltrating water to completely silt in the lower drainage layer
- Through year 10,000 the infiltrating water volume was 10975.0 ft³

Determine water volume remaining after year 10,000 to completely silt in the lower drainage layer:

$$V = 13,269.8 \text{ ft}^3 - 10,975.0 \text{ ft}^3 = 2,294.8 \text{ ft}^3$$

Determine length of time to obtain this volume at 14.1 inches per year over a 1-ft² area:

$$\text{Time} = 2,294.8 \text{ ft}^3 \div (14.1 \text{ in/yr/ft}^2 \div 12 \text{ in/ft}) = 1,953 \text{ years}$$

Determine time to completely silt in the lower drainage layer:

$$\text{Time} = 10,000 \text{ years} + 1,953 \text{ years} = 11,953 \text{ years}$$

Preliminary 10,000 Year Input Data:

Input Parameter (HELP Model Query)				Generic Input Parameter Value			
Landfill area =				19.63 acres			
Percent of area where runoff is possible =				100%			
Do you want to specify initial moisture storage? (Y/N)				Y			
Amount of water or snow on surface =				0 in			
CN Input Parameter (HELP Model Query)				CN Input Parameter Value			
Slope =				3 %			
Slope length =				450 ft			
Soil Texture =				5 (HELP model default soil texture)			
Vegetation =				4 (i.e., a good stand of grass)			
HELP Model Computed Curve Number = 54.4							
Layer		Layer Number			Layer Type		
Topsoil		1			1 (vertical percolation layer)		
Upper Backfill		2			1 (vertical percolation layer)		
Erosion Barrier		3			1 (vertical percolation layer)		
Middle Backfill		4			1 (vertical percolation layer)		
Upper Drainage Layer		5			2 (lateral drainage layer)		
Upper GCL		6			4 (flexible membrane liner)		
Lower Backfill		7			1 (vertical percolation layer)		
Lower Drainage Layer		8			2 (lateral drainage layer)		
Lower GCL		9			3 (barrier soil liner)		
	Layer Type	Layer Thickness (in)	Soil Texture No.	Total Porosity (Vol/Vol)	Field Capacity (Vol/Vol)	Wilting Point (Vol/Vol)	Initial Moisture (Vol/Vol)
1	1	4.0		0.4	0.11	0.058	0.11
2	1	30		0.37	0.24	0.136	0.24
3	1	12		0.088	0.0726	0.0596	0.0726
4	1	12		0.375	0.16	0.0745	0.16
5	2	12		0.375	0.16	0.0745	0.16
6 *	4	0.2		0.75	0.747	0.40	0.75
7	1	58.57		0.37	0.24	0.136	0.24
8	2	24		0.37	0.24	0.136	0.24
9	3	0.2		0.75	0.747	0.40	0.75

* The input porosity, field capacity, and wilting point values of the upper GCL are ignored by the HELP model, since the upper GCL is designated as an geomembrane in order for the HELP model to take into account the holes produced by root penetration.

Preliminary 10,000 Year Input Data (continued):

	Layer Type	Sat. Hyd. Conductivity * (cm/sec)	Drainage Length (ft)	Drain Slope (%)	Leachate Recirc. (%)	Recirc. to Layer (#)	Subsurface Inflow (in/yr)
1	1	1.00E-03					
2	1	1.00E-04					
3	1	4.51E-04					
4	1	3.20E-03					
5	2	3.20E-03	450	3			
6	4	5.00E-09					
7	1	1.00E-04					
8	2	1.00E-04	150	11.4			
9	3	5.00E-09					
	Layer Type	Geomembrane Pinhole Density (#/acre)	Geomembrane Instal. Defects (#/acre)	Geomembrane Placement Quality	Geotextile Transmissivity (cm ² /sec)		
1	1						
2	1						
3	1						
4	1						
5	2						
6	4	0	728,360	1			
7	1						
8	2						
9	3						

The lack of values in the table for particular parameters in particular layers denotes that no HELP model input was required for that parameter in that layer. No data is missing from the table.

* The HELP model output often produces an increased number of significant digits for the Effective Saturated Hydraulic Conductivity over that of the actual input.

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*****
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**
**          HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE
**          HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)
**          DEVELOPED BY ENVIRONMENTAL LABORATORY
**          USAE WATERWAYS EXPERIMENT STATION
**          FOR USEPA RISK REDUCTION ENGINEERING LABORATORY
**
**
*****
*****
```

```
PRECIPITATION DATA FILE:  D:\HELP3\Hweather\ZPREC.D4
TEMPERATURE DATA FILE:   D:\HELP3\Hweather\ZTEMP.D7
SOLAR RADIATION DATA FILE: D:\HELP3\Hweather\ZSOLAR.D13
EVAPOTRANSPIRATION DATA:  D:\HELP3\Hweather\ZEVAP.D11
SOIL AND DESIGN DATA FILE: D:\HELP3\Hsdfmse\ZMSE10K.D10
OUTPUT DATA FILE:         D:\HELP3\Hsdfmse\ZMSE10Ko.OUT
```

TIME: 10: 6 DATE: 11/18/2003

```
*****

TITLE:  Degraded SDF MSE Vault Closure Cap - 10,000 Year Condition

*****
```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER
WERE SPECIFIED BY THE USER.

LAYER 1

```
TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 0
THICKNESS                =      4.00  INCHES
POROSITY                  =      0.4000 VOL/VOL
FIELD CAPACITY            =      0.1100 VOL/VOL
WILTING POINT            =      0.0580 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.1100 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.100000005000E-02 CM/SEC
```

LAYER 2

```
TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 0
THICKNESS                =     30.00  INCHES
POROSITY                  =      0.3700 VOL/VOL
FIELD CAPACITY            =      0.2400 VOL/VOL
WILTING POINT            =      0.1360 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.2400 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.999999975000E-04 CM/SEC
```

LAYER 3

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.0880	VOL/VOL
FIELD CAPACITY	=	0.0726	VOL/VOL
WILTING POINT	=	0.0596	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0726	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.451000000000E-03	CM/SEC

LAYER 4

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3750	VOL/VOL
FIELD CAPACITY	=	0.1600	VOL/VOL
WILTING POINT	=	0.0745	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1600	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.319999992000E-02	CM/SEC

LAYER 5

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3750	VOL/VOL
FIELD CAPACITY	=	0.1600	VOL/VOL
WILTING POINT	=	0.0745	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1600	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.319999992000E-02	CM/SEC
SLOPE	=	3.00	PERCENT
DRAINAGE LENGTH	=	450.0	FEET

LAYER 6

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.0000	VOL/VOL
FIELD CAPACITY	=	0.0000	VOL/VOL
WILTING POINT	=	0.0000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0000	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC
FML PINHOLE DENSITY	=	0.00	HOLES/ACRE
FML INSTALLATION DEFECTS	=	728360.00	HOLES/ACRE
FML PLACEMENT QUALITY	=	1	- PERFECT

LAYER 7

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	58.57	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC

LAYER 8

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	24.00	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC
SLOPE	=	11.40	PERCENT
DRAINAGE LENGTH	=	150.0	FEET

LAYER 9

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.7500	VOL/VOL
FIELD CAPACITY	=	0.7470	VOL/VOL
WILTING POINT	=	0.4000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.7500	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT
 SOIL DATA BASE USING SOIL TEXTURE # 5 WITH A
 GOOD STAND OF GRASS, A SURFACE SLOPE OF 3. %
 AND A SLOPE LENGTH OF 450. FEET.

SCS RUNOFF CURVE NUMBER	=	54.40	
FRACTION OF AREA ALLOWING RUNOFF	=	100.0	PERCENT
AREA PROJECTED ON HORIZONTAL PLANE	=	19.630	ACRES
EVAPORATIVE ZONE DEPTH	=	22.0	INCHES
INITIAL WATER IN EVAPORATIVE ZONE	=	4.760	INCHES
UPPER LIMIT OF EVAPORATIVE STORAGE	=	8.260	INCHES
LOWER LIMIT OF EVAPORATIVE STORAGE	=	2.680	INCHES
INITIAL SNOW WATER	=	0.000	INCHES
INITIAL WATER IN LAYER MATERIALS	=	32.318	INCHES
TOTAL INITIAL WATER	=	32.318	INCHES
TOTAL SUBSURFACE INFLOW	=	0.00	INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM
AUGUSTA GEORGIA

STATION LATITUDE = 33.22 DEGREES
 MAXIMUM LEAF AREA INDEX = 3.50
 START OF GROWING SEASON (JULIAN DATE) = 68
 END OF GROWING SEASON (JULIAN DATE) = 323
 EVAPORATIVE ZONE DEPTH = 22.0 INCHES
 AVERAGE ANNUAL WIND SPEED = 6.50 MPH
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 68.00 %
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 70.00 %
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 77.00 %
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 73.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
4.38	3.95	4.68	2.91	3.56	4.99
5.43	5.41	3.93	3.12	2.96	3.45

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
46.30	50.00	57.20	64.30	72.10	78.40
81.60	80.30	75.20	65.10	56.70	48.80

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA
AND STATION LATITUDE = 33.30 DEGREES

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 100

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	4.56	3.57	4.76	2.74	3.60	4.97
	5.81	5.32	4.41	2.99	2.75	3.41
STD. DEVIATIONS	2.44	1.60	2.47	1.31	2.12	2.60
	2.83	2.95	2.54	2.28	1.72	1.90

RUNOFF

TOTALS	0.004	0.000	0.005	0.000	0.000	0.002
	0.035	0.102	0.019	0.009	0.002	0.000

STD. DEVIATIONS	0.021	0.000	0.031	0.003	0.003	0.018
	0.118	0.428	0.087	0.070	0.016	0.002

EVAPOTRANSPIRATION

TOTALS	1.585	2.108	3.139	3.595	3.564	4.118
	4.884	4.502	3.371	1.616	0.951	1.122

STD. DEVIATIONS	0.216	0.228	0.561	0.787	1.523	1.541
	1.589	1.382	1.045	0.605	0.211	0.203

LATERAL DRAINAGE COLLECTED FROM LAYER 5

TOTALS	0.0061	0.0040	0.0043	0.0018	0.0006	0.0009
	0.0015	0.0019	0.0017	0.0018	0.0023	0.0039

STD. DEVIATIONS	0.0044	0.0032	0.0038	0.0018	0.0011	0.0016
	0.0022	0.0026	0.0028	0.0027	0.0029	0.0034

PERCOLATION/LEAKAGE THROUGH LAYER 6

TOTALS	2.8111	1.8484	1.9611	0.8245	0.2546	0.3913
	0.7036	0.8544	0.7993	0.8077	1.0512	1.7855

STD. DEVIATIONS	2.0300	1.4710	1.7572	0.8068	0.5189	0.7108
	1.0035	1.2114	1.2709	1.2375	1.3250	1.5606

LATERAL DRAINAGE COLLECTED FROM LAYER 8

TOTALS	0.4182	0.4907	0.5871	0.5667	0.4900	0.3788
	0.3217	0.2945	0.2785	0.2837	0.2830	0.3071

STD. DEVIATIONS	0.2832	0.2913	0.2837	0.2594	0.2084	0.1475
	0.1180	0.1321	0.1514	0.1573	0.2004	0.2202

PERCOLATION/LEAKAGE THROUGH LAYER 9

TOTALS	0.8280	0.9637	1.1544	1.1168	0.9762	0.7602
	0.6480	0.5933	0.5605	0.5709	0.5665	0.6141

STD. DEVIATIONS	0.5440	0.5496	0.5330	0.4857	0.3999	0.2890
	0.2346	0.2621	0.2975	0.3100	0.3861	0.4260

 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 6

AVERAGES	0.1639	0.1180	0.1143	0.0495	0.0148	0.0235
	0.0410	0.0498	0.0481	0.0470	0.0633	0.1040
STD. DEVIATIONS	0.1185	0.0941	0.1025	0.0486	0.0302	0.0428
	0.0585	0.0707	0.0766	0.0722	0.0799	0.0910

DAILY AVERAGE HEAD ON TOP OF LAYER 9

AVERAGES	31.2091	39.9104	43.5916	43.5755	36.8323	29.6012
	24.3827	22.3049	21.7702	21.4581	22.0050	23.0932
STD. DEVIATIONS	20.6375	22.8578	20.2177	19.0370	15.1675	11.3251
	8.8948	9.9418	11.6603	11.7583	15.1337	16.1600

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 100

	INCHES	CU. FEET	PERCENT
	-----	-----	-----
PRECIPITATION	48.90 (7.734)	3484469.2	100.00
RUNOFF	0.181 (0.4657)	12875.48	0.370
EVAPOTRANSPIRATION	34.556 (3.5776)	2462356.25	70.667
LATERAL DRAINAGE COLLECTED FROM LAYER 5	0.03075 (0.01239)	2191.156	0.06288
PERCOLATION/LEAKAGE THROUGH LAYER 6	14.09278 (5.66993)	1004207.940	28.81954
AVERAGE HEAD ON TOP OF LAYER 6	0.070 (0.028)		
LATERAL DRAINAGE COLLECTED FROM LAYER 8	4.69999 (1.66647)	334906.437	9.61141
PERCOLATION/LEAKAGE THROUGH LAYER 9	9.35258 (3.20171)	666435.500	19.12588
AVERAGE HEAD ON TOP OF LAYER 9	29.978 (10.348)		
CHANGE IN WATER STORAGE	0.080 (3.8058)	5703.87	0.164

PEAK DAILY VALUES FOR YEARS		1 THROUGH	100
		(INCHES)	(CU. FT.)
PRECIPITATION		6.87	489534.875
RUNOFF		2.803	199717.7340
DRAINAGE COLLECTED FROM LAYER	5	0.00426	303.65695
PERCOLATION/LEAKAGE THROUGH LAYER	6	1.950070	138955.95300
AVERAGE HEAD ON TOP OF LAYER	6	3.527	
MAXIMUM HEAD ON TOP OF LAYER	6	6.344	
LOCATION OF MAXIMUM HEAD IN LAYER	5		
(DISTANCE FROM DRAIN)		44.9 FEET	
DRAINAGE COLLECTED FROM LAYER	8	0.03765	2682.47388
PERCOLATION/LEAKAGE THROUGH LAYER	9	0.070386	5015.48437
AVERAGE HEAD ON TOP OF LAYER	9	82.570	
MAXIMUM HEAD ON TOP OF LAYER	9	101.074	
LOCATION OF MAXIMUM HEAD IN LAYER	8		
(DISTANCE FROM DRAIN)		63.2 FEET	
SNOW WATER		2.36	168188.7190
MAXIMUM VEG. SOIL WATER (VOL/VOL)			0.3685
MINIMUM VEG. SOIL WATER (VOL/VOL)			0.1218

*** Maximum heads are computed using McEnroe's equations. ***

Reference: Maximum Saturated Depth over Landfill Liner
by Bruce M. McEnroe, University of Kansas
ASCE Journal of Environmental Engineering
Vol. 119, No. 2, March 1993, pp. 262-270.

FINAL WATER STORAGE AT END OF YEAR 100

LAYER	(INCHES)	(VOL/VOL)
1	1.1692	0.2923
2	9.0114	0.3004
3	0.8712	0.0726
4	2.9221	0.2435
5	2.3601	0.1967
6	0.0000	0.0000
7	15.8699	0.2710
8	7.9688	0.3320
9	0.1500	0.7500
SNOW WATER	0.000	

Worse Case Infiltration through Upper GCL at 280,000 years Input Data:

Input Parameter (HELP Model Query)				Generic Input Parameter Value			
Landfill area =				19.63 acres			
Percent of area where runoff is possible =				100%			
Do you want to specify initial moisture storage? (Y/N)				Y			
Amount of water or snow on surface =				0 in			
CN Input Parameter (HELP Model Query)				CN Input Parameter Value			
Slope =				3 %			
Slope length =				450 ft			
Soil Texture =				5 (HELP model default soil texture)			
Vegetation =				4 (i.e., a good stand of grass)			
HELP Model Computed Curve Number = 54.4							
Layer			Layer Number		Layer Type		
Erosion Barrier			1		1 (vertical percolation layer)		
Middle Backfill			2		1 (vertical percolation layer)		
Upper Drainage Layer			3		2 (lateral drainage layer)		
Upper GCL			4		4 (flexible membrane liner)		
Lower Backfill			5		1 (vertical percolation layer)		
Lower Drainage Layer			6		2 (lateral drainage layer)		
Lower GCL			7		3 (barrier soil liner)		
	Layer Type	Layer Thickness (in)	Soil Texture No.	Total Porosity (Vol/Vol)	Field Capacity (Vol/Vol)	Wilting Point (Vol/Vol)	Initial Moisture (Vol/Vol)
1	1	12		0.147	0.095	0.054	0.095
2	1	12		0.375	0.16	0.0745	0.16
3	2	12		0.375	0.16	0.0745	0.16
4 *	4	0.2		0.75	0.747	0.40	0.75
5	1	58.57		0.37	0.24	0.136	0.24
6	2	24		0.37	0.24	0.136	0.24
7	3	0.2		0.75	0.747	0.40	0.75

* The input porosity, field capacity, and wilting point values of the upper GCL are ignored by the HELP model, since the upper GCL is designated as an geomembrane in order for the HELP model to take into account the holes produced by root penetration.

Worse Case Infiltration through Upper GCL at 280,000 years Input Data (continued):

	Layer Type	Sat. Hyd. Conductivity * (cm/sec)	Drainage Length (ft)	Drain Slope (%)	Leachate Recirc. (%)	Recirc. to Layer (#)	Subsurface Inflow (in/yr)
3	1	3.97E-04					
4	1	3.20E-03					
5	2	3.20E-03	450	3			
6	3	3.20E-03					
7	1	1.00E-04					
8	2	1.00E-04	150	11.4			
9	3	5.00E-09					
	Layer Type	Geomembrane Pinhole Density (#/acre)	Geomembrane Instal. Defects (#/acre)	Geomembrane Placement Quality	Geotextile Transmissivity (cm ² /sec)		
1	1						
2	1						
3	2						
4	3						
5	1						
6	2						
7	3						

The lack of values in the table for particular parameters in particular layers denotes that no HELP model input was required for that parameter in that layer. No data is missing from the table.

* The HELP model output often produces an increased number of significant digits for the Effective Saturated Hydraulic Conductivity over that of the actual input.


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**
**      HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE
**      HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)
**      DEVELOPED BY ENVIRONMENTAL LABORATORY
**      USAE WATERWAYS EXPERIMENT STATION
**      FOR USEPA RISK REDUCTION ENGINEERING LABORATORY
**
**
*****
*****

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PRECIPITATION DATA FILE:  D:\HELP3\Hweather\ZPREC.D4
TEMPERATURE DATA FILE:   D:\HELP3\Hweather\ZTEMP.D7
SOLAR RADIATION DATA FILE: D:\HELP3\Hweather\ZSOLAR.D13
EVAPOTRANSPIRATION DATA:  D:\HELP3\Hweather\ZEVAP.D11
SOIL AND DESIGN DATA FILE: D:\HELP3\Hsdfmse\ZMSEW.D10
OUTPUT DATA FILE:         D:\HELP3\Hsdfmse\ZMSEWout.OUT

```

TIME: 10:14 DATE: 11/18/2003

```

*****
TITLE:  Degraded SDF MSE Vault Closure Cap - Worse Case Infiltration
*****

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NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER
WERE SPECIFIED BY THE USER.

LAYER 1

```

      TYPE 1 - VERTICAL PERCOLATION LAYER
      MATERIAL TEXTURE NUMBER 0
THICKNESS           = 12.00 INCHES
POROSITY             = 0.1470 VOL/VOL
FIELD CAPACITY       = 0.0950 VOL/VOL
WILTING POINT        = 0.0540 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.0950 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.396999996000E-03 CM/SEC

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LAYER 2

```

      TYPE 1 - VERTICAL PERCOLATION LAYER
      MATERIAL TEXTURE NUMBER 0
THICKNESS           = 12.00 INCHES
POROSITY             = 0.3750 VOL/VOL
FIELD CAPACITY       = 0.1600 VOL/VOL
WILTING POINT        = 0.0745 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.1600 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.319999992000E-02 CM/SEC

```

LAYER 3

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3750	VOL/VOL
FIELD CAPACITY	=	0.1600	VOL/VOL
WILTING POINT	=	0.0745	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1600	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.319999992000E-02	CM/SEC
SLOPE	=	3.00	PERCENT
DRAINAGE LENGTH	=	450.0	FEET

LAYER 4

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.0000	VOL/VOL
FIELD CAPACITY	=	0.0000	VOL/VOL
WILTING POINT	=	0.0000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0000	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.319999992000E-02	CM/SEC
FML PINHOLE DENSITY	=	0.00	HOLES/ACRE
FML INSTALLATION DEFECTS	=	0.00	HOLES/ACRE
FML PLACEMENT QUALITY	=	4 - POOR	

LAYER 5

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	58.57	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC

LAYER 6

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	24.00	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC
SLOPE	=	11.40	PERCENT
DRAINAGE LENGTH	=	150.0	FEET

LAYER 7

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.7500	VOL/VOL
FIELD CAPACITY	=	0.7470	VOL/VOL
WILTING POINT	=	0.4000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.7500	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT
 SOIL DATA BASE USING SOIL TEXTURE # 5 WITH A
 GOOD STAND OF GRASS, A SURFACE SLOPE OF 3. %
 AND A SLOPE LENGTH OF 450. FEET.

