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A Statistical Review of Composition Data from DWPF's Process Samples for Macro-Batch 1

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by

T. B. Edwards

Westinghouse Savannah River Company Savannah River Site Aiken, South Carolina 29808 Technical Assistance Request: HLW/DWPF-TAR-990002

A Statistical Review of Composition Data from DWPF's Process Samples for Macro-Batch 1 (U)

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ABSTRACT

The measurements derived from samples taken during the processing of macro-batch 1 (MB1) at the Defense Waste Processing Facility (DWPF) have been reviewed and compared in this report. Batches 22 through 93 were the focal point of this study.

Statistical control charts were developed for each analyte for each vessel to identify influential or exceptional results in the variation, central tendency, or both for the measurements. These charts should serve as a basis for observing the (expected) impact of some decisions made during the processing of this macro-batch.

Statistical comparisons were made between the two dissolution methods used to prepare these MB1 samples: mixed acid (MA) and peroxide fusion (PF), where both were available. Statistically significant differences (at the 5% significance level) are seen in the results from the two dissolution methods for several analytes. However, for all of the major cations (except that for silicon) the differences are less than 5%. For silicon, the MA values tend to be biased low while the PF values tend to be biased high. The average of the MA and PF values is used to represent this cation concentration in DWPF's Product Composition Control System (PCCS), which mitigates the differences in silicon measurements derived by the two dissolution methods.

A comparison of the results for the Slurry Mix Evaporator (SME) versus those of the Melter Feed Tank (MFT), shows a statistically significant difference (at the 5% level) for Total and Calcined Solids (SME value > MFT value for each with a Mean Difference = 2.3 wt%), for Insoluble Solids (SME value > MFT value with a Mean Difference = 2.5 wt%), and for density (SME value > MFT value with a Mean Difference = 0.02 g/mL). A higher Total Solids in the SME versus the MFT is not unexpected since the MFT is not sampled immediately following the transfer from the SME but is sampled somewhat later, potentially, after the melter feed pumps have been primed with water.

No cation concentrations (by either dissolution method) show a statistically significant difference between the SME and MFT (at the 5% significance level) including the ratios of iron to lithium (Fe/Li) and iron to aluminum (Fe/Al). In an earlier study, there was an indication of concern for differences in the aluminum, iron and copper concentrations between the two tanks. The analyses of this study show no indication of such differences between the two tanks for these cations over the complete set of results for MB1.

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1.0 Introduction

The Defense Waste Processing Facility (DWPF) began processing the first macro-batch of radioactive waste at the Savannah River Site (SRS) in 1996. This first macro-batch, designated Macro-Batch 1 or MB1, began with the first radioactive processing batch, Batch 19. The processing of MB1 ended with Batch 93, and Batch 94 began Macro-Batch 2, MB2. In the DWPF, samples are taken at the Sludge Receipt and Adjustment Tank (SRAT) upon receipt of the sludge into the SRAT and immediately prior to transfer of the sludge from the SRAT, at the Slurry Mix Evaporator (SME), and at the Melter Feed Tank (MFT) for each batch processed. The DWPF Analytical Facility (DWPF lab) analyzes these samples for various elemental concentrations as well as density, total solids, and calcined solids. The data from these composition measurements for batches 19 through 93, which were reported by the DWPF laboratory, are the subject of this report; specifically, this will include SRAT Receipt, SRAT Product, SME, and MFT results.

A statistical review of these reported, analytical data has been conducted with the objectives:

- 1. Perform a general review of the data in an attempt to identify outliers or anomalies.
- 2. Explore for possible trends in mean level or variation for each vessel over the available sample history.
- 3. Identify possible differences in SME versus MFT sample results.
- 4. Investigate the components of variation (batch-to-batch versus sample-to-sample) for each vessel.

2.0 BACKGROUND

The elemental concentrations of samples from the SRAT, SME, and MFT are measured by analytical procedures conducted by the DWPF laboratory (DWPF lab). The SME and MFT concentrations are measured on a vitrified basis; that is, the results provided by the DWPF lab are in terms of grams of element per 100 grams of vitrified material. Analyses of the SRAT material (both receipt and product) are reported as percentages of total dried solids; that is, the results are provided in grams of element per 100 grams of total solids. For all three vessels, the anions of interest are reported in parts per million (ppm).

Table 1 in the Appendix provides a listing of the results by vessel, batch, and sample for MB1. The unit of measure for each column of results is identified. Note that values are not provided for all analytes for all samples, for all batches, or for all vessels. However, the set of data in Table 1 is the starting place for this study, and this table represents all of the data considered in this report. Also, note that a value which was below the detection limit of the analytical method being used (indicated by a "<" in Table 1) was set to the detection limit in the analyses of this report.

SME acceptability decisions conducted as part of the Product Composition Control System (PCCS) require measurements on at least 4 SME samples [1]. DWPF routinely acquires 4 or more samples of the SME as part of the acceptability process but frequently enters results from only 4 samples into PCCS. The results from these 4 samples then become part of the production record for the SME batch. However, Table 1 provides results from all of the available samples even results from samples that were subsequently renanalyzed or from SME batches that were subsequently remedied and re-sampled. In the discussion that follows, all of the data provided in Table 1 are reviewed regardless of whether or not they were used in the SME acceptability decision.

Another complexity, that must be addressed in the discussion that follows, involves DWPF's use of two dissolution methods (mixed acid microwave, MA, and peroxide fusion, PF) to conduct the analyses for all

Also, note that the detection limit for a particular type of measurement varies over these MB1 process batches.

of the required cations. In general, concentrations for all relevant cations except for boron are available by the MA method and all except for sodium by the PF method. However, all of these data (even though available for each SME sample) are not entered into PCCS for acceptability decisions, and for the earlier SME batches of MB1, all of these data were not saved in the files accessed to compile the measurements being studied here.

During the processing of MB1, and even today, the concentrations for the eations of calcium (Ca), chromium (Cr), copper (Cu), iron (Fe), potassium (K), lithium (Li), magnesium (Mg), manganese (Mn), sodium (Na), nickel (Ni), titanium (Ti), uranium (U), zirconium (Zr) that are entered into PCCS as those determined using the MA method. The boron (B) concentrations are those derived via PF. Early during MB1, the aluminum (Al) measurements entered into PCCS were those determined using MA. As of process batch 46, the Al values determined using PF have been entered into PCCS. Also, as of that SME batch, the average of the PF and MA measurements for silicon (Si) for each sample has been entered into PCCS. For earlier SME batches, only the MA value for each sample was entered for Si.

Note that the "Sample" column of Table 1 indicates the dissolution method (along with the sample number) for the SME samples beginning with batch 44 and for the MFT samples beginning with batch 39. For the earlier samples from these tanks (where no dissolution method is indicated in Table 1), the dissolution method used to acquire the reported cation measurement is assumed to be as follows: the MA method for Al, Ca, Cr, Cu, Fe, K, Li, Mg, Mn, Na, Ni, Si, Ti, U, and Zr; and the PF method for B. In the discussion that follows, comparisons are made between the results from these two dissolution/preparation methods for the SME and MFT.

An earlier report [2] provided an analysis of batches 19 through 30 of MB1. An observation discussed in that report concerned the results for batches 19, 20, and 21 versus the remaining batches of that study. For some analytes, these earlier results differed from the latter results due to the composition of the initial heels of the four vessels being different from the actual waste composition received from the tank farm. These initial heel compositions were of the simulated slurry used during the Waste Qualification Runs prior to the beginning of radioactive operations. Some short-lived trends over the initial batches were seen as a consequence of the impact of these heels [2]. Accordingly, the MB1 analyses presented in this current report do not include batches 19 through 21. For a complete discussion of the results from batches 19 through 21, see reference [2].

3.0 DISCUSSION

In this section, the various statistical analyses conducted for these data are discussed. JMP[®] Version 3.2.2, a statistical software package from SAS Institute, Inc., was used to generate these statistical analyses [3].

3.1 INITIAL REVIEW OF DATA

A preliminary step in conducting any statistical analyses for a set of data is the investigation for possible outliers in the data. The investigation for outliers in Table 1 will be an on-going effort throughout this report. Summary statistics, including histograms, were prepared for the data from batches 22 through 93 to begin this process. These results are presented in Exhibits 1-4 in the Appendix. An additional overview of these data is provided by Exhibit 5 in the Appendix. In this exhibit, a chart is displayed for each analyte. This chart provides a look at the sample measurements for each batch for each of the four vessels considered in this study.

A review of these exhibits reveals several observations, including:

- the values of total solids and calcined solids for a few batches are lower than the values of these measurements for the other batches for each of the four vessels,
- one density value appears to stand out (higher than the others) for the SRAT Receipt and Product vessels.

- no values for MFT batch 54.
- several negative values for the potassium cation concentration measurements for the SRAT Product, SME, and MFT.

3.2 STATISTICAL CONTROL CHARTS

The next step in reviewing the measurements of Table 1 for possible outliers or anomalies takes the form of statistical control charts. Such charts utilize statistical principles and process knowledge to provide graphical records of a process. These graphics allow for visualization of the variation, trends, or other patterns in the process over time, or for these data, over the batches comprising MB1. Each control chart includes a line indicating the central tendency of the process statistic (either mean or moving range) for the measurement and upper and lower control limits that should bound a large portion (~ 99%) of the values of the process statistic if the process is statistically stable and the distribution of the measurement is approximately normal.

For these data, the control charts for each analyte of each vessel are constructed as follows.²

- the measurements of the analyte are averaged for each batch,
- a moving range chart looking at each sequential pair of batch averages for the analyte is developed,
 and
- an individuals chart (for the batch averages) is prepared for each analyte.

The exhibits providing these charts can be found in the Appendix. Exhibit 6 provides these charts for the SRAT Receipt analytes and Exhibit 7 the SRAT Product. Exhibit 8a gives the control charts for the SME anions; Exhibit 8b the SME cations determined using the MA dissolution method; and Exhibit 8c the SME cations determined using the PF method. Exhibits 9a, 9b, and 9c provide the anions, cations by MA, and cations by PF, respectively, for the MFT.

A review of these charts provides an opportunity for insights into the processing of MB1. It is expected that the impact of some decisions made during the processing of MB1 is directly visible in the behavior of the relevant measurements. This tempers the concern for some of the behavior demonstrated in these charts. There are some situations indicated in these charts where values fall outside the control limits for the moving range chart, the individuals charts, or both. In addition to these indicators, there are several other ways for detecting out-of-control situations on a control chart. These other techniques are not fully employed in this review, and the following table is provided in an attempt to highlight some situations of interest for the individuals charts by giving the batch number where they occur.

These charts were prepared using JMP®. See [1] for details concerning the preparation of both the moving range and individuals charts.

Analyte	SRAT Receipt	SRAT Product	SME	MFT
Total Solids	92 and 93	92 and 93	32, 60 (1 st), and 61	45, 61, and 93
Calcined	93	62, 92, and 93	32, 60 (1 st), 61, and 93	
Solids				
Insoluble				
Solids				
Density			23 and 27	22, 32, 33, 40, and
				60
Total	93			
Hydroxide				
Format	56 and 66	22, 81, 85, and 88-91	52	52
Chloride		26	38 (1 st)	52
Fluoride		26	38 (1 st)	48, 49 (higher limits)
Nitrate	22, 23, 26, and 34	23, 24, 36, and 57	22, 20, 92, and 93	24, 45
Nitrite	34 and 93	31 and 36	38 (1 st)	
Phosphate		76 and 92	38 (1 st), 78, 81, 91, 93 (1 st)	
Sulfate		48	38 (1 st)	42
Aluminum		89, 92, and 93	MA and PF: 60 (1 st)	MA: 55; PF: 55
Boron				PF: 90
Calcium		89, 92, and 93		MA: 77
Chromium	34	92 and 93	MA: 57, 57; PF: 85, 86	MA: 30: PF: 84-86
Copper	34	Major shift at 37/38	MA: shift at 37/38; PF: 87,	MA: shift at 37/38;
**		_	92	PF: 39,40,64
Iron		92 and 93	MA and PF: 60 (1st)	MA and PF: 55
Potassium	22	71 and 72	MA: 60 (1 st); PF: 79	MA: 25, 93; PF: 4,
				72
Lithium				MA: 26: FP: 42, 86
Magnesium		29, 89, and 93	MA: 35	MA: 82; PF: 75, 86
Manganese		92 and 93	MA and PF: 60 (1")	MA and PF: 55
Sodium		29, 76, 92, and 93	MA: 92 and 93	MA: 93
Nickel		92 and 93	Ma: 55 and 57	MA: 30, 72; PF: 44,
				72
Silicon	22	35, 36, 45, and 72	MA: 60 (1 st); PF: 90	MA: 26; PF: 42
Titanium	30	24, 60, 71, and 72	MA: 22, 87; PF: 85, 87	MA: 40, 68, 70, 77;
				PF: 44, 72
Uranium		92 and 93		MA: 65
Zirconium	24	23, 24, and 44	MA: 49 and 59	MA: 59, 68 (outlier)
TIC	22, 25, 42, and			
	70			
Mercury				
TOC	ļ		22	
Fe/Li			MA and PF: 60 (1 st)	MA and PF: 55
Fe/Al		89	MA: 36, 93; PF: 92	MA: 76, 82; PF: 93

In preparing Exhibits 6 through 9c, the results from each sample set (for batches with multiple sample sets) were kept separate and are displayed as part of these charts. Also, results from each of the two dissolution methods (MA and PF) are presented where available for the SME and MFT

3.3 DIFFERENCES BETWEEN DISSOLUTION METHODS

The data from MB1 provide an opportunity to conduct comparisons between the two different dissolution methods used by the DWPF lab: mixed acid (MA) and peroxide fusion (PF). Exhibit 10 in the Appendix provides paired (by processing batch for the SME, for the MFT, and for the two vessels combined) comparisons between the cation concentration measurements for the two methods. The averages of the sample measurements for each batch at each vessel are the basis for these comparisons.

The following analytes show a statistically significant difference between the two dissolution methods over the SME and MFT (at the 5% significance level):

Aluminum (wt%)	MA value > PF value	(Mean difference = 0.02 wt%; 0.8% of SME PF value)
Calcium (wt%)	MA value > PF value	(Mean difference = 0.07 wt%; 8.0% of SME MA value)
Chromium (wt%)	MA value < PF value	(Mean difference = -0.006 wt%; 8.7% of SME MA value)
Copper (wt%)	MA value < PF value	(Mean difference = -0.001 wt%; 1.4% of SME MA value)
Iron (wt%)	MA value > PF value	(Mean difference = 0.14 wt%; 1.7% of SME MA value)
Potassium (wt%)	MA value > PF value	(Mean difference = 0.02 wt%; .15.4% of SME MA value)
Lithium (wt%)	MA value > PF value	(Mean difference = 0.04 wt%; 2.4% of SME MA value)
Magnesium (wt%)	MA value > PF value	(Mean difference = 0.03 wt%; 2.4% of SME MA value)
Manganese (wt%)	MA value > PF value	(Mean difference = 0.02 wt%; 2.4% of SME MA value)
Nickel (wt%)	MA value > PF value	(Mean difference = 0.002 wt%; 2.0% of SME MA value)
Silicon (wt%)	MA value < PF value	(Mean difference = -1.70 wt%, 7.4% of SME MA value)
Fe/Al	MA value > PF value	(Mean difference = 0.03; 0.9% of the SME MA/PF value)

Thus, statistically significant differences are seen between the two dissolution methods in the results for several analytes. However, for all of the major cations (except for silicon) the differences are less than 5%. For silicon, the MA values tend to be biased low while the PF values tend to be biased high. The average of the MA and PF values is used to represent this cation concentration in PCCS, which mitigates the differences in Si measurements derived by the two dissolution methods.

3.4 DIFFERENCES BETWEEN SME AND MFT BY DISSOLUTION METHOD

Comparisons between the SME and MFT vessels are of primary interest, and several approaches are available to conduct these comparisons. Exhibit 11 in the Appendix provides paired (by processing batch) comparisons between the anion concentration measurements for the two tanks. The averages of the sample measurements for each method for each batch at each vessel are the basis for these comparisons

The following analytes show a statistically significant difference between the SME and MFT (at the 5% significance level):

Total Solids (wt%)	SME value > MFT value	(Mean difference = 2.32 wt%)
Calcined Solids (wt%)	SME value > MFT value	(Mean difference = 2.33 wt%)
Insoluble Solids (wt%)	SME value > MFT value	(Mean difference = 2.54 wt%)
Density (g/mL)	SME value > MFT value	(Mean difference = 0.02 g/mL)

A higher Total Solids in the SME versus the MFT is not unexpected since the MFT is not sampled immediately following the transfer from the SME but is sampled somewhat later, potentially, after the melter feed pumps have been primed with water.

The next set of comparisons between these two tanks again focuses (in turn) on the two dissolution methods. Exhibit 12 in the Appendix provides comparisons between cation measurements for the SME and MFT derived using the MA method and comparisons between cation measurements for the SME and MFT derived using the PF method. The averages of the sample measurements by the MA for each batch at each vessel are the basis for the first set of comparisons and the averages of the sample measurements by the PF method for each batch at each vessel are the basis for the second set.

No cations (by either dissolution method) show a statistically significant difference between the SME and MFT (at the 5% significance level) including the ratios of Fe/Li and Fe/Al. In the earlier study [2], there was an indication of concern for differences in the aluminum, iron, and copper concentrations between the

two tanks. This complete MB1 study shows no indication of differences between the two tanks for these cations.

3.5 SOURCES OF VARIATION BY VESSEL

The set of measurements on each analyte for each batch at each vessel provides an opportunity to explore the sources of variation in these values. For some of the analytes of the SME and MFT, there is also an opportunity to look at these sources of variations for each of the two dissolution methods. Specifically, for each analyte, dissolution method, and vessel, a random effects model such as the following can be fit to the available data:

$$y_{ij} = \mu + a_i + e_{j[i]} \tag{1}$$

where

i=1, 2, ..., n, (the batch index, corresponding to batches 22, 20,, 93),

j=1, 2, ..., m (the sample index, corresponding to sample 1, 2, 3, ...),

 y_{ij} is the jth measurement for the given analyte/vessel/dissolution method at batch i,

- is the true average analyte concentration value for the given vessel (by the given dissolution method, if appropriate) over these batches of MB1,
- a; is the random effect for batch i (this includes batch-to-batch differences as well as effects due to longer-term differences in the analytical procedures such as instrument calibrations), and
- $e_{j[i]}$ is the residual random effect (due to sample-to-sample and analytical/measurement errors) attributable to the i^{th} sample for batch i.

For this model, each term present (except for μ) is considered as a random variable (i.e., both batch and residual effects are considered as random effects) with a zero mean and a constant variance. These random variables are assumed to be independent, and each is assumed to follow a normal probability distribution. Let σ_b^2 and σ^2 denote the variances due to batch and residual variation, respectively. The objective of this analysis is to estimate each of these variances: a measure of the variability from each of the identified sources. This will also lead to an understanding of the errors associated with estimating μ

Model (1) was fit in turn to the SRAT Receipt, SRAT Product, SME, and MFT sample results for batches 22 through 93. For the SME and MFT, the cation measurements for both the MA and PF dissolution methods are considered separately. The results from these analyses are provided in Exhibits 13 through 20 in the Appendix. Information from these exhibits has been summarized in Tables 2 through 5 of the Appendix.³

The columns of these tables that are of primary interest are those showing the components of variation as percentages (batch versus residual) and those showing the percent coefficients of variation for the total, batch, and residual variations. The relative contributions of batch-to-batch versus residual, which includes analytical, are presented in these tables as well. For most of the analytes for each of the four vessels, the batch-to-batch variation is larger than the residual (or within-batch) variation. A feel for the consistency of MB1 at each vessel is provided for each analyte by the percent coefficient of variation for this batch-to-

Note that some analytes were below the detection limit of their analytical procedures and that in some instances the detection limits for some analytes (e.g., chloride, fluoride, and sulfate) were the same. Also, for some analytes there were not enough data to conduct some of the statistical procedures

batch variability for the analyte, which expresses the variation in the measurements for this analyte as the standard deviation divided by the average.

3.6 COMPARISONS BETWEEN THE VARIABILITIES OF THESE DATA AND THOSE USED IN PCCS

Table 6 in the Appendix provides an opportunity for comparisons between the SME variabilities demonstrated in batches 22 through 93 and the variabilities currently being used in PCCS [1]. The current version of PCCS computes the standard deviation of the measurement error for each constraint two ways, both use the historical relative standard deviations (RSD's). These RSD's are multiplied by the historical means of the elemental concentrations to compute one standard deviation, and they are multiplied by the average concentrations of the current samples to compute the other. The larger of the two is used by PCCS to determine the appropriate Measurement Acceptable Region.

In Table 6, the two approaches used in PCCS are applied only to the extent of computing standard deviations for the sample elemental concentrations. These values appear as the last two columns in the table.

How should the columns of this table be compared? The (historical) sample-to-sample standard deviations used in PCCS were based on prototypic studies, which involved samples taken at the same time being analyzed under different instrument calibrations. For the SME, the samples from each batch were usually analyzed under one instrument calibration. Thus, for the SME results, contributions are made to the between-batch variability from instrument calibrations, and thus are included in the "Batch" columns of Table 6. The "Residual" columns of the table are pooled estimates of variation that includes sampling methodology and equipment and analytical procedures. Thus, it would not be too surprising if the historical standard deviations are somewhat larger than the "Residual" portion of the SME results

No anomalies are seen in the data of Table 6, and these standard deviations (SME "Residual" versus PCCS in Table 6) can be compared statistically using information from Table 6 and Exhibits 13 through 20. The value (21) for the degrees of freedom associated with each of the PCCS standard deviations is available from [1]. The hypothesis of equality between these two standard deviations for each cation relies on the following test statistic (assuming normality for the underlying distributions)

$$F = \frac{Max(SME "Residual", PCCS)}{Min(SME "Residual", PCCS)}.$$

The hypothesis is rejected (at a 5% significance level) if $F > F_{0.025,n_1,n_2}$ where n_1 is the degrees of freedom associated with the numerator of F and n_2 is the degrees of freedom associated with the denominator. The value for the degrees of freedom of the estimate of the SME "Residual" standard deviation is available from the appropriate exhibit in the Appendix. Using this approach, the following conclusions can be drawn regarding potential differences in the SME "Residual" and PCCS variabilities:

The historical correlations among the analyte measurements are also considered in these variance calculations of PCCS. They are not considered in this report, however

	Dissolution			Dissolution	
Cation	Method	Conclusion	Cation	Method	Conclusion
Aluminum (wt%)	PF	Not Significant at 5%	Magnesium (wt%)	PF	Not Significant at 5%
	MA	Not Significant at 5%		MA	Not Significant at 5%
Boron (wt%)	PF	Not Significant at 5%	Manganese (wt%)	PF	PCCS > MB1
	MA	Not Available		MA	PCCS > MB1
Calcium (wt%)	PF	Not Significant at 5%	Sodium (wt%)	PF	Not Available
,	MA	Not Significant at 5%		MA	Not Significant at 5%
Chromium (wt%)	PF	PCCS > MB1	Nickel (wt%)	PF	PCCS > MB1
	MA	Not Significant at 5%		MA	PCCS > MB1
Copper (wt%)	PF	PCCS > MB1	Silicon (wt%)	PF	Not Significant at 5%
	MA	PCCS > MB1		MA	Not Significant at 5%
Iron (wt%)	ΡF	Not Significant at 5%	Titanium (wt%)	PF	PCCS > MB1
	MA	Not Significant at 5%		MA	MB1 > PCCS
Potassium (wt%)	PF	PCCS > MB1	Uranium (wt%)	PF	Not Available
	MA	PCCS > MB1		MΛ	Not Available
Lithiumn (wt%)	PF	Not Significant at 5%	Zirconium (wt%)	PF	Not Available
	MA	Not Significant at 5%		MA	Not Significant at 5%

The conclusion "SME > PCCS" for titanium (MA) indicates the only analyte for which the variability in the SME "Residual" is statistically (at a 95% confidence level) larger than that of PCCS, and this conclusion is supported for only one dissolution method. The other dissolution method indicates that the variability in the PCCS is larger than that of MB1. Therefore, no problems of practical concern are seen in the results presented in Table 6.

4.0 CONCLUSIONS

The measurements derived from samples taken during the processing of DWPF's MB1 have been reviewed and compared in this report. Batch 22 through 93 were the focal point of this study; the earliest batches of MB1, which were heavily influenced by the heels remaining after the qualification runs and which were studied in [2], were not investigated in this report.

Statistical control charts were developed for each analyte for each vessel to identify influential or exceptional results in the variation, central tendency, or both for the measurements. These charts should serve as a basis for observing the (expected) impact of some decisions made during the processing of this macro-batch.

Statistical comparisons were made between the two dissolution methods (MA and PF), where both were utilized. Statistically significant differences (at the 5% significance level) are seen in the results for several analytes from the two dissolution methods. However, for all of the major cations (except for silicon) the differences are less than 5%. For silicon, the MA values tend to be biased low while the PF values tend to be biased high. The average of the MA and PF values is used to represent this cation concentration in PCCS, which mitigates the differences in Si measurements derived by the two dissolution methods.

A comparison of the results for the SME versus those of the MFT, shows a statistically significant difference (at the 5% level) for Total and Calcined Solids (SME value > MFT value for each with a Mean Difference = 2.3 wt%), for Insoluble Solids (SME value > MFT value with a Mean Difference = 2.5 wt%), and for density (SME value > MFT value with a Mean Difference = 0.02 g/mL). A higher Total Solids in the SME versus the MFT is not unexpected since the MFT is not sampled immediately following the transfer from the SME but is sampled somewhat later, potentially, after the melter feed pumps have been primed with water.

No cation concentrations (by either dissolution method) show a statistically significant difference between the SME and MFT (at the 5% significance level) including the ratios of Fe/Li and Fe/Ai. In an earlier study [2], there was an indication of concern for differences in the aluminum, iron and copper concentrations between the two tanks. The analyses of this study show no indication of such differences between the two tanks for these cations over the complete set of results for MB1.

REFERENCES:

- [1] Brown, K. G. and R. L. Postles, "SME Acceptability Determination For DWPF Process Control (U)," WSRC-TR-95-0364, Rev. 3, February 21, 1996.
- [2] Edwards, T. B., "Statistical Review of Data from DWPF's Process Samples for Batches 19 Through 30 (LI)," WSRC-RP-97-207, Revision 0, March 18, 1997
- [3] SAS Institute, JMP[®]: Statistics and Graphics Guide, Version 3.0, SAS Institute, Inc., Cary, NC, 1994.

