

**Adapting The CANBERRA Q² To Assay
High-Density Solid Waste From 321-M**

Saleem R. Salaymeh

and

Raymond A. Dewberry

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Westinghouse Savannah River Company
Savannah River Site
Aiken, SC 29808



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Publication Date: January 8, 2001

Saleem R. Salaymeh, Author	Date
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R.A. Dewberry, Author	Date
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Ann Gibbs, Technical Reviewer	Date
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P. E. Filpus-Luyckx, Manager, A&RRG-ADS	Date
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Westinghouse Savannah River Company
Savannah River Site
Aiken, SC 29808



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ABSTRACT

The Analytical Development Section of Savannah River Technology Center (SRTC) was requested by the Facilities Disposition Division (FDD) to determine the holdup of enriched uranium in the 321-M facility as part of an overall deactivation project of the facility. The 321-M facility was used to fabricate highly enriched uranium (HEU) fuel assemblies, lithium-aluminum target tubes, neptunium assemblies, and miscellaneous components for the production reactors. The facility also includes the 324-M storage building and the passageway connecting it to 321-M. The results of the holdup assays are essential for determining compliance with the Waste Acceptance Criteria, Material Control & Accountability, and to meet criticality safety controls. As part of the preparation for the start of the dismantling and removal of the HEU, loose and small items were placed in 55 gal drums for shipment to Solid Waste. A large number of drums contained low to medium density materials, and 72 drums contained high-density items. The materials in the 72 drums with high-density waste included scrap metal, metal hand-tools, power tools, motors, pumps, tool boxes, computer parts, gages, etc. All the drums containing low to medium density materials were assayed using the 315-M Canberra Q² Waste Assay System. This system is optimized for the assay of small, evenly distributed quantities of gamma emitting radionuclides. The Q² gives the most accurate results when measuring lightly packaged, hydrocarbon-type materials such as paper, plastics, and cardboard. We developed a novel adaptation of the M-Area Q² using its three detectors and a U-235 transmission source to make multiple measurements of uranium-235 in each drum. The conventional Q² combines the three detector outputs and makes a single density correction measurement based solely on sample mass. This makes the instrument suitable to assay only uniformly distributed low-density waste. We were able to adapt the instrument for assaying non-uniform high-density waste. Each detector's output was collected as a unique measurement. Using three different uranium-235 transmission source locations, we were able to identically measure U-235 gamma transmission through three drum segments. This multiple correction approach is used in segmented gamma scanners. This greatly reduces the impact that variations in the high-density materials would have on the results. This report covers measurements of uranium-235 content in high-density waste within a 55 gal container. We were able to report defensible U-235 contents in 65 of the 72 drums. Our results indicated that the 65 drums contain a total amount of 24.88 g of enriched uranium with values ranging from 2 mg to 3.66 g. This report will discuss the methodology, measurements, assumptions, and results of the U-235 content calculations for each of the 72 drums.

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Adapting The CANBERRA Q² To Assay High-Density Solid Waste From 321-M

By Saleem R. Salaymeh and Raymond A. Dewberry

**Westinghouse Savannah River Company
Savannah River Site
Aiken SC 29808**

1. INTRODUCTION

The 321-M facility was used to fabricate enriched uranium fuel assemblies, lithium-aluminum target tubes, neptunium assemblies, and miscellaneous components for the production reactors. The facility also includes the 324-M storage building and the passageway connecting it to 321-M. The facility operated for 25 years; during this time, thousands of uranium-aluminum-alloy (U-Al) fuel tubes were produced. After the facility ceased operations in 1995, all of the easily accessible U-Al was removed from the building and only residual amounts remained. The bulk of this residue is located in the equipment that generated and handled small U-Al particles and the exhaust systems for this equipment (e.g., Chip compactor, casting furnaces, log saw, lathes A & B, cyclone separator, Freon[®] cart, riser crusher, ...etc).¹

Prior to the start of the dismantling and removal of the HEU, loose and small items were placed in 55 gal drums for shipment to Solid Waste.² A large number of drums contained low to medium density materials, and 72 drums contained high-density items. The materials in the 72 drums with high-density waste included scrap metal, metal hand-tools, power tools, motors, pumps, tool boxes, computer parts, gages, etc.