SCS RUNOFF CURVE NUMBER	=	54.40	
FRACTION OF AREA ALLOWING RUNOFF	=	100.0	PERCENT
AREA PROJECTED ON HORIZONTAL PLANE	=	19.630	ACRES
EVAPORATIVE ZONE DEPTH	=	22.0	INCHES
INITIAL WATER IN EVAPORATIVE ZONE	=	2.740	INCHES
UPPER LIMIT OF EVAPORATIVE STORAGE	=	5.514	INCHES
LOWER LIMIT OF EVAPORATIVE STORAGE	=	1.393	INCHES
INITIAL SNOW WATER	=	0.000	INCHES
INITIAL WATER IN LAYER MATERIALS	=	24.947	INCHES
TOTAL INITIAL WATER	=	24.947	INCHES
TOTAL SUBSURFACE INFLOW	=	0.00	INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM
 AUGUSTA GEORGIA

STATION LATITUDE	=	33.22	DEGREES
MAXIMUM LEAF AREA INDEX	=	3.50	
START OF GROWING SEASON (JULIAN DATE)	=	68	
END OF GROWING SEASON (JULIAN DATE)	=	323	
EVAPORATIVE ZONE DEPTH	=	22.0	INCHES
AVERAGE ANNUAL WIND SPEED	=	6.50	MPH
AVERAGE 1ST QUARTER RELATIVE HUMIDITY	=	68.00	%
AVERAGE 2ND QUARTER RELATIVE HUMIDITY	=	70.00	%
AVERAGE 3RD QUARTER RELATIVE HUMIDITY	=	77.00	%
AVERAGE 4TH QUARTER RELATIVE HUMIDITY	=	73.00	%

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING
 COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL -----	FEB/AUG -----	MAR/SEP -----	APR/OCT -----	MAY/NOV -----	JUN/DEC -----
4.38	3.95	4.68	2.91	3.56	4.99
5.43	5.41	3.93	3.12	2.96	3.45

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL -----	FEB/AUG -----	MAR/SEP -----	APR/OCT -----	MAY/NOV -----	JUN/DEC -----
46.30	50.00	57.20	64.30	72.10	78.40
81.60	80.30	75.20	65.10	56.70	48.80

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA
AND STATION LATITUDE = 33.30 DEGREES

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 100

	JAN/JUL -----	FEB/AUG -----	MAR/SEP -----	APR/OCT -----	MAY/NOV -----	JUN/DEC -----
PRECIPITATION -----						
TOTALS	4.56 5.81	3.57 5.32	4.76 4.41	2.74 2.99	3.60 2.75	4.97 3.41
STD. DEVIATIONS	2.44 2.83	1.60 2.95	2.47 2.54	1.31 2.28	2.12 1.72	2.60 1.90
RUNOFF -----						
TOTALS	0.000 0.000	0.000 0.011	0.000 0.001	0.000 0.001	0.000 0.000	0.000 0.000
STD. DEVIATIONS	0.000 0.002	0.000 0.067	0.000 0.005	0.000 0.009	0.000 0.000	0.000 0.000
EVAPOTRANSPIRATION -----						
TOTALS	1.690 4.134	2.159 3.680	3.068 2.853	2.683 1.542	2.899 1.096	3.642 1.308
STD. DEVIATIONS	0.207 1.358	0.242 1.215	0.626 0.988	0.929 0.681	1.233 0.275	1.379 0.183

LATERAL DRAINAGE COLLECTED FROM LAYER 3

TOTALS	0.0008	0.0004	0.0006	0.0001	0.0002	0.0003
	0.0007	0.0012	0.0006	0.0004	0.0003	0.0004
STD. DEVIATIONS	0.0010	0.0008	0.0008	0.0004	0.0005	0.0006
	0.0012	0.0030	0.0012	0.0010	0.0007	0.0007

PERCOLATION/LEAKAGE THROUGH LAYER 4

TOTALS	2.9374	1.5545	1.9390	0.4182	0.7096	1.1286
	1.6798	1.6670	1.5253	1.2088	1.3831	1.9667
STD. DEVIATIONS	2.1374	1.4918	1.9054	0.6376	1.1873	1.3010
	1.5902	1.8269	1.6880	1.6071	1.4554	1.7034

LATERAL DRAINAGE COLLECTED FROM LAYER 6

TOTALS	0.5667	0.5846	0.6452	0.5865	0.4836	0.4112
	0.4215	0.4714	0.4704	0.4870	0.4528	0.4781
STD. DEVIATIONS	0.2933	0.2630	0.2670	0.2508	0.2069	0.1793
	0.1902	0.2291	0.2192	0.2254	0.2358	0.2441

PERCOLATION/LEAKAGE THROUGH LAYER 7

TOTALS	1.1134	1.1444	1.2654	1.1550	0.9630	0.8223
	0.8426	0.9371	0.9352	0.9680	0.8984	0.9484
STD. DEVIATIONS	0.5537	0.4871	0.4955	0.4677	0.3943	0.3467
	0.3696	0.4405	0.4206	0.4305	0.4447	0.4654

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 4

AVERAGES	0.0443	0.0284	0.0300	0.0070	0.0116	0.0180
	0.0297	0.0412	0.0274	0.0188	0.0224	0.0294
STD. DEVIATIONS	0.0378	0.0321	0.0326	0.0134	0.0213	0.0246
	0.0390	0.0832	0.0395	0.0323	0.0274	0.0291

DAILY AVERAGE HEAD ON TOP OF LAYER 7

AVERAGES	42.0370	47.4128	47.8032	45.0757	36.3302	32.0331
	31.7643	35.3471	36.4579	36.5203	35.0154	35.7764
STD. DEVIATIONS	21.0024	20.2134	18.7953	18.3316	14.9590	13.5913
	14.0198	16.7107	16.4870	16.3315	17.4309	17.6528

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS				1 THROUGH	100
				INCHES	CU. FEET
				PERCENT	
PRECIPITATION	48.90	(7.734)	3484469.2	100.00	
RUNOFF	0.013	(0.0681)	930.67	0.027	
EVAPOTRANSPIRATION	30.755	(3.0768)	2191490.50	62.893	
LATERAL DRAINAGE COLLECTED FROM LAYER 3	0.00600	(0.00409)	427.798	0.01228	
PERCOLATION/LEAKAGE THROUGH LAYER 4	18.11800	(6.24708)	1291032.500	37.05105	
AVERAGE HEAD ON TOP OF LAYER 4	0.026	(0.012)			
LATERAL DRAINAGE COLLECTED FROM LAYER 6	6.05887	(1.88577)	431736.125	12.39030	
PERCOLATION/LEAKAGE THROUGH LAYER 7	11.99337	(3.58072)	854610.312	24.52627	
AVERAGE HEAD ON TOP OF LAYER 7	38.464	(11.538)			
CHANGE IN WATER STORAGE	0.074	(3.2947)	5273.99	0.151	

PEAK DAILY VALUES FOR YEARS			1 THROUGH	100
			(INCHES)	(CU. FT.)
PRECIPITATION			6.87	489534.875
RUNOFF			0.588	41918.4062
DRAINAGE COLLECTED FROM LAYER 3			0.01519	1082.25757
PERCOLATION/LEAKAGE THROUGH LAYER 4			3.401600	242387.45300
AVERAGE HEAD ON TOP OF LAYER 4			12.569	
MAXIMUM HEAD ON TOP OF LAYER 4			19.880	
LOCATION OF MAXIMUM HEAD IN LAYER 3 (DISTANCE FROM DRAIN)			93.8 FEET	
DRAINAGE COLLECTED FROM LAYER 6			0.03765	2682.47388

PERCOLATION/LEAKAGE THROUGH LAYER	7	0.070386	5015.48437
AVERAGE HEAD ON TOP OF LAYER	7	82.570	
MAXIMUM HEAD ON TOP OF LAYER	7	101.074	
LOCATION OF MAXIMUM HEAD IN LAYER	6		
(DISTANCE FROM DRAIN)		63.2 FEET	
SNOW WATER		2.36	168188.7190
MAXIMUM VEG. SOIL WATER (VOL/VOL)			0.1884
MINIMUM VEG. SOIL WATER (VOL/VOL)			0.0633

*** Maximum heads are computed using McEnroe's equations. ***

Reference: Maximum Saturated Depth over Landfill Liner
by Bruce M. McEnroe, University of Kansas
ASCE Journal of Environmental Engineering
Vol. 119, No. 2, March 1993, pp. 262-270.

FINAL WATER STORAGE AT END OF YEAR 100

LAYER	(INCHES)	(VOL/VOL)
-----	-----	-----
1	1.2473	0.1039
2	2.5310	0.2109
3	2.0266	0.1689
4	0.0000	0.0000
5	17.7582	0.3032
6	8.6350	0.3598
7	0.1500	0.7500
SNOW WATER	0.000	

Appendix G, Degraded SDF MSE Vault Closure Cap (100 Years): HELP Model Input Data and Output File
(output file name: ZMSED1ou.OUT)

Input Data:

Input Parameter (HELP Model Query)				Generic Input Parameter Value			
Landfill area =				19.63 acres			
Percent of area where runoff is possible =				100%			
Do you want to specify initial moisture storage? (Y/N)				Y			
Amount of water or snow on surface =				0 inches			
CN Input Parameter (HELP Model Query)				CN Input Parameter Value			
Slope =				3 %			
Slope length =				450 ft			
Soil Texture =				5 (HELP model default soil texture)			
Vegetation =				4 (i.e., a good stand of grass)			
HELP Model Computed Curve Number = 54.4							
Layer			Layer Number		Layer Type		
Topsoil			1		1 (vertical percolation layer)		
Upper Backfill			2		1 (vertical percolation layer)		
Erosion Barrier			3		1 (vertical percolation layer)		
Middle Backfill			4		1 (vertical percolation layer)		
Upper Drainage Layer			5		2 (lateral drainage layer)		
Upper GCL			6		3 (barrier soil liner)		
Lower Backfill			7		1 (vertical percolation layer)		
Lower Drainage Layer			8		2 (lateral drainage layer)		
Lower GCL			9		3 (barrier soil liner)		
	Layer Type	Layer Thickness (in)	Soil Texture No.	Total Porosity (Vol/Vol)	Field Capacity (Vol/Vol)	Wilting Point (Vol/Vol)	Initial Moisture (Vol/Vol)
1	1	5.980		0.4	0.11	0.058	0.11
2	1	30		0.37	0.24	0.136	0.24
3	1	12		0.06	0.056	0.052	0.056
4	1	12		0.37	0.236	0.133	0.236
5	2	12		0.38	0.084	0.016	0.084
6	3	0.2		0.75	0.747	0.40	0.75
7	1	58.57		0.37	0.24	0.136	0.24
8	2	24		0.38	0.08	0.013	0.08
9	3	0.2		0.75	0.747	0.40	0.75

Input Data (continued):

	Layer Type	Sat. Hyd. Conductivity * (cm/sec)	Drainage Length (ft)	Drain Slope (%)	Leachate Recirc. (%)	Recirc. to Layer (#)	Subsurface Inflow (in/yr)
1	1	1.00E-03					
2	1	1.00E-04					
3	1	3.97E-04					
4	1	1.20E-04					
5	2	8.60E-02	450	3			
6	3	5.00E-09					
7	1	1.00E-04					
8	2	1.00E-01	150	11.4			
9	3	5.00E-09					
	Layer Type	Geomembrane Pinhole Density (#/acre)	Geomembrane Instal. Defects (#/acre)	Geomembrane Placement Quality	Geotextile Transmissivity (cm ² /sec)		
1	1						
2	1						
3	1						
4	1						
5	2						
6	3						
7	1						
8	2						
9	3						

The lack of values in the table for particular parameters in particular layers denotes that no HELP model input was required for that parameter in that layer. No data are missing from the table.

* The HELP model output often produces an increased number of significant digits for the Effective Saturated Hydraulic Conductivity over that of the actual input.

```
*****
*****
**
**
**
**      HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE
**      HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)
**      DEVELOPED BY ENVIRONMENTAL LABORATORY
**      USAE WATERWAYS EXPERIMENT STATION
**      FOR USEPA RISK REDUCTION ENGINEERING LABORATORY
**
**
*****
*****
```

```
PRECIPITATION DATA FILE:  D:\HELP3\Hweather\ZPREC.D4
TEMPERATURE DATA FILE:   D:\HELP3\Hweather\ZTEMP.D7
SOLAR RADIATION DATA FILE: D:\HELP3\Hweather\ZSOLAR.D13
EVAPOTRANSPIRATION DATA:  D:\HELP3\Hweather\ZEVAP.D11
SOIL AND DESIGN DATA FILE: D:\HELP3\Hsdfmse\ZMSED1.D10
OUTPUT DATA FILE:        D:\HELP3\Hsdfmse\ZMSED1ou.OUT
```

TIME: 10: 3 DATE: 11/14/2003

```
*****
TITLE:  Degraded SDF MSE Vault Closure Cap - 100 years
*****
```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER
WERE SPECIFIED BY THE USER.

LAYER 1

```
TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 0
THICKNESS           =      5.98  INCHES
POROSITY             =      0.4000 VOL/VOL
FIELD CAPACITY       =      0.1100 VOL/VOL
WILTING POINT       =      0.0580 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.1100 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.100000005000E-02 CM/SEC
```

LAYER 2

```
TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 0
THICKNESS           =     30.00  INCHES
POROSITY             =      0.3700 VOL/VOL
FIELD CAPACITY       =      0.2400 VOL/VOL
WILTING POINT       =      0.1360 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.2400 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.999999975000E-04 CM/SEC
```

LAYER 3

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.0600	VOL/VOL
FIELD CAPACITY	=	0.0560	VOL/VOL
WILTING POINT	=	0.0520	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0560	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.396999996000E-03	CM/SEC

LAYER 4

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2360	VOL/VOL
WILTING POINT	=	0.1330	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2360	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.119999997000E-03	CM/SEC

LAYER 5

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3800	VOL/VOL
FIELD CAPACITY	=	0.0840	VOL/VOL
WILTING POINT	=	0.0160	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0840	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.860000029000E-01	CM/SEC
SLOPE	=	3.00	PERCENT
DRAINAGE LENGTH	=	450.0	FEET

LAYER 6

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.7500	VOL/VOL
FIELD CAPACITY	=	0.7470	VOL/VOL
WILTING POINT	=	0.4000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.7500	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC

LAYER 7

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	58.57	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC

LAYER 8

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	24.00	INCHES
POROSITY	=	0.3800	VOL/VOL
FIELD CAPACITY	=	0.0800	VOL/VOL
WILTING POINT	=	0.0130	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0800	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.100000001000	CM/SEC
SLOPE	=	11.40	PERCENT
DRAINAGE LENGTH	=	150.0	FEET

LAYER 9

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.7500	VOL/VOL
FIELD CAPACITY	=	0.7470	VOL/VOL
WILTING POINT	=	0.4000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.7500	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT
SOIL DATA BASE USING SOIL TEXTURE # 5 WITH A
GOOD STAND OF GRASS, A SURFACE SLOPE OF 3. %
AND A SLOPE LENGTH OF 450. FEET.