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Appendix:

Tables and Exhibits

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Table 1: Sample Results for DWPF's Macro-Batch 1

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Table 1: Sample Results for DWPF's Macro-Batch 1

		Sank_Batch Sample	Solids (*t%)	(6) Solids R1 (w(%)	(g/m.) IIy	droxide [(cq/L)	(ppm) (ppm)	(ppm) (ppm)	Nitric Phosp (ppn) (ppr	hate; Sulfate - Afur n) (ppm) (v	minum Boton Calci	um Chreatium 5) (wff)	Cupper: Irin (*15) j (*16)	Potasslum J (#1%) (tlium Magnesium	Manganew Sodi (wl 7-) (wt	wn Nickel Si) 9-) (wt?e) (w	lcon : "Haniom L (4) : (41%)	Iraniam Zircoaian (*CS) (*CS)	(mdd) (mdd).	Mercuri d) (ppm)
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		eccipi-77	16.82	2.5	1.657		5250	12300		2											917
		ecci14-78	16.96		1.034	0.169	3610	13400		2012				-		-				< 482	<u>.</u>
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Table 1: Sample Results for DWPF's Macro-Batch 1

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Table 1: Sample Results for DWPF's Macro-Batch 1

Table 1: Sample Results for DWPF's Macro-Batch 1

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			Î			0 0 0	0.011	0.012	Ē.		100	100	<u> </u>		0.012	100	0 0 0	0.013	0.012	100	\$100	1 S	0.115 1.125	0.015	0.1024 0.1023	6,4126	0.021	900	0.1M2	11.12.4 0.04.1	0,019 11.114.	0.016	0.015	0.021	9000	1 2	100	# H	0.017	100	ΞΞ	0.014 0.013	0.019 0.012 0.013	
		0.642	0.595	790	57.6	0.59	0.616	5990	90	0.726	19'0	0.595	6 62 5	66970	0.X17 0.891	0.744	0.763	0.572	6690	74.3	0.697	0.616	0.596 0.514	0.658	0.682	0.782	0.637	0.626 0.658	0.649	0.653	0.662	0.673	0.7FR	0.719	0.871	0.619	9.48	0.52	# 766 # 717	0,64JR	287.0	0.772	0.211 0.568 0.571 0.551	
Nickel : 5		27.5	7,00	997 0	0.243	0.369	0.261	1,264	0.254	27.4	\$ 3X	6.28 6.28	0.274 0.28	1 289	0.281	0.287	0.297	0.251	0.266	0.267	0 264	0.267	0.28 0.275	0.268	0.283	0.291.	0.268	0.283	0.26K	0.252	0.254	0.277	0.264	0.283	0.275	0.296 0.296	0.259	392	0.261	0.274 0.283	0.2X6 0.275	0.363	0.249 0.257 0.262 0.257	1.77
Sodium N) (318)				5.645	7	7.19	6.69%	7.291				35.5	1							6.832	2 6	6.79	I.		6 15°	- 1		8.25		8.43	7.26°	7.837 8.408	8 JR	71.7	6.725 x 23	744	- 17 - 17 - 17	,	2.07	6 X 46	6.842	× 57 × 39 × 19 × 30	ē
Samean		27.14	2.568	57.7	7.5	2-173	2.315	2, 199	2.378	377	26.55	2.628	2605	2 6497	2.505	2.565	2.65	2.333	2.473	7 7 7	2.488	2.548 2.484	2.556	2.5.5	2.582	2.597	2.449	2.38R	2.423	2.381	2.38	2.492	2.412	2.541	2.538	2 64X	2,488	2.523	2.499	2.566	2.616	2.536	2,437 2,437 2,43 2,43	
guestum: [1]	() () ()	85 G C	1.172	979.0	10.01	0.976	0.942	0.941 0.843	1.02	0,873, 0,873, 0,873,	6880	956.0	0.945	0.854	0.886	68.4	0.875	976.0 1.019	0.825	0.764	1.021	1.03	(00)	6.97.5	966.0	0.986	0.887	1.103	1946	0.994	1.038	5.84 c	1.053	0.98K	0.902	0.857	900		0.79 0.874	0.923	X160	1.053	1 081 1 1,012 1,012	
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i i	(M15)	24 87]	24.24	23.617	23.682	21.86	23.136 22.48	23.138	22.32	23.45	25.55	25.616	25.425 25.425	25.925	24.789	2.5	26.5l3	22.0Kg 23.539	23.195	21.818	23.391	23.96	24.25	24.051	24 #2	24.77	23.069	24.055 22.479	22.981	22. ILS 21.578	22.04	24.158	22.884	22 942	24 477	25 694	22.927	23.73	2423 22 W2	24.25 25.28	25.128 25.342	24.686	2223 22.714 22.941 22.889	
addo	(3)	0.023		0.022	0.021	0.02	0.021	0.022	0.021	20.2	0.025	0.025	0.025	0.024	0.024		0.026	0.022 22.089 0.023 23.59	0.023	0.022 21.818			0.022	0.022	0.024	0.024	0.023	0.024		0.022	0.022	0.022	0.023	0.026	0.023		0.021		0.02		0.024		0.021	
- E	(#E)	2 2	<u> </u>	1.158	1147	9 =	ž <u>2</u>	1.158 1.08	1153	3.3	92	<u> </u>	1.176	72.	1172	2 2	1179	87 C	X15x	1153	1.57	1.59	29 T	0.10	5.165	59 Z	1157	<u> </u>	2.156	1148	1153	5 7 5 7 7	0.157 0.15	3,205	. 168	ž 2	\$51.0	9 0	1.157	2 2	0.0	0.204	0.156 0.159 0.159	
	(r)	1981	2. 2.	2.046	1.897	2.058	2.016	566	= T	1.95x	2.047	2.045	2.141	1.No	1.87	1.895	1.X67	2.03	1904	16.2	2 101	2.116	2.051	2.054	2 122	2 H37	1.894	2325	2.192	2.138	2.227	2.123	2.171	2.221	2051	2.2	2,093	= 1	1.93	2.012	2.005	2.001:	2.125	
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	(add)	o Inc		576>	< 11Kg.	96112		< 945	A 1170		< 1120	486	, .	< 1080	0.05	< 1046		0,000 v 0,000 v	× 1020 × 1040		< 1080	. O	<u>.</u>		2 (S)	2 T V		0 0 V			< 1050 < 1060	× 1000 ×		< 1210	< 1170 × 11411		> 1080 - 1080	v 1070		< 1070	< 1220 < 1190	< 1210	< 1070 < 985 < 1220 < 1160	
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Juride	fuld			×9785) (1) (2) (3)	95		< 170	0.00 >	,	0.120	5	ž v	080 >	Ī	, (140)		9 6 V	200		× 080	E	<u> </u>	9	=	2 E			\$ \$ \$ \$ \$,	0.00	2 E		< 210 < 200	2 2		0.00	2.	Š.	< .070	25 ×	< 210	< 985 < 220 < 160	
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oluble	(%)			†				ľ													l			1	; •									15.81	2 2								13.58	
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Total ((#1%)	22.9		21.77	21.74	21.84		22.95	22.94		22.19	22.14	7 77	51.03	21.05	21.12	1	18.91	1X 72		24.16	23.95	74.62	- 12	21.75	21.72		22.86	22.92		24.03	27.93		22.57	22.64		7.7	23.65	777	23.02	23.04	22.67	25.13 25.09 25.08 25.08	
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Table 1: Sample Results for DWPF's Macro-Batch 1

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unhum (i		2657 2745 2683	2.616 2.695	2639 2636 2525 2515 2665	2.675 2.765 2.564 2.634 2.649	2.799 2.86 2.911 2.712 2.775	2.825 2.885 2.683 2.701 2.808 2.784	2.192 2.461 2.585 2.568 2.659	2.648 2.614 2.71 2.704 2.82 2.82	2,703 2,68 2,629 2,544 2,723 2,723	2.7.2 2.83 2.813 2.813	27.2 127.2 27.06 12.7.05	2.878 2.878 2.912 3.071 2.852 2.931	2.75K 2.75Z 2.75X 2.754 2.754 2.754	2,785 2,809 2,664 2,662 2,672	2.58r 2.512 2.65 2.65 2.521	
minnar Ura	0.016	91018 91018 1248	0.021	0.017 0.018 0.014	200 200 200 200 200 7100	0.027 0.015 0.019 0.039	0.015 0.027 0.018 0.018	0.086 0.087 0.027 0.028	0.037 0.017 0.034 0.038	0.053 0.071 0.047 0.014 0.014	0015 0014 0013 0013	0.012 0.012 0.012	0.05 0.05 0.026 0.018 0.018	0.027 0.027 0.027 0.022 0.02	0.014 0.013 0.012 0.013	0.015 0.012 0.013 0.013	
Silicon Tila	9.5	1	l	1,648 1,663 1,578 0,63	l	0.671 0.708 0.616 0.615	0.837 0.765 0.771 0.823	1,427 1,446 1,71 1,417 1,378	0.82 0.679 0.774 0.714 0.714	U.686 0.687 0.526 0.704 0.637	0.76 0.58 0.954 0.462	0.812 0.615 0.615	0.707 0.707 0.758 0.758 0.712	0.694 0.691 0.71 0.696 0.691	0.694 0.647 0.618 0.635	0.982 1.012 0.909 1.023	
Nickel Sil		1			0.273 0.273 0.255 0.255	0.287 0.286 0.286 0.288	0.28 0.287 0.267 0.266 0.281	0.243 0.25 0.265 0.256 0.284	0.263 0.269 0.269 0.273 0.276	0.283 0.265 0.259 0.269 0.269	0.279 0.281 0.281 0.278	0.277 0.273 0.27 0.27	0.505 0.292 0.297 0.286 0.292	0.277 0.281 0.281 0.275 0.282	0.291 0.283 0.271 0.276 0.274	0.262 0.255 0.274 0.26	
Sadium N					8 1868 6,698 7,05 5,792 7,223		6.78 7.56 7.3 6.72 6.72 6.73	X X X X X X X X X X X X X X X X X X X	7.715 7.66 7.55 7.02 7.02	8.427 8.427 8.427 7.66 7.403	; I			l	i	[1.1
anganese S	V: 8	2.438 2.478 2.478	2,42,4	2.467 2.447 2.369 2.353 7.47	2.49 2.543 2.364 2.388 2.388	2,608 2,65 2,703 2,525 2,582	2.643 2.667 2.518 2.524 2.621 2.604	2.268 2.313 2.424 2.424 2.434 2.492	2.44 2.42 2.489 2.478 2.58	2.527 2.51 2.461 2.357 2.537 2.537	2.548 2.652 2.646 2.582	2.534 2.477 2.469 2.517,	2 662 2 704 2 721 2 588 2 588 2 662	2.585	2 582 2 562 2 415 2 437 2 441	2.48 2.334 2.461 2.352	
×		992 900 900 900 900	197	15 55 55 1 15 1	0.966 0.923 0.924 0.809	1912 1937 1989 1989	7.996 1.046 1.023 1.995 1.996	1008 1058 1035 1075	1.02 0.99 0.991 1.013 0.947	1.152 1.132 1.142 1.079	0.988 0.988 0.985 0.992	0.895 0.892 0.994	0.808 0.888 0.53 0.544 0.742	0.956 0.938 0.878 0.869 0.969	0.943 0.828 0.945	0.983 0.986 0.935 1.057	
Magnesium (wf%)									,								
(Lithum	0.0	a	> 3	+ 0, 85, 47 €	g' &' &' a' a' a'	হয় এন ধ	5,5,5,5,5	<u> </u>	2255**	\$_6'5'5'5'E'*	2 4 4 2	≈ 3 ° ≥	7 <u>4 5 8 8 5</u>	\$ \$ \$ \$ \$ B B	25 5 5 5 8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	इंडिक	.
ufussjon (*1%)	0.0	10 m 0 m	0.03	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	100000	0.03 0.036 0.036 0.036	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			0.054 0.067 0.065 0.067 0.088							
Frot 1.	23.6.1	24.13	23.22	21.138 22.97 22.308 22.052 23.734	23.636 24.415 22.515 22.514 23.514	24.994 25.313 25.911 24.666	25.08 25.85 23.76 23.99 24.89	21.21 21.697 22.83 22.55 23.408	23.088 23.792 23.792 23.705 24.751 24.79	0.023 23.556 0.023 23.36 0.023 23.36 0.055 22.85 0.023 23.58 0.023 24.63	2404 2499 24.73 24.19	23.67	2593 4 26.05 5 26.93 5 26.47 5 26.47 5 25.68	24.54 24.79 5.24.79 5.24.16 5.24.38 5.24.33	7 24.59 5 24.14 5 22.17 6 23.81 4 22.82	3 22 196 5 22 132 4 23 134 2 22 161	
Capper	0.022	l	- 1	0.022	t	l	0.024 0.025 0.024 0.024				•	1		5 0.025 5 0.025 7 0.026 2 0.025 6 0.026	2 0.025 9 0.025 1 0.025 2 0.026 5 0.024	8 0.02 3 0.02 1 0.02 2 0.02	
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alchum (2.1KJ 2.241	21.22.23	2.073 2.073 2.11	2.153 2.145 2.227 2.141 2.141	2319 2319 1917 181	2.026 2.026 1.979 2.114 2.163	2.098 2.107 2.131 2.095 2.083 2.083	2.067 2.186 2.089	2.172 2.142 2.151 2.165 2.103 2.103	2.206 2.233 2.263 2.28 2.184 2.155	1.936 2.074 2.085 2.095	1.905	1.862 1.914 1.914 1.626 1.626 1.734	2.02 2.02 2.022 1.94 2.036 1.994	2.035 1.911 1.828 1.988 2.031	1.987 2.019 1.98 2.144	
Barin C															- 1-1-2-2-1-3		
Aluminum (*15)	6.262	5.592 6.292 6.292	6.16	6.231 6.157 5.993 5.897 6.196	6.156 6.579 6.047 6.049	6.0652 6.769 6.395 6.395	6.748 0.816 6.4 6.415 0.695 6.65	5.863 5.776 6.088 6.056 6.303	6.194 6.194 6.348 6.348 6.69	6.319 6.324 5.976 6.416	6.457 6.709 6.715 6.557	6.428 5.829 6.428 6.427	57.12 7.123 7.124 8.738 6.009	6.568 6.548 6.335 6.548 6.548	6.687 6.546 5.945 6.247 6.333	5.17 5.93 5.43 5.43	
Sufface Al		5.6.8		091 V 091 V 091 V	0801 8/6 0 0 0 7	1 8 8 B	180 E 180 E	020 1 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1630 1630 1630	* * * * * * * * * * * * * * * * * * *	92 53 8 180 45	<u>8 2 8 8</u>	8,3,3,6,	2227	98.1 98.1 98.0 198.0	2988	8 8
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Noride (}	8,8,5	2	10601070107010801060	< 874 < 927 < 976 < 976	0 1 1 0 0 0	966 V 966 V 1086 V	< 1984 < 972 < 931 < 1020	< 944 < 976 < 982 < 896	25.125 0 1250 0 1250 0 1250	2 0 0 0 0 0 0 0 0 0 0 0	× 120 × 210 × 200 × br>200 × 200 × 200 × 200 × 200 × 200 × 200 × 200 × 200 × 200 × 200	< 822 < 739 < 7010 < 1010	< 9.89 < 9.89 < 1070	8 8 8 8 V V V V	\$771 \$1030 \$908 \$988	< 858 < 849
ormate. C	 }	23900 23900 23900	7. P. I.	23000 22000 22000 21600	23100 23500 22500 22500	2360 2360 2260 21900	22800 2400 2700 2200 2200	21900 21900 21900 21500	22400 23600 22100 22200	20000 20000 20000	20918 20018 2.700 1.800	2 200 2 200 2 200 2 200	20230 2330 2330 2 400 2 400	24800 26700 27300 26800	2,000 2,000 2,100 2,0700	18000 18100 18400 21900	11200
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Insoluble De Solids	(8)	<u> </u>			4 5 4 5 7 4 6 9	16.04 16.47 15.67 15.58	14.51 14.43 14.17	12.74 12.09 12.63 18.39	14.97 14.87 14.91		12.22 12.16 15.51 12.73						
Cateined Insu- Solids So	ځ 9	2 & & C	, K	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	2,71 2,71 8,71	2 6 8 8 2 6 8 8 2 6 9 8	17.13 17.13 17.43 16.6	17.7 17.2 17.2 17.2	17.16 17.16 17.9	16.65 17.31 17.41 17.38	2 2 0 X	8.18 18.18 18.18 18.18	2 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	2 2 2 2 2 4 5 2	5161 8161 8161 8161	2.4 2.7 2.7 2.4	4 2
Total Cate Solids Sel	ري (چ)	24.35		1 2777	22.77 22.84 22.65 22.65	23.71 23.63 23.63 23.51	23.22 23.16 23.05 23.05		22.78 22.75 22.75 22.75	22.45, 22.54 22.41 22.36	24.51 24.34 24.45 24.38			24 69 25.38 25.29 25.29		3 5 5 E	ŀ
To Sample Sol	. "vr"¢			- 2 - 4 - 6 - 2 - 4 - 6			-'ମ୍ୟୁଲ୍ଲ		- <u> </u>	4		2 2 2 4	<u> </u>		-:श्राह्मक -:श्राह्मक	- 7 6 4	1 6
1	ê &	\$ 8 8 8	e e e	66666	* * * * *	<u> </u>	<u> </u>		27: 27: 27: 27: 27: 27: 27: 27: 27: 27:	E E E E E	22 22 22	27. 27. 28.	21	77. 77. 77. 77.	178 178 178 178	I	1.793
Tank_Batch	UT Prod	AT Prod	VT Prod	RAT Prod RAT Prod RAT Prod VAT Prod- VAT Prod-	K/1 Prod- K/1 Prod- K/1 Prod- V/1 Prod- V/1 Prod-	RZT Prodi RZT Prodi RZT Prodi SZT Prodi SZT Prodi	RAT Prod RAT Prod RAT Prod RAT Prod SAT Prod	RAT Prod RAT Prod RAT Prod RAT Prod	RAT Prod RAT Prod RAT Prod RAT Prod	SRAT Prost-73 SRAT Prost-73 SRAT Prost-73 SRAT Prost-73 SRAT Prost-73 SRAT Prost-73	RAT Prod RAT Prod RAT Prod RAT Prod	RAT Prod RAT Prod RAT Prod	RAT Prod RAT Prod RAT Prod RAT Prod	RAT Prod	RAT Prod RAT Prod RAT Prod RAT Prod RAT Prod	RAT Prod RAT Prod RAT Prod	RAT Prod
	:# X	18 8 8 8 B	7 7 X	# # # # # # # # # # # # # # # # # # #	<u>ស្រីស៊ីស៊ីស៊ី</u>	<u>ಾಹಕಹಹಿತ್</u>	<u> </u>	<u>និសីសិស</u>	្រីស៊ីស៊ីស៊ីស៊ីស៊ី ស៊ីស៊ីស៊ីស៊ីស៊ីស៊ីស៊ីស៊ី	<u>នៃសស់សំពី</u>	\$ 5 5 5	<u> </u>	N N N N N N	ស្តីស្តីស្តីស្តីស្តី	សីសីសីស	থাজাজাজ	Tec es

Table 1: Sample Results for DWPF's Macro-Batch 1

Mercury (ppm)						Γ		Τ				K) v			1			Γ								Γ				T				
TIC Me		-		1				-		-		-			-			-		.,										.				
) (mild)	•			1				-		1		.						1-												.				
(freetium		0.023 0.016	0.027	Sino Sino	0.015 0.016 0.016	etoro etoro	0.015 0.015 0.015	0.014	9100	0.013	9000	0.012	0.012		0.012	2000	0.00	0.023	0.012	100	0.014	0.012	0.012	0,012 0,012	0.017	0.014		0.013	0.012	2000	3	= = = = = = = = = = = = = = = = = = =	0.01	0.02% 0.02%
frantum (2.83H 2.635	2.564 2.705 2.705	2714	2.748 2.73 2.754	2.619. 2.485	2.64%	2.84 2.584	2.451	2.761	2.227	5882	2.48	2.511	2 587	2.557	2.739	2.578	2.526	2.44	2.524	2.47	2.511	2.712	2.633	2.74	2.8.1	2.816	2.517 2.563 2.286	2.718	2014	2 036	8.7	2.027 1.869 1.847
Thankum U		0.011		0.034	20 0 20 0 20 0	0.021	0.025	0.016	0.027	2 5	0.012	\$10.0	0.015	2 'S '	80.0	5 6	0.005	0.015	5 6 8	7 TO 10	0.012	0.013	0.012	0.013	0 0 2	0.012 0.012	0.012	0.012	0 0 15 10 0 0 15	0.012	100	10.00	0.009	0.013 0.014
Silken D		3120	0 701	0.729	0.753 0.726 0.718	1.507	0.554	0.68K	0.50	0.71	0.701	0.71	0.592	0.602	0.743	2690	0.584	0,644	1699	0.43	0.647 0.621	0.611	0.47	0.678	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.752	0.662	0.722	0.694	8890	1542	8 5 4 5 5 4 5 5 4 5 5 4 5 5 5 5 5 5 5 5	0.473	0.578 0.557 0.528
Nickel (w1%)		1					0.261 0.261											ł		22.2	ı		- 1	0.261		1			0.248	. 1			0.18	0.159 0.182 0.184
Sodiun (wt%)			277	1		l	2083 7.114 7.052	1		1		1			1		6.822	5. 7.02							2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	Ι.,			9 8.23.1 8 9.181 2 6.897	-1-	==	10.782	6 12.65	6 11.55(4 12.1% 8 12.42;
Vanganes (wt%)		2.54 2.39	245	5 5	2.55	2.29	241	2.70	27.7.2	247	2.19	2.29	222	2.29	2.42	2 367	2.48	2.36	2353	2.805	2316	2.296	231	2.451	2.53	2.592	2.62	2.631	2.289	2.41 X	6.8	7.83.1 7.83.1	89 7	684 1684
Magnesium Nanganese (w1%) : (wt%)		0.959	0.982	S 5	9 2 2	20 E	187	0.861 0.959	1.107	1.057	5101	0.776	0.973	0.986	1076	18	0.984	0.881	10.1	1.037	0.976	0.967	0.926	0.755	2 4 9	0.913	0.856	0.893	1 037	0.824 0.864	0.889	0.763	0.745	0.707,
Lithum Mag		١.		-						-		-		.				-		- -	<u> </u>		-							+				
Potassium Lithum (w1%) (w1%)		0.055	0.0057 0.0048 0.0052	0.058	0.036	0.039	\$ 60 F	9100	0.027	0.027	0.045	0 144	S # 9	900	0.025	9100	0.024	0.00K	5 00	0000	0.036 0.03K	# FE 00	0.043	0.02	0.028 0.028	0.000	0.015	0.011	0.031	0.025	01151	5 0 0 0	0.03R 0.034	0.031
Iros Pota (w15) (w		# %	2 2 2 2	5 8 8 8	£ £ £	7.8	£ \$ 5	1881	\$ \$ \$ \$	874 1017	35 H 25	<u>~</u>	2 2 2	21.74	675	£ 3	10.7	58.5	, 6, 3	6.50	315	776	231	. 414	2 2 £	757	5 19	9.6	22.19 20.561 19.907	7.1	17.656	£ ± 5	22.2	18.053 16.02 16.519
		0.025 24	0.024 22.99	0.025 2	2	0.024 22	0.086 0.086 2.23 0.025	0.024 25	0.024 21	0.023 2	0.025 23.355 0.019 19.911	0.022	2200	0.022 23	0.022 23.099	0.023	0.023 24	0.022 27	0.021	0.021 21.807 0.019 19.39	0.022 22.459 0.022 22.335	0.021	0.021 23	0.022 2	0.024 24.834 0.022 23.1% 0.022 22.78	0.022 24.747 0.028 25.04	0.023	0.022	0.022 20 20 20 20 19	0.023		5000	0.016	8 9 9
Chronium Copper (wt?) (wt%)	, .	4.168 4.156	1.163 1.153 1.153	<u> </u>	333	1152	2. 2. 2. 2.	1169	£ - 5	1161	<u> </u>	¥ :	3 5 5	7 5 7	4 2	0 T	181	1.154	151	5 5	1,154	1.147	1.144	98.1		3,166	168	1163	0.14 7.138	1183	Ē Ē	<u> </u>	1129	1132
kium Ch		2.058	2.127	2.141	2.158 2.208	2.157	2.021 2.126 2.039	1.959 1.959	2.204	1.904	2.12 2.147 2.107	2015	2,048	2.069	2 1×7	2.075	1.99	1.959	2.074	2.09	2.056 2.088	2.037	2.075 1.916	1847	54 5 5 54 5 5 54 5 5 5 5 5 5 5 5 5 5 5 5	1.862	892	1.908	2031 2.135 1.711	1.83R	1785	11.	1.562	228
Born Cakium (wrf.) (w19.)				-						 		ļ			١.		• •••						.							\dagger				
Aluminum (wt%)		6.179	6.366 6.366 4.36	6.434	6.484	5,777	5.8 6.1 6.26	6.387	5.722	6.28	6.24 5.326 5.326	5.377	5.629	5.697	6.074	5.112	5.382	5.842	6.046	5 893	5.898	5.724	6.021 5.683	5.05	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6.753	6.946	6.714	\$ 52.5 5.41.5 5.	4.916	4.954	5.061	4.546	4.612
	12.00	590	2 <u>5</u>	1250	1230	<u> </u>	2 1	1.590	25.	1230	1250	1380	0.5	1777	12kg 1280	£ 5		1130	<u> </u>		1 <i>27</i> 0. 1290.	ž ž		15. 15. 15. 15.	1270	1750 1480	0.51 1.50 1.50 1.50 1.50 1.50 1.50 1.50		∯ & 8	980	1450	₹	8 4	£ £
Phosplate Sulfate (ppm) (ppm)	< 1100	< 1120 < 1080	9.8	× 1040 × 1020	020	< 864 < 974	866 > 866 >	00712	9 9 	S 2.	- 1260 - 100	901 >	0.00	V	0HU V	< 971		< 1060 0707	9		< 995 < 1120	<u> </u>		< 1120 < 983	=	< 1100 < 1050	6.05 0.05 0.05		92.05 20.05	< 981 1400	1320. 1320.	1270	9. 00 - 00 - 00 - 00 - 00 - 00 - 00 - 00	\$ E
Nitrik (ppn)	< 11t0 < 9t7	0001 >	2 2	× 10.0	v v	2.0		^ 120 ^ 130	\$ 5	2 DS	= <u>\$</u>	0.00	99		2 8 2 8			< HK0	0.0	,	< 95 < 113	9 9 2 9 2 9		011 v		0.01 >	2 8 0 8 0 v		2 5 5 2 5 0 2 5 0 2 5 0	0 × 100 ×	88	00 V	<u> </u>	≣.E.
,		35400		34500		2970XI 3030XI		30400		3660x		384(x)	2 2 2		35100 33900			•	35800		3471X0	32600 27200		34900		37100			38,500 38,500 36,300	38900 41400			4280X)	
(ppn)	5 ICE	< 120 < 080	v. v	0.040 0.00 0.00	v v	<864 <974		0.1 > 1.00 > 1.00	V V	07 V V V	v v	٧.	8	·	000 ×			ı	0.00		< 120			0 %		0.00	v v		ê' <u>≨</u> 8				× ×	v v
(ppm)	< 1100 < 967	<1120 <1080		× 1040 × 1020		< 864 < 974	1	< 1200		011.0		1	9 9		0401 >				0.5		< 1120		- 1	× 1116		0011>		- 1			× 1030 × 1030		2 Z	
Total Formate Chloride Plucide Hydraxlide (ppn) (ppm) (ppn)	23100	21200	2500	2,550.0	2%00	00.86	21800	19500	<u> </u>	22XH)	2/10/10	ZYSON	2000		31400	3.1800		CHINK	19800		31100	28200		0000	34200	34400	3200		39200	23500	21500	29400	19800	1,000
Total Hydroxida (eq/L)																																		
Solids (g/ml) H (wt%)		F.1.	2.2	2.2	13	2 2	5 6 1	6.11 1.11	* :-	1.13	= =	8			2 6	<u> </u>		= =	= 2		Ξ Σ	===		= = :	:E	1.5			= = ×		35	Ξ.	8 2 3	= =
Solids (wt%)																																		
Solids (w1%)	15.0	16.01 16.91		¥ %	18.5	16.31	15.65	16.81	4 4 5 4	16.4 17.13		5 2	2 2 2		18.4				¥ 9 £ 5		25 V	E E		× × ×	B .	2 x (∞ ∞ (8 8 2 2		S 2 2	1			2 2	- 1
Total Solids (wt%)	3 19.84 4 19.88	21.54	2 4 5 5 7 7 8 5 5	23.62	5 23.63 5 23.63	21.31	3 21.38 4 21.46 5 21.46	21.59	2 7 2 7 2 7 3 7	22 22 22 22 18	3 22.68 4 22.18 5	F	22.82	 	23.66		iv c		2.45		2 2 2 8 8 12 2			22.89		23.33	23.25		2 2 21 2			4 V 4	15.65	5 52
Samp										ļ		L						_	·				_									\perp	: 	
Jank_Batch	Prod-79a	Prod-80	SRAT Prod-80 SRAT Prod-80 SRAT Prod-80	Prod-81	Prod-81	Prod-82 Prod-82	Prod-82 Prod-82	Prod-8.3 Proxl-8.3	Prod-83	Prod-84 Prod-84	Prod-84 Prod-84 Prod-84	Prod-85	Prod 85	Prod-85	Prod-86 Prod-86	Prod-86 Prod-86	Prod-86 Prod-86	Prod-87	Prod-87	Prod-87	Prod-88	F. 2. 3.	Prod 88	Prod-89	Prod-89	Prod-90	3.5	Prod-90	Pod-9	Prod-92	Prod-92 Prod-92	Prod-92 Prod-92	Prod-93	Prod-93
ق ا	SRAT	SRAT	28.27 7.38.77 7.38.77	SR/T	SR/T	SR/T	SR/T	SR/T SR/T	SR.7	SR/T	SR/T SR/T SR/T	SRVT	SR/T	SRAT	SRZT	SRAT	SRAT	SRAT	SRAT	SRAT	X X X	S. S.	SE X	X X X	X X X	SKA	S. S.	SRAT	8.8.4 8.4.4	SRAT	SRAT	SRAT	SIS:	SRAT