Each low level waste package presented for disposal in the E-Area Vaults must meet the radionuclide limits specified in WSRC 1S WAC, 3.17.³ WSRC 1S, WAC 2.02⁴ specifies acceptable methods for quantifying waste package activity. Among the acceptable methods are Dose-to-Curie (DTC), direct sampling, and direct assay. Examples of acceptable assay equipment include use of the Canberra Q² system as specifically cited in WAC 2.02. Using the assay results, together with a known radiological distribution, the generator can quantify waste package isotopic activity and compare against WSRC 1S, WAC 3.17 limits to certify compliance with the radiological criteria.³

All the drums containing low to medium density materials were assayed using the 315-M Canberra Q² Waste Assay System. This system is optimized for the assay of small, evenly distributed quantities of gamma-emitting radionuclides. The Q² gives the most accurate results when measuring lightly packaged, hydrocarbon-type materials such as paper, plastics, and cardboard.⁵

The 72 drums containing high-density waste containing enriched uranium were scheduled for assay using the passive neutron shuffler system existing in F-Area. However, due to the work priority and backlog existing at the time of assay, the F-Area shuffler was not available for use to quantify these drums.

Using neutron-counting techniques is by far the preferred method of assaying very high-density items. To assay for HEU requires a neutron activation technique. Either of the FB-Line or M-Area Cf-shufflers would be a good choice for these assays, but neither was available. An active-well neutron coincidence counter does not have adequate sensitivity to measure U-235 in the range of milligrams or grams per drum.⁶ A passive neutron drum counter is not useful for measurement of U-235 content. We were constrained to use some kind of a γ -ray acquisition system to perform these requested assays. A far-field γ -ray assay was unsuitable for the same reasons that the Q^2 instrument procedure was unsuitable. The extreme densities and extreme non-uniformity of the waste made the use of a single transmission correction completely unreliable. To perform the assays we adapted the 313-M Q^2 instrument to operate approximately like a segmented gamma scanner.

This report discusses how the Canberra Q^2 was adapted for measuring U-235 content in high-density waste. It also includes the methodology, non-destructive assay (NDA) measurements, assumptions, and results of the assay of 72 drums containing high-density waste.



Figure 1. A photograph of the Q^2 showing its detector arrangement.

2. EXPERIMENTAL

Limitations of the method:

- This system is optimized for the assay of small, evenly distributed quantities of gamma emitting radionuclides.
- The Q2 gives the most accurate results when measuring lightly packaged, hydrocarbon-type materials such as paper, plastics, and cardboard.
- The 185 KeV will not be detected through $\frac{3}{4}$ in of steel, thus any object, such as pumps that have $>\frac{3}{4}$ " thick walls and contains internal contamination, will not be detected.
- An additional uncertainty is introduced because the detectors are not collimated. This allows cross talk between the three vertical segments, making the system effectively a hybrid between a close-field and segmented system. Therefore we have two distinct correction factors for calculating the content.
- Often the top half of the drum is empty which could lead to an error in the transmission.
- Since the waste in the drum is not homogeneous, and the drum is rotating, a metal object may be in the field of view of the detector only part of the time. The $k\ln(1/T)$ form of the transmission correction factor partly compensates for this uncertainty.

To accomplish the measurements requested we adapted the 313-M Canberra Q² instrument to acquire data in a mode approximately equivalent to a three segment segmented gamma scanner. The 313-M Canberra Q² Waste Assay System is a quantitative and qualitative gamma-ray pulse height analysis system capable of measuring very low amounts of U-235. It uses three 20% efficient intrinsic high purity germanium detectors with 7.5 liter cryostats. The sample is placed on a turntable mounted on the door of the shielding and then rotated at a nominal 10 RPM. An electronic load cell on the turntable weighs the sample and displays the result. A four-inch thick low-background steel shield surrounds the sample and detectors in all directions. The data acquisition system contains a PC-based Canberra AccuSpec Multichannel Analyzer system, appropriate high voltage power supply, and amplifiers. The three AccuSpec boards are controlled by Canberra's Genie-PC Gamma Waste Assay System.⁷

A photograph of the Canberra Q² is shown in Figure 1. Note that the instrument has three vertically stacked detectors to acquire close field γ -ray data from three portions of a 55-gallon drum. When operated by its normal procedure to assay for U-235, the system sums the three spectra acquired and fits the peak area in the summed spectrum to determine the detection rate for the 185-keV γ -ray from U-235 decay. The system then applies a pre-determined detection efficiency and a density correction factor to relate detected events to measured content.⁸ An important feature is that the three detectors are not collimated. The transmission correction factor used by the Q² is determined from a simple measure of the mass of the drum being assayed, and so the instrument assumes a completely uniform distribution of mass in the drum and that each detector is looking at the same transmission characteristics. For these 72 drums of solid waste those two assumptions are especially

poor. In addition, since the drums have very high densities up to 1.3 g/cc, they are out of the reliable range for the Q^2 . Local densities ranged up to 8 g/cc, and so the transmission of the 185-keV γ -ray out of individual components of the waste will be as low as fractions of a percent. Therefore the only reliable measure of U-235 content using γ -ray acquisitions would be with a segmented scanner.