SCS RUNOFF CURVE NUMBER	=	54.40	
FRACTION OF AREA ALLOWING RUNOFF	=	100.0	PERCENT
AREA PROJECTED ON HORIZONTAL PLANE	=	19.630	ACRES
EVAPORATIVE ZONE DEPTH	=	22.0	INCHES
INITIAL WATER IN EVAPORATIVE ZONE	=	4.503	INCHES
UPPER LIMIT OF EVAPORATIVE STORAGE	=	8.319	INCHES
LOWER LIMIT OF EVAPORATIVE STORAGE	=	2.526	INCHES
INITIAL SNOW WATER	=	0.000	INCHES
INITIAL WATER IN LAYER MATERIALS	=	28.647	INCHES
TOTAL INITIAL WATER	=	28.647	INCHES
TOTAL SUBSURFACE INFLOW	=	0.00	INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM
AUGUSTA GEORGIA

STATION LATITUDE = 33.22 DEGREES
MAXIMUM LEAF AREA INDEX = 3.50
START OF GROWING SEASON (JULIAN DATE) = 68
END OF GROWING SEASON (JULIAN DATE) = 323
EVAPORATIVE ZONE DEPTH = 22.0 INCHES
AVERAGE ANNUAL WIND SPEED = 6.50 MPH
AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 68.00 %
AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 70.00 %
AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 77.00 %
AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 73.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
4.38	3.95	4.68	2.91	3.56	4.99
5.43	5.41	3.93	3.12	2.96	3.45

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
46.30	50.00	57.20	64.30	72.10	78.40
81.60	80.30	75.20	65.10	56.70	48.80

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA
AND STATION LATITUDE = 33.30 DEGREES

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 100

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	4.56	3.57	4.76	2.74	3.60	4.97
	5.81	5.32	4.41	2.99	2.75	3.41
STD. DEVIATIONS	2.44	1.60	2.47	1.31	2.12	2.60
	2.83	2.95	2.54	2.28	1.72	1.90

RUNOFF

TOTALS	0.004	0.000	0.004	0.000	0.000	0.002
	0.027	0.091	0.016	0.006	0.002	0.001

STD. DEVIATIONS	0.020	0.000	0.027	0.000	0.002	0.015
	0.093	0.404	0.086	0.058	0.015	0.004

EVAPOTRANSPIRATION

TOTALS	1.577	2.093	3.072	3.553	3.657	4.141
	4.898	4.520	3.385	1.619	0.948	1.115

STD. DEVIATIONS	0.221	0.236	0.582	0.761	1.521	1.545
	1.589	1.377	1.040	0.606	0.207	0.205

LATERAL DRAINAGE COLLECTED FROM LAYER 5

TOTALS	2.4637	2.0770	1.9305	1.2378	0.4334	0.3122
	0.5454	0.8086	0.7465	0.7762	0.8953	1.4750

STD. DEVIATIONS	1.7880	1.5043	1.4526	1.0508	0.4452	0.5705
	0.7811	1.0159	1.0054	1.0565	1.1950	1.2982

PERCOLATION/LEAKAGE THROUGH LAYER 6

TOTALS	0.0705	0.0597	0.0558	0.0377	0.0163	0.0121
	0.0180	0.0252	0.0237	0.0243	0.0271	0.0429

STD. DEVIATIONS	0.0501	0.0418	0.0382	0.0287	0.0120	0.0156
	0.0214	0.0275	0.0276	0.0289	0.0323	0.0351

LATERAL DRAINAGE COLLECTED FROM LAYER 8

TOTALS	0.0570	0.0532	0.0544	0.0394	0.0137	0.0081
	0.0140	0.0206	0.0187	0.0201	0.0235	0.0377

STD. DEVIATIONS	0.0354	0.0340	0.0407	0.0385	0.0217	0.0149
	0.0199	0.0253	0.0244	0.0260	0.0305	0.0319

PERCOLATION/LEAKAGE THROUGH LAYER 9

TOTALS	0.0051	0.0049	0.0054	0.0051	0.0050	0.0039
	0.0037	0.0041	0.0040	0.0039	0.0037	0.0043

STD. DEVIATIONS	0.0009	0.0002	0.0003	0.0005	0.0009	0.0017
	0.0020	0.0020	0.0019	0.0020	0.0021	0.0019

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)						
DAILY AVERAGE HEAD ON TOP OF LAYER 6						
AVERAGES	2.4840	2.2841	1.9194	1.2805	0.4305	0.3204
	0.5418	0.8032	0.7723	0.7744	0.9190	1.4652
STD. DEVIATIONS	1.8885	1.7392	1.4460	1.1237	0.4423	0.5856
	0.7759	1.0092	1.0497	1.0610	1.2266	1.2896
DAILY AVERAGE HEAD ON TOP OF LAYER 9						
AVERAGES	0.0043	0.0044	0.0041	0.0031	0.0010	0.0006
	0.0011	0.0016	0.0015	0.0015	0.0018	0.0029
STD. DEVIATIONS	0.0027	0.0028	0.0031	0.0030	0.0016	0.0012
	0.0015	0.0019	0.0019	0.0020	0.0024	0.0024

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 100						
	INCHES		CU. FEET		PERCENT	
PRECIPITATION	48.90	(7.734)	3484469.2		100.00	
RUNOFF	0.154	(0.4339)	10950.01		0.314	
EVAPOTRANSPIRATION	34.578	(3.6236)	2463907.00		70.711	
LATERAL DRAINAGE COLLECTED FROM LAYER 5	13.70162	(5.47438)	976335.062		28.01962	
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.41335	(0.15024)	29453.703		0.84529	
AVERAGE HEAD ON TOP OF LAYER 6	1.166	(0.472)				
LATERAL DRAINAGE COLLECTED FROM LAYER 8	0.36024	(0.14546)	25669.234		0.73668	
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.05310	(0.00792)	3783.417		0.10858	
AVERAGE HEAD ON TOP OF LAYER 9	0.002	(0.001)				
CHANGE IN WATER STORAGE	0.054	(1.9521)	3824.79		0.110	

PEAK DAILY VALUES FOR YEARS 1 THROUGH 100		
	(INCHES)	(CU. FT.)
PRECIPITATION	6.87	489534.875
RUNOFF	2.648	188654.3750
DRAINAGE COLLECTED FROM LAYER 5	0.39526	28164.91210
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.032853	2341.00708
AVERAGE HEAD ON TOP OF LAYER 6	38.433	
MAXIMUM HEAD ON TOP OF LAYER 6	50.445	
LOCATION OF MAXIMUM HEAD IN LAYER 5 (DISTANCE FROM DRAIN)	156.8 FEET	
DRAINAGE COLLECTED FROM LAYER 8	0.01464	1042.84534
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.000199	14.20408
AVERAGE HEAD ON TOP OF LAYER 9	0.034	
MAXIMUM HEAD ON TOP OF LAYER 9	0.071	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	0.0 FEET	
SNOW WATER	2.36	168188.7190
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3691
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.1148

*** Maximum heads are computed using McEnroe's equations. ***

Reference: Maximum Saturated Depth over Landfill Liner
by Bruce M. McEnroe, University of Kansas
ASCE Journal of Environmental Engineering
Vol. 119, No. 2, March 1993, pp. 262-270.

FINAL WATER STORAGE AT END OF YEAR 100

LAYER	(INCHES)	(VOL/VOL)
1	1.6080	0.2689
2	8.9916	0.2997
3	0.7200	0.0600
4	4.2406	0.3534
5	2.1757	0.1813
6	0.1500	0.7500
7	14.0568	0.2400
8	1.9215	0.0801
9	0.1500	0.7500
SNOW WATER	0.000	

Appendix H, Degraded SDF MSE Vault Closure Cap (300 Years): HELP Model Input Data and Output File
(output file name: ZMSSED2ou.OUT)

Input Data:

Input Parameter (HELP Model Query)				Generic Input Parameter Value			
Landfill area =				19.63 acres			
Percent of area where runoff is possible =				100%			
Do you want to specify initial moisture storage? (Y/N)				Y			
Amount of water or snow on surface =				0 inches			
CN Input Parameter (HELP Model Query)				CN Input Parameter Value			
Slope =				3 %			
Slope length =				450 ft			
Soil Texture =				5 (HELP model default soil texture)			
Vegetation =				4 (i.e., a good stand of grass)			
HELP Model Computed Curve Number = 54.4							
Layer			Layer Number		Layer Type		
Topsoil			1		1 (vertical percolation layer)		
Upper Backfill			2		1 (vertical percolation layer)		
Erosion Barrier			3		1 (vertical percolation layer)		
Middle Backfill			4		1 (vertical percolation layer)		
Upper Drainage Layer			5		2 (lateral drainage layer)		
Upper GCL			6		4 (flexible membrane liner)		
Lower Backfill			7		1 (vertical percolation layer)		
Lower Drainage Layer			8		2 (lateral drainage layer)		
Lower GCL			9		3 (barrier soil liner)		
	Layer Type	Layer Thickness (in)	Soil Texture No.	Total Porosity (Vol/Vol)	Field Capacity (Vol/Vol)	Wilting Point (Vol/Vol)	Initial Moisture (Vol/Vol)
1	1	5.940		0.4	0.11	0.058	0.11
2	1	30		0.37	0.24	0.136	0.24
3	1	12		0.06	0.0562	0.0521	0.0562
4	1	12		0.371	0.229	0.128	0.229
5	2	12		0.379	0.089	0.021	0.089
6 *	4	0.2		0.75	0.747	0.40	0.75
7	1	58.57		0.37	0.24	0.136	0.24
8	2	24		0.38	0.0803	0.0134	0.0803
9	3	0.2		0.75	0.747	0.40	0.75

* The input porosity, field capacity, and wilting point values of the upper GCL are ignored by the HELP model, since the upper GCL is designated as an geomembrane in order for the HELP model to take into account the holes produced by root penetration.

Input Data (continued):

	Layer Type	Sat. Hyd. Conductivity * (cm/sec)	Drainage Length (ft)	Drain Slope (%)	Leachate Recirc. (%)	Recirc. to Layer (#)	Subsurface Inflow (in/yr)
1	1	1.00E-03					
2	1	1.00E-04					
3	1	3.98E-04					
4	1	1.60E-04					
5	2	6.30E-02	450	3			
6	4	5.00E-09					
7	1	1.00E-04					
8	2	9.98E-02	150	11.4			
9	3	5.00E-09					
	Layer Type	Geomembrane Pinhole Density (#/acre)	Geomembrane Instal. Defects (#/acre)	Geomembrane Placement Quality	Geotextile Transmissivity (cm ² /sec)		
1	1						
2	1						
3	1						
4	1						
5	2						
6	4	0	7,432	1			
7	1						
8	2						
9	3						

The lack of values in the table for particular parameters in particular layers denotes that no HELP model input was required for that parameter in that layer. No data are missing from the table.

* The HELP model output often produces an increased number of significant digits for the Effective Saturated Hydraulic Conductivity over that of the actual input.

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**
**          HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE
**          HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)
**          DEVELOPED BY ENVIRONMENTAL LABORATORY
**          USAE WATERWAYS EXPERIMENT STATION
**          FOR USEPA RISK REDUCTION ENGINEERING LABORATORY
**
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*****

```

```

PRECIPITATION DATA FILE:  D:\HELP3\Hweather\ZPREC.D4
TEMPERATURE DATA FILE:   D:\HELP3\Hweather\ZTEMP.D7
SOLAR RADIATION DATA FILE: D:\HELP3\Hweather\ZSOLAR.D13
EVAPOTRANSPIRATION DATA:  D:\HELP3\Hweather\ZEVAP.D11
SOIL AND DESIGN DATA FILE: D:\HELP3\Hsdfmse\ZMSED2.D10
OUTPUT DATA FILE:        D:\HELP3\Hsdfmse\ZMSED2ou.OUT

```

TIME: 13: 3 DATE: 11/14/2003

```

*****
TITLE:  Degraded SDF MSE Vault Closure Cap - 300 years
*****

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NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER
WERE SPECIFIED BY THE USER.

LAYER 1

```

          TYPE 1 - VERTICAL PERCOLATION LAYER
          MATERIAL TEXTURE NUMBER 0
THICKNESS           =      5.94  INCHES
POROSITY             =      0.4000 VOL/VOL
FIELD CAPACITY       =      0.1100 VOL/VOL
WILTING POINT        =      0.0580 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.1100 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.100000005000E-02 CM/SEC

```

LAYER 2

```

          TYPE 1 - VERTICAL PERCOLATION LAYER
          MATERIAL TEXTURE NUMBER 0
THICKNESS           =     30.00  INCHES
POROSITY             =      0.3700 VOL/VOL
FIELD CAPACITY       =      0.2400 VOL/VOL
WILTING POINT        =      0.1360 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.2400 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.999999975000E-04 CM/SEC

```

LAYER 3

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.0600	VOL/VOL
FIELD CAPACITY	=	0.0562	VOL/VOL
WILTING POINT	=	0.0521	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0562	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.398000004000E-03	CM/SEC

LAYER 4

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3710	VOL/VOL
FIELD CAPACITY	=	0.2290	VOL/VOL
WILTING POINT	=	0.1280	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2290	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.159999996000E-03	CM/SEC

LAYER 5

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3790	VOL/VOL
FIELD CAPACITY	=	0.0890	VOL/VOL
WILTING POINT	=	0.0210	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0890	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.630000010000E-01	CM/SEC
SLOPE	=	3.00	PERCENT
DRAINAGE LENGTH	=	450.0	FEET

LAYER 6

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.0000	VOL/VOL
FIELD CAPACITY	=	0.0000	VOL/VOL
WILTING POINT	=	0.0000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0000	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC
FML PINHOLE DENSITY	=	0.00	HOLES/ACRE
FML INSTALLATION DEFECTS	=	7432.00	HOLES/ACRE
FML PLACEMENT QUALITY	=	1	- PERFECT

LAYER 7

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	58.57	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC

LAYER 8

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	24.00	INCHES
POROSITY	=	0.3800	VOL/VOL
FIELD CAPACITY	=	0.0803	VOL/VOL
WILTING POINT	=	0.0134	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0803	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.997999981000E-01	CM/SEC
SLOPE	=	11.40	PERCENT
DRAINAGE LENGTH	=	150.0	FEET

LAYER 9

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.7500	VOL/VOL
FIELD CAPACITY	=	0.7470	VOL/VOL
WILTING POINT	=	0.4000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.7500	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT
 SOIL DATA BASE USING SOIL TEXTURE # 5 WITH A
 GOOD STAND OF GRASS, A SURFACE SLOPE OF 3. %
 AND A SLOPE LENGTH OF 450. FEET.

SCS RUNOFF CURVE NUMBER	=	54.40	
FRACTION OF AREA ALLOWING RUNOFF	=	100.0	PERCENT
AREA PROJECTED ON HORIZONTAL PLANE	=	19.630	ACRES
EVAPORATIVE ZONE DEPTH	=	22.0	INCHES
INITIAL WATER IN EVAPORATIVE ZONE	=	4.508	INCHES
UPPER LIMIT OF EVAPORATIVE STORAGE	=	8.318	INCHES
LOWER LIMIT OF EVAPORATIVE STORAGE	=	2.529	INCHES
INITIAL SNOW WATER	=	0.000	INCHES
INITIAL WATER IN LAYER MATERIALS	=	28.478	INCHES
TOTAL INITIAL WATER	=	28.478	INCHES
TOTAL SUBSURFACE INFLOW	=	0.00	INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM
AUGUSTA GEORGIA

STATION LATITUDE = 33.22 DEGREES
 MAXIMUM LEAF AREA INDEX = 3.50
 START OF GROWING SEASON (JULIAN DATE) = 68
 END OF GROWING SEASON (JULIAN DATE) = 323
 EVAPORATIVE ZONE DEPTH = 22.0 INCHES
 AVERAGE ANNUAL WIND SPEED = 6.50 MPH
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 68.00 %
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 70.00 %
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 77.00 %
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 73.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
4.38	3.95	4.68	2.91	3.56	4.99
5.43	5.41	3.93	3.12	2.96	3.45

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
46.30	50.00	57.20	64.30	72.10	78.40
81.60	80.30	75.20	65.10	56.70	48.80

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA
AND STATION LATITUDE = 33.30 DEGREES

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 100

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	4.56	3.57	4.76	2.74	3.60	4.97
	5.81	5.32	4.41	2.99	2.75	3.41
STD. DEVIATIONS	2.44	1.60	2.47	1.31	2.12	2.60
	2.83	2.95	2.54	2.28	1.72	1.90

RUNOFF

TOTALS	0.004	0.000	0.004	0.000	0.000	0.002
	0.027	0.091	0.016	0.006	0.002	0.001

STD. DEVIATIONS	0.019	0.000	0.027	0.000	0.002	0.014
	0.092	0.404	0.086	0.058	0.014	0.004

EVAPOTRANSPIRATION

TOTALS	1.577	2.094	3.075	3.555	3.655	4.138
	4.896	4.521	3.385	1.618	0.948	1.115

STD. DEVIATIONS	0.221	0.236	0.581	0.760	1.525	1.545
	1.588	1.379	1.041	0.606	0.207	0.205

LATERAL DRAINAGE COLLECTED FROM LAYER 5

TOTALS	1.9675	1.6811	1.5612	1.0183	0.3681	0.2529
	0.4394	0.6497	0.6048	0.6276	0.7212	1.1759

STD. DEVIATIONS	1.4134	1.1907	1.1489	0.8430	0.3598	0.4555
	0.6216	0.8081	0.8015	0.8449	0.9563	1.0331

PERCOLATION/LEAKAGE THROUGH LAYER 6

TOTALS	0.5469	0.4622	0.4273	0.2803	0.1015	0.0710
	0.1209	0.1782	0.1674	0.1730	0.1974	0.3210

STD. DEVIATIONS	0.4156	0.3409	0.3176	0.2402	0.0971	0.1234
	0.1688	0.2203	0.2228	0.2328	0.2601	0.2812

LATERAL DRAINAGE COLLECTED FROM LAYER 8

TOTALS	0.1837	0.3398	0.4655	0.4517	0.4250	0.2963
	0.1338	0.0828	0.1195	0.1636	0.1507	0.1796

STD. DEVIATIONS	0.1968	0.3374	0.3167	0.2435	0.2283	0.1928
	0.1367	0.1042	0.1457	0.1809	0.1784	0.2299

PERCOLATION/LEAKAGE THROUGH LAYER 9

TOTALS	0.0044	0.0047	0.0058	0.0058	0.0060	0.0048
	0.0040	0.0038	0.0038	0.0040	0.0038	0.0041

STD. DEVIATIONS	0.0016	0.0016	0.0012	0.0009	0.0009	0.0019
	0.0020	0.0021	0.0021	0.0022	0.0021	0.0021

 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 6

AVERAGES	2.7195	2.5205	2.1254	1.4394	0.4991	0.3543
	0.5958	0.8820	0.8562	0.8558	1.0106	1.5945
STD. DEVIATIONS	2.0691	1.8623	1.5804	1.2367	0.4879	0.6382
	0.8428	1.0989	1.1477	1.1616	1.3399	1.4009

DAILY AVERAGE HEAD ON TOP OF LAYER 9

AVERAGES	0.0140	0.0283	0.0354	0.0355	0.0323	0.0233
	0.0102	0.0063	0.0094	0.0124	0.0118	0.0137
STD. DEVIATIONS	0.0150	0.0280	0.0241	0.0191	0.0174	0.0151
	0.0104	0.0079	0.0114	0.0138	0.0140	0.0175

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 100

	INCHES		CU. FEET	PERCENT
	-----	-----	-----	-----
PRECIPITATION	48.90	(7.734)	3484469.2	100.00
RUNOFF	0.153	(0.4340)	10931.62	0.314
EVAPOTRANSPIRATION	34.578	(3.6248)	2463907.00	70.711
LATERAL DRAINAGE COLLECTED FROM LAYER 5	11.06777	(4.39790)	788655.062	22.63344
PERCOLATION/LEAKAGE THROUGH LAYER 6	3.04724	(1.22367)	217136.625	6.23156
AVERAGE HEAD ON TOP OF LAYER 6	1.288	(0.519)		
LATERAL DRAINAGE COLLECTED FROM LAYER 8	2.99194	(1.09253)	213196.031	6.11847
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.05487	(0.00829)	3909.907	0.11221
AVERAGE HEAD ON TOP OF LAYER 9	0.019	(0.007)		
CHANGE IN WATER STORAGE	0.054	(2.1676)	3869.66	0.111

PEAK DAILY VALUES FOR YEARS 1 THROUGH 100		
	(INCHES)	(CU. FT.)
PRECIPITATION	6.87	489534.875
RUNOFF	2.646	188573.8440
DRAINAGE COLLECTED FROM LAYER 5	0.28968	20641.51170
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.239722	17081.85940
AVERAGE HEAD ON TOP OF LAYER 6	36.972	
MAXIMUM HEAD ON TOP OF LAYER 6	48.836	
LOCATION OF MAXIMUM HEAD IN LAYER 5 (DISTANCE FROM DRAIN)	154.2 FEET	
DRAINAGE COLLECTED FROM LAYER 8	0.08807	6275.57715
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.000347	24.69121
AVERAGE HEAD ON TOP OF LAYER 9	0.207	
MAXIMUM HEAD ON TOP OF LAYER 9	0.410	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	0.0 FEET	
SNOW WATER	2.36	168188.7190
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3688
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.1149

*** Maximum heads are computed using McEnroe's equations. ***

Reference: Maximum Saturated Depth over Landfill Liner
by Bruce M. McEnroe, University of Kansas
ASCE Journal of Environmental Engineering
Vol. 119, No. 2, March 1993, pp. 262-270.