Table 1: Sample Results for DWPF's Macro-Batch 1

(mdd)					<u> </u>	<u> </u>							,	_		
1		1		L	l	1	ļ		T	l	l					
(Ing		950	GFS:	7610	29430	55	790811	9720	K9K0	0450		8180	8010		ואוני	17.68
(wt%) (wt%) (ppm) (ppm) 0.025 2.013 0.035		0.115 0.125 0.109	1		0 0 0 0 0 0 1 7 1 8 0 0 0	0.038 0.025 0.05 0.048	10.0 10.0 10.0 10.0 10.0	0.015 0.016 0.018	0.012 0.012 0.011	90 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1000 0 000 0 000 0 000 0 000 0 000 0 000 0	0.00% 0.00% 0.00%	0.039 0.011 0.012 0.01		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.022 0.022 0.021 0.021
(wf%) 2.013			1 1		l .	1.022 1.032 0.936 0.953	1	i	I		1			}	2 2 2 2 2	50 1 10 1 10 1 10 1 10 1 10 1 10 1 10 1
0.025		0.052	L l		l	i	l	i	1	1		i i				9 9 9 9
1 0.712		23.241 2.25.67 2.25.947 3.23.369 7.23.829 7.23.829								6 23.834 11 24.833 11 24.428 24.323						13 23 338 11 22 734 11 21 991 12 23 105 77 23 463
10.70		0.184 0.182 0.182 0.183 0.167	1 1	9 0.113 0.104 7 0.106 1 0.108									7 0.148 8 0.094 5 0.199 4 0.152	ſ	I	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
= 15		X X X X X X X X X X X X X X X X X X X	!!			8.5.49 8.5.49 8.5.49 8.5.40 8.5.40	}	F	Į.	1	ŧ				2 X X X X X X X X X X X X X X X X X X X	
1.622		1.067 1.089 1.083 1.051 1.051	0.942 0.905 0.944 0.985	0.793 0.92 759.0 809.0	0.792 0.794 0.86 0.778	0.744 0.775 0.738 0.746 0.748	0.732 0.742 0.792 0.802	76.0 79.0 139.0 78.0	0.863 0.863 0.861 0.903	0,781 0,787 0,808 787.0	0.942 0.813 0.919	0.794 0.843 0.812	0.811 0.847 0.869 0.869		0.815 0.754 0.821 0.782 0.783	0.86
18.36 0.022 11.16d n.204		233	1.219 1.237 1.296 1.318	1.229 1.937 1.376 1.274	1.33	22.2 1.249 712.1 202.1	1.251 1.214 1.197 1.255	1.44	308 1.308 1.312	1277 1291 1211 1241	1.778 1.286 1.226 1.314	1,222	1.245 1.306 1.291 1.177		1.153	134 134 1316 1316 1316
		\$ E 27.25											7.85 1.715 1.715 1.306 1.306			8 6 6 6 6 6
0.022		0.449 0.462 0.453 0.453 0.453	0.138 0.124 0.172	0.131 0.095 0.097 0.076	0.128 0.093 0.081	0.118 0.115 0.114 0.067 0.055	0.092 0.106 0.106 0.086	0.031 0.051 0.069 0.065	0.062 0.066 0.109	0.025 0.159 0.631 0.045	0.023 0.031 0.051 0.024	0.033 0.039 0.036	0.045 0.101 0.085 0.078		0.102 0.102 0.104 0.104 0.105 0.105	720 0 720 0 70 0 7
0.017 18.136		\$ 25 25 25 25 25 25 25 25 25 25 25 25 25													275 815 8412 9.196 8214	
0.017		0.324 0.324 0.304 0.317													1	2.4 (2.8)
0.145		0.075 0.092 0.088 0.084 0.076				0.076 0.129 0.037 0.11									0.072 0.068 0.071 0.071	9:0:0 0 0 0 9:3:0 0 0 0
61.5		0.76 0.915 0.9 0.884 0.884	1 1			ł		l .	1	1	l				0.758 0.728 0.842 0.928	
		2.82 2.63 2.67 2.67 2.679				2732 2911 2924 2992							270X 2723 2723 2696 2688		27.53	2556 2647 2666 2293
5.196 1.539 0.145 0.017		2.192 2.246 2.246 2.038 2.038	2.264 2.227 2.154 2.242	2.131 2.333 2.357 2.297	2.204							2.29 2.102 2.147 2.344	2.279 2.216 2.313 2.313		2.458 2.216 2.358 2.358 2.358 2.358	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
		2 8 8 0	051 179 190	792 808 148 1070	05 H 05 H 05 H	2 5 E	102 1070 1980 866	175 1870 1160	050 85 86 080	05.1 10.5 10.5 10.5 10.5 10.5 10.5 10.5		0 1180 0 1130 0 1130	71.0 01.11.0 03.11.3 0.11.80	S 00 5 3	£ 3 5 £	4 E 2 E 2 E
	,	5.5 5 5	2360 964 1120 971	592 808 948 1070	1120 1030 1080	1010 969 1130 1240	102 1070 1080 966	975 1070 1160 1140	9111 956 956 1080	1240 1270 1250 1360	894 (DCO) (DSO) 954	081 V 081 V 081 V 081 V 081 V	\$ = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = * = = * = = = = = = = = = = = = = = = = = = =	6000	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	22 22 22 22 22 22 22 22 22 22 22 22 22
		8538	8 5 2 K	88.8 100 1	200 200	130 130 130 130	10.0 10.0 10.0 85.6	25 25 3E	2 8 8	8 5 8 8	25 E8 E8	2	76 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	5 5 5 5	5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 2 2 2 2 2
		22,900 22,900 20,800 21,700	27(0)0 286(0) 263(0) 263(0)	39200 40400 42700 42300	35000 36200 35100 35600	24700 24200 27000 26800	26500 27000 26600 23600	26200 26200 26200 24100	27100 27000 26100 24200	28900 26500 26500 26100	34700 29400 27600	22600 19800 18500 19300	23806 23806 22800 22800	28 Set 30 Set 26 Zet 26 Zet	24100 24500 24600 24600	20200
		j	838 971 1120 1190									<1100 <1180 <1130		i	R 9 B R 9 7 7 7	27.02 2 880 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
		26.7 26.8 24.1	838 971 1120 1190				102 1070 1080 966		1110 1050 956 1080			< 1100 < 1180 < 1130	2 - 2 - 2 5 - 2 - 3 5 -	02 02 02 02 02 02 02 02 02 02 02 02 02 0		2 4 80 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
,		35700 37100 38300 38300	33500 31600 33600	3500 35100 37200 38200	33200 33000 33000	33,300 30,400 35,900 33,400	29800 32100 33000 29900	33640	35100 33700 33200 33600	37200 37200 38200 38500	38800 37800 38700 34500	22.20X1 2980X1 2860X1 26.20X1	28100	20500	36300 36000 36000 36000	23,510
(m1%) (m1%) (m1%) (cq/L)		K = 41K	51415	r & 3 v	(a) (a) (b)	7200	W. 90, P.	- তান	യി ട ്കിക്കി	lett⇔tierki	e'≐'o'ki		-14:0° ×		5 7 = 7	m m n n w
		1.41				95 1.79 73 1.29 48 1.12						25 59 57 1-27 1-27 1-27 1-28 1-28 1-28 1-28 1-28 1-28 1-28 1-28			1.39	1.83
(M1%)		2.0.4.4	3 35.7 5 36.91 9 36.51			l			1			8 39.72 2 39.59 9 39.61 1 39.52			أمالواسات	3 K 3 K
(8)4)		2039 4735 4374 4774	4326 4233 4175 4169			Ì						4048 4339 4.1			4089 4089	3299 3337 3329 2663
(*1 4%)		2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		1 47.73 2 48.31 3 48.99 4 48.14	3, 48.24 48.24 4, 47.81	2 22 13 2 52 13 2 52 14 5 2 14	1 49.37 2 49.42 3 48.51 4 49.68	1 48.23 2 48.31 3 46.82 4 50.54	1 50.59 2 51.12 3 51.19 4 50.07	1 53.09 2 51.95 3 53.11 4 53.62	1 49.56 2 50.26 3 49.54 4 50.67	1 45.88 3 48.01 4 46.4	2 4 4 4 3 7 2 4 4 4 3 7 2 4 4 4 3 7 2 4 4 4 3 7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	- 0 E 4	2 2 2 2 2 2 3 2 4 4 7 2 8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	3 37 38 3 37 57 4 35 4
	· · · · · · · · · · · · · · · · · · ·			:		ļ								<u> </u>		
SRAT Prod-93		SWE-19 SWE-19 SWE-19 SWE-19 SWE-19	620 620 620 620	SNE-21 SNE-21 SNE-21 SNE-21	6 6 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	SVE 23 SVE 23 SVE 23 SVE 23 SVE 23	6.24 6.24 6.24 6.24	8 8 8 8 8 8 8 8	SNE-26 SNE-26 SNE-26 SNE-26	YE-27 YE-27 YE-27 YE-27	25 25 25 25 25 25 25 25 25 25 25 25 25 2		SNE 30 SNE 30 SNE 30 SNE 30	ले ले ले क इ.इ.इ.इ.इ	·	SNE 32 SNE 32 SNE 32 SNE 32 SNE 32 SNE 32
8		बाद दे के के हैं	នេសនិង	\$ \$ \$ 5	8888	<u>ភេសសស</u>	5555	8888	8 8 8 8	S S S S	8888	\$ \$ 5 5	ର ଜାନ୍ତାନ ର	ह है है है	ය යායායායාය	(8 8 8 8 8 8

Values at their detection limits (<) were set equal to their detection limits.

Sample #'s indicate dissolution method for latter SME and MFT batches.

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Table 1: Sample Results for DWPF's Macro-Batch 1

	(ppm)												<u> </u>	
roision				 							*			
2	(W.		1.20031	1.20 8 3)	802		ewstt.	E26	10700	KIRA		1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	13109	10800
	(wt%) (wt%) (ppm)			0.013	0.000 0.000 0.000 0.000		0.0019 0.0021 0.0021 0.0024	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.013 0.012 0.011 0.014	0.013 0.027, 0.016, 0.016	8000 8000 8000 8000 8000 8000 8000 800	X 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1100 1000 1000 1000	0.023 0.023 0.023 0.025 0.025
	(*tt.%)		1,425 1,478 1,517 1,238	22.54.5	1.082 1.03 1.047 1.073 0.969		1.234	1.077	0.947 1.028 0.84 0.84 1.114	1.019 0.934 0.979 0.956 0.956	0.967 0.967 1.048 0.972 1.008	0.809 0.777 0.856 1.129	0,999 0,099 1,081 4,98 0,989	0.987 1.062 1.071 1.073 1.073
	(%t%)		# 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0.00 0.017 0.000 0.000	8100 8101 8101 8101 8101 8101 8101 8101		0.027 0.025 0.025 0.024 0.026	0.027 0.027 0.021 0.027 0.027	0.02 0.021 0.021 0.022 0.022	0.035 0.035 0.024 0.024	0.024 0.019 0.021 0.021	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	# # # # # # # # # # # # # # # # # # #	0.025 0.025 0.025 0.026 0.026
	(MT%) (MT%)		20.836 22.289 24.369 22.602 23.198 22.672		23.44k 22.484 23.895 23.895 23.561		21.709 22.413 22.54 22.222 21.911	23,345 21,128 22,843 23,501 24,092 23,817			21.245 23.559 23.027 22.264 23.156	23 624 23 267 24 473 23 507 22 114 22 114		23.77 22.995 22.968 21.562 24.177 12.925
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	(k (k (k		2 9 9 9 12 12 12 12 12 12 12 12 12 12 12 12 12		0.089 0.1 0.084 0.103 0.096		8	1	0 072 0 078 0 074 0 064 0 064		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		0 115 0 138 0 115 0 115	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
3	(M1%)		9 000 9 000 9 000 9 000 9 000 9 000 9 000	ĺ	25.8 25.8 25.8 25.8 25.8 25.8 25.8		8.07 8.377 8.548 8.648	i	8.55 8.94 8.45 8.45 8.51	1 1	8.7.8 8.7.8 8.5.3 8.7.8	217.8 217.8 27.8 21.9 21.9 21.9 21.9 21.9	I	41.52 % 18.58 % 5.50 % 18.50 %
	(91%)		0.906 0.93 1.011 0.925 0.923 0.889	0.758 0.907 0.847 0.884	0.8.14 0.814 0.786 0.871		0.918 0.918 0.827 0.907 0.957	0.844 0.829 0.815 0.815 0.816	0.637 0.709 0.749 0.616 0.788	0.789 0.772 0.733 0.817 0.816	0.778 0.778 0.84 0.804	0.785 777.0 0.738 0.73 0.740	0.874 0.902 0.943 0.855 0.92	0.702 0.785 0.775 0.798 0.694 0.798
	(wt%) (wt%)		2362 236 236 236 236 236 236 236 236	1.267 1.334 1.282	1.05 0.957 0.024 1.024		1,226	1.323 1.259 1.256 1.298	8 5 2 2 2 E E E E E	1237 1.27 1.147 1.224 1.261	1.22	1.208 1.238 1.238 1.229 1.156	1.267 1.324 1.278 1.279 1.318	1.187 1.237 1.242 1.275 1.262 1.245
illin i	(w.F.E.)		16-18 16-37 16-37 16-25	1727 1686 1726 1623	1678 1.72 1678 1645 1649		1561 1671 1617 1573	17.51 17.25 16.79 17.06 17.85	1803 1795 1763 1763 1.848 1.88	1547 1.71 1.66 1.66 1.686	1709 1685 1685 1682	1722 1711 1746 1746 1747	1687 1684 1673 1673 1673	1723 1686 1771 1711 1776 1775
) i dansejima j	(wt%) (wf2)		14.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8.207 8.191 0.25	0 103 0 0071 0 0071		0.127 0.108 0.109 0.109	0.101 0.086 0.07 0.096 0.129	0.082 0.083 0.077 0.093	0.075 0.078 0.058 0.058	0.059 0.059 0.054 0.084	0.036 0.025 0.101 0.071 0.086	0.0072 0.0072 0.034	0.179 0.155 0.146 0.215 0.215
100	(w(f)		8.886	7.998 7.996 8.97	8.83 738 8.86 8.28		7.874 8.777 8.631 9.137	2.85. 2.85.	6.24 6.24 6.24 6.24 6.25 7.75	7.551 7.653 7.458 7.757	7.83 8.28 7.87 7.87	7.26 7.26 7.26 7.21 7.31 8.04	8.88.2.2.8 5.7.2.8.	753 8.158 7.75 8.293 7.26 7.36 5.619
1	(%) M		0.367 0.376 0.378 0.372 0.368	0.35 0.395 0.375 0.595	0.18K 0.377 0.378 0.41K 0.395		0.327 0.351 0.315 0.35 0.35	0.179 0.184 0.175 0.171 0.178	0.054 0.052 0.053 0.047 0.061	0.053 0.057 0.054	0.059 0.053 0.054 0.069	0.028 0.026 0.027 0.024 0.031	0.016 0.015 0.021 0.016 0.017	0.014 0.013 0.013 0.014 0.011
). omqua.4	(nte) (nte)		0.07 0.073 0.075 0.068 0.068	0.09 0.09 0.075 0.078	0.063 1.063 1.063 1.063		1085 1079 1075 10879	1063 1062 1061 1061 1065 0.06	2055 0.06 2059 2053 2051 0.07	10.07 10.65 10.65 10.65 10.65	1961 1965 1966 1966 1978	9.36 3.059 3.059 9.007 9.007	1079 1079 1.183 1.074 1.073	0.06 3.0863 3.0863 3.0865 3.0865 3.0865
Colcium	(% P.W.)		0.944 0.985 0.937 0.967	0.787 0.952 0.931 0.939	0.778 0.693 0.816 0.76		0.905 1.09 0.9 1.068	0.891 0.891 0.869 0.847 0.865	0.658 0.732 0.762 0.599 0.6186	0.807 0.799 0.737 0.825 0.836	0.765 0.848 0.822 0.818	0.729 0.743 0.714 0.89	0.897 0.978 0.893 0.893	0.737 0.779 0.842 0.749 0.744
Bonoli	v [e]			2.14 2.28 18.2 18.2 2.73	2.93 2.893 2.848 3.28 2.87 2.804	- 1	245 2.53 2.69 2.69 2.51			2.74 2.74 3.083 2.398	1		2.339 2.864 2.862 2.77 2.77 2.91	
- International	INT&)		2.546 2.588 2.82 2.592 2.547 2.547 2.547	2.279 2.424 2.291 2.381	2.016 2.173 1.835 2.034 2.057		2.347 2.347 2.559 2.636	2.296 2.459 2.247 2.249 2.26 2.26	1.962 2.093 2.113 1.863 1.931 2.163	2.243 2.243 2.139 2.308 2.235	2.13 2.23 2.23 2.234 2.488	2.425 2.244 2.058 2.229 2.545 2.546	2.455 2.568 2.548 2.548 2.476	2.318 2.391 2.274 2.44 2.156 2.156 1.649
Suffete	(tidd)			10.5010.5010.5010.5010.50	001 V 000 001 br>000 000 000 000 000 000 000 0	\$ 5 E		< 1050) < 1050) < 1040)	 1150 <li< th=""><th>0501 ^ 050</th><th></th><th>986 1081 > 1180 ></th><th> 1690 1140 1610 1630 1630 </th><th>821 ></th></li<>	0501 ^ 050		986 1081 > 1180 >	 1690 1140 1610 1630 1630 	821 >
Phosobate	(mdd)	2 KR39 2 KR39 2 KR05	< 1030 < 1040 < 1040 < 992	0.11.5 0.11.5 0.11.5	\$ 11300 \$ 1130 \$ 1130 \$ 1170 \$ 1170	5 0 0 6 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	< 992 < 1040 < 940 < 1050 :	0 1050 0 1050 0 1050 0 1050 0 1050 0 1050 0 1050 0 1050 0 1050	0 1 1 4 0 1 1 5 0 1 1 4 0 1 1 1 4 0 1 1 1 1 1 1 1 1 1 1		< 10k0 > 10k0 < 10k0 < 10k0 < 10k0	< 1090 < 1010 < 1140 < 1140	0 1170 0 1150 0 1450 0 1480 0 1340 0 1340
Nitri		< 8.9 < 8.9 < 1100	< 10.0 < 10.0 < 10.0 < 9.2	0,11 > 0,01 > 0,01 >	4 1000 4 1100 6 1100 6 1000		0.01 > 0.00 0.00 > 0.00 0.00 > 0.00 0.00 > 0.00		 (100) 	8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			 100 100 100 100 110 110 	6 1 5 0 5 1 5 0 5 1 5 0 5 1 5 0 5 1 5 0 5 1 5 1
Nitrate									27300 26900 26900 28100 27800 27800 27800 27800					32100 32300 30600 32900 24900
Tarride	(btm)			< 1050 < 1080 < 1140 < 1170	< 200 < 200 < 170 < 170 < 170	50 20 20 20 20 20 20 20 20 20 20 20 20 20	980 V V V V V V V V V V V V V V V V V V V	× 360 040 × 940 × 940 × 940	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0			4 020 4 020 4 020 4 080	090 > 010 0.00 > 020 0.00 >	2 95 95 2 95 95 2 95 95 2 95 95 3 95 95 3 95 95 3 95 95 3 95 95 3 95 95 3 95 95 3 95 95 3 95 95 3 95 95 3 95 95 3 95 95 3 95 95 95 3 95 3
Chitoride 3	(eq.f.) (ppm) (ptm) (ptm)	< 839 < 805 < 1100	< 1030 < 1040 < 1048 < 992	> 1050 > 1080 > 1140 > 1170	< 1200 < 1200 < 1130 < 1170 < 1070	0.00 0.00 0.00 0.00	7 1080 1080 1080 1080 1080 1080 1080 1080	< 992 < 1640 < 940 < 1050	 1050 1050 1050 1050 2060 <li< th=""><th>^ \ 150 \ \ 1020 \ \ 1030 \ \ 1030</th><th></th><th>< 956 < 1080 < 1080 < 1080</th><th>× 1030 × 1010 × 1050 × 1140</th><th>2 1 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</th></li<>	^ \ 150 \ \ 1020 \ \ 1030 \ \ 1030		< 956 < 1080 < 1080 < 1080	× 1030 × 1010 × 1050 × 1140	2 1 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Formate	(mdr)	25.300 22.900 25.100	3400 3400 3450 3350	35300 35400 35400 31500	3,900 3,900 2,800 2,500 2,500 3,6900	35200 37400 25800	47 20X1 47 20X1 47 20X1 37 60X1	3C2/X 3C2/X 347/X 311/X	27400 28300 27600 27600 27600 27500 27700	25900 25200 24800 25400		315/10 22/10 312/00 312/00	MICKO MICKO	3.50X 3.50X 3.50X 3.50X
Total	(eq.T.)	•										-		
Densky	(g/ml.)		4.1.3.9 2.1.3.9 2.1.3.9 2.1.3.9 3.0.0 3.0 3	4.5 4.5 4.9	<u> </u>	₹ 2 €	<u> </u>	7 4 4 5 7 4 4 5	2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	2 4 4 4 8 4 8 4 8 4 8 4 8 4 8 4 8 4 8 4		7 % T %	1.31 1.37 1.8	<u>¥ = ₹ ₹ 2</u>
nseluble	(wt%)	36.26 35.22 34.72												· · · · · · · · · · · · · · · · · · ·
atcind	2000 2000 2000 2000 2000 2000 2000 200	39.67		45.2 44.4 45.3 45.3	46.7 47.1 46.9 45.6	4 4 4 2 5 5	5.4.4.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.	8 4 4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	45.42 45.87 45.87	2 2 4 4 6 2 4 5 4 5 4 5 4 5 4 5 5 5 5 5 5 5 5 5 5	, =	80.04 80.04 81.14 11.12	7 7 7 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	17.5. 17.7. 17. 1
Total	(wt%)	4 5 4 4 8 8 13 8	47.18 48.54 47.47 48.17	50.48 50.5 50.64	52.15 52.15 52.67 51.66 51.02	50.26 50.26 52.12	51.01 49.49 51.91	1		47.64 47.9 47.16 47.14		46.57 46.29 46.39	49.89 50.22 49.57 50.03	53.16 52.07 53.07 53.27 54.27
	Sangale	- 27 67 79	- ''' (''' ''' ''' ''' ''' ''	- n'm'a'si	- 0 - 4 v c =	71 F. 4	- N * 4 * C C &	-02465	-[4] # [4] # (4] # (8]	- N F 4 V C	N ক ৰ জ ত	- N. T. T. C.	- NEW WOOL	- 0.00.4.00.6
	ank_baich	2 2 2 2	<u>គ</u> ្គគ.គ.១១	22222	వి. ది. ది. ది. ది. ది. ది. ది. ది. ది. ద	2 2 2	2 & 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		g: ge: ge: ge: ge: ge: ge: ge: ge:	SME-38 (rem) SME-38 (rem) SME-38 (rem) SME-38 (rem) SME-38 (rem) SME-38 (rem)	((cen) (cen) (cen) (cen)	2 2 2 2 2 2 2	<u> </u>	
1	e 6	S S S S	88888	SWE SWE	* * * * * * * * * * * * * * * * * * *	SW SW	S S S S S S S S S S S S S S S S S S S	N W W W W W	SM 5 34 5 34 5 34 5 34 5 34 5 34 5 34 5 3	N K K K K	SWE 3	S S N E S	SME40 SME40 SME40 SME40 SME40	X X X X X X X X X X X X X X X X X X X

Values at their detection limits (<) were set equal to their detection limits.