Figure 2. A photograph showing inside the Q^2 and transmission source positions.

Our technique of data acquisition to assay for U-235 content in each of the 72 drums is illustrated in the photograph shown in Figure 2. For each drum a 4.85-g source of U-235 was placed inside the Q^2 cavity opposite the top detector, and a γ -ray spectrum was acquired with the drum in place for 60 – 600 seconds. The area under the 185-keV γ -ray peak and the detector livetime were obtained manually for the top detector. Then successive acquisitions were obtained with the source opposite the middle and bottom detectors, and the data for each of the middle and bottom detectors were obtained manually. Finally the drum was counted for 600 – 3600 seconds without the source present. In this way we obtained data sufficient to measure the transmission of the photons from the 4.85-g source directly through each of the three barrel segments to the detector opposite the source.

This was a very expensive technique to use to assay the 72 drums. Each drum required four counts. None of the acquisitions was automated, and all of the data were obtained manually. For each acquisition the Q^2 stores the summed spectrum from all three detectors, but no single spectrum from an individual detector was ever available except on the instrument display immediately after the acquisition or when we aggressively stored it on a disk. Data were hand recorded in a laboratory notebook for subsequent analysis. We recorded data on thirteen separate days of acquisitions over a period of three months. For each distinct day of acquisition we recorded T_0 spectra with the transmission source

successively opposite each of the three detectors and with no sample drum present. These daily spectra served both as the unattenuated transmission spectra for determination of sample attenuation and as a QC check on the instrument. FDD management accepted the very large expense and the known and very large uncertainties of using this γ -ray technique in order to obtain a gram value for each of these high priority drums.

3. Data and Analysis

The data acquired for each drum are recorded and manipulated in the Excel™ spreadsheet of Table 1. The first eight columns in Table 1 serve to identify the drum and to record count times and peak areas obtained and to calculate cps and uncertainties for each detector segment for the transmission data and sample only data. Columns nine through thirteen contain calculated values that we describe below in an example calculation. The spreadsheet was formatted to round all results to two places past the decimal. The data for each drum are recorded in four blocks of three where the last block of three represents the manual counts obtained in each of the three detectors from the drum-only spectra. For each drum the first three blocks of three represent the data obtained with the source present. For each day of acquisition we have recorded three blocks of three T_0 data.

Looking at the first three blocks of T_0 data acquired on 25 July we begin a description of the calculations. The spectrum labeled T01725 is the unattenuated spectrum going into the top detector, the spectrum labeled T02det2 is the unattenuated spectrum going to the middle detector, and the spectrum labeled T03det3 is the unattenuated spectrum going to the bottom detector. These three spectra had count rates of 16.99, 16.48, and 16.52 cps respectively, as seen in column seven of Table 1. Taking the average, we record 16.66 cps as the unattenuated count rate for each detector.

Table 1. Sample Calculations for Drum FD000420.

Sample	File Name	Count Time	Area	% S	S	cps	S cps	1/T	C _r SQRT of 1/T	Segment Corrected cps	C _r of ln1/T	Segment Corrected cps
T ₀₁	T01725	281.52	4784	1.49	71.28	16.99	0.25					
T ₀₁	T01det2	281.52	4621	1.52	70.24	16.41	0.25					
T ₀₁	T01det3	281.52	3438	1.76	71.28	12.21	0.25					
T ₀₂	T02det1	300	4396	1.56	68.58	14.65	0.23					
T ₀₂	T02det2	300	4944	1.47	72.68	16.48	0.24					
T ₀₂	T02det3	300	4385	1.55	67.97	14.62	0.23					
T ₀₃	T03det1	300	3750	1.72	64.50	12.50	0.22					
T ₀₃	T03det2	300	4670	1.52	70.98	15.57	0.24					
T ₀₃	T03det3	300	4955	1.47	72.84	16.52	0.24					
T _{empty drum}	Dmtdet1	300	3151	1.85	58.29	10.50	0.19	1.59	1.26		1.19	
T _{empty drum}	Dmtdet2	300	3631	1.73	62.82	12.10	0.21	1.38	1.17		1.13	
T _{empty drum}	Dmtdet3	300	3230	1.83	59.11	10.77	0.20	1.55	1.24		1.18	
FD000420	T1420D1	271	2793	1.98	55.30	10.31	0.20	1.71	1.31		1.23	
FD000420	T1420D2	271	493	5.03	24.80	1.82	0.09					
FD000420	T1420D3	271	258	4.26	10.99	0.95	0.04					
FD000420	T2420D1	600	632	4.45	28.12	1.05	0.05					
FD000420	T2420D2	600	2140	2.36	50.50	3.57	0.08	6.41	2.53		1.90	
FD000420	T2420D3	600	1268	3.05	38.67	2.11	0.06					
FD000420	T3420D1	600	1644	2.66	43.73	2.74	0.07					
FD000420	T3420D2	600	1381	2.97	41.02	2.30	0.07					
FD000420	T3420D3	600	3325	1.28	42.56	5.54	0.07	3.37	1.83		1.55	
FD000420	420D1	1292.3	719	4.19	30.13	0.56	0.02			0.73		0.68
FD000420	420D2	1292.3	1252	3.14	39.31	0.97	0.03			2.45		1.84
FD000420	420D3	1292.3	766	4.04	30.95	0.59	0.02			1.09		0.92
								Sum (cps)		4.27		3.44