FINAL WATER STORAGE AT END OF YEAR 100

LAYER	(INCHES)	(VOL/VOL)
1	1.6020	0.2697
2	9.2013	0.3067
3	0.7200	0.0600
4	3.9758	0.3313
5	2.2321	0.1860
6	0.0000	0.0000
7	14.0999	0.2407
8	1.9272	0.0803
9	0.1500	0.7500
SNOW WATER	0.000	

Appendix I, Degraded SDF MSE Vault Closure Cap (550 Years): HELP Model Input Data and Output File
(output file name: ZMSED3ou.OUT)

Input Data:

Input Parameter (HELP Model Query)				Generic Input Parameter Value			
Landfill area =				19.63 acres			
Percent of area where runoff is possible =				100%			
Do you want to specify initial moisture storage? (Y/N)				Y			
Amount of water or snow on surface =				0 inches			
CN Input Parameter (HELP Model Query)				CN Input Parameter Value			
Slope =				3 %			
Slope length =				450 ft			
Soil Texture =				5 (HELP model default soil texture)			
Vegetation =				4 (i.e., a good stand of grass)			
HELP Model Computed Curve Number = 54.4							
Layer			Layer Number		Layer Type		
Topsoil			1		1 (vertical percolation layer)		
Upper Backfill			2		1 (vertical percolation layer)		
Erosion Barrier			3		1 (vertical percolation layer)		
Middle Backfill			4		1 (vertical percolation layer)		
Upper Drainage Layer			5		2 (lateral drainage layer)		
Upper GCL			6		4 (flexible membrane liner)		
Lower Backfill			7		1 (vertical percolation layer)		
Lower Drainage Layer			8		2 (lateral drainage layer)		
Lower GCL			9		3 (barrier soil liner)		
	Layer Type	Layer Thickness (in)	Soil Texture No.	Total Porosity (Vol/Vol)	Field Capacity (Vol/Vol)	Wilting Point (Vol/Vol)	Initial Moisture (Vol/Vol)
1	1	5.890		0.4	0.11	0.058	0.11
2	1	30		0.37	0.24	0.136	0.24
3	1	12		0.061	0.0566	0.0523	0.0566
4	1	12		0.371	0.220	0.121	0.220
5	2	12		0.379	0.10	0.028	0.10
6 *	4	0.2		0.75	0.747	0.40	0.75
7	1	58.57		0.37	0.24	0.136	0.24
8	2	24		0.378	0.0814	0.0150	0.0814
9	3	0.2		0.75	0.747	0.40	0.75

* The input porosity, field capacity, and wilting point values of the upper GCL are ignored by the HELP model, since the upper GCL is designated as an geomembrane in order for the HELP model to take into account the holes produced by root penetration.

Input Data (continued):

	Layer Type	Sat. Hyd. Conductivity * (cm/sec)	Drainage Length (ft)	Drain Slope (%)	Leachate Recirc. (%)	Recirc. to Layer (#)	Subsurface Inflow (in/yr)
1	1	1.00E-03					
2	1	1.00E-04					
3	1	3.99E-04					
4	1	2.30E-04					
5	2	4.30E-02	450	3			
6	4	5.00E-09					
7	1	1.00E-04					
8	2	9.89E-02	150	11.4			
9	3	5.00E-09					
	Layer Type	Geomembrane Pinhole Density (#/acre)	Geomembrane Instal. Defects (#/acre)	Geomembrane Placement Quality	Geotextile Transmissivity (cm ² /sec)		
1	1						
2	1						
3	1						
4	1						
5	2						
6	4	0	26,013	1			
7	1						
8	2						
9	3						

The lack of values in the table for particular parameters in particular layers denotes that no HELP model input was required for that parameter in that layer. No data are missing from the table.

* The HELP model output often produces an increased number of significant digits for the Effective Saturated Hydraulic Conductivity over that of the actual input.

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**
**          HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE
**          HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)
**          DEVELOPED BY ENVIRONMENTAL LABORATORY
**          USAE WATERWAYS EXPERIMENT STATION
**          FOR USEPA RISK REDUCTION ENGINEERING LABORATORY
**
**
*****
*****
```

```
PRECIPITATION DATA FILE:  D:\HELP3\Hweather\ZPREC.D4
TEMPERATURE DATA FILE:   D:\HELP3\Hweather\ZTEMP.D7
SOLAR RADIATION DATA FILE: D:\HELP3\Hweather\ZSOLAR.D13
EVAPOTRANSPIRATION DATA:  D:\HELP3\Hweather\ZEVAP.D11
SOIL AND DESIGN DATA FILE: D:\HELP3\Hsdfmse\ZMSED3.D10
OUTPUT DATA FILE:         D:\HELP3\Hsdfmse\ZMSED3ou.OUT
```

TIME: 13: 8 DATE: 11/14/2003

```
*****

TITLE:  Degraded SDF MSE Vault Closure Cap - 550 years

*****
```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER
WERE SPECIFIED BY THE USER.

LAYER 1

```
TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 0
THICKNESS           = 5.89 INCHES
POROSITY             = 0.4000 VOL/VOL
FIELD CAPACITY       = 0.1100 VOL/VOL
WILTING POINT        = 0.0580 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.1100 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.100000005000E-02 CM/SEC
```

LAYER 2

```
TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 0
THICKNESS           = 30.00 INCHES
POROSITY             = 0.3700 VOL/VOL
FIELD CAPACITY       = 0.2400 VOL/VOL
WILTING POINT        = 0.1360 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.2400 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.999999975000E-04 CM/SEC
```

LAYER 3

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.0610	VOL/VOL
FIELD CAPACITY	=	0.0566	VOL/VOL
WILTING POINT	=	0.0523	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0566	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.399000011000E-03	CM/SEC

LAYER 4

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3710	VOL/VOL
FIELD CAPACITY	=	0.2200	VOL/VOL
WILTING POINT	=	0.1210	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2200	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.230000005000E-03	CM/SEC

LAYER 5

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3790	VOL/VOL
FIELD CAPACITY	=	0.1000	VOL/VOL
WILTING POINT	=	0.0280	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1000	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.430000015000E-01	CM/SEC
SLOPE	=	3.00	PERCENT
DRAINAGE LENGTH	=	450.0	FEET

LAYER 6

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.0000	VOL/VOL
FIELD CAPACITY	=	0.0000	VOL/VOL
WILTING POINT	=	0.0000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0000	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC
FML PINHOLE DENSITY	=	0.00	HOLES/ACRE
FML INSTALLATION DEFECTS	=	26013.00	HOLES/ACRE
FML PLACEMENT QUALITY	=	1	PERFECT

LAYER 7

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	58.57	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC

LAYER 8

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	24.00	INCHES
POROSITY	=	0.3780	VOL/VOL
FIELD CAPACITY	=	0.0814	VOL/VOL
WILTING POINT	=	0.0150	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0814	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.988999978000E-01	CM/SEC
SLOPE	=	11.40	PERCENT
DRAINAGE LENGTH	=	150.0	FEET

LAYER 9

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.7500	VOL/VOL
FIELD CAPACITY	=	0.7470	VOL/VOL
WILTING POINT	=	0.4000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.7500	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT
 SOIL DATA BASE USING SOIL TEXTURE # 5 WITH A
 GOOD STAND OF GRASS, A SURFACE SLOPE OF 3. %
 AND A SLOPE LENGTH OF 450. FEET.

SCS RUNOFF CURVE NUMBER	=	54.40	
FRACTION OF AREA ALLOWING RUNOFF	=	100.0	PERCENT
AREA PROJECTED ON HORIZONTAL PLANE	=	19.630	ACRES
EVAPORATIVE ZONE DEPTH	=	22.0	INCHES
INITIAL WATER IN EVAPORATIVE ZONE	=	4.514	INCHES
UPPER LIMIT OF EVAPORATIVE STORAGE	=	8.317	INCHES
LOWER LIMIT OF EVAPORATIVE STORAGE	=	2.533	INCHES
INITIAL SNOW WATER	=	0.000	INCHES
INITIAL WATER IN LAYER MATERIALS	=	28.527	INCHES
TOTAL INITIAL WATER	=	28.527	INCHES
TOTAL SUBSURFACE INFLOW	=	0.00	INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM
AUGUSTA GEORGIA

STATION LATITUDE = 33.22 DEGREES
MAXIMUM LEAF AREA INDEX = 3.50
START OF GROWING SEASON (JULIAN DATE) = 68
END OF GROWING SEASON (JULIAN DATE) = 323
EVAPORATIVE ZONE DEPTH = 22.0 INCHES
AVERAGE ANNUAL WIND SPEED = 6.50 MPH
AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 68.00 %
AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 70.00 %
AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 77.00 %
AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 73.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
4.38	3.95	4.68	2.91	3.56	4.99
5.43	5.41	3.93	3.12	2.96	3.45

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
46.30	50.00	57.20	64.30	72.10	78.40
81.60	80.30	75.20	65.10	56.70	48.80

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA
AND STATION LATITUDE = 33.30 DEGREES

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 100

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	4.56	3.57	4.76	2.74	3.60	4.97
	5.81	5.32	4.41	2.99	2.75	3.41
STD. DEVIATIONS	2.44	1.60	2.47	1.31	2.12	2.60
	2.83	2.95	2.54	2.28	1.72	1.90

RUNOFF

TOTALS	0.004	0.000	0.004	0.000	0.000	0.002
	0.027	0.091	0.017	0.006	0.002	0.001
STD. DEVIATIONS	0.019	0.000	0.027	0.000	0.002	0.014
	0.092	0.405	0.087	0.058	0.014	0.004

EVAPOTRANSPIRATION

TOTALS	1.578	2.094	3.079	3.557	3.651	4.139
	4.896	4.520	3.383	1.619	0.948	1.116
STD. DEVIATIONS	0.221	0.236	0.581	0.759	1.525	1.546
	1.589	1.381	1.040	0.605	0.207	0.205

LATERAL DRAINAGE COLLECTED FROM LAYER 5

TOTALS	1.1341	0.9257	0.8726	0.5419	0.1879	0.1415
	0.2566	0.3693	0.3376	0.3535	0.4110	0.6826
STD. DEVIATIONS	0.8224	0.6765	0.6756	0.4618	0.2027	0.2667
	0.3678	0.4673	0.4642	0.4849	0.5508	0.6048

PERCOLATION/LEAKAGE THROUGH LAYER 6

TOTALS	1.4438	1.1770	1.1064	0.6896	0.2394	0.1811
	0.3262	0.4687	0.4304	0.4504	0.5215	0.8651
STD. DEVIATIONS	1.0609	0.8738	0.8575	0.5957	0.2560	0.3372
	0.4653	0.5914	0.5930	0.6196	0.6973	0.7657

LATERAL DRAINAGE COLLECTED FROM LAYER 8

TOTALS	0.8559	1.1571	1.1806	1.0663	0.7649	0.4994
	0.3038	0.2637	0.3633	0.4507	0.4561	0.4664
STD. DEVIATIONS	0.8485	0.9655	0.6764	0.7197	0.3397	0.2480
	0.2485	0.3425	0.4941	0.4482	0.5846	0.5382

PERCOLATION/LEAKAGE THROUGH LAYER 9

TOTALS	0.0057	0.0064	0.0074	0.0071	0.0068	0.0056
	0.0046	0.0039	0.0043	0.0047	0.0045	0.0045
STD. DEVIATIONS	0.0028	0.0027	0.0017	0.0018	0.0008	0.0015
	0.0021	0.0023	0.0025	0.0026	0.0026	0.0027

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)						
DAILY AVERAGE HEAD ON TOP OF LAYER 6						
AVERAGES	2.2638	2.0233	1.7350	1.1168	0.3732	0.2905
	0.5098	0.7337	0.6960	0.7048	0.8438	1.3561
STD. DEVIATIONS	1.6644	1.5031	1.3451	0.9661	0.4027	0.5475
	0.7307	0.9283	0.9618	0.9726	1.1308	1.2015
DAILY AVERAGE HEAD ON TOP OF LAYER 9						
AVERAGES	0.0656	0.0973	0.0905	0.0845	0.0587	0.0396
	0.0233	0.0202	0.0288	0.0346	0.0361	0.0358
STD. DEVIATIONS	0.0651	0.0813	0.0519	0.0570	0.0260	0.0197
	0.0191	0.0263	0.0392	0.0344	0.0463	0.0413

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 100						
	INCHES		CU. FEET		PERCENT	
PRECIPITATION	48.90	(7.734)	3484469.2		100.00	
RUNOFF	0.153	(0.4344)	10929.73		0.314	
EVAPOTRANSPIRATION	34.580	(3.6253)	2464038.00		70.715	
LATERAL DRAINAGE COLLECTED FROM LAYER 5	6.21423	(2.47878)	442806.406		12.70800	
PERCOLATION/LEAKAGE THROUGH LAYER 6	7.89958	(3.15969)	562899.812		16.15454	
AVERAGE HEAD ON TOP OF LAYER 6	1.054	(0.422)				
LATERAL DRAINAGE COLLECTED FROM LAYER 8	7.82825	(2.95993)	557816.812		16.00866	
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.06554	(0.01153)	4669.966		0.13402	
AVERAGE HEAD ON TOP OF LAYER 9	0.051	(0.019)				
CHANGE IN WATER STORAGE	0.059	(2.5916)	4208.62		0.121	

PEAK DAILY VALUES FOR YEARS 1 THROUGH 100		
	(INCHES)	(CU. FT.)
PRECIPITATION	6.87	489534.875
RUNOFF	2.652	188986.2810
DRAINAGE COLLECTED FROM LAYER 5	0.19569	13944.58300
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.447973	31921.14650
AVERAGE HEAD ON TOP OF LAYER 6	21.780	
MAXIMUM HEAD ON TOP OF LAYER 6	31.661	
LOCATION OF MAXIMUM HEAD IN LAYER 5 (DISTANCE FROM DRAIN)	122.6 FEET	
DRAINAGE COLLECTED FROM LAYER 8	0.31282	22290.66990
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.000802	57.18127
AVERAGE HEAD ON TOP OF LAYER 9	0.744	
MAXIMUM HEAD ON TOP OF LAYER 9	1.445	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	2.4 FEET	
SNOW WATER	2.36	168188.7190
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3691
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.1151

*** Maximum heads are computed using McEnroe's equations. ***

Reference: Maximum Saturated Depth over Landfill Liner
by Bruce M. McEnroe, University of Kansas
ASCE Journal of Environmental Engineering
Vol. 119, No. 2, March 1993, pp. 262-270.

FINAL WATER STORAGE AT END OF YEAR 100

LAYER	(INCHES)	(VOL/VOL)
1	1.5974	0.2712
2	9.1911	0.3064
3	0.7320	0.0610
4	3.8417	0.3201
5	2.3313	0.1943
6	0.0000	0.0000
7	14.6255	0.2497
8	1.9646	0.0819
9	0.1500	0.7500
SNOW WATER	0.000	

Appendix J, Degraded SDF MSE Vault Closure Cap (1,000 Years): HELP Model Input Data and Output File
(output file name: ZMSED4ou.OUT)

Input Data:

Input Parameter (HELP Model Query)				Generic Input Parameter Value			
Landfill area =				19.63 acres			
Percent of area where runoff is possible =				100%			
Do you want to specify initial moisture storage? (Y/N)				Y			
Amount of water or snow on surface =				0 inches			
CN Input Parameter (HELP Model Query)				CN Input Parameter Value			
Slope =				3 %			
Slope length =				450 ft			
Soil Texture =				5 (HELP model default soil texture)			
Vegetation =				4 (i.e., a good stand of grass)			
HELP Model Computed Curve Number = 54.4							
Layer		Layer Number		Layer Type			
Topsoil		1		1 (vertical percolation layer)			
Upper Backfill		2		1 (vertical percolation layer)			
Erosion Barrier		3		1 (vertical percolation layer)			
Middle Backfill		4		1 (vertical percolation layer)			
Upper Drainage Layer		5		2 (lateral drainage layer)			
Upper GCL		6		4 (flexible membrane liner)			
Lower Backfill		7		1 (vertical percolation layer)			
Lower Drainage Layer		8		2 (lateral drainage layer)			
Lower GCL		9		3 (barrier soil liner)			
	Layer Type	Layer Thickness (in)	Soil Texture No.	Total Porosity (Vol/Vol)	Field Capacity (Vol/Vol)	Wilting Point (Vol/Vol)	Initial Moisture (Vol/Vol)
1	1	5.8		0.4	0.11	0.058	0.11
2	1	30		0.37	0.24	0.136	0.24
3	1	12		0.062	0.0574	0.0526	0.0574
4	1	12		0.372	0.204	0.109	0.204
5	2	12		0.378	0.116	0.040	0.116
6 *	4	0.2		0.75	0.747	0.40	0.75
7	1	58.57		0.37	0.24	0.136	0.24
8	2	24		0.374	0.0851	0.0203	0.0851
9	3	0.2		0.75	0.747	0.40	0.75

* The input porosity, field capacity, and wilting point values of the upper GCL are ignored by the HELP model, since the upper GCL is designated as an geomembrane in order for the HELP model to take into account the holes produced by root penetration.

Input Data (continued):

	Layer Type	Sat. Hyd. Conductivity * (cm/sec)	Drainage Length (ft)	Drain Slope (%)	Leachate Recirc. (%)	Recirc. to Layer (#)	Subsurface Inflow (in/yr)
1	1	1.00E-03					
2	1	1.00E-04					
3	1	4.01E-04					
4	1	4.60E-04					
5	2	2.10E-02	450	3			
6	4	5.00E-09					
7	1	1.00E-04					
8	2	9.61E-02	150	11.4			
9	3	5.00E-09					
	Layer Type	Geomembrane Pinhole Density (#/acre)	Geomembrane Instal. Defects (#/acre)	Geomembrane Placement Quality	Geotextile Transmissivity (cm ² /sec)		
1	1						
2	1						
3	1						
4	1						
5	2						
6	4	0	59,458	1			
7	1						
8	2						
9	3						

The lack of values in the table for particular parameters in particular layers denotes that no HELP model input was required for that parameter in that layer. No data are missing from the table.

* The HELP model output often produces an increased number of significant digits for the Effective Saturated Hydraulic Conductivity over that of the actual input.

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**
**          HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE
**          HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)
**          DEVELOPED BY ENVIRONMENTAL LABORATORY
**          USAE WATERWAYS EXPERIMENT STATION
**          FOR USEPA RISK REDUCTION ENGINEERING LABORATORY
**
**
*****
*****

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PRECIPITATION DATA FILE:  D:\HELP3\Hweather\ZPREC.D4
TEMPERATURE DATA FILE:   D:\HELP3\Hweather\ZTEMP.D7
SOLAR RADIATION DATA FILE: D:\HELP3\Hweather\ZSOLAR.D13
EVAPOTRANSPIRATION DATA:  D:\HELP3\Hweather\ZEVAP.D11
SOIL AND DESIGN DATA FILE: D:\HELP3\Hsdfmse\ZMSED4.D10
OUTPUT DATA FILE:        D:\HELP3\Hsdfmse\ZMSED4ou.OUT