Table 1: Sample Results for DWPF's Macro-Batch 1

Mercury	(audd)							T								Γ	•				Γ							Τ					T	
IC M	- T		.		\dashv						-					-	•									1								
TOC TIC	d) (nude		+		-	956		0.126			-					0300					0000		-			0400		-			9980			,
	F (814)	0 0 1 X 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048	0.043	0.042	9 G G	0 0 0 0 0 0	0.009	0.024	0.00						0.021	9100	0 0 0			0.05	100 c	9.04			0.02	0.00 8.00 8.00 8.00 8.00 8.00 8.00 8.00	740			0.032 0.033	0.036		
ranium: Z.5		25.25.25.25.25.25.25.25.25.25.25.25.25.2	1.182	2 2 2	10	7 9 C	1.122	0.71	0.799	0.706 0.583	9/10/1		•			1.268	1.272	314			1.28	1.478	1 2849		٠	0.939	0.K96	£ .			1 (M) 1.118	0.976 0.904 1.053		٠
Tanhum, U		0.02	0.02	0.02	0.021	669	0.018	0.015	0.015	210.0	0.017	780 c	820.0	0.022	0.02	0 0 BK	0.019	910.0	0.021.	5 8 8	0.022	0.021	0.03	0.028	900	0.017	0.017	\$ 60 a	0.022	0.025	0.027,	0.026	1100	5000
Sifkon	(M1%) (Mt%)	20.501 27.721 22.568 26.196	22.327	22,727	21.257	22.544	22.55	23.375	23,415	23.77	24.423	27 US7 26 149	23.766	28.856	2K.289	22.423	22.867 22.414	22.336	0.092 21.431	20,717	24.857		23.853	25.09	22.891	24.072	0.087 23.477	2 2 2 2	24 267 25 244	25.351	22.42	0.127 23.429 0.091 23.231	25.261	23.488
Nickel	().	8 1 0 2 1 0 2 1 0 2 1 0	0.132	0 103	S THE	0.152	0 107	0.08	0.083 0.083	0.0% 0.0%	9500	0.117	0.088		170.0	0.09		0.095	0.092		0 107	3 2 3	0.084	0 1 2 2	0.13	0.085	0.087	<u> </u>	5 5	0.109	£ 5 0 0	0.127	0.112	0.092
udinn		8.53 10.67 9.77 10.81	7 (8 8 2 8 8	891	3	5 2	9.8	5F %	¥ 8	8.58 2.28	1			• • •		8.58	8.40) K.71	* * * *			X XI:	¥ % \$	×			x x2 76	¥ %		• · · · ·		0X X	× × × 5 5 5		
Sankanese		0.783 0.978 0.951 1.062	0.85	0 X 7 X 5	0.825	0.92	0.887	0.722	0.775	0.588	0.73	0.556	0.75%	189.0	0.585	0.809	0.743	0.804	0.713	X690	0.747	0,730 0,805 108.0	0.714	0.828	0.859	0.776	0.737	0.855	0.816	0.817	0.902. 0.887	0.826	0.988 0.814	0.7939 0.865 0.865
agnestum, H	(MES)	1 24.7 1 4 16 1 5 46.	124	1225	22	9 3	1.25 1.11x	1,295	1,294	1.281	Z 72	1.182	<u> </u>	1.274	22.9	1.26	1 265	1.22	3 2	2 E ×	1231	1.22	182	3,80	249	1.277	1.22.1	1219	1.236 1.257	1.259 1.28	1.319	1.274 1.162 1.248	1.325	1 273 1 273 1 328
idlum M.		1625 1039 1785 1962	213	1893 1893 1893 1893		1636	1.58	1775	1.7	1835	1518 1605	1.66	538			718	756	1697	777	2.5	1705	16.86	669	1863	515	1765	1677	1564	1674	1665	1616	1.68	1702	1803 1803 1803
- =		0.199	0.145	0.149	0 158	188	0.192	0.186	0.039	0.132	0.011	0.095	0.078	0.127	0 13	0.171	0.195	0.19	0.00	0.00	0.205	0.22	0.224	87.00 0 05.00	0.082	0.07 0.076	80.0	0.112	0.157	0.193	0.141	0.138	0 0 4 04	5,7,3,7 5,7,3,7
lra 1	(316.5)	7 × 5 × 5		8. 8. W	7.517	8 8	8.83 748	7 PS	7.04	7. 6. 5. 1. 8. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	ع ق	80°9	7.642	7.055	7.85	% % 52.	7 & 2 &				1.654	7.9.7 7.9.7 7.9.7	7.15	~ 50 50	× 0.3	1		× 78	-		8.723 8.50x		74.7	7.927 7.927 7.939
obber	(4.1M) (3.1M)		500			0.00	0.012	0.00	0.007	0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.03	0.029	0.018	0.011	0.009	0.014	0.016	0.015	0.016	E 6 8	910.0	0.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	100	0.017	0.018 0.018	0.000	9000	910.0	0.015	0.018	0.012	0.012 0.008	0.015 0.015	2 2 2
	(228)	0.166 0.087 0.106	0.082	D.061	0.054	0.123	0.075	0.049	0.058	0.057 0.044	0.048	1000 1000	0.067	0.057	0.049	0.07	0.068	70.0 7.00.0	0.00 0.000	0.057	0.07 0.075	0.085	0.068	0.00	0.07	0.059	0.054 0.062	1.086	0.072	0.075	70.0	0.08	1.184	0.07
Calcium	٤	0.856 1.042 1.057		0.954	- 1		0.921		0.78	0.582	ŀ	0.569				0.826	0.754			0.654	0.861	0.862	ļ			1	0.816			. 1	0.944	0.861 0.741		0.828
Been		2 2 8 2 2 1 2 4 5 5 1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5			- 1		2,128				2.59				2.51					2.22					2.4.2				284				l .	2 2 2 2
Atuminum	3,360	2.264	2.43	2.487	2.381	2.69	2.606	2.245	2.443	2.256	1,959	88.8	2.258	2,203	2.284	2,461 2,53	2335	2.409	2.059	1,983	2.12	2.471	2223	2.22	2.525	2.258	2 30 2	2.483 2.286	2.293	2,329	2.544	2.5 2.026 2.466	2.733	2.188 2.45 2.174
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	358	.894 .894 .046[>			. 1140	<u>1</u> <u>2</u> <u>2</u>	₹ 2	872	948	0 <u>%</u>		•				×1300 ×1350	02412				< 290 < 340	5.52 5.00 5.00	1			9162	080 >				2 S			:
Chloride	100	< 89.0 6 1340 6 1340	-		- 1	<u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u> - <u>-</u>		< 872	\$ ***	- 1080 V					-,-	< 1300 < 1350	× 45 × 45 × 45 × 45 × 45 × 45 × 45 × 45				0 1 2 3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	< 1270 < 1300	1			< 916 < 998	001. V 1100		++		0801 >			<u> </u>
Formute	i w	CAP MAST CAP CAP MAST CAP		2/700	26300	24900	2/400	26500	23600						31900	27.500				25100	2,500				2680N	27200	ļ.,			28930	2734X)			
Total Hydenxist	(eq.T.)																																	
Density (a/m)	3	€ 3 ₹			P.	2 %	<u>8</u>	- 46	€ ₩							1.429	2 2				1.479	<u> </u>				418	\$ *				4 5	4 4		
Insoluble Solids	(MC)								:																				. :	1			#	
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Fatal Solids	(*1.%) 20.76	50.5				48.0S			\$2.55					operator :		50.83			-		\$2.26			:		16.18					ğ 3			
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ank_Batch	2	9000	y 10: 61	ú.u.v	7 7		ne-					:	,			v. v	•		n.v	V5 15 15		c v										e loc		
Ę	SME	SNE 22 SNE 42 SNE 42	SWE	SNE	SNE-4	SNE 4	S. S. S.	SME	SW6.4	N SWEET	SME-4	SWE	N. N.	W.W.	SMS-4	SME	N N N	N N	N N N N N N	SMS	SM3-4	M S M S M S M S	SM:4	SM24	SMS A	SME	SME 4:	SME 4	S S S	SME4	N S	SME 48	N W W	SME 48 SME 48

Values at their detection limits (<) were set equal to their detection limits.

Table 1: Sample Results for DWPF's Macro-Batch 1

Mercury	(III.del)						Γ															Ī													
1 2	inder :		 							-															ļ ļ		<u> </u>							-	
Ursaium Zircunium TOC	(undd) (b) (b) (b)	(1) (1) (1)	6.5	-500			03.045 T0600 0.049	¥ 9	¥ 7			0.062 1170H 0.061	<u>ئۇ</u> ۋ	2 E			02 HH00	12.	0.021			101 9720	0041 0043	222			187 9770.	0.092	<u>z</u>			XXX 1.20XX	9 9 8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		
Zirconiu												1										1			ĺ										
Uranium	É.	1.218	280	886			1.043	1.132	0.897			1.194	0.956	<u> </u>			1.165	2 2	2 8			1919	1.073	0.994				0.902	0.84				2 2 2		
Hinnium (meg.)	Ē	0.027	0.025	0.024	0.025	0.026	0.02	0.017	8100	200	500 000 000	X X	0.017	0.017	0.025	2 2 2	0.015	2000	0.015	610.0	0.018	0.021	9 0	0.015	610.0	0.00	0.014	9.00	0.015	0.0	0.021	9100	0 0 0 8 0 0 1 7 0 0 1	10025	0,024 0,034 0,031
Silicon	()	24 6 18		22.44	25.125	24.489	25.275	~	24.5x 23.45	25.53		22 17x	24.714	21.97	26.582	26.047 26.39X	22.245	22 628 23 141	22.736	0.119 23 307 0.131 23 692	151 25.39 151 25.39 16.1 25.431	26,186	22.7% 23.536	0.104 23.495 0.086 23.168	0.101 24.631	24.894	0.108; 21.701 0.103; 22.863	23 681 23 142			25 292 25 192 25 193	23.79	23.135	22 KG 3	23.848 21.479 23.725
Nickel (w19)		0.093				8 0 0 1 0 0 1 0 0	ŧ			0.089	0.097	1		5 S	x600	20.00	0.103				0.55		0.099			S 2 2 3	0 108	0.08		0.092	0.033 0.093	0.107	3 7 8		0.191
Suding (wrs.)				X 28			Į.	2003 2003 2003 2003 2003 2003 2003 2003		a r :	si a ' c' s	× 34			26	20	1		8 978		e, 0, 1-	1	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8			~ ' ~ ' ~ '		2 × 791	F	- Z	e oc v	ı	× × -	l	- N.4
[attigation (wf %)		9.0	0 X 2	0 5	0.74X 0.74X 0.831	0.801	0.651	0.316	0.655	0.089	2 2 2	0.XS5	0.664	1.003	0.792	0.841	0.929	0.952	0.965	0.874	0.912 0.912 0.757	2,4	\$8.0 18.0	0.84	0.843	757 0 757 0 757 0	0.70	0.744	0.792	0.716	0.688	0.943	0 868 0 878 10 1	8,0 768,0	0 712 0 712 0.924
fagnesium ?		1.335 1.298	1.288	243	1.207	1.259	125.1 1.38	1.339	1.22	394	77.7	1.253	1.271	1.517	1271	1.286	1.265	1.296	1.381	1,329	1.187	1 255	1 282	1.202	1.263	1.23	1.204:	18. 18. 18.	1.244	241	28.5	1,291	1.362	1,243	1234 1.12 1.28
ithun 3		25. 2.51	1.64	1573	1686 1625	1556 1621 1635	1.67	17.5	1767 1668	1.75	182 183 183 183 183 183 183 183 183 183 183	1.61	77.	1554	1583	1,667 1731	1649	1672	3.2	583	242	1574	69.16	1716	3 3	619 648	19 19	725 718	869	678	25.5	705	618. 818.	256	8, 14, 25 15, 18, 18, 18, 18, 18, 18, 18, 18, 18, 18
Hen Polassium Lithum Magnesium Hanganese Sudium Nickel (MC) (MC) (MC) (MC) (MC)		0.22	0.197	0.131	0 0 0 85 0 85 0 85 0	0 18 8 0 18	0.201 0.165	0.199	0.161	2 2 3	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.196	0.10 0.165	0.161	0.098	0.088	0.151	0.15	0.152	9 9 8 8 4 8	0.134	0.159	0.083	0.088	870.0	0.136	0.084	0.122	0.112	0.106	0.138	0.211	0.173 0.173 0.295	0.176	0.139 0.14 0.216
					7.84		r ×.					9. 141.9 141.9		. 1	F. 2.	8 8 8 8 8 8	8.153		5 0C	}	2 8 C	828	30 F-	× 408	od "r	- 1- 2 3			7.413			-			2 735 2 735 8 24
Copper (w1%)		0.013				0.012	i	0.001	- 1	1 4 5		.i		1		0.000	0.014			l., .	8 8	000	<u> </u>				1	0.008	- 1					l	0.016
Aluminum Bann Calcium Chronium Copper (1912) (1913) (1913)		1062	1983	1059	1056	1062	1064	3000	3,052	200	1072	9000	105	0.07	99011	11174	170.0 13061	0.073	0.0673	0.074	0.08 0.08	0.0%	0.073	0.067 0.065	0.067	9900	0.121	900	\$ 500 \$ br>500 \$ 500 \$ 500 \$ 500 \$ 500 \$ 500 \$ 500 \$ 500 \$ 500 \$ 500 \$ 500	900	0.059	0.32	0.074	800	0.098 0.098
Calcium (0.865	0.872 0.819	0.833	0.774	9.3.0 1.8.0	0.915	1.915 2.7.11	1797	6.83 8.83 8.63 8.63 8.63 8.63 8.63 8.63	0.763	0.812	9730	1.048	1.056	0.518	0.938	19610	0.926	0.789	0.846	0.87	8 36 X	0.838	0.846	0.835	0.659 0.744	0.677	0.774	0.719	0.5K6 0.6K5	278.0 0.871	0.941	0.829	0.755
Salbin (1	2.65					2 E E	<u> </u>			2.45		···				2 2 2 2					25.43					2.75 2.15				22.2
luminum (*1%)		2.3K2	2.452	2.377	2.29	2.393	2.131	2.587	2.101	27.2	2,506	2.692	2 12	2.925	2.329 2.886	502 702 702 703 703 703 703 703 703 703 703 703 703	2.59	2.68	2.665	2.552	2.456	2.3%	2 48 2 39	2.242	23.2	2222	2.214	2.314	2.424	2.248	2.188 2.275	3.028	2.482	2.35	2.363 2.184 2.641
Suffite A		< 1050) < 1080) < 1080)	2 T V				- 16.50 - 16.50	0.03 V 1.08				5.77 0.1150	V 1031				× × (88)	< 1130 < 1130	,-			- 95.1	2 E	(JSI) >			<u>≨</u> §	10.00				02 I S	∰. 		
Nitrate Nitrie Phosphate Sulfate (upm) (ppm) (ppm)		0.11.0 0.001.0	× 10%0				< 1090 < 956	< 1050 < 1070				< 977 < 977	0/0 0/0 0/0 0/0 0/0 0/0 0/0 0/0 0/0 0/0				9/01 v 1080 v	0801 V				(ZII >	> (D) >	× 1150				0.85				< 1120	- 13 B		
Nitrik (ppn)) < 10 0 < 16 0	1 < 10% 1 × 10%				0.01 ×	976 > 1				< 9.7	2 2	_			0.010 × 1	9 7				DH > (3 8	9. 				€ 6 0 0 0 0				0.11 0	0 < 100 0 < 130		
		20,000			ļ		3 28900 ii 28700					7, 25500					1, 18500	:_:				ł.,	29(NX)	+				0 26900 9 27200	<u>.</u>			30600			
Flurrid (pm)			¥ 5			··-	2 × 1070		_			× 97			٠.;		1.	20 V	1			1	8 8				4962		ļ			21120			
Chloride (ppm)			× 1380 × 140				0.1090 0.1070					× 1000 × 774 ×					•	02 V				1	0.01 v 0.001 v		:			18.6 v			1	0211 >			
Formate (ppm)		2,800	227UD 22910				35900	31200				349(H)	3,600		· ·		50500	7,800				31300	3,300	32300			3.500	3,600			.,	3,000	2700		
Total 3 droxide	(F#Z)		-							_	-		_	Ĭ	-						-		•												
Density Hydroxtde (ppm) (ppm) (ppm)	,		₹ ₹				1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1				1.417	5 5				1,419	<u> </u>				1.424	77	14.			1.1.2. 2.1.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2	44. 8.44.	<u> </u>			9 €	3 3		
Insoluble Solids	(M1%)		_			:		_	T															.]									:]	ľ	ĺ
Calcind Insoluble Solids Solids	\$ 1 to	4 4	45.3				42.2					44.7 133						44.02				1	£ 44	- 1			<u> </u>	# # \$ 99				# 5 5	.		
Fotal Solid	at Se	ž ė	2.2		u. '5	6.1074	4863			27574	14550	49.94		أرير	re to "		48.48			n. 'n 'e	James Teles		50.88 V 52.16		E'n T			20.2 20.0 20.0 20.0 20.0 20.0 20.0 20.0	- تن ابت	62 6 7		49.27	4 × 08	(b. 1)	
Sumple	:	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	3:MA	ANA ANA	# H E	Į X Ż	2.414	AN 4	2 S.M.	I X I	# 2 7 F F F	2-MA	¥ 5	- X	- ~	2 2 2	1-11A	AM-4	5-1/1.A	2 % %		- I-MA	2-MA	4-MA 5-MA	= 1	1.4.2.2	2.44 4.44	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	X 2	Z Z Z	1.3.3	2.14	5.4.4 5.44	1.5	5 5 5
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Ę	5,00	SME	SME 4	SMS	SME-49 SME-49 SME-49	SME	SMES	SMS	SMS	N.S.	SMES	SWS-5	SME-5	SMES	S S S	SWS	SMS-S SMS-S	SMES	SMSS	S.W.S.	SWS	SMS S	SMES	SMSS	888	SWSS	SMSS	SMS	SMS	SMS	SWS	SWS	N S	SWS	SMSS

Table 1: Sample Results for DWPF's Macro-Batch 1

Mercury	(mdd)												<u></u>																								
2 2	(mdd)															_																					
TOC	(måd)	X 2					8.350	£ Ø 3				0916	7 7 7				5 K970	به تا سرا	· ·			X X X X X X X X X X	c ×			2 9180	- 24			-	i ising	: 'æ'æ	ا پ			2 4 4 6	- 3
Circonium	(3) W	0.028	100	0.029	0.00		60 B	0.086				970	7 7 8 0 0 0 0 0 0				0.099	50.0	9 8			0.078	6.07			0.073	0.07			1		6800				0.035	0.0
ranium 7		1.128	0.857	727.0	10/10		0.765	0.897				1 591	Z Z Z	-			1.044	0.929	876.0			0.94	0.974			1.383	7			3311	8 8	1035	1.16.1			1.127	1.085
lanium 1	(2)	F 0.0	3 3	Ĩ	200	0.00	0.03	0.018 0.038	100	0 0 0 0 1 0 0	0.017	0.023	0.025	0.016	0.016	0.00	0.014	0.134	1	0.02	0 0 0 X 6 5	0.016	0.013	0.021	0.02	6100 6100	0.021		8 0	0.018	0.022	0.018	0.036	0.015	2 2 2	0.016	0.021
Silicon 1	(w1%)	72.329	23.317	9 52	26.001	26.719 21.391	21,16	22.292	23.803	23,126	23.543	23.155	721.52 877.52	23.44X 26.577	24.014	21.169	23.139	22 474	21,666	25.271	24.566 24.384 23.474	24.925 25.911	25.548	26.743	27.78 26.742 27.435	23.37. 23.458		24.365	25.163	24.93	23 992	21.785	21.899	24 ×7	26.646	21.429	22.835
Nicket	(w15)	0.103	0.09		85.1.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.878 0.088	0.089	0.098	0.088		0 104		==	0 101	0.093	0.104			<u> </u>	2 8 2	0.085 0.08	- 1	0.082	8,03 E 0	\$0.00 \$0.00	- 1	0 0 0	8 8		= 2			0.0	0.089	0.10 0.10 0.10 0.10 0.10	
Sodium	ž			8.5	1		1	× × × ×			- 1		× × ×				L		8 52	ł		8.52	- 1			8.50 8.50	- 1			- 1	× ×				*0 *2#C	8.823	- 1
Manganese	(wt (E)	0.945	0.73	0.612	106.0	0.794	0.862	0.801	0.797	0.753	0.758	0.885	808.0 788.0 118.0	0.817	0.852	0,761	0.952	0.87	0.858 0.91	0.88X	0.882	0.581 0.581	1 24	0.592	0.567	0.786			0.707	0.83	0.714	0.766	0 934	0.824	0.707	9.77.0 11.8.0 20.7.0	0.79
agnesium	(M1%)	1.317	1.27	1.248	525	2 4	1.189 1.181	1.144	1 196	1.164	1.174	1.28	1.184	1.195	% %	1.111	1.388	1.211	225	1 322	1 274	1.251	1.229	1.268	1.285	1251	1 285	2 2 2	<u> </u>	122	1.15	24.	1.296.	1.22	1.169	1242	1.169
L'Aham M		16.42	1757	× 5	1712	1 3 E	1719 1689	1678	1588 1587	1569	1557	1668	1645	1574	1893	<u> </u>	6171	1633	1566	49. 1.64	E 2.3	1776	E 2	87. 187.	1753	1684	Ē	584	1617	1632	737	_ Z	678	1.63	624	721	1.71
Potassium L		10,01	0.027	0.031	0.079	0.036	-0.152 -0.098	751.0 751.0	0.139	0 162	0.106	0.248	0.168	0.03 0.13	0.1	0.094	0.084	0.054	0.03 0.03	0.179	0.21	0.124	0.201	0.152	0.202	0.235 0.167	0 223	0.05 7.00 7.00 7.00 7.00 7.00 7.00 7.00	0.084	97010	0.205	0.147	0.153	0.139	X 25.0	0.147	0.153
Ξ	(Mt-)	9.214 8.775	2.549	888	5 6 6 5 6	7.81	1,0%	7.924 X OK.4	511.7	7.78	x 48	8.613	8.7.8 2.7.8	9.213	* * *	7.98	9.013 8.25	8.28 8.25	7 S	8.152	8.22	6.35 8.92 8.00 8.00 8.00 8.00 8.00 8.00 8.00 8.0	5 64.5	g, <u>5</u> , 0,	5 8 8 E	8.24 8.621	X X	2 × ×	7.97	8.242			-1.			8.24 1.85 1.85	8155
Cupper	(wt%)				ł	0.000	1		0.009		- 1		0.0 4 10.0 4 10.0 10.0	-	-	0.007	0.007	9000		100		0.00 0.01	100	0.013		0.013	- 1	0.014			_	0.00 800 800 800 800 800 800 800 800 800	-1-		-	-	0.013
Chronium	(wt &)	1985	1052	2017	1083	990	1,341	8500 1901	\$501	1054	1054 000	1072	1071 9707 9707	1907	1064	1053	1063	11159	1.057	1167	6 17 8	1051	104	0.00	0.0.0	0.066 970.0 930.0				.,			-	_		0.055	
Calcium	(M1%)	0.912	0.682	155.0	0.79	0.53	0.945	0.741	0.763	0.726	0.783	0.85	0.819	0.761	0.864	0.769	0.963	0.799	0.885	0.879	0886	0.716	0.608	117.0 11.649 717.0	0.795	0.766	0.827	0.693	0.805	1.857	0.978	0.718	0.952	0.934	0.789 0.767 1.051	0.735	0.851
Born	(M1%)					187				2,97				2.45							2.65		. 1	201. 201. 27.	2.35		- 11	2.73		- t			- 1		2.02		
Aluminum	(MEGF)	2.576	2.142	55.5	2.485	2.221	3.111 2.416	2.183	2335	2.20% 2.373	2.26	2,388	2.512 2.281 2.446	2.321	2.432	2.124	2.681	2.352	2.345	2.509	2.501	1.915	1.73	2038	1.91	2437	2443	2.354	2.507	2.393	2.221	2.30H 2.319	2.576	2.5H4	2.309 2.141 2.624	2.2H2 2.321 2.15	2.199
allfate	(udd)		816 >				100 100 100 100 100 100 100 100 100 100	0 v v				2 E					< 974 < 1030	() () () () () () () () () () () () () (0901) V			18 8 1 18 1 18 1 18 1 18 1 18 1 18 1 18					168					× 160 180 180	< 1140
Phosphate	(mdd)	× 886	816 V	,			< 1060 < 1060	0.07 0.07 0.07 0.07 0.07				= =					1700. 1180.	1200				0601	< 10k0			< 1030 < 961 < 597	× 1060			126 >	986	< 1080				2 1 5 8 1 1 5 8 1 4 1 5	× 1080
Nich	(Бри		\$.				0 0 0 0 0 v	0 0 0 0 0 0	ļ			× 10.0 × 1.16	6 B				< 1070 < 974	0 00 V V				14900 < 1000 14400 < 10:0 1900 < 10:0	000			0.01 >	000				660				 !	8 2 8	< 1340
Nitrate	_		28900				22200	20/202				22500 22600	22500				21100	17800								23500	20200		:	22900	22600	23900				29500 27500 27500	27300
	_		\$ B	,			V V					0.0	v v		_		10 > 4974					0 10 10 V V V	′ ∨			< 0.00 1 0.00 1 0.00	V (160			F66 >	686	176>				× × ×	· V
Total Formate Chloride	(mdd)	× 886	828				o 10/01	0.010 0.010 0.010				0 0 0 v	980			'	< 1070 < 974	0.00	• •			5 9 9 0 0 0	> 1000	1		\$ 8 5 \$ 8 5	< 1000 ×			< 994	< 989 < 1080	L 6 >				× 11990 × 1140 × 1180	< 1140
Formate	(mdd)	32000	32100			•	2700	25100				4(500	3500				35600	32500				26200 22400 21900	2 PHX0			32000 34000 37500	30100			24900	26300	243tx0		-		3,000 3,2400 3,000 3,000	32500
Total	(-J								-																				*	T			-				
Density Hv	(m)	1.4.5	= 4		-		1.416	1 42				<u>4</u> 4	Ē.				1.377	35.				8 E E	=		<u> </u>	1312	1.318			113	33	<u> 3</u>	+			4 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1.13
Insoluble	(%14%)																														:		+		:		1
Calcinut In	(H)	8 G	47.13				2 5 9 8	5.6		**		2 4	- -	<u> </u>			38.89 38.73	2 4 3 2 2				78.5	37.05	:	:	79.77 79.55 18.51	5.05		···	26.85	37.89	37.65	-			413 43.58 42.55	42.2
Fotal	13.	50.38	50.39				49.38 49.51					49.45					43.86 43.97	41.54 41.82			:	40.52	41.29			4 5 4 4 8 2	5			42.13	42.9 42.29	42.26				47.08 50.03 49.23	
Sample		1-MA	3.84 4.84	S-MA	- ×	<u> </u>	1-15A 2-15A	4 HA	7 - F	7.5	5.5	7 H Z	4 4 4 4 4 4 4 4 4	¥. K.	55	ቷ፟፟፟ጟ	1-MA 2-MA	AMA AMA	S-MA	<u> </u>	115	A P A	4-MA	F E E	r r r	A A A	4-MA	<u> </u>	1 IL	- AA	3.NA 3.NA	4 4 4 4	A.	보고	4 4 4	2-MA	4-MA
Jank Butch		9. S.	8.8	8.8	556	556 56	5. 5.	5 5 5	57	25	5,2	SE SE !	5.35.35	85. 85 85. 85	8 , 8,	-58	65. 65.	8,89	-59	8 8	5.5	SME-60 SME-60 SME-60	12	\$ 8 8	5 5 5	60 (rem) -60 (rem) -60 (rem)	-60 (ren)	(Em) (Se) (Se) (Se) (Se) (Se) (Se) (Se) (Se	(man) (%) (%)	60 (Rem)	इंइ	इ इ	<u> </u>	द द	Ģ , Ģ Ģ	SME-62 SME-62 SME-62	62
Ĺ. <u>.</u>		N. N.	88	NS NS	3 8	N.S.	N S	N. S. S.	W SW	SM	N N	N N	N N N	WS WS	N. N.	NS SW	N. W.	<u>8</u> 8	SME	N. S.	S. S. S.	N W N	W.S	N N	SMS	SME	SW	N.W.	SW	X 8	S. S.	SME	8 8	N. N.	SME	WS SWS	WS.