Activity per drum (dps) = Sum cps/0.000885(0.53) = Sum cps/0.000469

= 9101.50

7340.10

Activity per drum (nCi) = dps*60/2220 = 9101.5*0.027

= 245.70

198.18

To obtain the transmission for detector 1 for drum FD000420, we use the transmission spectrum T1420D1 and the sample only spectrum 420D1. The transmission spectrum detection rate is 10.31 ± 0.20 cps, and the drum only detection rate is 0.56 ± 0.02 cps. The transmission value of column nine is calculated by

$$T = (10.31 - 0.56) / 16.66 = 0.585, \quad (1)$$

and the transmission factor of column nine is

$$1/T = 1.71.$$

We perform similar calculations to obtain transmission factors of 6.41 and 3.37 for the middle and bottom detectors. We then perform two distinct calculations of U-235 content based on two distinct transmission correction form factors. The first calculation assumes that the correction factor is equal to the square root of the transmission factor. This is based on the reasoning that the transmission source photons had to pass through the entire sample, but on average the sample photons have to transit only half of the sample. In column ten of Table 1 we determine and tabulate the correction factors for each segment to be equal to the square root of $1/T$ for that segment. Therefore for sample FD420 we obtain the correction factors 1.307 for the top detector, 2.533 for the middle, and 1.835 for the bottom detector. These correction factors are then applied to the measured detection rates tabulated in column seven to obtain the corrected count rates tabulated in column eleven.

$$\text{Corrected rate}(\text{det1, FD420}) = 1.307(0.56) = 0.727 \text{ cps.} \quad (2)$$

The corrected rate for detector 2 is 2.454 cps, and the corrected rate for detector 3 is 1.088 cps. The three corrected rates are summed as shown in Table 1. The total activity per drum is then determined by dividing by the overall Q^2 detection efficiency for the 185 keV γ -ray and by dividing by the branching ratio of 0.53 to obtain the total U-235 activity per drum. The total is listed at the bottom of Table 1 in units of decays per second. The summed efficiency for the 185-keV γ -ray is 0.000885.

$$\begin{aligned} [\text{U-235}]_{\text{FD420}} &= 4.269 / (0.000885)(0.53) = 4.269 / 0.000469 \\ &= 9102 \text{ dps.} \end{aligned} \quad (3)$$

Finally, we convert from decays/sec-drum to nCuries/drum by multiplying by 60/2220. The square root correction factor is applicable to a far field measurement where the rotated drum (sample) is much farther from the detector than the radius of the drum and where the correction factors are not far from unity. The far field correction factor considers that at large distances the photons passing all the way through from the back of the drum to the detector travel almost the same distance as those that pass from near the front of the drum to the detector.

The next set of calculations of U-235 content is based on the transmission correction factor for a close field measurement. This correction factor recognizes that in a close field measurement by far most of the photons that reach the detector came from portions of the sample that are near the detector when they leave the sample. This correction factor considers that when the sample self-absorption is large, those photons that originate from the back side of the sample have very little chance to reach the detector. Therefore by far most of the photons that reach the detector had the short path to the detector and had to transit only a fraction of the sample. Thus the effective correction factor is much smaller than the square root of $1/T$.