```

TIME: 13:11 DATE: 11/14/2003

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TITLE: Degraded SDF MSE Vault Closure Cap - 1,000 years

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NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER
WERE SPECIFIED BY THE USER.

LAYER 1

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

```

THICKNESS           =      5.80  INCHES
POROSITY             =      0.4000 VOL/VOL
FIELD CAPACITY       =      0.1100 VOL/VOL
WILTING POINT       =      0.0580 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.1100 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.100000005000E-02 CM/SEC

```

LAYER 2

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

```

THICKNESS           =     30.00  INCHES
POROSITY             =      0.3700 VOL/VOL
FIELD CAPACITY       =      0.2400 VOL/VOL
WILTING POINT       =      0.1360 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.2400 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.999999975000E-04 CM/SEC

```


LAYER 3

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.0620	VOL/VOL
FIELD CAPACITY	=	0.0574	VOL/VOL
WILTING POINT	=	0.0526	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0574	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.400999998000E-03	CM/SEC

LAYER 4

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3720	VOL/VOL
FIELD CAPACITY	=	0.2040	VOL/VOL
WILTING POINT	=	0.1090	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2040	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.460000010000E-03	CM/SEC

LAYER 5

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3780	VOL/VOL
FIELD CAPACITY	=	0.1160	VOL/VOL
WILTING POINT	=	0.0400	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1160	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.209999997000E-01	CM/SEC
SLOPE	=	3.00	PERCENT
DRAINAGE LENGTH	=	450.0	FEET

LAYER 6

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.0000	VOL/VOL
FIELD CAPACITY	=	0.0000	VOL/VOL
WILTING POINT	=	0.0000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0000	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC
FML PINHOLE DENSITY	=	0.00	HOLES/ACRE
FML INSTALLATION DEFECTS	=	59458.00	HOLES/ACRE
FML PLACEMENT QUALITY	=	1	- PERFECT

LAYER 7

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	58.57	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC

LAYER 8

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	24.00	INCHES
POROSITY	=	0.3740	VOL/VOL
FIELD CAPACITY	=	0.0851	VOL/VOL
WILTING POINT	=	0.0203	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0851	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.961000025000E-01	CM/SEC
SLOPE	=	11.40	PERCENT
DRAINAGE LENGTH	=	150.0	FEET

LAYER 9

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.7500	VOL/VOL
FIELD CAPACITY	=	0.7470	VOL/VOL
WILTING POINT	=	0.4000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.7500	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT
 SOIL DATA BASE USING SOIL TEXTURE # 5 WITH A
 GOOD STAND OF GRASS, A SURFACE SLOPE OF 3. %
 AND A SLOPE LENGTH OF 450. FEET.

SCS RUNOFF CURVE NUMBER	=	54.40	
FRACTION OF AREA ALLOWING RUNOFF	=	100.0	PERCENT
AREA PROJECTED ON HORIZONTAL PLANE	=	19.630	ACRES
EVAPORATIVE ZONE DEPTH	=	22.0	INCHES
INITIAL WATER IN EVAPORATIVE ZONE	=	4.526	INCHES
UPPER LIMIT OF EVAPORATIVE STORAGE	=	8.314	INCHES
LOWER LIMIT OF EVAPORATIVE STORAGE	=	2.540	INCHES
INITIAL SNOW WATER	=	0.000	INCHES
INITIAL WATER IN LAYER MATERIALS	=	28.616	INCHES
TOTAL INITIAL WATER	=	28.616	INCHES
TOTAL SUBSURFACE INFLOW	=	0.00	INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM
AUGUSTA GEORGIA

STATION LATITUDE = 33.22 DEGREES
MAXIMUM LEAF AREA INDEX = 3.50
START OF GROWING SEASON (JULIAN DATE) = 68
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EVAPORATIVE ZONE DEPTH = 22.0 INCHES
AVERAGE ANNUAL WIND SPEED = 6.50 MPH
AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 68.00 %
AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 70.00 %
AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 77.00 %
AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 73.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

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4.38	3.95	4.68	2.91	3.56	4.99
5.43	5.41	3.93	3.12	2.96	3.45

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
46.30	50.00	57.20	64.30	72.10	78.40
81.60	80.30	75.20	65.10	56.70	48.80

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA
AND STATION LATITUDE = 33.30 DEGREES

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 100

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	4.56	3.57	4.76	2.74	3.60	4.97
	5.81	5.32	4.41	2.99	2.75	3.41
STD. DEVIATIONS	2.44	1.60	2.47	1.31	2.12	2.60
	2.83	2.95	2.54	2.28	1.72	1.90

RUNOFF

TOTALS	0.003	0.000	0.004	0.000	0.000	0.002
	0.027	0.092	0.016	0.006	0.002	0.001

STD. DEVIATIONS	0.018	0.000	0.027	0.000	0.002	0.013
	0.093	0.405	0.086	0.058	0.014	0.004

EVAPOTRANSPIRATION

TOTALS	1.578	2.095	3.082	3.559	3.648	4.138
	4.895	4.520	3.383	1.618	0.949	1.116

STD. DEVIATIONS	0.220	0.236	0.580	0.763	1.523	1.546
	1.589	1.379	1.040	0.606	0.207	0.205

LATERAL DRAINAGE COLLECTED FROM LAYER 5

TOTALS	0.3927	0.2975	0.2914	0.1649	0.0552	0.0486
	0.0904	0.1249	0.1121	0.1190	0.1402	0.2395

STD. DEVIATIONS	0.2858	0.2265	0.2395	0.1471	0.0705	0.0939
	0.1316	0.1629	0.1621	0.1698	0.1887	0.2141

PERCOLATION/LEAKAGE THROUGH LAYER 6

TOTALS	2.2751	1.7252	1.6884	0.9555	0.3215	0.2825
	0.5245	0.7242	0.6502	0.6896	0.8127	1.3875

STD. DEVIATIONS	1.6563	1.3201	1.3880	0.8510	0.4075	0.5434
	0.7613	0.9431	0.9382	0.9830	1.0922	1.2393

LATERAL DRAINAGE COLLECTED FROM LAYER 8

TOTALS	1.6204	1.8444	1.7499	1.5010	0.9001	0.6044
	0.4122	0.4847	0.6129	0.6970	0.7249	0.8009

STD. DEVIATIONS	1.5405	1.4319	1.0925	1.0296	0.3834	0.3480
	0.3822	0.6385	0.7505	0.7434	0.9149	0.8815

PERCOLATION/LEAKAGE THROUGH LAYER 9

TOTALS	0.0075	0.0082	0.0088	0.0081	0.0071	0.0059
	0.0050	0.0045	0.0049	0.0053	0.0053	0.0053

STD. DEVIATIONS	0.0043	0.0035	0.0025	0.0023	0.0009	0.0016
	0.0021	0.0028	0.0029	0.0030	0.0031	0.0033

 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 6

AVERAGES	1.5980	1.3284	1.1858	0.6932	0.2247	0.2042
	0.3676	0.5081	0.4713	0.4839	0.5894	0.9744
STD. DEVIATIONS	1.1637	1.0167	0.9753	0.6182	0.2868	0.3947
	0.5352	0.6628	0.6814	0.6908	0.7931	0.8709

DAILY AVERAGE HEAD ON TOP OF LAYER 9

AVERAGES	0.1279	0.1596	0.1381	0.1224	0.0710	0.0493
	0.0325	0.0383	0.0500	0.0550	0.0591	0.0632
STD. DEVIATIONS	0.1216	0.1241	0.0862	0.0840	0.0303	0.0284
	0.0302	0.0504	0.0612	0.0587	0.0746	0.0696

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 100

	INCHES	CU. FEET	PERCENT
	-----	-----	-----
PRECIPITATION	48.90 (7.734)	3484469.2	100.00
RUNOFF	0.153 (0.4349)	10917.36	0.313
EVAPOTRANSPIRATION	34.581 (3.6232)	2464161.75	70.718
LATERAL DRAINAGE COLLECTED FROM LAYER 5	2.07646 (0.83367)	147962.172	4.24633
PERCOLATION/LEAKAGE THROUGH LAYER 6	12.03710 (4.83070)	857726.625	24.61571
AVERAGE HEAD ON TOP OF LAYER 6	0.719 (0.289)		
LATERAL DRAINAGE COLLECTED FROM LAYER 8	11.95268 (4.59408)	851710.875	24.44306
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.07579 (0.01481)	5400.314	0.15498
AVERAGE HEAD ON TOP OF LAYER 9	0.081 (0.031)		
CHANGE IN WATER STORAGE	0.061 (2.7895)	4316.20	0.124

PEAK DAILY VALUES FOR YEARS 1 THROUGH 100		
	(INCHES)	(CU. FT.)
PRECIPITATION	6.87	489534.875
RUNOFF	2.657	189337.1870
DRAINAGE COLLECTED FROM LAYER 5	0.09351	6663.55762
PERCOLATION/LEAKAGE THROUGH LAYER 6	0.696376	49621.60160
AVERAGE HEAD ON TOP OF LAYER 6	15.165	
MAXIMUM HEAD ON TOP OF LAYER 6	22.898	
LOCATION OF MAXIMUM HEAD IN LAYER 5 (DISTANCE FROM DRAIN)	102.0 FEET	
DRAINAGE COLLECTED FROM LAYER 8	0.51557	36738.02340
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.001243	88.55154
AVERAGE HEAD ON TOP OF LAYER 9	1.261	
MAXIMUM HEAD ON TOP OF LAYER 9	2.416	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	4.5 FEET	
SNOW WATER	2.36	168188.7190
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3690
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.1154

*** Maximum heads are computed using McEnroe's equations. ***

Reference: Maximum Saturated Depth over Landfill Liner
by Bruce M. McEnroe, University of Kansas
ASCE Journal of Environmental Engineering
Vol. 119, No. 2, March 1993, pp. 262-270.

FINAL WATER STORAGE AT END OF YEAR 100

LAYER	(INCHES)	(VOL/VOL)
1	1.5626	0.2694
2	8.9814	0.2994
3	0.7440	0.0620
4	3.8030	0.3169
5	2.4691	0.2058
6	0.0000	0.0000
7	14.9074	0.2545
8	2.0558	0.0857
9	0.1500	0.7500
SNOW WATER	0.000	

Appendix K, Degraded SDF MSE Vault Closure Cap (1,800 Years): HELP Model Input Data and Output File (output file name: ZMSED5ou.OUT)

Input Data:

Input Parameter (HELP Model Query)				Generic Input Parameter Value			
Landfill area =				19.63 acres			
Percent of area where runoff is possible =				100%			
Do you want to specify initial moisture storage? (Y/N)				Y			
Amount of water or snow on surface =				0 inches			
CN Input Parameter (HELP Model Query)				CN Input Parameter Value			
Slope =				3 %			
Slope length =				450 ft			
Soil Texture =				5 (HELP model default soil texture)			
Vegetation =				4 (i.e., a good stand of grass)			
HELP Model Computed Curve Number = 54.4							
Layer			Layer Number		Layer Type		
Topsoil			1		1 (vertical percolation layer)		
Upper Backfill			2		1 (vertical percolation layer)		
Erosion Barrier			3		1 (vertical percolation layer)		
Middle Backfill			4		1 (vertical percolation layer)		
Upper Drainage Layer			5		2 (lateral drainage layer)		
Upper GCL			6		4 (flexible membrane liner)		
Lower Backfill			7		1 (vertical percolation layer)		
Lower Drainage Layer			8		2 (lateral drainage layer)		
Lower GCL			9		3 (barrier soil liner)		
	Layer Type	Layer Thickness (in)	Soil Texture No.	Total Porosity (Vol/Vol)	Field Capacity (Vol/Vol)	Wilting Point (Vol/Vol)	Initial Moisture (Vol/Vol)
1	1	5.64		0.4	0.11	0.058	0.11
2	1	30		0.37	0.24	0.136	0.24
3	1	12		0.065	0.0587	0.0532	0.0587
4	1	12		0.374	0.176	0.0867	0.176
5	2	12		0.376	0.144	0.062	0.144
6 *	4	0.2		0.75	0.747	0.40	0.75
7	1	58.57		0.37	0.24	0.136	0.24
8	2	24		0.363	0.0935	0.0324	0.0935
9	3	0.2		0.75	0.747	0.40	0.75

* The input porosity, field capacity, and wilting point values of the upper GCL are ignored by the HELP model, since the upper GCL is designated as an geomembrane in order for the HELP model to take into account the holes produced by root penetration.

Input Data (continued):

	Layer Type	Sat. Hyd. Conductivity * (cm/sec)	Drainage Length (ft)	Drain Slope (%)	Leachate Recirc. (%)	Recirc. to Layer (#)	Subsurface Inflow (in/yr)
1	1	1.00E-03					
2	1	1.00E-04					
3	1	4.06E-04					
4	1	1.60E-03					
5	2	6.30E-03	450	3			
6	4	5.00E-09					
7	1	1.00E-04					
8	2	8.96E-02	150	11.4			
9	3	5.00E-09					
	Layer Type	Geomembrane Pinhole Density (#/acre)	Geomembrane Instal. Defects (#/acre)	Geomembrane Placement Quality	Geotextile Transmissivity (cm ² /sec)		
1	1						
2	1						
3	1						
4	1						
5	2						
6	4	0	118,916	1			
7	1						
8	2						
9	3						

The lack of values in the table for particular parameters in particular layers denotes that no HELP model input was required for that parameter in that layer. No data are missing from the table.

* The HELP model output often produces an increased number of significant digits for the Effective Saturated Hydraulic Conductivity over that of the actual input.