Values it their detection limits (<) ware set equal it their detection limits.

Table 1: Sample Results for DWPF's Macro-Batch 1

(hpm)																	T											Γ						T							Γ					-
(mild)		-								•			1				1.				<u> </u>								-		† -						1			•						
(mid) (midi)		1				NEW							1	Ş							8620							XR41						×7.84	•						9964					
(wt:3:1	0.035	2				2700	0.0	100	0.0				1	0.00	0.079	0.083	er.				10.0	900	# B	6800				7 7	0003	7 7 7 7				600	0.059	0.087	0.00				0.00	900	8 3	800		
(M1%)	010					1.091	-	1.076	1.085	-				0.97	0.942	1.034					0.982	0.0 14.0	0.916	0.893				103.1	000	7 2				1 txsk	12.1	1.132	1.341			•	1122	2	58			
(wt%) (wt%) (wt%) (wt%) (ppin)	610	9 17	7	100	7.2	50.0	0.027	500	500	\$ 10 0 0 0 0	6	9 10 10	100	12	2 E E	500	170	5100	0.017	8 9 0 0 0 0	0.017	500	0.018	×	Š	* ×	0.0 0.0 6, 5	0.019	0.019	2 2 3 2 2 3 3 0 0	9100			18110	0.02	0.017	0.027		7	2 2 2 2 2 2 2	101 0	8	. S. S.	0.02	6 2 0 0	
(wf ^c r) (w)	23,799			23.43	915		1.37k		Syl	2 2	24.823	723	1024		22.701		5.07	£ £	2	28.33	22.25	23.39	24.886	803	96	25.08	5.725	21.482	21.76	25.	9 9	960	17.699	2 ×	23.517	23.359	2(14	281	= [≅]	× 79.	980	2	52.5	5.07	24.159	
	0.082 23			0.134 2.		0.111, 22		0.115 22	2110	20 10 20 20 20 20 20 20 20 20 20 20 20 20 20		0.152 25	0.1.25		0.1011 22		6110	0 115		2 2 2	0.078 2	, ,		0.00K4 23		7	0.065	0.104 21 0.086 21	0.101		0.1			0.0K2 23		0.088 23 0.094 21	17	7,000	0.094 23	0.088 23 0.152 24	0.1.23	0.096 22	0.094 22			
N) (3534	8.297 (8.907								<u>و</u> پ									× 2.	-1-						7 7 7				•		2 SEP.					i		× 5.			
(%	0,703	1	0.75	0.803	0.853	0.89 0.899	0.912	5 E	0.896	27.0	0,908	0.975	6.0	0.862	0.832	0.859	9161	808	0.854	0.80	0.723	0.763	0.679	0.732	1590	0.70						28.0	6690	0.821	0.835	0.826	0.908	0.787	0.872	0.865	0.874 0.874	0.848	0.84	0.8.56	0.831	
Ě	1.213	. 5	3 , 3	203	7 7	32K	=	 F ž	18	2 1	347	283	2 5	3	385	£ 5	چ	39.5	2 3	125	216	: <u>'2</u> 'j	g <u>.</u>	727		2.5	2 2	1.2; .215	88		2.8	3	969	1 2	2 E	¥.	124	2.5	(2	# S	42.4 768.	`£^`;	숙절!	, W	64.5	
(E. F.	3 -	13	_ :	2 2			_						-1-						Ξ.		-	;		- -	: - .			=	= -	2.2.2			- S -	-			- -		3 2 .					-		
(34%)		1				16.39							l								1739			-	1749					16.2				T		1621		_	24			55.4		1655		
(w1%) (w6%) (w6%) (w6%) (w6%)	0.147	0.084	980.0	E 6	0.129	87 S	=	6 12	6116	0.153	0.165	2 3	0.051	7	0.137	8 E	0 112	0.0	0.094	0.00	0.11	0.074	0.074	0.094	0.035	4	0.03	0,102	5 C	9.144	5 5	0.067	0000	0.126	0 0 S	0.129	0.186		0.026	0.019	0.165	0.161	0 5	0.157	0.168	
) (1)	7.495	6.699	7.63	- F	X X X	8.88 8.74	8. 78.	× × ×	x.63	× ×	X.656.	8.67 8.67 8.67	X X	17.7	8.465	7.949 0.010	X.457	2 X S	× 29	7.73 1.73	753	7.886	17 S	7.496	6.75	7.26	7.425	8.29 913	× ×	87.6	8.36	9.4%	5.57	ž.	x 32 34 34	8. ESB 9. ES3	7.976	7.812	2.0	8. 72.2 (0.974	10.8 71.8	2	(1)	2 20	7.869	
(*1*)	0.01	0.009	0, 0	0.012	0.012	0.01	E .	7 =	100	<u> </u>	0.017	5 5	0000	0.007	0.007	0.009	0.007	0.00	1000	0,000	0,000	D.CNUS	0,00%	0.012	80000	(F.C.D.)	O.CHUS	0.014	210.0	0.014	0.012	000	2000	6000	0.012	0.01	0.009	0.00%	000	0.003	110.0	0.011	0.000	0.012	0.013	
#(½)	2058	3000	1997	707	3.076	0.076	101	1048	3006	1078	107	3.066	8500	7.057	0.059	500	3.088	1089	9000	79	3,052	9000	<u> </u>	1055	31118	105	1.052	1087	2062	0.00	1057	100	105	700	99	20065	1000	900	90.0), 1072), 1005	1082	900	<u> </u>	11K8	2063	
(41%) (41%) (41%) (41%)	1627	5xx	765	718	0.65	0.876 0.936	19.12	160	0.92	116	1927	0.869	1821	80.6	7 5	935	0.955	2 0	728	1728	0.631	7.5	2014	1725	549	¥.	588	1.01	1351	102	1735	803	0.489	3.746	0.828	977	914	728	774	9KS	0.929.	929	7 7	0.983	1975	
(≥)		1				_			- [2.42	-					26.5							2.00		- 1				İ		6151						2 2	- 1					2.91	
(E)	2.177	,		5		2.627	2.589	2.576				2 5 9 K	ı	2.424	2.473	2.692		25.5			2.005	2.29	2.08					2.447	2.348	2.533	í		1.93	1	2.463	2.151	- 1				2.572	2 6418	2.556			
(ppa) (ppm) (ppm) (nt3) (nt3)						160	8	ž.					- 10	i i	£ 2						<u> </u>	, e .	<u>.</u>	. .				< 499 < 1000 < 1000	E 2					68.	() ()	 g				-	Ø 9		-··- <u>-</u>	-		
<u>3</u>						001			- -			-	× (8)	< 1100 × 1100	7 07.						1140 < 1140 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 < 1150 <	210 < 1	√ }`					C 10KB C 10KB	050 × 1	;				NO .	240 V	240 					< 1140 < 1050 < 1100 < 150	0.00				
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rdd) (rudd)		L				29400 < 8'2 29200 < 10:0	200 < 10	2 V 2	-				- 006	24500 < 1100	. S					-	26100 < 11-0 22300 < 119	700 < 12	- - -	-				2660XI < 10KD 2570XI < 10KQ	E > 00					11 > 00	24700 < 12-0	700.	-				30900 < 110 32400 < 10%	700 < 10				
						<872 29 <1020; 29								<1100 24						- 1	2 2	2.0	 E				- 1	< UKI) 26- < UKI) 25-					-		5 .Z 6 .Z		-				050 32	ë 75		-		
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(M1%)						38.78																						37.22	17.5																	
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(%)						46.97 46.58								47.48 4x.23							5 5 5 4			İ				28 55 56 65							2.05						% % % %				-	
	S-MA		, <u>, , , , , , , , , , , , , , , , , , </u>	****	4	1.14 2.114	Y Y	S.H.S.	YH.	 	E 12.	i i i	1-14A	2-MA	4-13A	V V	1.5	. 5	4 5	-	Y A	3.31A	Ž.	P.F.	7	4 2		¥ ₹ ¥ ¥ - %	4 8 4 A A	5-MA, 6-MA,	1.2 1.2	# #	<u> </u>	- MA	¥.	4 4 E X 7 . 5	A H	#1 <u>#</u>	11 is	12	A W	Α Υ 4	Y X		15	
																											•								. 1					Ī	!		:			
	SME-62 SME-62	SME-62	SME-62	SME 62	SME-62	SMEG	SMB-63	SWE	SMERS	SM: 63	SMS63	SMEG	SMS	SMS	SM: 64	SMS	SMS-64	SN	3 . Z	SME-64	X X	SMESS	SW.65	SM: 65	SM265 SM265	59 WS	SM: 65	SM 66	SME-66	SME-66 SME-66	SME-66 SME-66	SME-66	SME-66 SME-66	SME-67	SME	SME 67	SME-67	SME-67	SME-67	SME-67	SME-68 SME-68	SMLes	SML-68	SME-68	SME-68	1111

Table 1: Sample Results for DWPF's Macro-Batch 1

احِ	Mercury (ppm)					•	Ì									•	٦			-			-						***	Ī .															
evision 0			١							+				+			-				+						+			 			ļ			-	+-		-				•		
Kev	TOC TRC	:	130							ž	- E							(60)						3			-			120						(93)						9			
	Ē		0.046 84	ž	0.45	3 3	١.	٠.			₹. ₹.	2 2	X	§ .			١٠٠٠	0.085 97			4			022: 04	023	0.022				0.022 90	023	2 2	-			21.0		5 S	ا			11.4	. S. S.	i v	
	Zirconiur (w1%)																ı																												
	(w1%)		1.36	2	57	123				-	121	1261	3571	118				1037	1.082	801				1.203	5.3	1.27				187	22	127				1.49	7	1.517	3			1.47	1.41	1.612	
Ī	Tanium (wf.g.)	0.023	5500	0.05	0.0	0.024	10.01	900	0.017	9100	0.035	0.029	2	0.015	0.018	\$10.0 \$10.0	5100	0.035	0.086	0.07	9100	0.017	0.015	710.0	0.03	10.072	100	Î	0012	0.025	0.021	0.024	9100	0.021	10.0	0.022	8100	0.033	0.014	0.015	0.0	0.024	0.033	0.051	0.00
	150 II	1,959	23.451	160	22.867	2 32X	4.2×2	2.956	25.099	24.74	1,612	3 272 3 173	3.242	24.385	24.47	24.735	3.748	21.42	7 2 2	95	94	24.495	24.266	2.948	22.764	22 248 21 918	24.713	24.569	1,979	22 243 24.824	22.147	23.516	24.188	25.1194	24 092	97.5	57.72	23.343 23.566	3.314	25 (189)	25 242	543	23.358	22 479	fare.
ŀ	Nickel Ni (wt%) (w	1112 2	0.152 2		_	0.094	1		5 Ξ		- Z - E - E - E		2 6110	2 2 2	1116	2 2 2	2 1179 2	1112 1098 Z					0.101	_1	0.121				2 6600	1117 2	0.112 2		2 1111	82.5	22.2	213		0.165	F	0.105.2		2 1601	2 2 2		
-	Socium N	٦	81.6										25	GI 5			•	8.9%								91.6				× 8								7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7				7.	8.4% 2.8%		Gara
-	2 S	3.822	X68.0					× 6×	0.788	- 1	1.K96				1,947	0.879	- 1		6.98		97.	1933	0.94	l	0.921			6.9	868	1	0.841			9160	250			0.936	1	3,945	717.0	. I			1018
	Mangane (wt%)																						2 12						7 6			· **	2.2	'n' *	i'm' in	1						T			
	Magnesium Manganese (w1%) (w1%)	1.26	7.7	5	77.	11	Ξ		2. 3.	2 2	2	2 2	133	\$ 2	7. %	1.398	1.23	2 2	Z 4	7.3	2	7.	1.252	25	5.7	1.271	28	3.3	1.26	1 292	22.	1.32	1.23	1.27	1.263	25.	2	36	- 25	22	1.34	* E	9 5	123	-
+	E (2	639	762	76.9	89.	747	1.617	. S. S.	1.637	F 5	266	5 5	5	919	1625	1 898	552	3 6	1612	87	15.	[N]	8 E	1.636	1,676	657	699	4	9	1.613	595	858 676	169	676	586	ج اج ج	2	20.	195	88. 89.	719	723	637	98.9	enn.
-	4 mm (%	188	1,239) 224	1.142	177	1,2(19	2 2	0.204	20%	£	0.16	0.177	0.00K3	1.146	8 T T D	1109	5.5	0.075	1092	6507	-	1086	11085	1.02	1072	1.058	100	23	1.168	2 5	0.137	0,07 VG02	990	0.063	0.24	1.238	315	1054	5 5	7 W	0.24	1236	1751	151
	Potasskum (wt%)	آ چ۔								1				İ			-															i				ı			ł			1			
-	Jupper Irm (w1%) (w1%	18 8.16							13 X4	_1_							. ₁[.				·			Л.		12 9.817				14 9.01 12 882			<u> </u>			l						. І.	G ≈ ∞ ×		
		8	9, 0.018		0.03					П	٠.	5 0012 8 0.015			A C.		- [100		2				100 100 100 100 100 100 100 100 100 100	2 0.012	0.0			-	E 8	7 0.012 2 0.012	8 E	2 0.015		1 0017		4.5.0 4.5.0	1.		0.009	-1-	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-	910#
	Chronium (wi%)	90.0	0,209	0.0	8	0.0	0.0	000	0.067	0.075	000	0 0	0.074	0.0	2 2	¥ \$	ž	2 2	ě	5.5	2 2	ä	0.065		9.0	0.067	5.5	8 8	0,06	0,068	8 8	90.0	000	0.00	0.085 0.07	0.097	0.0	0.0	0.05	200	e 8	0.071	9 9	00	5
	Calcium (wt%)	0.973	0.858	0.86.5	× 2	1787	0.914	0.80	0.882	0.959	11.964	986	0.977	0.928	0.956	0.983	0.9X7	0.969	1.006	0.99X	0.9415	0.938	0.936	0.84 2.84	0.937	0.972	0.878	0.937	11.892	0.964	189 189 189	0.97	0.846	2 2	0.938	75,00	0.962	0.962	0.751	0.753	6.9	0.859	0 887 24.	0.955	560
-	Rren (* %)	260%					2579	2613	26.52	282		- •		2585	2507	2576	2412			—	797	.5	2589	2566			2593	2539	2539				2.932	277	2,92				2556	4 K	2797	7.58			
-		2.536	2.856	2.574	2.423	2.449	2.36	2.572	2.374	2525	\$7	2.696	2.538	2.537	2.623	2.499	2383	2.567	2.679	2.624 2.678	2.629	2.658	2623	2.4134	2.488	2.568	2,422	2.4Kg	2.162	2.683	2.419	2.631	2.573	2.596	2.702	2.559	2.492	2 465	52	2.54	2.589	2655	2.545	2.529	. [192
			< > 56.8. < > 29.1.	Æ	<u>.</u>	-	٠.		٠	7	12. 1.	.		-			-	2 S.			-			75	2 1000 2 74	, ve 1			-	2 2	2 9					1040) < 1000)		· •				30	<u> </u>	ŝ	
-	nate Sulliste n) (ppm)		<.48. <			. [, 75 75	× 10,01	0 0 0 0 0 0				·		V 12.50	220 150 150 150 150					1	- × 828 × ×				_	2 Q.						< 761 P	070 < 1					-	9:3		_
	Phosphat (ppm)	П		٧																										V V-	v v	_				i				i		1			_
	le Nitalie) (ppn)		\$ 5	991 × (20	; ;					25H > 10	\$ 5 Q							2 2 V V	^ <u>^</u>					0 < 899	\$ <u>\$</u>	0; < 951				2.2. V V	2 2					0 < 751	0 × 100	V.				0×11×10	2 2	0:11 > 0	_
	(ppm)	- 1	25980								26900							2,75			ļ				00.17 00.17 00.17					22200						00202			_				24700		_
	ere Employed		896							- 1	5							927							× 1000					7 7 2 2 3						(761 <1080							\$ £		
	(F) (F) (F)		% ×							- 1	× 954					:	1180	22.5	× 122		."			< 879	× 828 × 1000	96 >				9 9	\$ \$					< 761 < 1080	5.07		:	:		V 1100	\$ \$ \$ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	< 1150	
	(pam)		35100	31400	NA.	1				Heax	1700	23800		1			- Street	H500	SONO				• • • •	901	2200	S) SKI			-	325x0	31100					29100 2764X0	272(XI	Ř.		-		31300	30200	21100	
e o	Solids Solies Solids (2010) Hydroxide Formate Chieride Fluoride (wt%) (wt%) (wt%) (wt%) (wt%) (wt%)						_				•				:		t							T																				-	
	16. (16. 16. (16. 16. (16.		177	1,164	<u>-</u> -	\dashv	_			89	181	7 6					- -	9	3.8					80	5 4 5	<u>=</u>			.	% €	7 7					1.44	8 5		-	+		242	5 G	24.	_
ible :	<u> </u>					+				1	42.45			-	:			8 8						-				·							<u> </u>		-:-	· !	-		:	-		<u></u> :	
d Insolt	Z.		=:=	ž.		_				1				<u> </u>			1							ļ.,	नाका	:				c	r. 194		 .			· ·		:			· :			:	
Calche	Sollis (W15)		423								4369						ı	. E						1	3 3	- 1			. 1	2.23						38.85							2.5		
Total	Solids (wt%)	1	7 5				·	٠,.٠,	. - , ,		49.71					رد. ردد.	- 1	\$ 5							50.34			:		47.72						43.3							5 Z		
	Sample	č	Z W Y	ž	× × ×	VW4	<u> </u>		4.4	ė į	2MA	A A	SMA	7 7	5 %:	* * .	ė W	2MA	4 WA	5MA 6MA	1.5	7.4	, v. 4	¥.	YW.	SMA	± 7.	- 4	7	2 X X	4.44	A 2.4A	7.7	× 4	7.4	2 4 A	4 4 4 A	¥ 2	7.	. 1.	4 4	¥.	Y Y	4 M 4	
	Tank_Batch	l																	. :																		:	,		: '					
	Tank	NE-68	NE.69	NE-69	NE 63	VE-69	2 4	(S)	2 6 5	NE 2	N.E. 73	NE-70	NE-70	NE-70	9	2.2	2 E 1 E 1	6	NB 71	NE-71	6.71	5.5	12.5	E.72	22.9	E.72	E 73	E-72	E-72	9 m 0		2 7	2.2	2 2	6.5 5.5	6.74 6.74	214	SME 74	6.74	2.5	7 S 8	22.5	9.6	SM ² 75	1

Sample #'s indicate dissolution method for later SME and MFT batches.

Table 1: Sample Results for DWPF's Macro-Batch 1

2	Mercury (ppm)		T				T							
evision	L Carlo		1		·				-	<u> </u>				
울 -) (mda)		0,5%		9640			0956		s 2 2		974кі.		8620
	Girconium (ntS-)		0.028 0.028 0.028 0.027	0.00	1800 1800 600 8800 1800	S		0.072 0.073 0.072 0.073		0.057 0.057 0.057 0.057 0.051 0.051 0.051	2500	0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03		0.02 0.021 0.017 0.016 0.018
-	(wt%)		A 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	676	1 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		<u> </u>	2 2 1 2 1 3 2 1 3 2 1 3 3 3 3 3 3 3 3 3		5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	<u>=</u>	0.991 1.041 1.068 0.976 0.978		0.86 0.824 0.824 0.829 0.866
	(wt%)	2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	X 50 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			8, 8, 9, 8, 8, 8, 8, 8, 8, 8, 8, 8, 8, 8, 8, 8,	1	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	6.02 6.02 6.01 6.01 6.01	0.016 0.015 0.025 0.025	0.017 0.017 0.018 0.021 0.031
	(wt%)	23.885		202222	22.289 22.289 22.491 22.491 21.966 22.17			22.873 22.271 21.805 22.409	24.704 24.428 24.428 24.428	22.437 22.138 21.987 22.134 22.134 22.292 22.338 22.338	22 2 2 2 2 2 2	21.903 22.567 22.537 22.727 23.285 22.864	24.376 24.376 23.936 25.066 21.643	21.022 21.459 22.21 22.512 22.227 21.32 24.183
ļ	m Nickel) (#1%)	0.101			25 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			2 2 2 2 2 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1	1	,		= 6 = 6 = 6	1
-	(wt%)	\$ 22 SE	55 K K41 182 K,466 181 9.39 11 8.714 122 K.858		0.909 8.717 9.03 0.926 9.038 0.926 9.038 0.938 0		1	89 9.051 27 9.086 89 8.684 02 8.834 14 8.94	1	0.945 9.171 0.915 8.967 0.878 8.861 0.857 8.88 0.857 9.106 0.853 8.834 0.883 8.639	0.886 0.916 0.845 0.861 0.927	0.829 9 0.009 0.873 8.882 0.851 8.809 0.851 9.001 0.804 8.766	0.864 0.857 0.844 0.736 0.82	0971 8805 0941 8726 0947 8854 0947 8854 0947 8432
	Mangan (41%)							ŀ						
	(41%)	22.1	66 2 5 3 2 3	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1222	6 2 6 2 6		25 C S S S S S S S S S S S S S S S S S S	82.2	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	22.22.22.23.23.23.23.23.23.23.23.23.23.2	1.32	18 18 18 18 18 18 18 18 18 18 18 18 18 1	1.380 1.380 1.435 1.275 1.335
	(*(%) *)	1559 1602 1572	1569 1634 1624	1587 1587 1586 1571 1434	588 572 572 572 573	8 8 8 8 8		<u> </u>	156 156 156 156 156 156 156 156 156 156	107 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1862 1892 1893 1893 1893 1893 1893 1893 1893 1893	25.1 1.65 1.65 1.705 1.865	632 832 832 833 833 833 833 833 833 833 8	1631 1.63 1.63 1.67 1.67 1.578
	(*t%)	0.045	0.187 0.158 0.16 0.19	0.129 0.067 0.081 0.044 0.168	0.245 0.245 0.234 0.234 0.192	0.15 0.143 0.159 0.174 0.279		0.174 0.174 0.207 0.186 0.186	0 123	0.119 0.146 0.148 0.157 0.157 0.162	0.164 0.231 0.231 0.221 0.221	0.087 0.079 0.115 0.115 0.102 0.102	0.175 0.129 0.125 0.12 0.12	0.02x 0.05 0.016 0.024 0.013
	(* t*)		ſ	Į.	8.83 X 8.	ľ		2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2	X X X X X X X X X X X X X X X X X X X	21.2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		1		1 1
	(v1%)		0.0013 0.0012 0.0012 0.0012 0.0013			000000	1	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	1		0.017 0.018 0.018 0.018 0.017 0.017	1	0.014 0.014 0.014 0.016 0.014	
	(*E)	2501 2501 7901 2001	107 107 107 107 107 108 108	2003 2003 2003 2003 2003 2003 2003 2003	201 150 150 150 150 150 150 150 150 150 1	200 200 200 200 200 200 200 200 200 200		1064 1065 1065 1065	1084 1188 1188 1083	1065 1065 1065 1065 1065 1075 1075 1075	200.00	1051 1061 1061 1059 1050 1050	1067 1073 1066 1069 1069 1071	0.05 0.05 0.05 0.05 0.05 0.05
	(# (#)	0.864 0.937 0.828	0.954 0.841 1.221 0.91	0.883 0.787 0.76 0.76	0 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.977 0.977 0.978 1.283		1.05 1.05 1.014 1.015 1.025	0.985 0.976 0.946 0.946	1.025 1.033 1.033 1.033 0.945 0.938 0.938 0.939	0.957 1.028 0.972 0.972 1.024 0.941	0.93 0.931 0.943 0.883 0.883	0.935	0.937 0.935 0.943 0.824 0.905 0.904
	(wt%)	8,8,2,2	l .	2.23 2.29 2.29 2.39		23.7.2.5.3.5.3.5.3.5.3.5.5.3.5.5.5.5.5.5.5.5			2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1	2.62 2.63 2.63 2.63 2.63 2.63 2.63 2.63	4	267 258 258 2702 2702 2702 2703	2.616
	(wt%)	2.383	2513 2481 2487 2483	2.28 2.79 2.159 2.358 2.358 2.358	2.7.2 2.7.17 2.7.13 2.7.13 2.81 2.81	2639 2639 2639 2655 2769		2.62 2.777 2.59 2.666 2.666 2.666	2683 2714 2714 2581 2674	2.73 2.73 2.65 2.65 2.65 2.65 2.65 2.65 2.65 2.65	2.734 2.535 2.536 2.567 2.704 2.704 2.704	2 5 2 2 2 3 5 6 2 4 18 2 3 6 2 6 3 6 3 6 3 6 3 6 3 6 3 6 3 6 3 6	2.407 2.534 2.138 2.174 2.103	2.553 2.481 2.497 2.502 2.502 2.502
	(udd)		05 05 05 05 05 05 05 05 05 05 05 05 05 0		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		1280 1480 1491	· v v		1750 1 320 1 230 1 230		900 H 5		8 8 8 8 8 8 8
	(nudd) (ndd)		200 200 300 300 300 300 300 300 300 300		2018 2010 2010 2010		1140 < 1000 < 1120 < 735	240 2240 2310 2310 2010		2040 2140 2220 2220 2220		2050 1990 1820 1640		2340 2290 2380 2140
			* * * * * * * * * * * * * * * * * * *		2 2 2 2 2 2 2 2 2 2 2 2 2		< 838 < 7.5 < 100 < 1120	< 1100 < 1100 < 1200 <		28400 < 908 28400 < 110 28400 < 110 29000 < 103		601 × 001 ×	:	0 0 0 0 0 0 0 0
	_ `		120 27500 1020 26700 140 26700 160 25900		220 28301 190 27200 210 26500 240 25500		8 31000 15 30600 00 29400 90 22200			* 0 0 0		25200 24700 11 21700 10 21200		0 27200 0 27200 0 26200 0 26100
			V V V V	ļ	V V V V		18 < 818 15 < 735 10 < 100 20 < 120			\$ 2 2 0		3:9:5 S		0.00 v 0.00 0.00 v 0.00 v 0.00 0.00 v 0.00 v 0.00 v 0.00 0.00 v 0.00
	Hdd)		62 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0 0 120 0 0 130 0 0 1210 0 0 1240	ļ	0 < 735 0 < 735 0 < 100 0 < 120			4 - 90X		0 0 10%0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	Solids Solids (g/ml) Hydroxide (ppm) (ppm) (ppm) (ppm) (ppm)		38200 38200 38800 38800		Melen Melen Melen Melen Melen		3734X1 3160X0 3424X0 3424X0	E75 # # # # # # # # # # # # # # # # # # #		3370 1437 1437 1437 1437 1437 1437 1437 1437		37000 37000 38000 36500	·····	3.40xx 3.40xx 3.30xx 3.30xx 3.30xx
Total	Hydrm) (eq/L)		g σ 10 →	ļ	a.w. a.r.		5 K K K K	r 0.8 8		r a m' c		∕c;4,9,∺,		S-2-8-2-
ale) (E)		0.4.1 0.4.1 0.4.1 1.4.1 1.4.1		<u> </u>	na mna pro pr a	1.43	2223		E () () () () () () () () () (\$ 1 5 E		245 275 1.66 1.16
lusolul	Solid (verse)				- v. 7 x		* N 4 4	***		7 6 8 2		(a) x (x (v (v (v (v (v (v (v (v (v (v (v (v (v	:	K 10 7 3
Celcino	s. Selle): (*1%		4 1 2 4 1 2 3 4 1 8 8		2 2 4 4 4 2 3 4 4 4 4 4 4 4 4 4 4 4 4 4		2 4 4 2 2 4 5 4 5			2.2.2.2. 2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.		43.8 43.8 43.8 43.8		8 4 4 4 8 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
Total	Sample Solkts (wt%)		MA 50.01 MA 50.14 MA 50.51	A	1-MA 50.68 2-MA 49.75 3-MA 50.00 4-MA 49.12 5-MA		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1-84 5191 2-84 5161 3-84 5208 4-84 5207 5-84 5207	<u>트</u> 및 및 및	48 48 48 48 48 48 48 48 48 48 48 48 48 4		1-MA 49.03 2-MA 49.11 4-MA 49.11 5-MA 49.03		1-NA 49.77 2-NA 50.15 3-NA 50.15 5-NA 50.15 5-NA 50.15
			 고성천출호(<u> </u>	12 2 2 3 3 3 :			<u> </u>	: "		=	= 2 2 2 2 2 E		TY 2 2 2 2
	Jank Hatch	27.27.27.27.27.27.27.27.27.27.27.27.27.2	8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	SM5.77 SM5.77 SM5.77 SM5.77 SM5.77	7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.	6-77-2 6-77-2 6-77-2 6-77-2	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	87.4 87.4 87.4 87.4	SME 79 SME 79 SME 79 SME 78 SME 79 SME 79 SME 79 SME 79 SME 79	E79 E79 E79 E79 E79	2.2.2.2.2.2	9.2121212 9.2121212	8 8 8 8 8 8 8 8 2 2 2 2 2 2
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Values at their detection limits (<) were set equal to their detection limits.