From reference 9, the correction factor is calculated by

$$Cf_{(\text{close field})} = -k \ln(1/T) / [1 - (1/T)^k], \quad (4)$$

where $k = \pi/4 = 0.785$. As above, we perform a separate calculation of the correction factor from the measured transmission for each segment for each drum. In column twelve of Table 1, we calculate the close-field transmission correction factors. Using drum FD420 again, we perform an example calculation. For the top segment of drum FD420 we measured a transmission factor of 1.709. The calculated correction factor for this segment then becomes

$$Cf_{(\text{close field})} = -0.785 \ln(1/1.709) / [1 - (1/1.709)^{0.785}] = -0.785(-0.535) / [1 - 0.656] = 1.225. \quad (5)$$

The correction factors for segments two and three are then 1.901 and 1.551 as shown in the appropriate elements of column twelve of Table 1. The corrected count rates are shown in column thirteen, where the corrected rate for the top segment of drum FD420, is

$$1.225 * 0.56 = 0.682 \text{ cps.}$$

The corrected segment rates are summed in column thirteen of Table 1, and for FD420 that sum is 3.443 cps. Dividing by the Q^2 efficiency we obtain

$$[U-235]_{FD420} = 3.443 / 0.000469 = 7340 \text{ dps,} \quad (6)$$

or 198 nCurie for drum FD420. The term 0.000469 is defined in equation 3 above.

Each of the 72 drums was assayed in this manner. The measured data and calculated parameters are all tabulated in the Appendix, which is a reproduction of an Excel spreadsheet that performs the two transmission-corrected calculations for each drum. The measured transmission values for each segment of each drum are listed in column eight of the Appendix. The reader can note that generally the transmission values for the top segment of each drum were in the range of 1.3 – 2.0, while those values for the middle and bottom portion varied widely in the range of 1.5 – 700. (Some even went negative, which we discuss below.) These widely varying transmission values are a manifestation that the drums clearly were not filled with a uniform distribution of solid waste.

For most drums the top portion was approximately empty of material, and the measured transmission correction was approximately equal to that of the drum only, as shown by the empty drum correction factors listed near the middle of Table 1. The middle and bottom portions of the drums all contained material of widely varying density. From these data it is clear that individual transmission correction factors for each segment are very important for a γ -PHA assay. All of the 72 drums are out of the boundary limit of the Q^2 assumption of uniform density.

4. Results and Discussion

We obtain two unique measures of U-235 content for each drum. One is based on a far field transmission correction factor, and one is based on a close field segmented gamma scanner correction factor, where the latter measure is without fail lower than the former. The adapted technique we have used with the Q^2 is clearly not representative of a far-field measurement. It is also not exactly representative of a close field segmented scanner because the detectors are not collimated. Thus neither calculation of the correction factor is quite correct. In all cases for our reported value we have used the average with a one sigma standard deviation precision. The two measured values along with the reported value and Q^2 value for each drum are listed in Table 2.

The reported values listed in the sixth column of Table 2 are equal to the average of the two calculations with an uncertainty equal to the standard deviation. In almost all cases the uncertainty of either single calculation is dominated by the uncertainty of the measured transmission factor. This is especially true when the transmission factor is large. That is, when a given transmission factor is large, its uncertainty is also large. The overall uncertainty in either single method of calculation of U-235 content can be determined by propagating the uncertainty of the transmission factors through the calculation. However we have observed that even when performing that rigorous propagation of uncertainty, the final uncertainty for each reported value is always dominated by the disagreement in the two methods of calculation. Thus there is no benefit to report the propagation of uncertainty.

The Q^2 value tabulated in column five of Table 2 is simply the instrumental value that the Q^2 made from the drum-only acquisition using its own efficiency curve and correction factor based on each individual drum mass. For most of the 72 cases all three of the measured values are in fairly good agreement, indicating that while our adapted technique has significantly improved the defensibility of the measurement, it has not significantly improved the accuracy. However for several cases our measured values differ significantly from the Q^2 values, and we believe ours are far superior. In seven cases we obtained physically unreal (i.e. negative) values of the transmission factor. From the form of equation (1) it is clear that this happens only when the drum-only detection rates are greater than the drum plus transmission source detection rates - or equivalently, when the transmission factors are so low that photons from the transmission source have no chance to reach the detector.

In drums where any one of the segments yielded a physically unreal transmission value, we have tabulated our measured value as "N/A". These seven drums represent cases where a γ -ray assay is not applicable. Even though in five of these seven cases the Q^2 instrument delivered a finite measured value using its own transmission corrected value based on mass, these measured values have to be considered completely unreliable and would under-report the actual contents. For those seven cases our transmission measurements have demonstrated that the sample must be considered infinitely thick with respect to the 185-keV γ -ray from U-235, and so any measured value based on γ -PHA is out of the boundary limits of the system. These seven drums will have to be assayed by a neutron counting system or repackaged for Q^2 assay or analyzed with special attention similar to the holdup assays performed for the riser crusher and casting furnaces.¹⁰

Table 2. A list of all the drums and measured contents.