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*****
*****
**
**
**
**      HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE
**      HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)
**      DEVELOPED BY ENVIRONMENTAL LABORATORY
**      USAE WATERWAYS EXPERIMENT STATION
**      FOR USEPA RISK REDUCTION ENGINEERING LABORATORY
**
**
*****
*****
```

```
PRECIPITATION DATA FILE:  D:\HELP3\Hweather\ZPREC.D4
TEMPERATURE DATA FILE:   D:\HELP3\Hweather\ZTEMP.D7
SOLAR RADIATION DATA FILE: D:\HELP3\Hweather\ZSOLAR.D13
EVAPOTRANSPIRATION DATA:  D:\HELP3\Hweather\ZEVAP.D11
SOIL AND DESIGN DATA FILE: D:\HELP3\Hsdfmse\ZMSED5.D10
OUTPUT DATA FILE:         D:\HELP3\Hsdfmse\ZMSED5ou.OUT
```

TIME: 13:14 DATE: 11/14/2003

```
*****

TITLE:  Degraded SDF MSE Vault Closure Cap - 1,800 years

*****
```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER
WERE SPECIFIED BY THE USER.

LAYER 1

```
TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 0
THICKNESS                =      5.64  INCHES
POROSITY                  =      0.4000 VOL/VOL
FIELD CAPACITY            =      0.1100 VOL/VOL
WILTING POINT            =      0.0580 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.1100 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.100000005000E-02 CM/SEC
```

LAYER 2

```
TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 0
THICKNESS                =     30.00  INCHES
POROSITY                  =      0.3700 VOL/VOL
FIELD CAPACITY            =      0.2400 VOL/VOL
WILTING POINT            =      0.1360 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.2400 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.999999975000E-04 CM/SEC
```

LAYER 3

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.0650	VOL/VOL
FIELD CAPACITY	=	0.0587	VOL/VOL
WILTING POINT	=	0.0532	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0587	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.406000006000E-03	CM/SEC

LAYER 4

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3740	VOL/VOL
FIELD CAPACITY	=	0.1760	VOL/VOL
WILTING POINT	=	0.0867	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1760	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.159999996000E-02	CM/SEC

LAYER 5

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3760	VOL/VOL
FIELD CAPACITY	=	0.1440	VOL/VOL
WILTING POINT	=	0.0620	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1440	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.630000001000E-02	CM/SEC
SLOPE	=	3.00	PERCENT
DRAINAGE LENGTH	=	450.0	FEET

LAYER 6

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.0000	VOL/VOL
FIELD CAPACITY	=	0.0000	VOL/VOL
WILTING POINT	=	0.0000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0000	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC
FML PINHOLE DENSITY	=	0.00	HOLES/ACRE
FML INSTALLATION DEFECTS	=	118916.00	HOLES/ACRE
FML PLACEMENT QUALITY	=	1 - PERFECT	

LAYER 7

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	58.57	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC

LAYER 8

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	24.00	INCHES
POROSITY	=	0.3630	VOL/VOL
FIELD CAPACITY	=	0.0935	VOL/VOL
WILTING POINT	=	0.0324	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0935	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.895999968000E-01	CM/SEC
SLOPE	=	11.40	PERCENT
DRAINAGE LENGTH	=	150.0	FEET

LAYER 9

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.7500	VOL/VOL
FIELD CAPACITY	=	0.7470	VOL/VOL
WILTING POINT	=	0.4000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.7500	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT
 SOIL DATA BASE USING SOIL TEXTURE # 5 WITH A
 GOOD STAND OF GRASS, A SURFACE SLOPE OF 3. %
 AND A SLOPE LENGTH OF 450. FEET.

SCS RUNOFF CURVE NUMBER	=	54.40	
FRACTION OF AREA ALLOWING RUNOFF	=	100.0	PERCENT
AREA PROJECTED ON HORIZONTAL PLANE	=	19.630	ACRES
EVAPORATIVE ZONE DEPTH	=	22.0	INCHES
INITIAL WATER IN EVAPORATIVE ZONE	=	4.547	INCHES
UPPER LIMIT OF EVAPORATIVE STORAGE	=	8.309	INCHES
LOWER LIMIT OF EVAPORATIVE STORAGE	=	2.552	INCHES
INITIAL SNOW WATER	=	0.000	INCHES
INITIAL WATER IN LAYER MATERIALS	=	28.816	INCHES
TOTAL INITIAL WATER	=	28.816	INCHES
TOTAL SUBSURFACE INFLOW	=	0.00	INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM
AUGUSTA GEORGIA

STATION LATITUDE = 33.22 DEGREES
 MAXIMUM LEAF AREA INDEX = 3.50
 START OF GROWING SEASON (JULIAN DATE) = 68
 END OF GROWING SEASON (JULIAN DATE) = 323
 EVAPORATIVE ZONE DEPTH = 22.0 INCHES
 AVERAGE ANNUAL WIND SPEED = 6.50 MPH
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 68.00 %
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 70.00 %
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 77.00 %
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 73.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
4.38	3.95	4.68	2.91	3.56	4.99
5.43	5.41	3.93	3.12	2.96	3.45

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
46.30	50.00	57.20	64.30	72.10	78.40
81.60	80.30	75.20	65.10	56.70	48.80

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA
AND STATION LATITUDE = 33.30 DEGREES

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 100

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	4.56	3.57	4.76	2.74	3.60	4.97
	5.81	5.32	4.41	2.99	2.75	3.41
STD. DEVIATIONS	2.44	1.60	2.47	1.31	2.12	2.60
	2.83	2.95	2.54	2.28	1.72	1.90

RUNOFF

TOTALS	0.003	0.000	0.004	0.000	0.000	0.002
	0.026	0.092	0.016	0.006	0.002	0.000

STD. DEVIATIONS	0.015	0.000	0.028	0.000	0.001	0.013
	0.093	0.406	0.086	0.058	0.013	0.004

EVAPOTRANSPIRATION

TOTALS	1.579	2.097	3.087	3.559	3.641	4.137
	4.892	4.519	3.382	1.619	0.949	1.116

STD. DEVIATIONS	0.220	0.234	0.583	0.762	1.521	1.548
	1.588	1.378	1.040	0.606	0.207	0.205

LATERAL DRAINAGE COLLECTED FROM LAYER 5

TOTALS	0.0700	0.0495	0.0502	0.0253	0.0081	0.0088
	0.0166	0.0221	0.0195	0.0205	0.0251	0.0438

STD. DEVIATIONS	0.0508	0.0387	0.0433	0.0239	0.0128	0.0167
	0.0245	0.0298	0.0298	0.0304	0.0334	0.0388

PERCOLATION/LEAKAGE THROUGH LAYER 6

TOTALS	2.6781	1.8952	1.9205	0.9690	0.3130	0.3356
	0.6367	0.8448	0.7456	0.7847	0.9621	1.6771

STD. DEVIATIONS	1.9460	1.4797	1.6539	0.9131	0.4905	0.6373
	0.9360	1.1402	1.1404	1.1611	1.2755	1.4820

LATERAL DRAINAGE COLLECTED FROM LAYER 8

TOTALS	1.9928	2.1103	2.0045	1.6221	0.9250	0.6154
	0.4429	0.5908	0.7472	0.7958	0.8309	0.9919

STD. DEVIATIONS	1.8473	1.6167	1.3180	1.1053	0.4060	0.4058
	0.4629	0.7955	0.8463	0.8817	1.0550	1.0806

PERCOLATION/LEAKAGE THROUGH LAYER 9

TOTALS	0.0088	0.0092	0.0096	0.0086	0.0072	0.0059
	0.0049	0.0046	0.0053	0.0057	0.0057	0.0060

STD. DEVIATIONS	0.0051	0.0041	0.0031	0.0027	0.0012	0.0018
	0.0023	0.0033	0.0033	0.0033	0.0036	0.0038

 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 6

AVERAGES	0.9493	0.7364	0.6806	0.3547	0.1104	0.1227
	0.2254	0.2992	0.2728	0.2780	0.3522	0.5944
STD. DEVIATIONS	0.6900	0.5751	0.5865	0.3348	0.1740	0.2335
	0.3320	0.4043	0.4179	0.4117	0.4674	0.5255

DAILY AVERAGE HEAD ON TOP OF LAYER 9

AVERAGES	0.1687	0.1959	0.1697	0.1419	0.0783	0.0538
	0.0375	0.0500	0.0654	0.0674	0.0727	0.0840
STD. DEVIATIONS	0.1564	0.1502	0.1116	0.0967	0.0344	0.0355
	0.0392	0.0673	0.0740	0.0746	0.0923	0.0915

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 100

	INCHES		CU. FEET	PERCENT
	-----	-----	-----	-----
PRECIPITATION	48.90	(7.734)	3484469.2	100.00
RUNOFF	0.153	(0.4366)	10870.63	0.312
EVAPOTRANSPIRATION	34.577	(3.6265)	2463843.25	70.709
LATERAL DRAINAGE COLLECTED FROM LAYER 5	0.35957	(0.14519)	25621.561	0.73531
PERCOLATION/LEAKAGE THROUGH LAYER 6	13.76236	(5.55344)	980663.312	28.14384
AVERAGE HEAD ON TOP OF LAYER 6	0.415	(0.167)		
LATERAL DRAINAGE COLLECTED FROM LAYER 8	13.66948	(5.30758)	974044.625	27.95389
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.08138	(0.01726)	5799.073	0.16643
AVERAGE HEAD ON TOP OF LAYER 9	0.099	(0.038)		
CHANGE IN WATER STORAGE	0.060	(2.7630)	4290.53	0.123

PEAK DAILY VALUES FOR YEARS 1 THROUGH 100		
	(INCHES)	(CU. FT.)
PRECIPITATION	6.87	489534.875
RUNOFF	2.665	189884.2500
DRAINAGE COLLECTED FROM LAYER 5	0.02681	1910.22375
PERCOLATION/LEAKAGE THROUGH LAYER 6	1.094036	77957.62500
AVERAGE HEAD ON TOP OF LAYER 6	12.024	
MAXIMUM HEAD ON TOP OF LAYER 6	18.107	
LOCATION OF MAXIMUM HEAD IN LAYER 5 (DISTANCE FROM DRAIN)	88.7 FEET	
DRAINAGE COLLECTED FROM LAYER 8	0.75273	53637.29300
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.001850	131.80533
AVERAGE HEAD ON TOP OF LAYER 9	1.975	
MAXIMUM HEAD ON TOP OF LAYER 9	3.720	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	6.9 FEET	
SNOW WATER	2.36	168188.7190
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3688
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.1160

*** Maximum heads are computed using McEnroe's equations. ***

Reference: Maximum Saturated Depth over Landfill Liner
by Bruce M. McEnroe, University of Kansas
ASCE Journal of Environmental Engineering
Vol. 119, No. 2, March 1993, pp. 262-270.

FINAL WATER STORAGE AT END OF YEAR 100

LAYER	(INCHES)	(VOL/VOL)
1	1.5522	0.2752
2	8.9327	0.2978
3	0.7800	0.0650
4	3.2243	0.2687
5	2.7466	0.2289
6	0.0000	0.0000
7	15.1942	0.2594
8	2.2567	0.0940
9	0.1500	0.7500
SNOW WATER	0.000	

Appendix L, Degraded SDF MSE Vault Closure Cap (3,400 Years): HELP Model Input Data and Output File (output file name: ZMSED6ou.OUT)

Input Data:

Input Parameter (HELP Model Query)				Generic Input Parameter Value			
Landfill area =				19.63 acres			
Percent of area where runoff is possible =				100%			
Do you want to specify initial moisture storage? (Y/N)				Y			
Amount of water or snow on surface =				0 inches			
CN Input Parameter (HELP Model Query)				CN Input Parameter Value			
Slope =				3 %			
Slope length =				450 ft			
Soil Texture =				5 (HELP model default soil texture)			
Vegetation =				4 (i.e., a good stand of grass)			
HELP Model Computed Curve Number = 54.4							
Layer			Layer Number		Layer Type		
Topsoil			1		1 (vertical percolation layer)		
Upper Backfill			2		1 (vertical percolation layer)		
Erosion Barrier			3		1 (vertical percolation layer)		
Middle Backfill			4		1 (vertical percolation layer)		
Upper Drainage Layer			5		2 (lateral drainage layer)		
Upper GCL			6		4 (flexible membrane liner)		
Lower Backfill			7		1 (vertical percolation layer)		
Lower Drainage Layer			8		2 (lateral drainage layer)		
Lower GCL			9		3 (barrier soil liner)		
	Layer Type	Layer Thickness (in)	Soil Texture No.	Total Porosity (Vol/Vol)	Field Capacity (Vol/Vol)	Wilting Point (Vol/Vol)	Initial Moisture (Vol/Vol)
1	1	5.320		0.4	0.11	0.058	0.11
2	1	30		0.37	0.24	0.136	0.24
3	1	12		0.069	0.0614	0.0545	0.0614
4	1	12		0.375	0.16	0.0745	0.16
5	2	12		0.375	0.16	0.0745	0.16
6 *	4	0.2		0.75	0.747	0.40	0.75
7	1	58.57		0.37	0.24	0.136	0.24
8	2	24		0.341	0.112	0.0586	0.112
9	3	0.2		0.75	0.747	0.40	0.75

* The input porosity, field capacity, and wilting point values of the upper GCL are ignored by the HELP model, since the upper GCL is designated as an geomembrane in order for the HELP model to take into account the holes produced by root penetration.

Input Data (continued):

	Layer Type	Sat. Hyd. Conductivity (cm/sec)	Drainage Length (ft)	Drain Slope (%)	Leachate Recirc. (%)	Recirc. to Layer (#)	Subsurface Inflow (in/yr)
1	1	1.00E-03					
2	1	1.00E-04					
3	1	4.15E-04					
4	1	3.20E-03					
5	2	3.20E-03	450	3			
6	4	5.00E-09					
7	1	1.00E-04					
8	2	7.56E-02	150	11.4			
9	3	5.00E-09					
	Layer Type	Geomembrane Pinhole Density (#/acre)	Geomembrane Instal. Defects (#/acre)	Geomembrane Placement Quality	Geotextile Transmissivity (cm ² /sec)		
1	1						
2	1						
3	1						
4	1						
5	2						
6	4	0	237,832	1			
7	1						
8	2						
9	3						

The lack of values in the table for particular parameters in particular layers denotes that no HELP model input was required for that parameter in that layer. No data are missing from the table.

* The HELP model output often produces an increased number of significant digits for the Effective Saturated Hydraulic Conductivity over that of the actual input.

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**
**      HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE
**      HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)
**      DEVELOPED BY ENVIRONMENTAL LABORATORY
**      USAE WATERWAYS EXPERIMENT STATION
**      FOR USEPA RISK REDUCTION ENGINEERING LABORATORY
**
**
*****
*****
```

```
PRECIPITATION DATA FILE:  D:\HELP3\Hweather\ZPREC.D4
TEMPERATURE DATA FILE:   D:\HELP3\Hweather\ZTEMP.D7
SOLAR RADIATION DATA FILE: D:\HELP3\Hweather\ZSOLAR.D13
EVAPOTRANSPIRATION DATA:  D:\HELP3\Hweather\ZEVAP.D11
SOIL AND DESIGN DATA FILE: D:\HELP3\Hsdfmse\ZMSED6.D10
OUTPUT DATA FILE:        D:\HELP3\Hsdfmse\ZMSED6ou.OUT
```

TIME: 13:18 DATE: 11/14/2003

```
*****

TITLE:  Degraded SDF MSE Vault Closure Cap - 3,400 years

*****
```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER
WERE SPECIFIED BY THE USER.

LAYER 1

```
TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 0
THICKNESS                =      5.32  INCHES
POROSITY                  =      0.4000 VOL/VOL
FIELD CAPACITY            =      0.1100 VOL/VOL
WILTING POINT            =      0.0580 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.1100 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.100000005000E-02 CM/SEC
```

LAYER 2

```
TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 0
THICKNESS                =     30.00  INCHES
POROSITY                  =      0.3700 VOL/VOL
FIELD CAPACITY            =      0.2400 VOL/VOL
WILTING POINT            =      0.1360 VOL/VOL
INITIAL SOIL WATER CONTENT =      0.2400 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.999999975000E-04 CM/SEC
```

LAYER 3

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.0690	VOL/VOL
FIELD CAPACITY	=	0.0614	VOL/VOL
WILTING POINT	=	0.0545	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0614	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.414999988000E-03	CM/SEC

LAYER 4

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3750	VOL/VOL
FIELD CAPACITY	=	0.1600	VOL/VOL
WILTING POINT	=	0.0745	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1600	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.319999992000E-02	CM/SEC

LAYER 5

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3750	VOL/VOL
FIELD CAPACITY	=	0.1600	VOL/VOL
WILTING POINT	=	0.0745	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1600	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.319999992000E-02	CM/SEC
SLOPE	=	3.00	PERCENT
DRAINAGE LENGTH	=	450.0	FEET

LAYER 6

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.0000	VOL/VOL
FIELD CAPACITY	=	0.0000	VOL/VOL
WILTING POINT	=	0.0000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0000	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC
FML PINHOLE DENSITY	=	0.00	HOLES/ACRE
FML INSTALLATION DEFECTS	=	237832.00	HOLES/ACRE
FML PLACEMENT QUALITY	=	1	PERFECT

LAYER 7

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	58.57	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC

LAYER 8

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	24.00	INCHES
POROSITY	=	0.3410	VOL/VOL
FIELD CAPACITY	=	0.1120	VOL/VOL
WILTING POINT	=	0.0586	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1120	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.755999982000E-01	CM/SEC
SLOPE	=	11.40	PERCENT
DRAINAGE LENGTH	=	150.0	FEET

LAYER 9

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.7500	VOL/VOL
FIELD CAPACITY	=	0.7470	VOL/VOL
WILTING POINT	=	0.4000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.7500	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT
 SOIL DATA BASE USING SOIL TEXTURE # 5 WITH A
 GOOD STAND OF GRASS, A SURFACE SLOPE OF 3. %
 AND A SLOPE LENGTH OF 450. FEET.

SCS RUNOFF CURVE NUMBER	=	54.40	
FRACTION OF AREA ALLOWING RUNOFF	=	100.0	PERCENT
AREA PROJECTED ON HORIZONTAL PLANE	=	19.630	ACRES
EVAPORATIVE ZONE DEPTH	=	22.0	INCHES
INITIAL WATER IN EVAPORATIVE ZONE	=	4.588	INCHES
UPPER LIMIT OF EVAPORATIVE STORAGE	=	8.300	INCHES
LOWER LIMIT OF EVAPORATIVE STORAGE	=	2.577	INCHES
INITIAL SNOW WATER	=	0.000	INCHES
INITIAL WATER IN LAYER MATERIALS	=	29.257	INCHES
TOTAL INITIAL WATER	=	29.257	INCHES
TOTAL SUBSURFACE INFLOW	=	0.00	INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM
AUGUSTA GEORGIA

STATION LATITUDE = 33.22 DEGREES
MAXIMUM LEAF AREA INDEX = 3.50
START OF GROWING SEASON (JULIAN DATE) = 68
END OF GROWING SEASON (JULIAN DATE) = 323
EVAPORATIVE ZONE DEPTH = 22.0 INCHES
AVERAGE ANNUAL WIND SPEED = 6.50 MPH
AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 68.00 %
AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 70.00 %
AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 77.00 %
AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 73.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
4.38	3.95	4.68	2.91	3.56	4.99
5.43	5.41	3.93	3.12	2.96	3.45

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
46.30	50.00	57.20	64.30	72.10	78.40
81.60	80.30	75.20	65.10	56.70	48.80

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA
AND STATION LATITUDE = 33.30 DEGREES

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 100

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	4.56	3.57	4.76	2.74	3.60	4.97
	5.81	5.32	4.41	2.99	2.75	3.41
STD. DEVIATIONS	2.44	1.60	2.47	1.31	2.12	2.60
	2.83	2.95	2.54	2.28	1.72	1.90