Sample #'s indicate dissolution method for later SME and NFF batches.

Table 1: Sample Results for DWPF's Macro-Batch 1

٦	È É		1	<u> </u>	Т		T		Γ	T			1		
	Mercury (ppm)				ļ				ļ	*	ļ		ļ		
	(bpm) (ppm)						=		9				ş		2
	 		0.017 0.023 0.023		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	<u> </u>	0.051 0.051 0.053 0.049		0.035 812 0.028 0.038 0.031		0063 0063 0063 0063 0063		0.055 0.053 0.053 0.053 0.052		0.056-1024 0.056 0.057 0.058
	(#4%) (#4%) (#4%) (ppm)								İ					i	
İ	ranium (*1%)		0.869 0.955 0.955 0.898 0.898	-	1.133		0.764 0.764 0.066 0.066		1275 1.479 1.462 1.888		1.183 1.149 1.149 1.114 1.153		0.938 0.938 1.051 1.057 0.987		1.043 1.045 1.066 0.939
-	itanium (#1%)	11000 0 11000 0 1000 0		0.012		V 7 3 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	4 3 5 4 5 6	0.02 0.02 0.017 0.017	0.015	000 3 000 3 000 3	0.021 0.017 0.016 0.017 0.017	0 0 0 0 0 0	0.019 0.019 0.019 0.025 0.025	0.021 0.018 0.021 0.021	0.052 0.051 0.051 0.781
	Silicon it (wt%) : (v	2 14 2 14 2 18	20,713 22,06 21,873 21,873 21,239	1883 1883 1893 1893 1893	22.939 22.952 22.976 22.976 22.244	29.386 26.395 24.392 26.634 22.2013	22,676 22,18 25,146 22,413 23,273 23,203	2 2 4 8 4 8 4 8 4 8 4 8 4 8 8 4 8 8 4 8 8 4 8	22.4 2.353 2.876 2.421 1.973	5748 1741 1835 24.55	2.174 2.034 1.597 2.068 2.105 1.105	24.82 1,222 1,991 1,838 1,984	2782 2782 1858 214 2175 1665	1 489 1 143 3 0 26 4 x 2 5 4 x 2 5	2.467; 2.482 2.489
		3 2 2 3		0 103 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1	0.092 0.093 0.093 2 0.093 2 0.085 2	0 115 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.094 0.096 0.106 0.1	8 10 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.088 2 0.094 2 0.094 2 0.098 2 0.097 2	0.091 24.82 0.095 24.222 0.1 23.991 0.12 23.838 0.101 23.984	0.109 21.524 0.101 22.782 0.099 21.858 0.1 21.4 0.097 22.175	0.146	0.105 2 0.099 2 0.12 2 0.094 2
-	Sodium Nickel (mf%); (mf%)		× × × × × × × × × × × × × × × × × × ×	1	8.58 8.58 8.23 8.23		14 2 2 2 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		8 X X X X X X X X X X X X X X X X X X X		8.777 8.900 8.900 8.900		8 8 8 44 8 8 7 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		X 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
-	mese No	0.955	0.943	4	1			0.823 0.805 0.603 0.868 0.868	1	0.902 0.921 0.921 0.908 0.808		0.898 0.898 0.916 7.910 7.910	0.952 0.948 0.926 0.925 0.913	0.949 0.939 0.774 0.92	0.839 0.839 0.856 0.856
	n Hang			*****		6604 454 125 212					3 7 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3				
	agnestur (*E)	<u> </u>	1855555	157555	555555	2 4 2 4 2 B	225225	1.267 1.298 1.293 1.295 2.295 2.295	25.52	<u> 111555</u>	255225		1348 1348 1327 1317	552-5	2522
	IFTA FORMAND LIRIUM MARKAMIN, HANGAINESS MES (WES) (WES) (WES)	1623 1581 1598	549 1584 1584 1584	25 52 E S S	1623 1623 1585 1582	1932 1793 1752 1.48	1.63 1.63 1.63 1.63 1.63	1629 1745 1.627 1.627	. 705 . 705 . 652 . 659	1.669 1.654 1.676 1.676	1609 1609 1609 1603	1628 1638 1638 1644	1.603 1.603 1.603 1.62 1.62	1.65 1.505 1.638 1.619	16.22 16.28 16.49 16.44
	7. (F.	0.03 0.034	0.059 0.085 0.085	0.045	01196 01174 01174	0.042 0.078 0.078 0.078	0.108 0.108 0.108 0.108 0.121	0.098 0.148 0.143 0.127	0.123 0.155 0.166 0.154	0.14 0.15 0.116 0.104 0.084	0.14 0.133 0.096 0.097 0.096	0 185 0 1 1 5 0 1 2 1 0 1 3 2 1 1 0	0.167 0.138 0.129 0.129 0.155	0.215 0.204 0.168 0.25 0.256	0.157 0.15 0.15
1.2	<u> </u>	22283	225 <u>7</u> 25	88.8 88.8 81.8 81.8 88.8 88.8 88.8 88.8	\$ 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	9.624 8.76 9.63 8.82 8.82 8.82	25 E E E E E E E E E E E E E E E E E E E	8.89 6.43 8.21 8.21	2	2.25.88	2	17.8 5 5 17.1 17.8 5 5 7.7 1.2 17.8 17.8 17.1	. 176 1.184 1.177 1.454	23 23 45	8 2 2 8 2
					1	_		0.022 8.8 0.002 8.4 0.0015 8.4 0.0015 8.4	[∞ ∞ ∞ ∞ ∞	4 9 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3 & 3 & & & &	55455	0.012 K.C. 0.012 K.C. 0.012 K.C. 0.012 K.S. 0.010 K.S. 0.010 K.S. 0.010 K.S. 0.000 K.S.
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,	Service of the servic	-8888		<u> </u>											
	(w1%)	0.914 0.881 0.916 0.926	0.904	0.92 0.896 0.914 0.921 0.923	0.894 0.890 0.876 0.89		0.846 0.529 0.529 0.801 0.801	0.90% 0.923 0.616 0.862 0.952 0.86	0.902 0.948 0.937 0.918 0.956	0.908 0.854 0.911 0.813	l i		0.988 0.911 0.947 0.967	0.993 0.972 0.861 0.989 0.989	0.928 0.928 0.919 0.892
	(*1*)	222		5 2 2 2 2 2 2 3 2 3 3 3 3 3 3 3 3 3 3 3		3.059 2.79 2.62 2.81 2.93 2.93	i e	2.126 2.126 2.126 2.621 2.656		2.21 2.21 2.45 2.27 2.63	t	8 8 2 3 2 8		2.27 2.42 2.45 2.689	
	(M1%)	2.576 2.484 2.586	2 2 2 2 2 2 3 2 3 3 3 3 3 3 3 3 3 3 3 3	25.25.25.25.25.25.25.25.25.25.25.25.25.2	2,594 3,026 2,629 2,55 2,629 2,653	3.159 2.846 2.626 2.858 2.501 2.439	2.513 2.472 1.901 2.469 2.445 2.63	2.537 2.626 1.936 2.438 2.524 2.434	2.417 2.557 2.462 2.499	2.546 2.487 2.526 2.535 2.49	2.373 2.616 2.541 2.528 2.659 2.598	2.561 2.5619 2.869 2.743 2.743	2.786 2.462 2.733 2.709 2.557 2.672	2.835 2.434 2.755 2.825	2.425 2.551 2.556 2.612 2.612
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tal Cal	Solids Solid (*1%) (*1%)				48.9 4 48.46 4 48.8 4		47.27		47.92 4 48.04 4 47.98 4		48.95 44.05 49.05 49.25 4	1	48.03 4 47.44 4 4 47.23 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	- 1	
To	Sumple Sol	다 <u>라 라</u> 타 다	<u> </u>	<u> </u>	2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4						* * * * * * * * * * * * * * * * * * *				1-MA 47.31 2-MA 47.74 3-MA 45.6 4-MA 46.37 5-MA
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Values at their detection limits (<) were set equal to their detection limits.

Sample #'s indicate dissolution method for later SME and MFT batches.

WSRC-RP-2000-00174 Eevision 0

Table 1: Sample Results for DWPF's Macro-Batch 1

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(81%)				900	8 8	8 5	<u>\$</u> \$					500	0.055	20.0	0.05				1900	90	900				0.03	0.082	0.0	8 8				900	6	0 0				9 9	0.073	0.072						0.216
11%) 0.948				0.885	\$660	1965	0.922					1.277	5.13	E.OR.	1,4178				1.359	ž	= <u>-</u>	-			1.189	1.21	1.228	2 5				K\$6.0	1,080	0.96				28.29	108	3						0.25
) (2) (0)	0.078 0.029	6100	600	0.013	7 0	2 2	0.015	8100	6 0 0 0 0	8100	0.02	8100	0.018 0.017	510.0	0.017	500	610	600	6100 8100	0.017	0.013	60018	0.023	0.021	81010	20 0 0 02	100	6 6	0017	8100	900	20.0	0.4123	0.024	0.02	1200	200	0.040 0.040	100	G 19	60024	0.023	2003			0.08
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11.76K	0.629	0.87	183	0.687	0.838	1 K	0.73	0.793	0.729	0.727	0.693	1960	2880	200.0	0.93	0.888	0.862	0.88	0.786	0.823	0.791	0.854	0.712	0.725	1.864	0.886	0.879	0.893	0.818	0.85	0.82	0.70	0.674	0.717	0.665	0.692	0.732	0.795	0 249	SIX O	0.698	0.752	0.741			<u> </u>
	1.099	\$	1317	1.225	1.279	7.7	188 188	1 2015	1 282	-	1233	9 5	274	306	325	1.216	173	1 222	1.164	1.172	1,229	1.205	323	17	1.178	<u> </u>	1.295	8 2	1227 1.2h5	1.278	235	26.1	181	1.19	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.191	168	1.189	1.239	5.52	200	# 55 133	1.117			288
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(wrs.)	0.133 0.056 0.087 0.02			1	8500		0.053 0.007	1	0.0891 0.015		0.067 0.015	Ľ	0.064 0.012			0.00 101.0	D.086 0.0				1900	Ι.		0.084 0.0	1-	0.066 0.01		9	0.072, 0.012	0.087, 0.01		1					. 1					0.071, 0.0	.J	· · · · · · · · · · · · · · · · · · ·		0.074
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Table 1: Sample Results for DWPF's Macro-Batch 1

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Silicon T	23.925	24 979	24.84	23.782	22.772	23.043	23, 497	24.559	25.35	74.31	23,624	23.166	23.503	23.635		24, 193 26,097	23.90	25.557	24.1177	25.112		22.914	23.964	22.865	23 823	24.396 24.57	5 ×	22.95X 22.903			23.759	22.35 21.584	21.537	72.079	23.017	22.283	23.568 23.862	22.623	7/957	23.2.98	23.447	
Nicket 3	0.22	0.22	2 2	0.313	1910	0 172	0.129	S S	701°0	7											0.087			<u>5</u>	0.097 0.098	0.078	500 C	0.311	0.25K	2 2	12 E	0.109	ĒĒ		0.107			0.092	- 1	# 1 0 0 0		
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ganese:	1.062	1.073	0.762	913	96.0	1843	0.863	0.766	0.926	0.863	0.879	0.826	0.814	746	0.58	0.67	0.985	0.817	0.912	X8.0	(8 ° 6 ° 8 ° 6 ° 6 ° 6 ° 6 ° 6 ° 6 ° 6 °	6.79	0.72	S X	0.818	0.684	1004X	0.902	0.882	0.87	0.90	0 84	25.0	, yes	0.833	0.862	0.822	2 2 3	1,189	0.83	0.885	
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dassium (91%)	0.712	0.744	0.267	0.286	D 208	0.163	0.195	0.135	0.132	0 :	1910	0 153	813	0.130	X200	0.08 80.0	0.00	0 101	0.071	0.079	0.113	0.055	0.00	¥ 100	0.081	0.065	20.0	0.094	0.192	0.18	0.20	0.097	0.126	171	0.162	0.11	0.08	2 5 5	y I To	0.00	0.00	
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opper (%)	0.312	0.281	0.286	0.256	0.165	Ž	0.356	a	0.365	0.337	0.126	0.32	0.32	0 5 4 C	0.256	0.32	0.384 0.328	0.373	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.153	95.0	0.313	X .	5	0.317	0.252	97.0	93.0	0.334	0.128	0.342	0.33	0 9 3 4 8 3	or I	0.339	0.337	0 0 8 8	0.376	0.350	9 9	0.378	•
onduns (8200	1072	Ş Ş	0.058	90.0	0.092	1080	540	3 5	0.053	7600	0.083	0.07	90.0	0.072	0.102	0.088	D 10	9.0	9711.0	0.086	0.073	90	200	0.069	0.00	900	0 148	0.074	0.07	0.071	0.069	0.067	701107	0.07	0.057	0 00	8 8 8	, S	0.076	0.050	
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Table 1: Sample Results for DWPF's Macro-Batch 1

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(*12) (*12) (*12) (*13) (*13) (*13) (*13) (*13) (*13) (*13) (*13) (*13) (*14) (*14) (*14)	2100	100	700			1100	0012	0.0XB	ĒĒ		0.012				0.02	200 000 000	0.022		0.037	0 0	500				0.037	0.034	8200 8200			1000	0.12	2000 2000 2000 2000 2000 2000 2000 200	E .		24.2	<u> </u>	240	
anium 2. *1%)	450	£ 3	= 5		,	1.031	0.931	0.857	0.954	8.37	1.00				1.017	- ×	301		0.776	0.683	717.0				0.915	. 0.928.	0.837			1 11 1	5660	1251	4		1.259	1 17	0.986	
) (2)	0.00	0.02	0.021			0.022	* * * *	0.017	0.032	150	0.031	0.031	0.028	9200	500	8.087 0.04	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	59 0	0.038 0.028	0.026	0.027	200	0.03K	0.03	0.022	0.023	0.022	1500	8000	0.033	0.019	0.00	0.02	0.023	0.021	000 S	0.02 0.02	0.589
452) (v	1077	23,990	7.5			5.16K 3.203	4 Z	4 1 1 X	2.818	507	3.139	24.255	21.36	20.67 5.142	22.805	22,095	21.525	2.976	4 736	4 284	24.87	24.15	6.761	6.364	23 507	3.168	21 216	8.651 6.467	6,073	1658	2.41k	20 514	1.217	5.182	1 686	2.911	25 29 25 29 5 638	9.396
w(%) ()	2 180	0.097	0.00%		,	0.095 25.168 0.106 23.203	200	0.097	0.096	0.078 24.105	2 2 2	0.087	2 XC00	0.0%2 0.0%5 2	0.109 2	0.159 22.095	0.116		0.091	0.096 24 539	0.087 24.87	0.104	0.087 26.761	0.074	0.0941 23 505	0.104 23.068	0.111.2	0.118: 28:651 0.143: 26:467	0.152 26.079	0.099 28.591	0.094 22.41K	128.	0.115 23.217	2 2 2	0 12 2	0.103 22.931 0.096 22.362	0.088	0.703
(*1%)	N 67	% % % %	× × ×			9.31				8 X X						8.80e	K. 82		8.50		K 43.		•			888 X						8.74				8.704 77.8		
18 mm (%)	0.733	9.8.0 0.88.0	20.0			0.722		0.84	0.72	0.657	0.83	0.791	0.74	0.541	0.821	0.883	0.722	0.768	0.654	0.63	0.637	0.863	0.623	0.625	0.828 0.882	0.862	0.791	0.87	18.0 18.0	0 K S	0.00k	1984	656:0	0.748	11.X64	- S	0.834 0.834 0.834	1.253
1 :	259	1 268 293	727			¥ ¥	7.738 7.738	. 2	7.9	66.5	, XZ	X 1	<u>=</u> =	1968	157	278	- 2	. 1 24.	225	, <u>8</u> , <u>8</u> ,	207	199	287	172	12 <u>8</u>	5 2 3	212	5 5	27.3	36.7	÷ 5	× 2	285	¥ 5	292	269	25 XV 75	263
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(84%)	0	0.063	0.0			0.0077 10.104	0.074	0.0	0.16	0.107	9	0.09	0.09	0.131	0.074	0.12	0.174	0.135	0.05	900 900	0.07	0.066	0.105	0.097	0.089	0.048	0.07	0.03	0.082	0.135	7 6	0.0	= 8	0.0	0.183 U.189	0.133	980	.08.0
1 S	7.91	8.23.8				Z Z			2.87	28.5	5	2 2	8.575	7.53	8.514	8.33	- 1		181	7.059	7.0K3	8. 8. 2. 24 2. 24		~ ¢	X 8.35	80 80 82 64 54 52 80	٩	5.5.5	8.112	8 89 2 5	8.475 8.475	¥ 5	78.6	8.116			8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	
(wt%); (wt%)	0.312	0.356			1	0.12		- 1	0.065		S	11156	0.057	0.062	150.0		0.037	0.038	0.03	0,012	100	0.023	0.021	0.016	0.015	0.017	9100	0.029	0.021	0.018	10.0		0.012		1		0.028	
(2,4)	0.058	0.061	0.06			0.065	0.067	3000	599	105	New	50.	8.0	1048	3.066	3,171	190	3084	3,066	1,062	2051	2,075	10.65	3.057	3.068	2 5 6	3075	1119	0 12	870. 70.0	11862	1083	57113	1067	0.07	£ 8	2901	£ 61
(%)	0.793	0.96 0.96	1.832 1.898			£ 9 5	0.826	0.823	92.0	0.671	18.89	1 6 1 4	0.742	0.391	0.833	11.861	1 667	0.849	0.673	0.628	0.651	0.813 0.827	0.686	0.645	0.854	6.893	1 3 E	0.819	0.78	0.83	0.827	014	0.759	0.626	0.916	0.865	0.852	0.858
() ()	276	2.194	279 2:K3	ļ		2.78 2.48	3 2 3	2.67				S 2	236	231			2.63	2.21	× -			2.d1	3.74	2.92		٠.		2.45	3.279	546			2.16	2.34	-		2.763	2.04
(wf?) (wf?) (wf%) (wf?) (wf?)	2.204	2.466	2.291	l		7 7 5	2.495	3	2.246	2019	2426	777	2.448	2.186	2.386	2.376 2.29X	2.194	2.386 2.286	2.122	2061	2.07	2535	2.272	2.042	2.588	2.54	2.149	2.539	2,42	2.484	2.476	2.867	2.849	2.463	2 489	2.502	2.512	
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Table 1: Sample Results for DWPF's Macro-Batch 1

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(w1%)		572.1 F72.1	74. X	287		1.528	242			I K	1058			<u> </u>	2 2 3			1.101 1.19%	10.05			1.1034 1.103	1.221			1.122	0.821	600
wts.)	0.045	27.70	0.02	0.022	0.022	200 500 602 700	0.02	0.024	0.02 0.02 0.02 0.02 0.02	0.025	0.02	0.02	6 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.026	2000	0.028	0.028	9000 9000 9000 9000	0.025	0.02K 0.027 0.026	0.027 0.09X	0.02 0.021	0.023	0.022	0.021	0.019	\$ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.024
(Mt/c)	25.502	21.064	22.754 22.498 22.719	22.27	24.54 24.54 24.54	23.8.19	0.109 23.113 0.121 23.017 0.116 24.044	0.03kg 25.563 0.107 24.795	25.548	23.734 23.88	0.105 24.247	25.56.3 26.182 25.388	25.144 25.229 23.816	23.337	22.74K 22.61S	0.117 24.879	25.003 24.603 24.603	0.105 24.107 0.117 24.509 0.123 22.472	22.921	26.941 24.422 24.459	0.107 25.257 0.077 25.33 0.115 27.44	22.959	22.779	24.746	0.069 24.486 0.087 25.98	23.867	0.081 24.012	25.072
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(w(3))	9C ~	0.834	0.805	2 8 8 0 0 8 8 0	0.818	88.9	0.918	0.854	858 B 858	0.812	0.754	0.713	0.759	0.851 0.85	0.931 0.918 0.844	0.912	0.858 0.832 0.832	0.772	0.811	0.887	0.763 0.763	0.775	0.742	0.865 0.869	1.73 7.74 7.74	0.776	7 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	0.767 0.748
(MIS)		1.245	245	246	1,307 1,307	55.52	1.306 1.31 1.273	1.266	52.25	7 E	177	# E E E	2.37 1.237 1.29	1.26	1308	<u> </u>	198	. 408 . 489	. 318. 1.318. 1.519.	1.192 1.192 1.294	286 1 286 1 - 1	1.245 1.305	1.256	1.302	2 % % 2 % %	67 E	2 2 2	23.7
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w19) (nth) (nth) (nth) (nth)	7 7	6.203 0.196	1880	2 2	0 122	0.22 I.I.S	0.153	0.13	1 X Z Z	0.172	77 III 0	0.076 0.075	0.077	0.126	0 149	0.159	0.177	0.167 0.165 0.162	0 125	0 10	0.208	0 169	6.155 0.145	0.138	2 2 2	0 0 1 34	\$ 5 E	2 2 2
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(*,34	0.90%	0.857	0.843 0.86	0.865	0.747	0.87	0.972 0.956 0.879	0.869	7 7 7	0.757	0.91X	0.73 0.715 0.71	0.77	0.859	0.976 0.964 0.842	0.852	0.728 0.779	0.804 0.927 1.014	0.83	0.952 0.625 0.79	0.771 0.771 0.901	1.896	0.309	20 0 20 0 20 0 20 0	0.772	0.785	0.85 7.54	0.759
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Tabk 1: Sample Results for DWPF's Macro-Batch 1

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24.669 24.721 35.065	21.784	25.297 23.341 27.94 22.197	22.744 22.744 22.744 22.058 22.766	21.286 21.286 21.556 21.129	90827		24.142 23.765 25.071 24.366	24.536 24.389 22.656 25.502	27.12 22.74 23.807 23.391 23.153 22.633	25.039 26.307 24.818	2 0.094 21.453 22 0.093 22.169 3 0.089 22.605 5 0.088 22.63	25.028 26.046 25.028 25.029 25.03	27 133 21.909 21.809 22.424 22.029	22 043
80.00	0.107 21.56	0,109 25,297 0,097 23,341 0,118 27,294 0,109 22,197	0.117 22.457 0.117 22.457 0.117 22.744 0.105 23.02 0.104 22.736,	0.1 22.477 0.104 23.299 0.1 23.556 0.114 23.329			0.003	0.005 24.636 0.005 24.836 0.007 24.389 0.009 22.656 0.004 25.502	0.095 27.12 0.095 22.74 0.079 23.807 0.143 23.153 0.103 22.633	0.101 25.039 0.109 25.48 0.109 26.407 0.098 24.818	0.094	0.000 25.029 0.0078 26.494 0.0079 25.595 0.0092 25.629	0.115 21.909 0.11 21.809 0.101 22.424 0.101 22.029	22 2
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0.787 0.787 0.787	0.934	0.837 0.741 0.861 0.836	0.935 0.935 0.934 0.934	0.876 0.879 0.896 0.896 0.84			0.657 0.522 0.522	0.526 0.532 0.501 0.501	0.851 0.862 0.882 0.893	0.81 0.75 0.75 0.75 0.75 0.75 0.75 0.75	0.811 0.851 0.73	0.756 0.781 0.831 0.831	0.949	0.923
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(A174) (A	0.196	0.137 0.00 0.066 0.086	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	25 5 4 3 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8			0.087 0.112 0.108 0.153	0.158	0.152 0.138 0.138 0.191 0.204	2 1 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	0 149 0 149 0 172	0.25 0.25 0.25 0.157	0.11 0.11 0.11	0.094
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Table 1: Sample Results for DWPF's Macro-Batch 1