Drum ID	Description	C _r (SqRt)	C _r (ln/T)	Q ²	nCi per Drum	s nCi per Drum	g/Drum
Empty Drum	Empty Drum	4	3		4	1	0.00
FD000402	Computer Equipment	227	169	152±5	198	41	0.09
FD000403	Scrap Metal; Tools; Aluminum Cans	421	332	255±7	376	63	0.17
FD000405	Computer Equipment	12	9		10	2	0.00
FD000406	Widen Pumps (2)	151	102	114±6	126	35	0.06
FD000407	Air Sample; Drop Light	131	110	158±6	120	15	0.06
FD000410	Tools; Grinding Brushes; Dolly Face Cover; Computer Screen	768	306	216±4	537	327	0.25
FD000412	Computer Equipment	7	6	7±2	6	1	0.00
FD000413	Scrap Metal; Tools; Plastic	132	99	181±4	116	23	0.05
FD000414	Computer Equipment	4683	2543	2390±35	3613	1513	1.67
FD000416	Plastic; Monitor Meter	220	153	165±4	186	47	0.09
FD000417	Computer Parts	17	14	>10	16	2	0.01
FD000418	Scrap Metal; Tools	327	253	352±11	290	52	0.13
FD000420	Scrap Metal; Tools; Calibration Item; Electric Motor; Scale; Electric Cords	246	198	228±6	222	34	0.10
FD000421	Scrap Metal; Power Supply; Meter Gages	1095	790	998±21	942	216	0.44
FD000554	Tool Box; Scale	128	109	128±5	118	13	0.05
FD000555	Scale; Computer Monitors; Power Conditioner; Scrap Metal	11	7	8±2	9	3	0.00
FD000556	Scrap Metal; Tools	154	135	145	144	13	0.07
FD000557	Tools; Scrap Metal	283	246	273±9	264	26	0.12
FD000559	Scrap Metal; Motor	75	41	28±3	58	24	0.03
FD000560	Computer Parts; Scrap Metal	2	2	<4	2	0	0.00
FD000561	Duct Hoses; Plastic Trash Cans; Fuse Boxes	991	524	524±24	758	330	0.35
FD000562	Graphite Molds; Silver Aprons & Jackets; Press Plate	2059	1139	1130±23	1599	651	0.74
FD000563	Scrap Metal; Tools	N/A					0.00
FD000564	Scale; Air Gun; Power Tools; Scrap Metal	373	270	237±7	322	73	0.15
FD000565	Plastic Rack; Scrap Metal	2133	1351		1742	553	0.81
FD000566	Wooden Box; Caution Cones	684	590	620±13	637	66	0.29
FD000567	Apron Jackets; Computer Parts; Air Pump; Motor; Calculator	77	42	40±5	60	25	0.03
FD000569	Plastic Hose; Scrap Metal	774	645	769±16	710	91	0.33
FD000570	Calibrated Standards; Scrap Metal	850	673	790	762	125	0.35
FD000571	Scale; Scrap Metal	8005	3748	2900±57	5876	3010	2.72
FD000573	Scrap Metal	150	126	114±6	138	17	0.06
FD000578	Computer Parts; Scrap Metal	4	3	<10	4	1	0.00
FD000579	Tool Box; Scrap Metal	72	60	52±4	66	8	0.03

Drum ID	Description	C _f (SqRt)	C _f (ln/T)	Q ²	nCi per Drum	s nCi per Drum	g/Drum
FD000580	Floppy Disk, Scrap Metal, Computer Equipment	23	18	15±1	20	4	0.01
FD000581	Scale; Computer Equipment; Scrap Metal	48	33	31±2	40	11	0.02
FD000582	Scrap Aluminum; Scrap Metal	5035	3021	2380±59	4028	1424	1.86
FD000583	Scrap Aluminum ; Scrap Metal	70	41	34±4	56	21	0.03
FD000594	Scrap Aluminum; Fiberglass; Electrical Cords; Scrap Metal	60	37	29±1	48	16	0.02
FD0000595	Container returned unused	6	5	<10	6	1	0.00
FD000596	Electrical Cords; Fiberglass; Scrap Metal	271	214	194±3	242	40	0.11
FD000597	Scrap Metal	143	121	140±4	132	16	0.06
FD000378	No Description available	8375	5702	9740±110	7038	1890	3.26
FD000394	No Description available	8066	5011	4600±87	6538	2160	3.03
FD000382	No Description available	1058	165	107±2	612	631	0.28
FD000385	No Description available	N/A		265±5			0.00
FD000379	No Description available	N/A					0.00
FD000396	No Description available	208	111		160	69	0.07
FD000399	No Description available	398	283		340	81	0.16
FD000408	No Description available	103	80	77±3	92	16	0.04
FD000397	No Description available	228	128	125±3	178	71	0.08
FD000404	No Description available	161	126	109±6	144	25	0.07
FD000384	No Description available	N/A		595±15			0.00
FD000400	No Description available	243	165	143±6	204	55	0.09
FD000398	No Description available	904	417	351±12	660	344	0.31
FD000415	No Description available	174	116	111±3	145	41	0.07
FD000377	No Description available	105	83	78±5	94	16	0.04
FD000411	No Description available	66	53	55±3	60	9	0.03
FD000389	No Description available	5212	1445	1580±54	3328	2664	1.54
FD000386	No Description available	2637	602	558±17	1620	1439	0.75
FD000391	No Description available	606	313	312±11	460	208	0.21
FD000392	No Description available	2271	1597	1530±26	1934	477	0.90
FD000381	No Description available	220	96	82±3	158	88	0.07
FD000380	No Description available	N/A		112±4			0.00
FD000401	No Description available	87	58	51±4	72	21	0.03
FD000390	No Description available	1678	761	1200±22	1220	648	0.56
FD000388	No Description available	N/A		1880±42			0.00
FD000395	No Description available	1464	844	768±19	1154	438	0.53
FD000383	No Description available	3978	1866	2350±48	2922	1493	1.35
FD000387	No Description available	N/A		8950±110			0.00