RUNOFF

TOTALS	0.003	0.000	0.004	0.000	0.000	0.001
	0.027	0.092	0.016	0.007	0.002	0.000

STD. DEVIATIONS	0.018	0.000	0.027	0.000	0.003	0.010
	0.096	0.406	0.085	0.058	0.012	0.003

EVAPOTRANSPIRATION

TOTALS	1.581	2.100	3.102	3.564	3.620	4.135
	4.894	4.514	3.379	1.618	0.949	1.118

STD. DEVIATIONS	0.217	0.232	0.570	0.774	1.518	1.544
	1.591	1.379	1.041	0.606	0.209	0.204

LATERAL DRAINAGE COLLECTED FROM LAYER 5

TOTALS	0.0185	0.0126	0.0130	0.0060	0.0019	0.0024
	0.0045	0.0057	0.0051	0.0054	0.0067	0.0117

STD. DEVIATIONS	0.0133	0.0099	0.0114	0.0058	0.0035	0.0045
	0.0066	0.0080	0.0080	0.0081	0.0087	0.0103

PERCOLATION/LEAKAGE THROUGH LAYER 6

TOTALS	2.7669	1.8857	1.9557	0.9004	0.2867	0.3563
	0.6795	0.8575	0.7684	0.8050	1.0118	1.7608

STD. DEVIATIONS	1.9888	1.4840	1.7064	0.8759	0.5289	0.6697
	0.9921	1.2030	1.2063	1.2172	1.3089	1.5409

LATERAL DRAINAGE COLLECTED FROM LAYER 8

TOTALS	2.0604	2.0833	2.0322	1.6062	0.9464	0.6431
	0.4864	0.6193	0.7343	0.8150	0.8581	1.0438

STD. DEVIATIONS	1.9061	1.6308	1.3617	1.0531	0.4006	0.3762
	0.4640	0.8203	0.7920	0.8766	1.0482	1.1181

PERCOLATION/LEAKAGE THROUGH LAYER 9

TOTALS	0.0099	0.0100	0.0105	0.0093	0.0077	0.0065
	0.0055	0.0053	0.0057	0.0062	0.0063	0.0068

STD. DEVIATIONS	0.0060	0.0047	0.0037	0.0029	0.0013	0.0017
	0.0023	0.0035	0.0034	0.0036	0.0038	0.0042

AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)						
DAILY AVERAGE HEAD ON TOP OF LAYER 6						
AVERAGES	0.4926	0.3679	0.3481	0.1654	0.0509	0.0654
	0.1208	0.1525	0.1412	0.1432	0.1860	0.3134
STD. DEVIATIONS	0.3543	0.2898	0.3040	0.1613	0.0942	0.1232
	0.1767	0.2143	0.2220	0.2168	0.2409	0.2745
DAILY AVERAGE HEAD ON TOP OF LAYER 9						
AVERAGES	0.2067	0.2292	0.2039	0.1665	0.0949	0.0667
	0.0488	0.0621	0.0761	0.0818	0.0890	0.1047
STD. DEVIATIONS	0.1912	0.1793	0.1366	0.1092	0.0402	0.0390
	0.0466	0.0823	0.0821	0.0879	0.1087	0.1122

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 100						
	INCHES		CU. FEET		PERCENT	
PRECIPITATION	48.90	(7.734)	3484469.2		100.00	
RUNOFF	0.153	(0.4378)	10886.89		0.312	
EVAPOTRANSPIRATION	34.575	(3.6119)	2463673.75		70.704	
LATERAL DRAINAGE COLLECTED FROM LAYER 5	0.09355	(0.03765)	6665.974		0.19131	
PERCOLATION/LEAKAGE THROUGH LAYER 6	14.03487	(5.64284)	1000081.060		28.70110	
AVERAGE HEAD ON TOP OF LAYER 6	0.212	(0.085)				
LATERAL DRAINAGE COLLECTED FROM LAYER 8	13.92841	(5.42028)	992495.500		28.48341	
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.08953	(0.01941)	6379.354		0.18308	
AVERAGE HEAD ON TOP OF LAYER 9	0.119	(0.046)				
CHANGE IN WATER STORAGE	0.061	(2.7396)	4367.94		0.125	

PEAK DAILY VALUES FOR YEARS 1 THROUGH 100		
	(INCHES)	(CU. FT.)
PRECIPITATION	6.87	489534.875
RUNOFF	2.661	189584.9220
DRAINAGE COLLECTED FROM LAYER 5	0.00949	676.41058
PERCOLATION/LEAKAGE THROUGH LAYER 6	1.422909	101392.05500
AVERAGE HEAD ON TOP OF LAYER 6	7.856	
MAXIMUM HEAD ON TOP OF LAYER 6	13.160	
LOCATION OF MAXIMUM HEAD IN LAYER 5 (DISTANCE FROM DRAIN)	72.8 FEET	
DRAINAGE COLLECTED FROM LAYER 8	0.99945	71217.62500
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.002813	200.46278
AVERAGE HEAD ON TOP OF LAYER 9	3.108	
MAXIMUM HEAD ON TOP OF LAYER 9	5.724	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	10.1 FEET	
SNOW WATER	2.36	168188.7190
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3692
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.1171

*** Maximum heads are computed using McEnroe's equations. ***

Reference: Maximum Saturated Depth over Landfill Liner
by Bruce M. McEnroe, University of Kansas
ASCE Journal of Environmental Engineering
Vol. 119, No. 2, March 1993, pp. 262-270.

FINAL WATER STORAGE AT END OF YEAR 100

LAYER	(INCHES)	(VOL/VOL)
1	1.4484	0.2723
2	8.9111	0.2970
3	0.8280	0.0690
4	2.9062	0.2422
5	2.7051	0.2254
6	0.0000	0.0000
7	15.5532	0.2655
8	2.8846	0.1202
9	0.1500	0.7500
SNOW WATER	0.000	

Appendix M, Degraded SDF MSE Vault Closure Cap (5,600 Years): HELP Model Input Data and Output File (output file name: ZMSED7ou.OUT)

Input Data:

Input Parameter (HELP Model Query)				Generic Input Parameter Value			
Landfill area =				19.63 acres			
Percent of area where runoff is possible =				100%			
Do you want to specify initial moisture storage? (Y/N)				Y			
Amount of water or snow on surface =				0 inches			
CN Input Parameter (HELP Model Query)				CN Input Parameter Value			
Slope =				3 %			
Slope length =				450 ft			
Soil Texture =				5 (HELP model default soil texture)			
Vegetation =				4 (i.e., a good stand of grass)			
HELP Model Computed Curve Number = 54.4							
Layer			Layer Number		Layer Type		
Topsoil			1		1 (vertical percolation layer)		
Upper Backfill			2		1 (vertical percolation layer)		
Erosion Barrier			3		1 (vertical percolation layer)		
Middle Backfill			4		1 (vertical percolation layer)		
Upper Drainage Layer			5		2 (lateral drainage layer)		
Upper GCL			6		4 (flexible membrane liner)		
Lower Backfill			7		1 (vertical percolation layer)		
Lower Drainage Layer			8		2 (lateral drainage layer)		
Lower GCL			9		3 (barrier soil liner)		
	Layer Type	Layer Thickness (in)	Soil Texture No.	Total Porosity (Vol/Vol)	Field Capacity (Vol/Vol)	Wilting Point (Vol/Vol)	Initial Moisture (Vol/Vol)
1	1	4.880		0.4	0.11	0.058	0.11
2	1	30		0.37	0.24	0.136	0.24
3	1	12		0.075	0.0651	0.0562	0.0651
4	1	12		0.375	0.16	0.0745	0.16
5	2	12		0.375	0.16	0.0745	0.16
6 *	4	0.2		0.75	0.747	0.40	0.75
7	1	58.57		0.37	0.24	0.136	0.24
8	2	24		0.310	0.137	0.0949	0.137
9	3	0.2		0.75	0.747	0.40	0.75

* The input porosity, field capacity, and wilting point values of the upper GCL are ignored by the HELP model, since the upper GCL is designated as an geomembrane in order for the HELP model to take into account the holes produced by root penetration.

Input Data (continued):

	Layer Type	Sat. Hyd. Conductivity * (cm/sec)	Drainage Length (ft)	Drain Slope (%)	Leachate Recirc. (%)	Recirc. to Layer (#)	Subsurface Inflow (in/yr)
1	1	1.00E-03					
2	1	1.00E-04					
3	1	4.27E-04					
4	1	3.20E-03					
5	2	3.20E-03	450	3			
6	4	5.00E-09					
7	1	1.00E-04					
8	2	5.62E-02	150	11.4			
9	3	5.00E-09					
	Layer Type	Geomembrane Pinhole Density (#/acre)	Geomembrane Instal. Defects (#/acre)	Geomembrane Placement Quality	Geotextile Transmissivity (cm ² /sec)		
1	1						
2	1						
3	1						
4	1						
5	2						
6	4	0	401,341	1			
7	1						
8	2						
9	3						

The lack of values in the table for particular parameters in particular layers denotes that no HELP model input was required for that parameter in that layer. No data are missing from the table.

* The HELP model output often produces an increased number of significant digits for the Effective Saturated Hydraulic Conductivity over that of the actual input.

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**
**      HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE
**      HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)
**      DEVELOPED BY ENVIRONMENTAL LABORATORY
**      USAE WATERWAYS EXPERIMENT STATION
**      FOR USEPA RISK REDUCTION ENGINEERING LABORATORY
**
**
*****
*****
```

```
PRECIPITATION DATA FILE:  D:\HELP3\Hweather\ZPREC.D4
TEMPERATURE DATA FILE:   D:\HELP3\Hweather\ZTEMP.D7
SOLAR RADIATION DATA FILE: D:\HELP3\Hweather\ZSOLAR.D13
EVAPOTRANSPIRATION DATA:  D:\HELP3\Hweather\ZEVAP.D11
SOIL AND DESIGN DATA FILE: D:\HELP3\Hsdfmse\ZMSED7.D10
OUTPUT DATA FILE:        D:\HELP3\Hsdfmse\ZMSED7ou.OUT
```

TIME: 13:21 DATE: 11/14/2003

```
*****

TITLE:  Degraded SDF MSE Vault Closure Cap - 5,600 years

*****
```

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER
WERE SPECIFIED BY THE USER.

LAYER 1

```
TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 0
THICKNESS           = 4.88 INCHES
POROSITY             = 0.4000 VOL/VOL
FIELD CAPACITY       = 0.1100 VOL/VOL
WILTING POINT        = 0.0580 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.1100 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.100000005000E-02 CM/SEC
```

LAYER 2

```
TYPE 1 - VERTICAL PERCOLATION LAYER
MATERIAL TEXTURE NUMBER 0
THICKNESS           = 30.00 INCHES
POROSITY             = 0.3700 VOL/VOL
FIELD CAPACITY       = 0.2400 VOL/VOL
WILTING POINT        = 0.1360 VOL/VOL
INITIAL SOIL WATER CONTENT = 0.2400 VOL/VOL
EFFECTIVE SAT. HYD. COND. = 0.999999975000E-04 CM/SEC
```

LAYER 3

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.0750	VOL/VOL
FIELD CAPACITY	=	0.0651	VOL/VOL
WILTING POINT	=	0.0562	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0651	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.426999992000E-03	CM/SEC

LAYER 4

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3750	VOL/VOL
FIELD CAPACITY	=	0.1600	VOL/VOL
WILTING POINT	=	0.0745	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1600	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.319999992000E-02	CM/SEC

LAYER 5

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3750	VOL/VOL
FIELD CAPACITY	=	0.1600	VOL/VOL
WILTING POINT	=	0.0745	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1600	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.319999992000E-02	CM/SEC
SLOPE	=	3.00	PERCENT
DRAINAGE LENGTH	=	450.0	FEET

LAYER 6

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.0000	VOL/VOL
FIELD CAPACITY	=	0.0000	VOL/VOL
WILTING POINT	=	0.0000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0000	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC
FML PINHOLE DENSITY	=	0.00	HOLES/ACRE
FML INSTALLATION DEFECTS	=	401341.00	HOLES/ACRE
FML PLACEMENT QUALITY	=	1	PERFECT

LAYER 7

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	58.57	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC

LAYER 8

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	24.00	INCHES
POROSITY	=	0.3100	VOL/VOL
FIELD CAPACITY	=	0.1370	VOL/VOL
WILTING POINT	=	0.0949	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1370	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.562000014000E-01	CM/SEC
SLOPE	=	11.40	PERCENT
DRAINAGE LENGTH	=	150.0	FEET

LAYER 9

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.7500	VOL/VOL
FIELD CAPACITY	=	0.7470	VOL/VOL
WILTING POINT	=	0.4000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.7500	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT
SOIL DATA BASE USING SOIL TEXTURE # 5 WITH A
GOOD STAND OF GRASS, A SURFACE SLOPE OF 3. %
AND A SLOPE LENGTH OF 450. FEET.

SCS RUNOFF CURVE NUMBER	=	54.40	
FRACTION OF AREA ALLOWING RUNOFF	=	100.0	PERCENT
AREA PROJECTED ON HORIZONTAL PLANE	=	19.630	ACRES
EVAPORATIVE ZONE DEPTH	=	22.0	INCHES
INITIAL WATER IN EVAPORATIVE ZONE	=	4.646	INCHES
UPPER LIMIT OF EVAPORATIVE STORAGE	=	8.286	INCHES
LOWER LIMIT OF EVAPORATIVE STORAGE	=	2.611	INCHES
INITIAL SNOW WATER	=	0.000	INCHES
INITIAL WATER IN LAYER MATERIALS	=	29.853	INCHES
TOTAL INITIAL WATER	=	29.853	INCHES
TOTAL SUBSURFACE INFLOW	=	0.00	INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM
AUGUSTA GEORGIA

STATION LATITUDE = 33.22 DEGREES
 MAXIMUM LEAF AREA INDEX = 3.50
 START OF GROWING SEASON (JULIAN DATE) = 68
 END OF GROWING SEASON (JULIAN DATE) = 323
 EVAPORATIVE ZONE DEPTH = 22.0 INCHES
 AVERAGE ANNUAL WIND SPEED = 6.50 MPH
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 68.00 %
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 70.00 %
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 77.00 %
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 73.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
4.38	3.95	4.68	2.91	3.56	4.99
5.43	5.41	3.93	3.12	2.96	3.45

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
46.30	50.00	57.20	64.30	72.10	78.40
81.60	80.30	75.20	65.10	56.70	48.80

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA
AND STATION LATITUDE = 33.30 DEGREES

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 100

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	4.56	3.57	4.76	2.74	3.60	4.97
	5.81	5.32	4.41	2.99	2.75	3.41
STD. DEVIATIONS	2.44	1.60	2.47	1.31	2.12	2.60
	2.83	2.95	2.54	2.28	1.72	1.90

RUNOFF

TOTALS	0.003	0.000	0.004	0.000	0.000	0.001
	0.028	0.093	0.017	0.007	0.002	0.000
STD. DEVIATIONS	0.017	0.000	0.026	0.000	0.002	0.009
	0.100	0.412	0.084	0.060	0.014	0.001

EVAPOTRANSPIRATION

TOTALS	1.583	2.102	3.114	3.573	3.599	4.130
	4.890	4.510	3.379	1.617	0.950	1.120
STD. DEVIATIONS	0.217	0.231	0.570	0.784	1.518	1.539
	1.588	1.379	1.042	0.606	0.209	0.203

LATERAL DRAINAGE COLLECTED FROM LAYER 5

TOTALS	0.0110	0.0074	0.0078	0.0034	0.0011	0.0015
	0.0027	0.0034	0.0031	0.0032	0.0041	0.0071
STD. DEVIATIONS	0.0080	0.0058	0.0069	0.0034	0.0021	0.0028
	0.0039	0.0048	0.0049	0.0049	0.0052	0.0062

PERCOLATION/LEAKAGE THROUGH LAYER 6

TOTALS	2.7836	1.8675	1.9591	0.8652	0.2705	0.3734
	0.6899	0.8524	0.7855	0.8140	1.0352	1.7829
STD. DEVIATIONS	2.0180	1.4745	1.7347	0.8474	0.5318	0.7042
	0.9934	1.2032	1.2476	1.2381	1.3092	1.5546

LATERAL DRAINAGE COLLECTED FROM LAYER 8

TOTALS	2.0981	2.0464	2.0430	1.5722	0.9337	0.6243
	0.4902	0.6397	0.7510	0.8199	0.8511	1.0811
STD. DEVIATIONS	1.9548	1.5809	1.4156	1.0091	0.4004	0.3635
	0.4752	0.8390	0.7733	0.8911	1.0444	1.1379

PERCOLATION/LEAKAGE THROUGH LAYER 9

TOTALS	0.0124	0.0119	0.0124	0.0107	0.0085	0.0073
	0.0068	0.0072	0.0075	0.0079	0.0078	0.0089
STD. DEVIATIONS	0.0072	0.0059	0.0052	0.0036	0.0015	0.0013
	0.0018	0.0032	0.0029	0.0033	0.0039	0.0042

 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 6

AVERAGES	0.2942	0.2162	0.2069	0.0943	0.0285	0.0407
	0.0728	0.0900	0.0857	0.0860	0.1130	0.1884
STD. DEVIATIONS	0.2135	0.1710	0.1835	0.0926	0.0562	0.0769
	0.1050	0.1272	0.1363	0.1309	0.1431	0.1644

DAILY AVERAGE HEAD ON TOP OF LAYER 9

AVERAGES	0.2831	0.3028	0.2757	0.2192	0.1260	0.0871
	0.0662	0.0863	0.1047	0.1106	0.1187	0.1459
STD. DEVIATIONS	0.2638	0.2340	0.1910	0.1407	0.0540	0.0507
	0.0641	0.1132	0.1078	0.1203	0.1456	0.1536

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 100

	INCHES		CU. FEET	PERCENT
	-----	-----	-----	-----
PRECIPITATION	48.90	(7.734)	3484469.2	100.00
RUNOFF	0.155	(0.4458)	11053.73	0.317
EVAPOTRANSPIRATION	34.566	(3.6067)	2463066.00	70.687
LATERAL DRAINAGE COLLECTED FROM LAYER 5	0.05570	(0.02249)	3969.001	0.11391
PERCOLATION/LEAKAGE THROUGH LAYER 6	14.07915	(5.67674)	1003236.310	28.79165
AVERAGE HEAD ON TOP OF LAYER 6	0.126	(0.051)		
LATERAL DRAINAGE COLLECTED FROM LAYER 8	13.95068	(5.44356)	994082.125	28.52894
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.10931	(0.02037)	7789.155	0.22354
AVERAGE HEAD ON TOP OF LAYER 9	0.161	(0.063)		
CHANGE IN WATER STORAGE	0.063	(2.7107)	4509.50	0.129

PEAK DAILY VALUES FOR YEARS 1 THROUGH 100		
	(INCHES)	(CU. FT.)
PRECIPITATION	6.87	489534.875
RUNOFF	2.694	191995.7030
DRAINAGE COLLECTED FROM LAYER 5	0.00687	489.31158
PERCOLATION/LEAKAGE THROUGH LAYER 6	1.733660	123535.20300
AVERAGE HEAD ON TOP OF LAYER 6	5.683	
MAXIMUM HEAD ON TOP OF LAYER 6	9.834	
LOCATION OF MAXIMUM HEAD IN LAYER 5 (DISTANCE FROM DRAIN)	60.3 FEET	
DRAINAGE COLLECTED FROM LAYER 8	1.07658	76713.51560
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.004000	285.03003
AVERAGE HEAD ON TOP OF LAYER 9	4.504	
MAXIMUM HEAD ON TOP OF LAYER 9	8.100	
LOCATION OF MAXIMUM HEAD IN LAYER 8 (DISTANCE FROM DRAIN)	13.4 FEET	
SNOW WATER	2.36	168188.7190
MAXIMUM VEG. SOIL WATER (VOL/VOL)		0.3698
MINIMUM VEG. SOIL WATER (VOL/VOL)		0.1187

*** Maximum heads are computed using McEnroe's equations. ***

Reference: Maximum Saturated Depth over Landfill Liner
by Bruce M. McEnroe, University of Kansas
ASCE Journal of Environmental Engineering
Vol. 119, No. 2, March 1993, pp. 262-270.

FINAL WATER STORAGE AT END OF YEAR 100

LAYER	(INCHES)	(VOL/VOL)
1	1.4151	0.2900
2	9.0114	0.3004
3	0.7812	0.0651
4	2.8376	0.2365
5	2.7251	0.2271
6	0.0000	0.0000
7	15.5211	0.2650
8	3.7397	0.1558
9	0.1500	0.7500
SNOW WATER	0.000	

Appendix N, Degraded SDF MSE Vault Closure Cap (10,000 Years): HELP Model Input Data and Output File (output file name: ZMSED8ou.OUT)

Input Data:

Input Parameter (HELP Model Query)				Generic Input Parameter Value			
Landfill area =				19.63 acres			
Percent of area where runoff is possible =				100%			
Do you want to specify initial moisture storage? (Y/N)				Y			
Amount of water or snow on surface =				0 inches			
CN Input Parameter (HELP Model Query)				CN Input Parameter Value			
Slope =				3 %			
Slope length =				450 ft			
Soil Texture =				5 (HELP model default soil texture)			
Vegetation =				4 (i.e., a good stand of grass)			
HELP Model Computed Curve Number = 54.4							
Layer			Layer Number		Layer Type		
Topsoil			1		1 (vertical percolation layer)		
Upper Backfill			2		1 (vertical percolation layer)		
Erosion Barrier			3		1 (vertical percolation layer)		
Middle Backfill			4		1 (vertical percolation layer)		
Upper Drainage Layer			5		2 (lateral drainage layer)		
Upper GCL			6		4 (flexible membrane liner)		
Lower Backfill			7		1 (vertical percolation layer)		
Lower Drainage Layer			8		2 (lateral drainage layer)		
Lower GCL			9		3 (barrier soil liner)		
	Layer Type	Layer Thickness (in)	Soil Texture No.	Total Porosity (Vol/Vol)	Field Capacity (Vol/Vol)	Wilting Point (Vol/Vol)	Initial Moisture (Vol/Vol)
1	1	4		0.4	0.11	0.058	0.11
2	1	30		0.37	0.24	0.136	0.24
3	1	12		0.088	0.0726	0.0596	0.0726
4	1	12		0.375	0.16	0.0745	0.16
5	2	12		0.375	0.16	0.0745	0.16
6 *	4	0.2		0.75	0.747	0.40	0.75
7	1	58.57		0.37	0.24	0.136	0.24
8	2	24		0.248	0.188	0.168	0.188
9	3	0.2		0.75	0.747	0.40	0.75

* The input porosity, field capacity, and wilting point values of the upper GCL are ignored by the HELP model, since the upper GCL is designated as an geomembrane in order for the HELP model to take into account the holes produced by root penetration.

Input Data (continued):

	Layer Type	Sat. Hyd. Conductivity * (cm/sec)	Drainage Length (ft)	Drain Slope (%)	Leachate Recirc. (%)	Recirc. to Layer (#)	Subsurface Inflow (in/yr)
1	1	1.00E-03					
2	1	1.00E-04					
3	1	4.51E-04					
4	1	3.20E-03					
5	2	3.20E-03	450	3			
6	4	5.00E-09					
7	1	1.00E-04					
8	2	1.74E-02	150	11.4			
9	3	5.00E-09					
	Layer Type	Geomembrane Pinhole Density (#/acre)	Geomembrane Instal. Defects (#/acre)	Geomembrane Placement Quality	Geotextile Transmissivity (cm ² /sec)		
1	1						
2	1						
3	1						
4	1						
5	2						
6	4	0	728,360	1			
7	1						
8	2						
9	3						

The lack of values in the table for particular parameters in particular layers denotes that no HELP model input was required for that parameter in that layer. No data are missing from the table.

* The HELP model output often produces an increased number of significant digits for the Effective Saturated Hydraulic Conductivity over that of the actual input.

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**
**      HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE
**      HELP MODEL VERSION 3.07  (1 NOVEMBER 1997)
**      DEVELOPED BY ENVIRONMENTAL LABORATORY
**      USAE WATERWAYS EXPERIMENT STATION
**      FOR USEPA RISK REDUCTION ENGINEERING LABORATORY
**
**
*****
*****
```

```
PRECIPITATION DATA FILE:  D:\HELP3\Hweather\ZPREC.D4
TEMPERATURE DATA FILE:   D:\HELP3\Hweather\ZTEMP.D7
SOLAR RADIATION DATA FILE: D:\HELP3\Hweather\ZSOLAR.D13
EVAPOTRANSPIRATION DATA:  D:\HELP3\Hweather\ZEVAP.D11
SOIL AND DESIGN DATA FILE: D:\HELP3\Hsdfmse\ZMSED8.D10
OUTPUT DATA FILE:         D:\HELP3\Hsdfmse\ZMSED8ou.OUT
```