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<u>.</u>	.0100	0.02	0.01X	0.017	0.02	0.023	0.021	0.015	0.017	0.016	0.0161	6.01	0.018	0.019	8 0 0 0 0 1 5	0.016	10.0	0.014	910'0	0.017	0.014 0.014	1 2	9 X	0.02X	0.029	XIO	5 10 0	1 E	200	5100	0.018	6100	0.012	0.015	8,00 0,018	0.017	1200	0.01x	60019	6018	 	0.018 0.04	0.017	0.036	(E018)	0.015	5100	0.016	-10-1
\$ } }	24 443	24.683	S 758	2.129	22.541	2 48.0	× 2	22.8.1	23.821	3.458	24.21	22.425	23.16	5.272	24.481	25.01	7.513	2.104	22.246	5.458	20.642	18.4	4 ×72	=	21.764	2 tyk	6.371 4.748	7.161 5.082	5.63X	2.819	18.094	24.016	X 417	23.227	5 K K	4.26.I	2 555	23.232	1.987	Ξ.	5 5 5 2 7 2 7 2 7 2 7 2	3 554	2 6-12	2 706.	2.546	2.897	4.376	4.545	
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Table 1: Sample Results for DWPF's Macro-Batch 1

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	xonlum #13-)	100	7400	0.0	9700				72(1)	6.00	8 8			9500	0.055	0.056	0.034				150.0	0.039	5 0 0	0.052				0.048	2 5	0.1143	ž,		•		0.055	0.084	0.057			·	61.13	800	200	0.017		
	nhun Zu 1%)	1.084	X 20	Ē	1 245		• • •		1.201	1.2.1	1 167			- I 30 I	1.129	77	5 T				1 072	158	1 (1986)	5				0.KX2	77.	0.929	0.924				3 S	3 8	1.156				26.7	707	6 5 5 6 7 5	ž .		•
-	alom Un	34128	0.03	0.026	870	7017		2 0 2	2010	1022	6.03	9100	2007	1016	0.026	0.025	0.0	0.018	0.623	1,023	0.04	1033	1027	5707		<u> </u>	10 E	1026				, SI 94 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	E 17.	E	1, EF (10)	0.04	100	× 3	7 6100	910	0.02	Ž.	1200	¥2.91	7 2 3	1015
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-	15kg 15kg 15kg	0.102 2		0.103		1			0.112, 22.294	77 TH 77 TH 10 TH				0.116	0.092	0.086	0.092 24	0.072 25.726	0.099 26	0.073 25	0.107, 22.664	0.1114 22.296	0.09, 22	22 201 0		2 2	2 12 K	24 24	0.084 25		0.078: 25		0.082	27.5	0.11 22	0 109 25		0.101	0.10	0.11 24	0.244 23	6.609		0.843 22	0.139 33 0.107, 25	
	odium N MISE) (S	27.0			2 3	1					8.77×				8.908						8.901							1		8.585							8 K29 I						2 (XXX			
	Polassium J.Himm Magnesium Hanganese Sodium Nickel Silkon (Hanium Chanlum Alexanium; TOC TW Meecury), (n.18) (n.18) (n.18) (n.18) (n.18) (n.18) (n.18) (n.18) (n.18) (n.18) (n.18)	816.0	0.848	0.846	0.895	0.856	58.0	0.83	0.926	0.924	0.791	0.807	0.913	190	0.775	0.742	0.719	0.732	0.714	0.572	0.87 0.874	0.93R	0.887	0 XX	68.39	0.857	0.782	0.751	0 X X	0.761	1.741	0.689	0.775	0.759	0.974	0.983	0.862	5,0	6.919	0.954	0.919	S S	0.7%2	=	0.748 0.978 0.738	7 80
-	表 2 単元 元	162	71.2	127	9 50 2 60	SOL E	265	74 X	17.5	11.	262,	265	2 4 5	95	292	₹;	28.5	162	27. 27.	51-	1.27 29X	9	2.2	2HZ	502	23.5	284	296	<u> </u>	303	247 248	X 55	202	207	12	319	E 12	303	£ 8	38.5 266.	297	268	1.25	150	684 124	2.17
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	Potassium (w1%)	6.07	9 9	60.0	5 d	0.0	700	0.084	0.174	6	0.27	0.05	0.00	0.20	0.195	6.15	1770	800	600	87	0.128	0.0	<u> </u>	2 0	2	92.0	0.102 0.098	0.103	2 5	0.097	0.09	0.17	0.115	ã	0 32	0.17	0.172	810	0.0	0.127	0.209	0.176	0.24	2.26	0.095	0.11
	(wts)	35				ŀ							2.52	. L	2.5					- 4	8.5×			1				7 612					7.879	- 1	1 2 2 2				7 8	- 1			7.7.5	1 .	7.61	
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	hroniun (w4%)	31165	Z Z	0.0	0.0	5907	2000	1,066	1.073 2.014	7	1150	997	26.00 26.00 26.00 26.00	9507	1058 1058	1907	1087	1063	5803	1059	0 0 1 1 1 1 1 1 1	1088	901	187	5000	990	0.07	6501	1	900	1002	0.05	6.062	1919	200	1073	1062	6000	6.0	11175	5 5	1803	0.07	X0.0	E E E	9.1
	alchum.i (wt%)	1.019	0.892	0.N70	0.923	1,845	0.733	0.726	1.042	3	0.72	7 2	0.879	0.709	0.727	0.776	5	0.593	0.634	965 0	# 75 5 5 5 5	0.986	26	2160	0.845	0.896	0.937	0.7X3	0.854	0.80	1 695	0.663	0.719	1,684	203	0.0	1.456	890	8	SOS	0.768	0.876	0.792	0.955	0.759	0.821
1	(w1%)					211.5 2.5%	2.59	2.63				2.43	2.55	2				2.11X	2.35	27.12				2.618	2 607	2.635	2.58	-			2.465	2.389	2.628	255				256	2.6%	252		•		2.54	2.73 2.73 2.73	2.575
	uminum (wt%)	2.697	2.438	2.402	2.536	2.519	2.528	2.42	2.756	2.714	2.257	2.558 2.561	2.692	2.131	2.245	2.408	2.5	2.159	2,441	666	2.547 2.538	2.672	2.599	2 495	2.519	17.	2.616	2.366	2417	2.353	2.348	2.129	2.355	2.234	2.614	2 6.92	2.389	2 586 2 682	2.578	2638	2621	2.534	2.298	2.409	2.2	2 392
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F	Sample Solids Solids (Mark) Hydroxide variant Characterination (ppm) (pp		3-11A	4-15.4 4-15.4	6-MA	<u>4 .4</u>	÷ 4.	- L	1-MA 2-MA	3-MA	S-MA	- K	<u> </u>	1-MA	3.4A	4:NA 5:MA	AMA F	1	1 2	4	Z N Z	4.4 4.4 4.4	S.A.A.	1	14. 14. 14. 14.	[<u>14</u>]	4	I-MA 2-MA	Y.W.Y	4 4 4 4 7 4	٠,	¥. T .	<u>14</u>	-NA	N S	N-N-	6-NA	n n	<u>14</u> 14	1	7-N-2	4 X X	S-NA 6-NA	E W	("#\"\#\"\# :	1
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ـــــ	- 1:	_ 2	. 4.	- 2	. <u> </u>		<u>e 2.</u>	z	< ×.	K 2	قائب	2 5412	22	14 2	. 2	42	4 2	22	٠	212	. 2	<u> </u>	22	12	27	2.2	<u> </u>	≥Σ	2.2	2 2 2	£ }	4 2	2 2 3	<u> </u>	2.2	Σ	≥ ⊠ :	ZΣ	Z Z	Z[Z	: (<u>Z</u> i	2.Σ	ZZ	<u> </u>	 	Ē.

Sample #'s indicate dissolution method for later SME and XFT batches.

Table 1: Sample Results for DWPF's Macro-Batch 1

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20.02	3 22 275	5 22.466			3 25.511 6 26.154		22.38	0.12 23.598		0.103 25 079	0.111 23.541	0.12 26.53	6 22.879	7 23.05	0.114 22 648	9 22.96 8 24.95	0.115 23.882 0.118 28.28	~ .	6 26.45	R 23.97	0.092 24.754	6 24.658 H 24.867	5 25 13	27.854	27.73	23.43	0.122 23.645	0.134 23.04	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.13 26.204	28.06	0.114 22.10	7 22.52	0.119 22.702	10X 24 SA	0.117, 24.061	22	3 24.49 9 22.8	0.173 22.209	2 22 54	2 23.08
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Table 1: Sample Results for DWPF's Macro-Batch 1

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Table 1: Sample Results for DWPF's Macro-Batch 1

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Table 2: Components of Variation for SRAT Receipt Sample Results

Data from Batches 22-93		%	Сотвро	ments of Va	riation	% Coeffic	ients of Va	ariation
Analyte	Mean	S. E. Mean	%Batch	%Residual	Variance	Total	Batch	Residual
Total Solids (wt%)	15.811	2.1%	98.6%	1.4%	1.923	8.8%	8.7%	1.1%
Calcine Solids (wt%)	13.432	2.0%	90.9%	9.1%	1.068	7.7%	7.3%	2.3%
Insoluble Solids (wt%)	12.011	3.9%	76.8%	23.2%	0.508	5.9%	5.2%	2.9%
Density (g/mL)	1.078	0.5%	76.7%	23.3%	0.001	2.4%	2.1%	1.2%.
Total Hydroxide (eq/L)	0.177	2.7%	25.6%	74.4%	0.0004	11.3%	5.7%	9.8%
Format (ppm)	4139.2	4.6%	94.4%	5.6%	662514.2	19.7%	19.1%	4.6%
Chloride (ppm)	1025.4	4.5%	21.1%	78.9%	10304.7	9.9%	4.6%	8.8%
Fluoride (ppm)	1025.4	4.5%	21.1%	78.9%	10304.7	9.9%	4.6%	8.8%
Nitrate (ppm)	12441.3	2.6%	87.4%	12.6%	2056380.9	11.5%	10.8%	4.1%
Nitrite (ppm)	7276.5	1.7%	86.8%	13.2%	288907.2	7.4%	6.9%	2.7%
Sulfate (ppm)	1075.5	1.7%	52.7%	47.3%	8879.6	8.8%	6.4%	6.0%
Aluminum (wt%)	6.764	2.0%	53.3%	46.7%	0.082	4.2%	3.1%	2.9%
Boron (wt%)								
Calcium (wt%)	2.441	4.3%	83.0%	17.0%	0.039	8.1%	7.3%	3.3%
Chromium	0.180	7.6%	25.2%	74.8%	0.001	20.2%	10.1%	17.5%
Copper (wt%)	0.326	21.5%	97.8%	2.2%	0.015	37.6%	37.2%	5.6%
Iron (wt%)	25.958	2.4%	73.6%	26.4%	1.420	4.6%	3.9%	2.4%
Potassium (wt%)	0.039	27 4%	66 2%	33.8%	0.000	55.3%	45.0%	32.1%
Magnesium (wt%)	1.233	5.8%	82.8%	17.2%	0.018	10.8%	9.8%	4.5%
Manganese (wt%)	2.737	2.3%	73.9%	26.1%	0.015	4.5%	3.8%	2.3%
Sodium (wt%)	6.413	9.1%	77.0%	23.0%	1.236	17.3%	15.2%	8.3%
Nickel (wt%)	0.297	2.9%	90.5%	9.5%	0.002	15.2%	14 5%	47%
Silicon (wt%)	0.843	21.1%	63.4%	36.6%	0.132	43.1%	34.3%	26.1%
Titanium (wt%)	0.016	24.5%	57.7%	42.3%	0.000	51.5%	39.1%	33.4%
Uranium (wt%)	2.861	2.2%	72.6%	27.4%	0.015	4.3%	3.7%	2.3%
Zirconium (wt%)	0.027	51.0%	55.8%	44.2%	0.001	108.8%	81.3%	72.3%
TIC (ppm)	584.606	6.0%	94.9%		22792.786	25.8%	25.2%	5.8%
Fe/Al	3.838	0.8%	29.3%	70.7%	0.006	2.0%	1.1%	1.7%

Table 3: Components of Variation for SRAT Product Sample Results

Data from Ratches 22-93		%c	Compo	onents of Va	riation	% Coeffic	% Coefficients of Variation				
Analyte	Mean	S. E. Mean	%Batch	%Residual	Variance	Total	Batch	Residual			
Total Solids (wt%)	22.334	1.7%	93.0%	7.0%	2.591	7.2%	7.0%	1.9%			
Calcine Solids (wt%)	17.552	2.0%	87.6%	12.4%	2.463	8.9%	8.4%	3.2%			
Insoluble Solids (wt%)	14.809	5.2%	64.9%	35.1%	2.997	11.7%	9.4%	6.9%			
Density (g/mL)	1.147	0.5%	72.2%	27.8%	0.001	2.3%	1.9%	1.2%			
Format (ppm)	20902.8	5.0%	89.0%	11.0%	21206134	22.0%	20.8%	7.3%			
Chloride (ppm)	1074.6	1.7%	45.9%	54.1%	10268.7	9.4%	6.4%	6.9%			
Fluoride (ppm)	1081.4	1.7%	38.2%	61.8%	11180.0	9.8%	6.0%	1.1%			
Nitrate (ppm)	36598.2	2.8%	84.0%	16.0%	20783674	12.5%	11.4%	5.0%			
Nitrite (ppm)	1109.7	4.2%	87.4%	12.6%	42802.3	18.6%	17.4%	6.6%			
Phosphate (ppm)	1084.1	1.9%	50.0%	50.0%	11146.4	9.7%	6.9%	6.9%			
Sulfate (ppm)	1213.5	2.5%	70.8%	29.2%	21048.6	12.0%	10.1%	6.5%			
Aluminum (wt%)	6.214	1.5%	68.1%	31.9%	0.223	7.6%	6.3%	4.3%			
Boron (wt%)											
Calcium (wt%)	2.012	1.6%	67.8%	32.2%	0.022	7.5%	6.1%	4.2%			
Chromium (wt%)	0.162	1.4%	12.2%	87.8%	0.001	15.8%	5.5%	14.8%			
Copper (wt%)	0.135	55.3%	99.9%	0.1%	0.093	225.1%	225.0%	7.5%			
Iron (wt%)	23.474	1.6%	76.9%	23.1%	2.844	7.2%	6.3%	3.4%			
Potassium (wt%)	0.040	10 0%	76 1%	23.9%	0.000	45.1%	39.4%	22.1%			
Magnesium (wt%)	0.945	2.3%	64.9%	35.1%	0.011	11.2%	9.0%	6.6%			
Manganese (wt%)	2.450	1.6%	82.1%	17.9%	0.031	7.2%	6.6%	3.1%			
Sodium (wt%)	7.168	3.6%	83.0%	17.0%	1.302	15.9%	14.5%	6.6%			
Nickel (wt%)	0.268	1.8%	43.8%	56.2%	0.001	0.0%	6.6%	7.4%			
Silicon (wt%)	0.711	4.9%	51.5%	48.5%	0.033	25.6%	18.4%	17.9%			
Titanium (wt%)	0.019	18.8%	77.0%	23.0%	0.000	84.9%	74.5%	40.7%			
Uranium (wt%)	2.647	1.6%	75.3%	24.7%	0.036	7.2%	6.2%	3.6%			
Zirconium (wt%)	0.017	17.5%	74.4%	25.6%	0.000	80.0%	69.0%	40.4%			
Fe/Al	3.781	0.8%	62.7%	37.3%	0.021	3.8%	3.0%	2.3%			

Table 4: Components of Variation for SME Sample Results

Data from Batches 22-93	Diss.		%	Comp	onents of Va	riation	% Coef	ficients of '	ariation
Analyte	Method	Mean	S. E. Mean	%Batch			Total	Batch	Residual
Total Solids (wt%)		48.821	1.2%	83.9%	16.1%	7.680	5.7%	5.2%	2.3%
Calcine Solids (wt%)		43.098	1.4%	78.9%	21.1%	7.316	6.3%	5.6%	2.9%
Insoluble Solids (wt%)		40.764	3.6%	91.9%	8.1%	7.000	6.5%	6.2%	1.8%
Density (g/mL)		1.415	0.7%	83.4%	16.6%	0.002	3.2%	2.9%	1.3%
Format (ppm)		32735.2	3.6%	83.4%	16.6%	28237665	16.2%	14.8%	6.6%
Chloride (ppm)		1159.6	11.4%	33.3%	66.7%	689330.2	71.6%	41.3%	58.5%
Fluoride (ppm)		1160.8	11.4%	33.3%	66.7%	689362.5	71.5%	41.3%	58.4%
Nitrate (ppm)		25244.1	3.8%	84.4%	15.6%	19549200	17.5%	16.1%	6.9%
Nitrite (ppm)		1159.6	11.4%	33.3%	66.7%	689330.2	71.6%	41.3%	58.5%
Phosphate (ppm)		1358.3	11.4%	40.6%	59.4%	838581.2	67.4%	43.0%	52.0%
Sulfate (ppm)		1205.4	11.0%	33.5%	66.5%	691804.8	69.0%	39.9%	56.3%
Aluminum (wt%)	PF	2.453	1.8%	41.2%	58.8%	0.0482	8.9%	5.7%	6.9%
1 1141111111111111111111111111111111111	MA	2.452	1.5%	51.2%	48.8%	0.0430	8.5%	6.1%	5.9%
Boron (wt%)	PF	2,645	1.0%	26.5%	73.5%	0.0294	6.5%	3.3%	5.6%
201011 ()	MA			Not.	Available for	this Analysi	s.		
Calcium (wt%)	PF	0.823	3.6%	58.0%	42.0%	0.0169	15.8%	12.0%	10.2%
Calciam (wtw)	MA	0.877	2.6%	55.0%	45.0%	0.0157	14.3%	10.6%	9.6%
Chromium (wt%)	PF	0.074	8.3%	64.1%	35.9%	0.0007	34.6%	27.7%	20.7%
omonaum (w//s)	MA	0.069	4.1%	12.5%	87.5%	0.0005	33.4%	11.8%	31.2%
Copper (wt%)	PF	0.013	8.8%	41.9%	58.1%	0.0000	41.4%	26.8%	31.5%
Copper (with)	MA	0.070	40.6%	99.7%	0.3%	0.0152	175.7%	175.4%	9.8%
Iron (wt%)	PF	8.205	1.8%		57.4%	0.5392	8.9%	5.8%	6.8%
non (were)	MA	8.393	1.3%	44.6%	55.4%	0.4172	7.7%	5.1%	5.7%
Potassium (wt%)	PF	0.114	15.9%	70.4%	29.6%	0.0053	64.2%	53.9%	34.9%
r ottassiam (were)	MA	0.130	10.7%	84.8%	15.2%	0.0042	49.5%	45.6%	19.3%
Lithium (wt%)	PF	1.620	0.9%	15.9%	84.1%	0.0092	5.9%	2.4%	5.4%
	MA	1.674	0.7%	33.4%	66.6%	0.0058	4.6%	2.6%	3.7%
Magnesium (wt%)	PF	1.254	1.2%	34.3%	65.7%	0.0066	6.5%	3.8%	5.2%
	MA	1.275	1.0%	46.1%	53.9%	0.0058	6.0%	4.1%	4.4%
Manganese (wt%)	PF	0.830	2.5%	54.2%	45.8%	0.0086	11.2%	8.2%	7.6%
and the same of the same,	MA	0.849	1.9%	56.8%	43.2%	0.0074	10.1%	7.6%	6.7%
Sodium (wt%)	PF			Not.	Available for				
Bodium (W170)	MΛ	8.860	0.9%	50.3%	19.7%	0.2182	5.3%	3.7%	3.7%
Nickel (wt%)	PF	0.103	2.9%	34.3%	65.7%	0.0002	15.0%	8.8%	12.2%
11101101 (111111)	MA	0.105	4.9%	8.7%	91.3%	0.0020	42.4%	12.5%	40.5%
Silicon (wt%)	PF	24.523	1.0%	23.2%	76.8%	2.0754	5.9%	2.8%	5.1%
Smoon (were)	MA	22.881	0.8%	22.8%	77.2%	1.6687	5.6%	2.7%	5.0%
Titanium (wt%)	PF	0.020	7.9%	22.7%	77.3%	0.0001	46.8%	22.3%	41.1%
11	MA	0.026	17.0%	6.7%	93.3%	0.0016	153.3%	39.8%	148.0%
Uranium (wt%)	PF	0.020	17.070		Available for				
Cianan (wine)	MA	1,112	3.4%	78.0%	22.0%	0.0330	16.3%	14.4%	7.6%
Zirconium (wt%)	PF		±.,,,,		Available for				
Zii Comain (we)o)	MA	0.043	13.8%	97.1%	2.9%	0.0007	60.2%	59.3%	10.2%
Fe/Li	PF	5.076	2.1%	51.3%	48.7%	0.2281	9.4%	6.7%	6.6%
1011	MA	5.027	1.7%	54.6%	45.4%	0.2262	9.5%	7.0%	6.4%
Fe/Al	PF	3.348	0.9%	63.9%	36.1%	0.0161	3.8%	3.0%	2.3%
10/11	MA	3.429	0.9%	63.4%	36.6%	0.0260	4.7%	3. 7 %	2.8%

Table 5: Components of Variation for MFT Sample Results

Data from Batches 22-93			%	Comp	onents of Va	riation	% Coef	ficients of \	Variation
Analyte		Mean	S. E. Mean	%Batch	% Residual	Variance	Total	Batch	Residual
Total Solids (wt%)				Not A	Available for	this Analysi	s.		
Calcine Solids (wt%)				Not 2	Available for	this Analysi	s.		
Insoluble Solids (wt%)*		39.239	6.7%	0.0%	100.0%	41.182	16.4%	0.0%	16.4%
Density (g/mL)†				Not a	Available for	this Analysi	s.		
Format (ppm)		30804.3	4.3%	93.9%	6.1%	31834321	18.3%	17.8%	4.5%
Chloride (ppm)		1518.0	55.8%	99.7%	0.3%	12831852	236.0%	235.7%	12.2%
Fluoride (ppm)		1092.7	2.5%	73.0%	27.0%	16035.5	11.6%	9.9%	6.0%
Nitrate (ppm)		24556.9	2.7%	81.3%	18.7%	8893900	12.1%	11.0%	5.2%
Sulfate (ppm)		1147.6	4.1%	88.7%	11.3%	42709.0	18.0%	17.0%	6.1%
Aluminum (wt%)	PF	2.450	1.9%	40.9%	5 9.1%	0.0556	9.6%	6.2%	7.4%
	MA	2.457	1.5%	55.8%	44.2%	0.0355	7.7%	5.7%	5.1%
Boron (wt%)	PF	2.669	1.0%	21.1%	78.9%	0.0354	7.1%	3.2%	6.3%
Boron (merce)		2.712	4.7%	51.9%	48.1%	0.0304	6.4%	4.6%	4.5%
Calcium (wt%)	PF	0.795	3.5%	55.5%	44.5%	0.0163	16.1%	12.0%	10.7%
Carolain (*****)	MA	0.868	2.4%	56.1%	43.9%	0.0121	12.6%	9.5%	8.4%
Chromium (wt%)	PF	0.073	5.6%	57.9%	42.1%	0.0003	25.7%	19.5%	16.7%
Chroniaum (wese)	MA	0.069	3.7%	85.1%	14.9%	0.0010	46.3%	42.7%	17.9%
Copper (wt%)	PF	0.015	34.6%	82.4%	17.6%	0.0005	138.4%	125.6%	58.1%
Copper (were)	MA	0.074	40.3%	99.4%	0.6%	0.0157	169.5%	169.0%	13.5%
Iron (wt%)	PF	8.234	2.0%	44.1%	55.9%	0.6970	10.1%	6.7%	7.6%
Hon (wtw)	MA	8.385	1.5%	60.4%	39.6%	0.4211	7.7%	6.0%	4.9%
Potassium (wt%)	PF	0.131	15.3%	2.2%	97.8%	0.0279	127.5%	18.8%	126.1%
1 Otassiani (we/e)	MA	0.141	8.1%	69.9%	30.1%	0.0030	39.0%	32.6%	21.4%
Lithium (wt%)	PF	1.634	1.0%	13.8%	86.2%	0.0134	7.1%	2.6%	6.6%
Estinum (wt/8)	MA	1.685	0.8%	62.7%	37.3%	0.0044	3.9%	3.1%	2.4%
Magnesium (wt%)	PF	1.250	1.3%	16.4%	83.6%	0.0118	8.7%	3.5%	7.9%
Wagnesium (W170)	MA	1.282	1.0%	55.7%	44.3%	0.0043	5.1%	3.8%	3.4%
Manganese (wt%)	PF	0.820	2.6%	43.3%	56.7%	0.0118	13.3%	8.7%	10.0%
Manganese (We76)	МΛ	0.835	2.0%	57.5%	42.5%	0.0073	10.2%	7.7%	6.7%
Sodium (wt%)	PF	0.050	2.5.			this Analysi	S.		
Sodiam (west)	MA	8.846	0.8%	55.9%	44.1%	0.1409	4.2%	3.2%	2.8%
Nickel (wt%)	PF	0.105	6.4%	1.7%	98.3%	0.0032	53.7%	6.9%	53.2%
TVICKET (W170)	MA	0.108	4.9%	59.6%	40.4%	0.0007	25.3%	19.5%	16.1%
Silicon (wt%)	PF	24.668	1.1%	17.4%	82.6%	3.3443	7.4%	3.1%	6.7%
billeon (with)	MA	23.128	0.8%	55.2%	44.8%	0.9760	4.3%	3.2%	2.9%
Titanium (wt%)	PF	0.024	23.6%	0.0%	100.0%	0.0025	208.6%	0.0%	208.6%
Thanium (wt/b)	MA	0.024	8.1%	51.5%	48.5%	0.0001	43.8%	31.4%	30.5%
Uranium (wt%)	PF	0.025				this Analysi			
Cramum (wrw)	MA	1.124	3.4%	78.2%	21.8%	0.0308	15.6%	13.8%	7.3%
Zirconium (wt%)	PF	1,124	2.170			this Analysi			
Zircomum (wt///)	MA	0.044	13.1%	51.1%	48.9%	0.0010	70.6%	50.5%	49.3%
Fe/Li	PF	5.055	2.2%	51.4%	48.6%	0.2772	10.4%	7.5%	7.3%
1.5/1.5/	MA	4.991	2.0%	61.7%	38.3%	0.2473	10.0%	7.8%	6.2%
Fe/Al	PF	3.362	0.8%	48.5%	51.5%	0.0175	3.9%	2.7%	2.8%
I WAI	MA	3.416	1.0%	73.4%	26.6%	0.0280	4.9%	4.2%	2.5%