5. CONCLUSION

We have used a special acquisition procedure that adapts the Canberra Q² instrument to a transmission corrected three-segment segmented gamma scanner to assay 72 drums of high density non-uniform solid waste from the 321-M deactivation project. We have reported defensible U-235 contents in 65 of the 72 drums. The measured values range from 4 nCi/drum (2 mg) to 7040 nCi/drum (3.66 g) with one sigma uncertainties generally of about 20%. Seven drums contained solid waste of such extreme density that we could obtain no finite transmission correction. That is, these seven drums contained waste that in at least one of the acquisition segments was infinitely thick to the 185 keV γ -ray. As discussed in the **Introduction**, these seven drums must be assayed by a neutron-based counting instrument such as a californium shuffler.

Our special acquisition procedure used a 4.85 g source of U-235 as a movable and removable transmission source so that we could obtain a transmission measurement for each of three segments in each of the 72 drums of solid waste. The measured transmission factors varied over the range of 1.3 up to almost 800, clearly demonstrating extreme non-uniformity in the waste assayed. The widely varying transmission factors also clearly demonstrate that the measured values obtained from the normal operation of the Q² would be completely indefensible for these drums.

In our determinations of U-235 content we have used two distinct calculations of the transmission correction factor. Because the acquisition configuration is an adapted one, neither method of calculation quite fits the physical situation. Therefore our reported values are based on the resulting average of the two calculations, and the reported uncertainty for each value is equal to the standard deviation of the average. This standard deviation dominates the uncertainty (imprecision) of each individual measurement so that it was not necessary to propagate the individual measurement uncertainties through for each calculation.

6. ACKNOWLEDGEMENTS

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8. APPENDIX

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Sample	File Name	Count Time	Area	% s	s	cps	s cps	1/T	Cf= SQRT(1/T)	Corr. cps	Corr. Sum (cps)	Drum Activity (dps)	Drum Activity (nCi)	C _f of ln1/T	Corr. Sum (cps)	Drum Activity (dps)	Drum Activity (nCi)
T ₀₁	T01det1	57.13	889	3.48	30.94	15.56	0.54										
T ₀₁	T01det2	100	1701	2.5	42.53	17.01	0.43										
T ₀₁	T01det3	100	1214	2.98	30.94	12.14	0.31										
T ₀₂	T02det1	100	1314	2.89	37.97	13.14	0.38										
T ₀₂	T02det2	58.79	995	3.24	32.24	16.92	0.55										
T ₀₂	T02det3	100	1578	2.6	37.97	15.78	0.38										
T ₀₃	T03det1	72.82	807	3.66	29.54	11.08	0.41										
T ₀₃	T03det2	72.82	1163	3	34.89	15.97	0.48										
T ₀₃	T03det3	58.29	1032	3.24	29.54	17.70	0.51										
								16.73									
FD379	T1379D1	305.55	3897	1.69	65.86	12.75	0.22	1.45	1.204					1.15			
	T1379D2	305.55	4526	1.61	72.87	14.81	0.24										
	T1379D3	305.55	3880	2.05	79.54	12.70	0.26										
	T2379D1	165.56	1736	2.56	44.44	10.49	0.27										
	T2379D2	165.56	1163	3.28	38.15	7.02	0.23	5.64	2.374					1.83			
	T2379D3	165.56	1432	2.96	42.39	8.65	0.26										
	T3379D1	425.69	1259	3.19	40.16	2.96	0.09										
	T3379D2	425.69	2507	2.26	56.66	5.89	0.13										
	T3379D3	425.69	3600	1.85	66.60	8.46	0.16	-147.87	N/A					N/A			
	379D1	300	366	6.28	22.98	1.22	0.08			1.469				1.41			
	379D2	300	1217	3.37	41.01	4.06	0.14			9.631	N/A	N/A	N/A	7.41	N/A	N/A	N/A
	379D3	300	2571	2.17	55.79	8.57	0.19			N/A				N/A			