TIME: 13:24 DATE: 11/14/2003

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*****
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TITLE: Degraded SDF MSE Vault Closure Cap - 10,000 years

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NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER
WERE SPECIFIED BY THE USER.

LAYER 1

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	4.00	INCHES
POROSITY	=	0.4000	VOL/VOL
FIELD CAPACITY	=	0.1100	VOL/VOL
WILTING POINT	=	0.0580	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1100	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.100000005000E-02	CM/SEC

LAYER 2

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	30.00	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC

LAYER 3

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.0880	VOL/VOL
FIELD CAPACITY	=	0.0726	VOL/VOL
WILTING POINT	=	0.0596	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0726	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.451000000000E-03	CM/SEC

LAYER 4

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3750	VOL/VOL
FIELD CAPACITY	=	0.1600	VOL/VOL
WILTING POINT	=	0.0745	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1600	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.319999992000E-02	CM/SEC

LAYER 5

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	12.00	INCHES
POROSITY	=	0.3750	VOL/VOL
FIELD CAPACITY	=	0.1600	VOL/VOL
WILTING POINT	=	0.0745	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1600	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.319999992000E-02	CM/SEC
SLOPE	=	3.00	PERCENT
DRAINAGE LENGTH	=	450.0	FEET

LAYER 6

TYPE 4 - FLEXIBLE MEMBRANE LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.0000	VOL/VOL
FIELD CAPACITY	=	0.0000	VOL/VOL
WILTING POINT	=	0.0000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.0000	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC
FML PINHOLE DENSITY	=	0.00	HOLES/ACRE
FML INSTALLATION DEFECTS	=	728360.00	HOLES/ACRE
FML PLACEMENT QUALITY	=	1	PERFECT

LAYER 7

TYPE 1 - VERTICAL PERCOLATION LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	58.57	INCHES
POROSITY	=	0.3700	VOL/VOL
FIELD CAPACITY	=	0.2400	VOL/VOL
WILTING POINT	=	0.1360	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.2400	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.999999975000E-04	CM/SEC

LAYER 8

TYPE 2 - LATERAL DRAINAGE LAYER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	24.00	INCHES
POROSITY	=	0.2480	VOL/VOL
FIELD CAPACITY	=	0.1880	VOL/VOL
WILTING POINT	=	0.1680	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.1880	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.174000002000E-01	CM/SEC
SLOPE	=	11.40	PERCENT
DRAINAGE LENGTH	=	150.0	FEET

LAYER 9

TYPE 3 - BARRIER SOIL LINER

MATERIAL TEXTURE NUMBER 0

THICKNESS	=	0.20	INCHES
POROSITY	=	0.7500	VOL/VOL
FIELD CAPACITY	=	0.7470	VOL/VOL
WILTING POINT	=	0.4000	VOL/VOL
INITIAL SOIL WATER CONTENT	=	0.7500	VOL/VOL
EFFECTIVE SAT. HYD. COND.	=	0.499999997000E-08	CM/SEC

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT
 SOIL DATA BASE USING SOIL TEXTURE # 5 WITH A
 GOOD STAND OF GRASS, A SURFACE SLOPE OF 3. %
 AND A SLOPE LENGTH OF 450. FEET.

SCS RUNOFF CURVE NUMBER	=	54.40	
FRACTION OF AREA ALLOWING RUNOFF	=	100.0	PERCENT
AREA PROJECTED ON HORIZONTAL PLANE	=	19.630	ACRES
EVAPORATIVE ZONE DEPTH	=	22.0	INCHES
INITIAL WATER IN EVAPORATIVE ZONE	=	4.760	INCHES
UPPER LIMIT OF EVAPORATIVE STORAGE	=	8.260	INCHES
LOWER LIMIT OF EVAPORATIVE STORAGE	=	2.680	INCHES
INITIAL SNOW WATER	=	0.000	INCHES
INITIAL WATER IN LAYER MATERIALS	=	31.070	INCHES
TOTAL INITIAL WATER	=	31.070	INCHES
TOTAL SUBSURFACE INFLOW	=	0.00	INCHES/YEAR

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM
AUGUSTA GEORGIA

STATION LATITUDE = 33.22 DEGREES
 MAXIMUM LEAF AREA INDEX = 3.50
 START OF GROWING SEASON (JULIAN DATE) = 68
 END OF GROWING SEASON (JULIAN DATE) = 323
 EVAPORATIVE ZONE DEPTH = 22.0 INCHES
 AVERAGE ANNUAL WIND SPEED = 6.50 MPH
 AVERAGE 1ST QUARTER RELATIVE HUMIDITY = 68.00 %
 AVERAGE 2ND QUARTER RELATIVE HUMIDITY = 70.00 %
 AVERAGE 3RD QUARTER RELATIVE HUMIDITY = 77.00 %
 AVERAGE 4TH QUARTER RELATIVE HUMIDITY = 73.00 %

NOTE: PRECIPITATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY PRECIPITATION (INCHES)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
4.38	3.95	4.68	2.91	3.56	4.99
5.43	5.41	3.93	3.12	2.96	3.45

NOTE: TEMPERATURE DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA

NORMAL MEAN MONTHLY TEMPERATURE (DEGREES FAHRENHEIT)

JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
46.30	50.00	57.20	64.30	72.10	78.40
81.60	80.30	75.20	65.10	56.70	48.80

NOTE: SOLAR RADIATION DATA WAS SYNTHETICALLY GENERATED USING
COEFFICIENTS FOR AUGUSTA GEORGIA
AND STATION LATITUDE = 33.30 DEGREES

AVERAGE MONTHLY VALUES IN INCHES FOR YEARS 1 THROUGH 100

	JAN/JUL	FEB/AUG	MAR/SEP	APR/OCT	MAY/NOV	JUN/DEC
PRECIPITATION						
TOTALS	4.56	3.57	4.76	2.74	3.60	4.97
	5.81	5.32	4.41	2.99	2.75	3.41
STD. DEVIATIONS	2.44	1.60	2.47	1.31	2.12	2.60
	2.83	2.95	2.54	2.28	1.72	1.90

RUNOFF

TOTALS	0.004	0.000	0.005	0.000	0.000	0.002
	0.035	0.102	0.019	0.009	0.002	0.000

STD. DEVIATIONS	0.021	0.000	0.031	0.003	0.003	0.018
	0.118	0.428	0.087	0.070	0.016	0.002

EVAPOTRANSPIRATION

TOTALS	1.585	2.108	3.139	3.595	3.564	4.118
	4.884	4.502	3.371	1.616	0.951	1.122

STD. DEVIATIONS	0.216	0.228	0.561	0.787	1.523	1.541
	1.589	1.382	1.045	0.605	0.211	0.203

LATERAL DRAINAGE COLLECTED FROM LAYER 5

TOTALS	0.0061	0.0040	0.0043	0.0018	0.0006	0.0009
	0.0015	0.0019	0.0017	0.0018	0.0023	0.0039

STD. DEVIATIONS	0.0044	0.0032	0.0038	0.0018	0.0011	0.0016
	0.0022	0.0026	0.0028	0.0027	0.0029	0.0034

PERCOLATION/LEAKAGE THROUGH LAYER 6

TOTALS	2.8111	1.8484	1.9611	0.8245	0.2546	0.3913
	0.7036	0.8544	0.7993	0.8077	1.0512	1.7855

STD. DEVIATIONS	2.0300	1.4710	1.7572	0.8068	0.5189	0.7108
	1.0035	1.2114	1.2709	1.2375	1.3250	1.5606

LATERAL DRAINAGE COLLECTED FROM LAYER 8

TOTALS	2.1246	2.0599	2.0191	1.5171	0.8924	0.5721
	0.4621	0.6511	0.7839	0.8055	0.8492	1.1155

STD. DEVIATIONS	1.9402	1.5671	1.4295	0.9680	0.4016	0.3762
	0.5028	0.8779	0.7824	0.9085	1.0739	1.1815

PERCOLATION/LEAKAGE THROUGH LAYER 9

TOTALS	0.0294	0.0283	0.0284	0.0225	0.0155	0.0116
	0.0103	0.0125	0.0139	0.0143	0.0146	0.0179

STD. DEVIATIONS	0.0226	0.0182	0.0165	0.0112	0.0048	0.0044
	0.0059	0.0102	0.0091	0.0105	0.0125	0.0137

 AVERAGES OF MONTHLY AVERAGED DAILY HEADS (INCHES)

DAILY AVERAGE HEAD ON TOP OF LAYER 6

AVERAGES	0.1639	0.1180	0.1143	0.0495	0.0148	0.0235
	0.0410	0.0498	0.0481	0.0470	0.0633	0.1040
STD. DEVIATIONS	0.1185	0.0941	0.1025	0.0486	0.0302	0.0428
	0.0585	0.0707	0.0766	0.0722	0.0799	0.0910

DAILY AVERAGE HEAD ON TOP OF LAYER 9

AVERAGES	0.9261	0.9846	0.8801	0.6833	0.3890	0.2577
	0.2014	0.2838	0.3531	0.3511	0.3825	0.4862
STD. DEVIATIONS	0.8457	0.7497	0.6231	0.4360	0.1751	0.1694
	0.2192	0.3827	0.3524	0.3960	0.4837	0.5150

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1 THROUGH 100

	INCHES		CU. FEET	PERCENT
	-----	-----	-----	-----
PRECIPITATION	48.90	(7.734)	3484469.2	100.00
RUNOFF	0.181	(0.4657)	12875.48	0.370
EVAPOTRANSPIRATION	34.556	(3.5776)	2462356.25	70.667
LATERAL DRAINAGE COLLECTED FROM LAYER 5	0.03075	(0.01239)	2191.156	0.06288
PERCOLATION/LEAKAGE THROUGH LAYER 6	14.09278	(5.66993)	1004207.940	28.81954
AVERAGE HEAD ON TOP OF LAYER 6	0.070	(0.028)		
LATERAL DRAINAGE COLLECTED FROM LAYER 8	13.85254	(5.41675)	987088.687	28.32824
PERCOLATION/LEAKAGE THROUGH LAYER 9	0.21922	(0.06364)	15620.731	0.44830
AVERAGE HEAD ON TOP OF LAYER 9	0.515	(0.201)		
CHANGE IN WATER STORAGE	0.061	(2.5632)	4336.44	0.124

PEAK DAILY VALUES FOR YEARS		1 THROUGH	100
		(INCHES)	(CU. FT.)
PRECIPITATION		6.87	489534.875
RUNOFF		2.803	199717.7340
DRAINAGE COLLECTED FROM LAYER	5	0.00426	303.65695
PERCOLATION/LEAKAGE THROUGH LAYER	6	1.950070	138955.95300
AVERAGE HEAD ON TOP OF LAYER	6	3.527	
MAXIMUM HEAD ON TOP OF LAYER	6	6.344	
LOCATION OF MAXIMUM HEAD IN LAYER	5		
(DISTANCE FROM DRAIN)		44.9 FEET	
DRAINAGE COLLECTED FROM LAYER	8	1.27885	91127.16410
PERCOLATION/LEAKAGE THROUGH LAYER	9	0.014865	1059.20911
AVERAGE HEAD ON TOP OF LAYER	9	17.280	
MAXIMUM HEAD ON TOP OF LAYER	9	27.052	
LOCATION OF MAXIMUM HEAD IN LAYER	8		
(DISTANCE FROM DRAIN)		31.1 FEET	
SNOW WATER		2.36	168188.7190
MAXIMUM VEG. SOIL WATER (VOL/VOL)			0.3685
MINIMUM VEG. SOIL WATER (VOL/VOL)			0.1218

*** Maximum heads are computed using McEnroe's equations. ***

Reference: Maximum Saturated Depth over Landfill Liner
by Bruce M. McEnroe, University of Kansas
ASCE Journal of Environmental Engineering
Vol. 119, No. 2, March 1993, pp. 262-270.

FINAL WATER STORAGE AT END OF YEAR 100

LAYER	(INCHES)	(VOL/VOL)
1	1.1692	0.2923
2	9.0114	0.3004
3	0.8712	0.0726
4	2.9221	0.2435
5	2.3601	0.1967
6	0.0000	0.0000
7	15.8699	0.2710
8	4.8018	0.2001
9	0.1500	0.7500
SNOW WATER	0.000	

Appendix O, Technical Report Design Checklist

TECHNICAL REPORT DESIGN CHECKLIST

Report Title: Saltstone Disposal Facility Reviewer: Jones, William E.

Mechanically Stabilized Earth Vault Closure Activity Code: _____

Cap Degradation Base Case: Institutional Control to Pine Forest Scenario (u)
Document No. WSRC-TR-2003-00523 Current Date: 12/09/03

Authors(s): Phifer, Mark A. Date Needed: 12/10/03

Location of report and supplemental information: Final report available through Document Center

Supp. Info. available thru Mark A. Phifer; design check focused on report's HELP modeling.

☒ Analytical/Experimental Approach Instruction: The modeling is appropriate. The HELP model is long-established and widely accepted for water-balance analyses of cover systems.

☒ Mathematical Check Instruction: Verified correct output for equation is presented. Inputs are correct in magnitude. Units are correct.

☒ Inputs Instruction: Inputs are applicable, representative and accurate. Selected values are reasonable for geographic location and expected construction.

☒ Assumptions Instruction: Model assumptions, approach and input are reasonable and clearly presented.

☒ Output Instruction: Model and report results are reasonable and clearly presented.

☒ Transcription Instruction: Post-processing software not used, and therefore not checked against final results. Input spreadsheet tables were checked against model printouts.

Design check completed by: William E. Jones Date: 12/09/03
Comment resolution accepted by: Mark A. Phifer Date: 12/09/03
Date: _____

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