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Sample	File Name	Count Time	Area	% s	s	cps	s cps	1/T	Cf= SQRT(1/T)	Corr. cps	Corr. Sum (cps)	Drum Activity (dps)	Drum Activity (nCi)	C _f of ln1/T	Corr. Sum (cps)	Drum Activity (dps)	Drum Activity (nCi)
FD561	T1561D1	310.62	558	4.91	27.40	1.80	0.09	39.81	6.309					3.06			
	T1561D2	310.62	528	5.04	26.61	1.70	0.09										
	T1561D3	310.62	408	5.6	22.85	1.31	0.07										
	T2561D1	600	1194	3.19	38.09	1.99	0.06										
	T2561D2	600	1526	2.96	45.17	2.54	0.08	11.03	3.32					2.22			
	T2561D3	600	1648	2.72	44.83	2.75	0.07										
	T3561D1	449.84	794	4.06	32.24	1.77	0.07										
	T3561D2	449.84	1443	2.93	42.28	3.21	0.09										
	T3561D3	449.84	586	4.85	28.42	1.30	0.06	34.73	5.893					2.97			
	561D1	252.95	351	6.03	21.17	1.39	0.08			8.755				4.25			
	561D2	252.95	270	7.28	19.66	1.07	0.08			3.544	17.21	36706	991.06	2.37	9.10	19394	524
	571D3	252.95	211	7.75	16.35	0.83	0.06			4.916				2.48			

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Sample	File Name	Count Time	Area	% s	s	cps	s cps	1/T	Cf= SQRT(1/T)	Corr. cps	Corr. Sum (cps)	Drum Activity (dps)	Drum Activity (nCi)	C _f of ln1/T	Corr. Sum (cps)	Drum Activity (dps)	Drum Activity (nCi)
FD000414	T1414D1	154.69	1971	2.38	46.91	12.74	0.30	2.94	1.72					1.48			
	T1414D2	154.69	2039	2.36	48.12	13.18	0.31										
	T1414D3	154.69	468	5.13	24.01	3.03	0.16										
	T2414D1	63.11	771	3.84	29.61	12.22	0.47										
	T2414D2	63.11	537	4.65	24.97	8.51	0.40	45.04	6.71					3.15			
	T2414D3	63.11	205	8.07	16.54	3.25	0.26										
	T3414D1	300	2385	2.19	52.23	7.95	0.17										
	T3414D2	300	2408	2.22	53.46	8.03	0.18										
	T3414D3	300	981	3.61	35.41	3.27	0.12	26.67	5.16					2.79			
	414D1	655.81	4864	1.53	74.42	7.42	0.11			12.73				11.00			
	414D2	655.81	5352	1.46	78.14	8.16	0.12			54.77	81.35	173454	4683.27	25.69	44.17	94173	2542.67
	414D3	655.81	1759	2.65	46.61	2.68	0.07			13.85				7.48			
FD000402	T1402D1	324.1	1307	2.98	38.95	4.03	0.12	4.23	2.06					1.67			
	T1402D2	324.1	1674	2.62	43.86	5.17	0.14										
	T1402D3	324.1	408	5.87	23.95	1.26	0.07										
	T2402D1	300	1445	2.81	40.60	4.82	0.14										
	T2402D2	300	678	4.27	28.95	2.26	0.10	9.35	3.06					2.12			
	T2402D3	300	773	4.9	37.88	2.58	0.13										
	T3402D1	300	569	4.62	26.29	1.90	0.09										
	T3402D2	300	673	4.23	28.47	2.24	0.09										
	T3402D3	300	1072	3.28	35.16	3.57	0.12	5.35	2.31					1.80			
	402D1	1200	392	6.12	23.99	0.33	0.02			0.67				0.55			

Sample	File Name	Count Time	Area	% s	s	cps	s cps	1/T	Cf= SQRT(1/T)	Corr. cps	Corr. Sum (cps)	Drum Activity (dps)	Drum Activity (nCi)	C _f of ln1/T	Corr. Sum (cps)	Drum Activity (dps)	Drum Activity (nCi)
	402D2	1200	699	4.33	30.27	0.58	0.03			1.78	3.94	8397.97	226.75	1.24	2.94	6262.51	169.09
	402D3	1200	771	4.05	31.23	0.64	0.03			1.49				1.16			