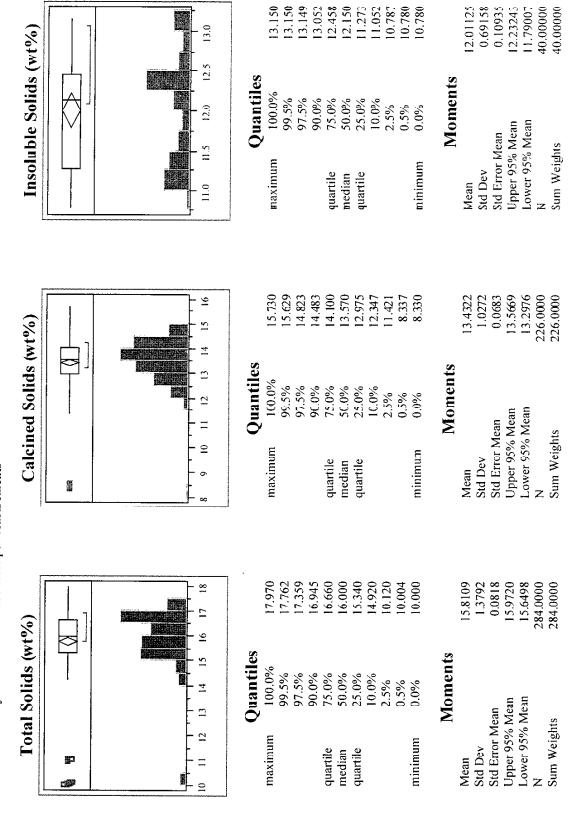
Table 6: Comparison of SME Sample-to-Sample Error versus PCCS Historical⁴

			s			P C	CS				
			Compo	nents of Va	ariation	% Coef	ficients	Historica	l (Hist)	Std Dev Ba	ised Upon
	Diss.		Stand	lard Devia	tions	of Var	iation		$% \frac{1}{2}\left(-\frac{1}{2}\left(t. Avg.	MB1 Avg.	
Analyte	Method	Mean	Total	Batch	Residual	Batch	Residual	Average	RSD	Std Dev	Std Dev
Aluminum (wt%)	PF	2.453	0.2195	0.1409	0.1683	5.7%	6.9%	2.222	5.1%	0.113	0.125
	MA	2.452	0.2073	0.1484	0.1448	6.1%	5.9%	2.222	5.1%	0.113	0.125
Boron (wt%)	PF	2.645	0.1716	0.0884	0.1470	3.3%	5.6%	2.093	7.2%	0.151	0.190
	MA						for this Ana				
Calcium (wt%)	PF	0.823	0.1300	0.0990	0.0843	12.0%	10.2%	1.077	5.9%	0.064	0.049
	MA	0.877	0.1254	0.0930	0.0841	10.6%	9.6%	1.077	5.9%	0.064	0.052
Chromium (wt%)	PF	0.074	0.0257	0.0206	0.0154	27.7%	20.7%	0.064	33.5%	0.021	0.025
	MA	0.069	0.0232	0.0082	0.0217	11.8%	31.2%	0.064	33.5%	0.021	0.023
Copper (wt%)	PF	0.013	0.0056	0.0036	0.0042	26.8%	31.5%	0.25	5.8%	0.015	0.001
	MA	0.070	0.1231	0.1229	0.0069	175.4%	9.8%	0.25	5.8%	0.015	0.004
Iron (wt%)	PF	8.205	0.7343	0.4794	0.5561	5.8%	6.8%	6.235	4.8%	0.299	0.394
	MA	8.393	0.6459	0.4316	0.4805	5.1%	5.7%	6.235	4.8%	0.299	0.403
Potassium (wt%)	PF	0.114	0.0731	0.0613	0.0397	53.9%	34.9%	2,455	6.5%	0.160	0.007
	MA	0.130	0.0645	0.0594	0.0252	45.6%	19.3%	2.455	6.5%	0.160	0.008
Lithium (wt%)	PF	1.620	0.0961	0.0383	0.0881	2.4%	5.4%	1.963	4.1%	0.080	0.066
	MA	1.674	0.0762	0.0440	0.0622	2.6%	3.7%	1.963	4.1%	0.080	0.069
Magnesium (wt%)	PF	1.254	0.0811	0.0475	0.0657	3.8%	5.2%	0.842	4.8%	0.040	0.060
İ	MA	1.275	0.0765	0.0519	0.0561	4.1%	4.4%	0.842	4.8%	0.040	0.061
Manganese (wt%)	PF	0.830	0.0929	0.0684	0.0628	8.2%	7.6%	2.111	5.2%	0.110	0.043
	MA	0.849	0 08 5 9	0 0648	0.0565	7 6%	6.7%	2.111	5.2%	0.110	0.044
Sodium (wt%)	PF						for this Ana	•			
	MA	8.860	0.4671	0.3314	0.3292	3.7%	3.7%	7.463	4.5%	0.336	0.399
Nickel (wt%)	PF	0.103	0.0155	0.0091	0.0125	8.8%	12.2%	0.643	13.2%	0.085	0.014
	MA	0.105	0.0446	0.0132	0.0426	12.5%	40.5%	0.643	13.2%	0.085	0.014
Silicon (wt%)	PF	24.523	1.4406	0.6943	1.2623	2.8%	5.1%	23.31	5.7%	1.329	1.398
	MA	22.881	1.2918	0.6171	1.1349	2.7%	5.0%	23.31	5.7%	1.329	1.304
Titanium (wt%)	PF	0.020	0.0094	0.0045	0.0082	22.3%	41.1%	0.256	4.5%	0.012	0.001
	MA	0.026	0.0395	0.0102	0.0381	39.8%	148.0%	0.256	4.5%	0.012	0.001
Uranium (wt%)	PF						for this Ana				
ł	MA	1.112	0.1815	0.1604	0.0851	14.4%	7.6%	0	0.0%	0.000	0.000
Zirconium (wt%)	PF						for this Ana				
	MA	0.043	0.0256	0.0253	0.0044	59.3%	10.2%	0.029	9.0%	0.003	0.004

⁴The current version of PCCS computes the variance for each constraint two ways, both using the historical relative standard deviations (RSD's). These RSD's are multiplied by the historical means of the elemental concentrations to compute one variance, and they are multiplied by the average concentrations of the current samples to compute the other. The larger of the two is used by PCCS to determine the appropriate Measurement Acceptable Region

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Exhibit 1: Summary Statistics for SRAT Receipt Measurements



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Exhibit 1: Summary Statistics for SRAT Receipt Measurements (Continued)

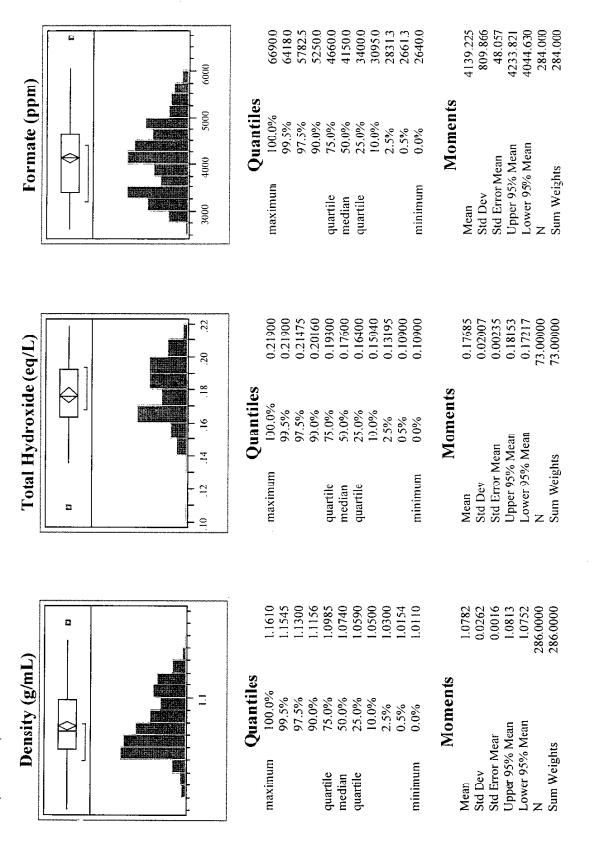
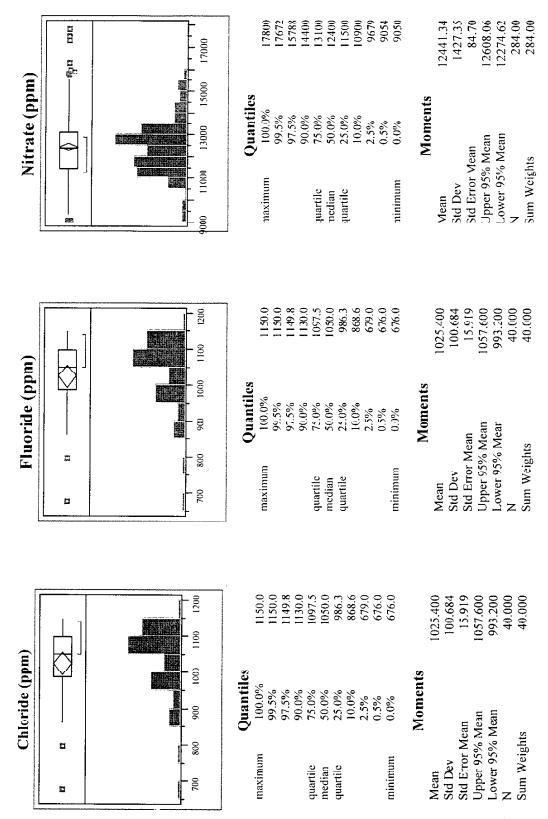


Exhibit 1: Summary Statistics for SRAT Receipt Measurements (Continued)



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Exhibit 1: Summary Statistics for SRAT Receipt Measurements (Continued)

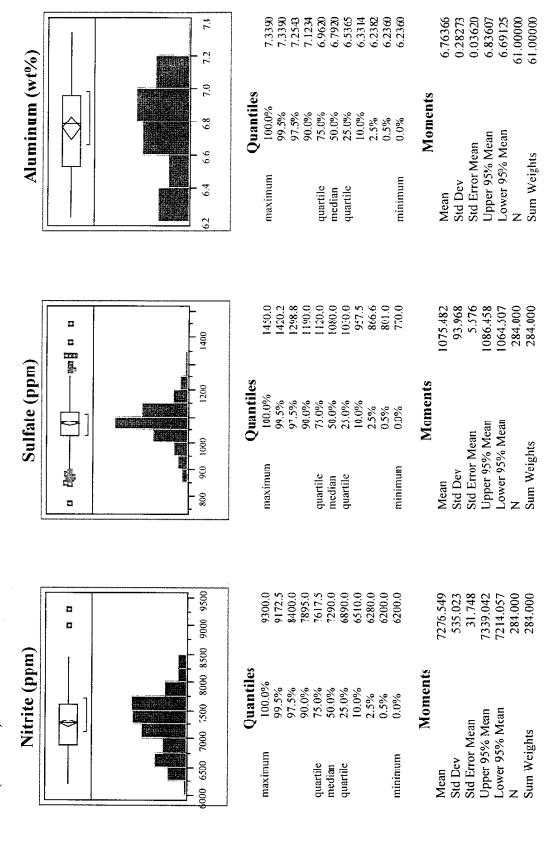
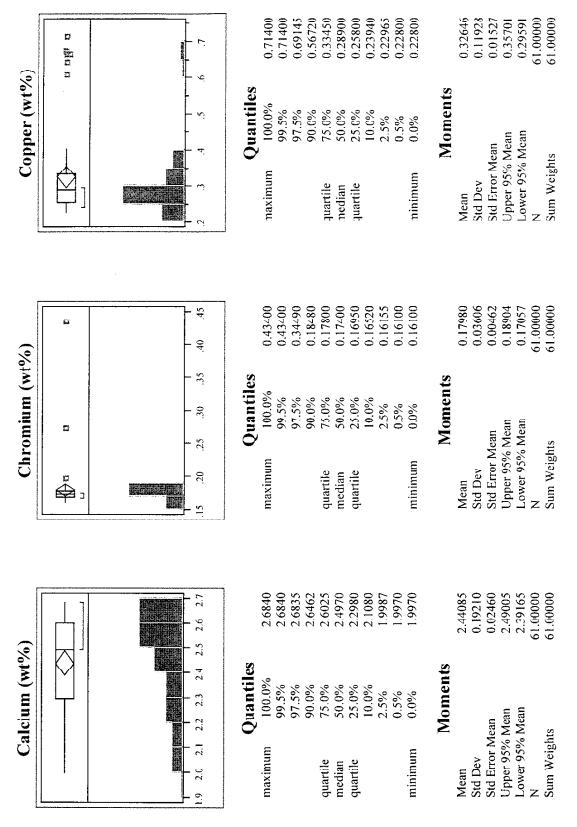


Exhibit 1: Summary Statistics for SRAT Receipt Measurements (Continued)



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Exhibit 1: Summary Statistics for SRAT Receipt Measurements (Continued)

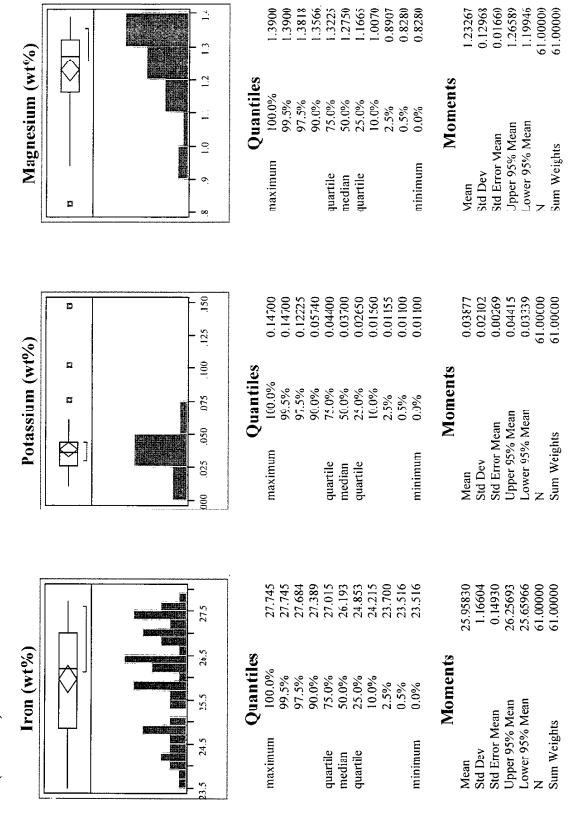
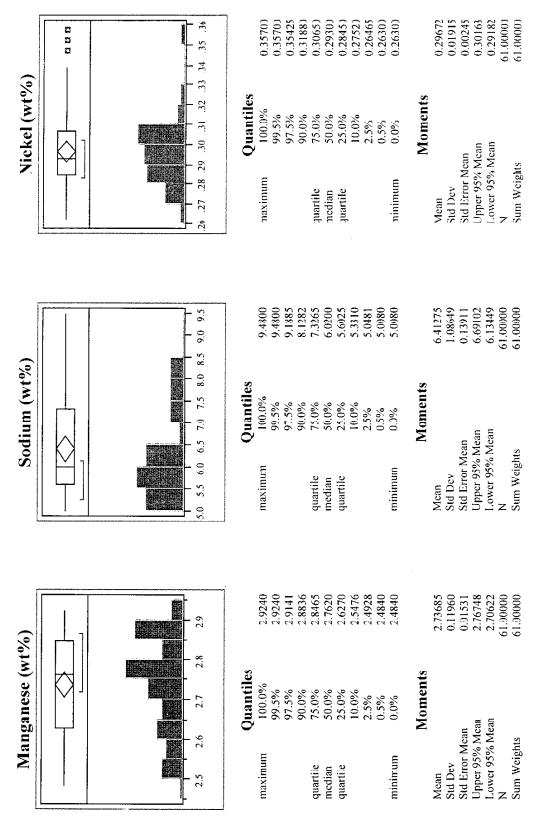


Exhibit 1: Summary Statistics for SRAT Receipt Measurements (Continued)



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Exhibit 1: Summary Statistics for SRAT Receipt Measurements (Continued)

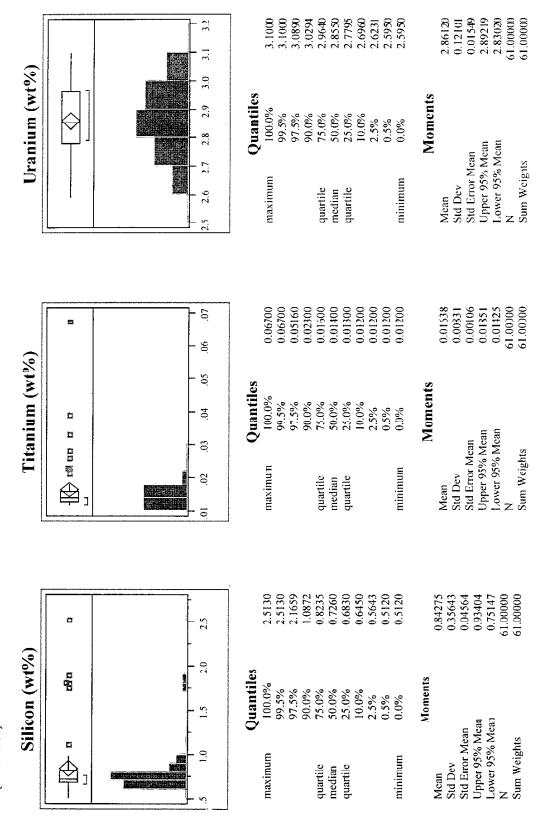


Exhibit I: Summary Statistics for SRAT Receipt Measurements (Continued)

Mercury (ppm)			30) 400 500 600	Quantiles	100.0%										0.0% 203.00	Moments	296.0000	112.4953		7			
			50)		maximum						quartile				ninimum		Mean	Std Dev		Upper 95% Mean			Sum Weights
TIC (ppm)	High a fulla-	And the state of t	700 800 900 1000 1100	es	_	_	_	90.0% 827.8				. •		0.5% 424.8	0.0% 424.6	Moments	584.6057	150.1355	an 9.5529	4ean 603.4218			
L			400 800 600		maximum				quartile	median	quartile				minimum		Mean	Std Dev	Std Error Mean	Upper 95% Mean	Lower 95% Mean	Z	Sum Weights
vt%)	T _{tt}		. 15		0.15300	0.15300	0.15190	0.03300	0.02200	0.01700	0.01500	0.01400	0.01300	0.01300	0.01300		0.02674	0.02863	0.00367	0.03407	0.01940	0000019	61.00000
Zirconium (wt%)	8		.05 .10	Quantiles		99.5%	97.5%	%0.06	75.0%	50.0%	25.0%	10.0%	2.5%	0.5%	%0.0	Moments			Mean	% Mean	% Mean	2	ghts
Zire			00.		maximum				quartile	median	quartile				minimum		Mean	Std Dev	Std Error Mean	Upper 95% Mean	Lowe: 95% Mean	Z (Sum Weights

Exhibit 1: Summary Statistics for SRAT Receipt Measurements (Continued)

8	4.19
5 p	4.30
	. 3.90
	3.8
	70

	4.1148	4.1148	4.0568	3.9572	3.8642	3.8200	3.7841	3.7634	3.7249	3.7211	3.7211		3.83813	0.07651	0.00980	3.85772	3.81853	61.00000	61.00000
Quantiles	100.0%	99.5%	97.5%	%0'06	75.0%	50.0%	25.0%	10.0%	2.5%	0.5%	%0.0	Moments			an	Acar	dean		
	maximum				quartile	median	quartile				minimum		Mean	Std Dev	Std Error Mean	Upper 95% Mear	Lower 95% Mean	Z	Sum Weights

Exhibit 2: Summary Statistics for SRAT Product Measurements

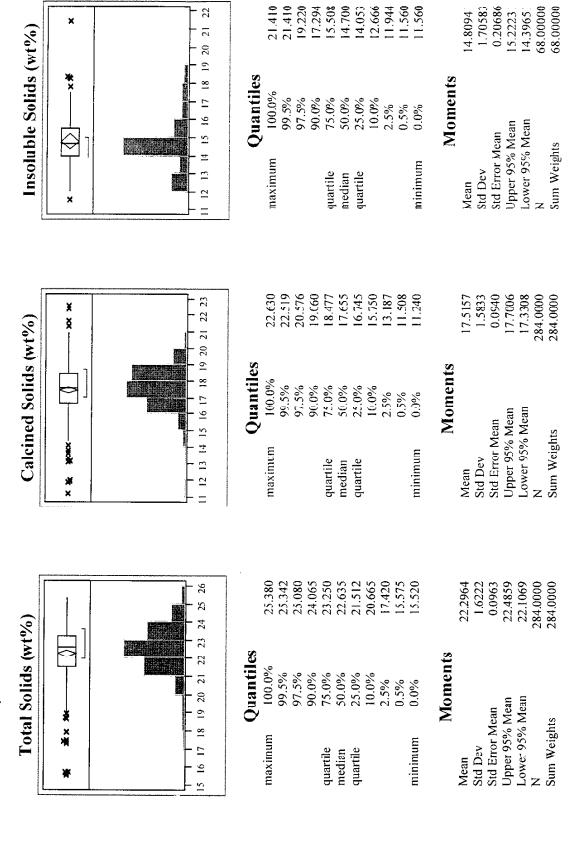


Exhibit 2: Summary Statistics for SRAT Product Measurements (continued)

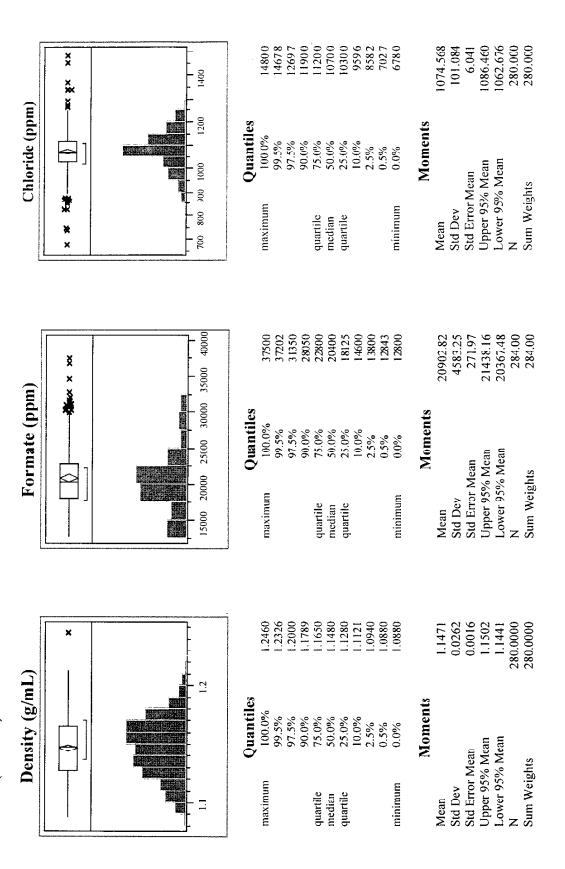


Exhibit 2: Summary Statistics for SRAT Product Measurements (continued)

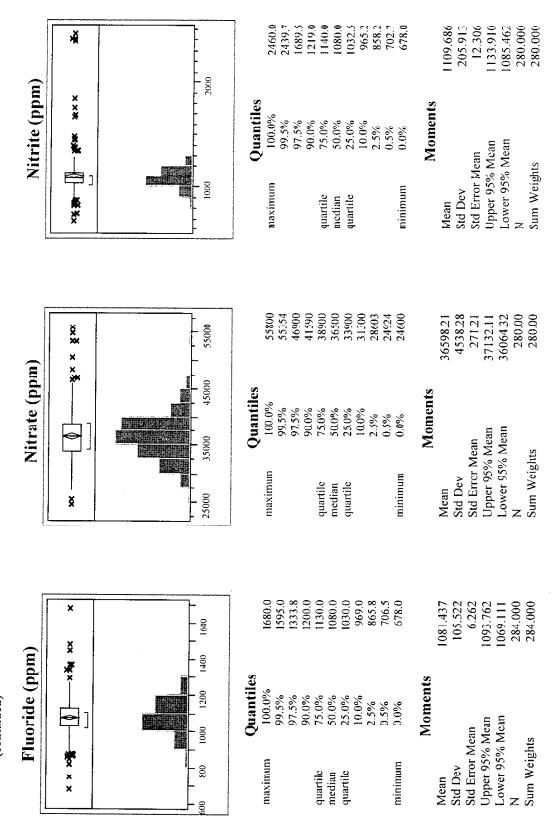


Exhibit 2: Summary Statistics for SRAT Product Measurements (continued)

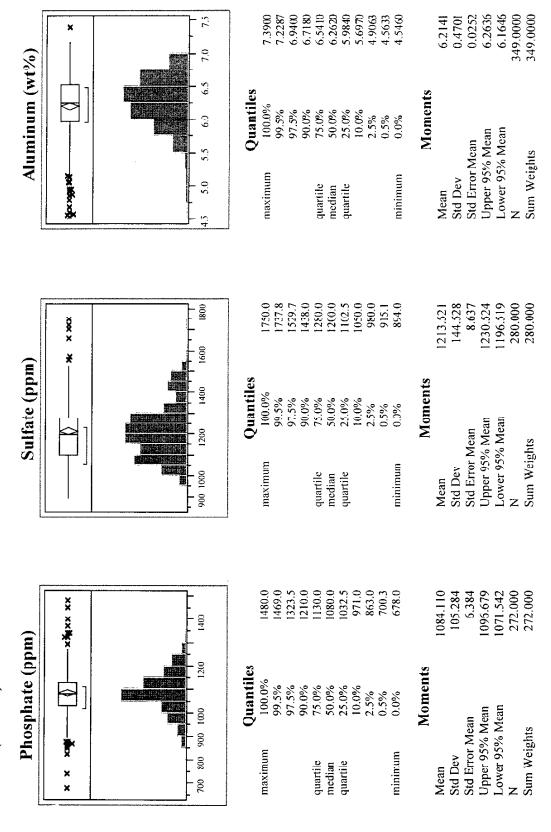


Exhibit 2: Summary Statistics for SRAT Product Measurements (continued)

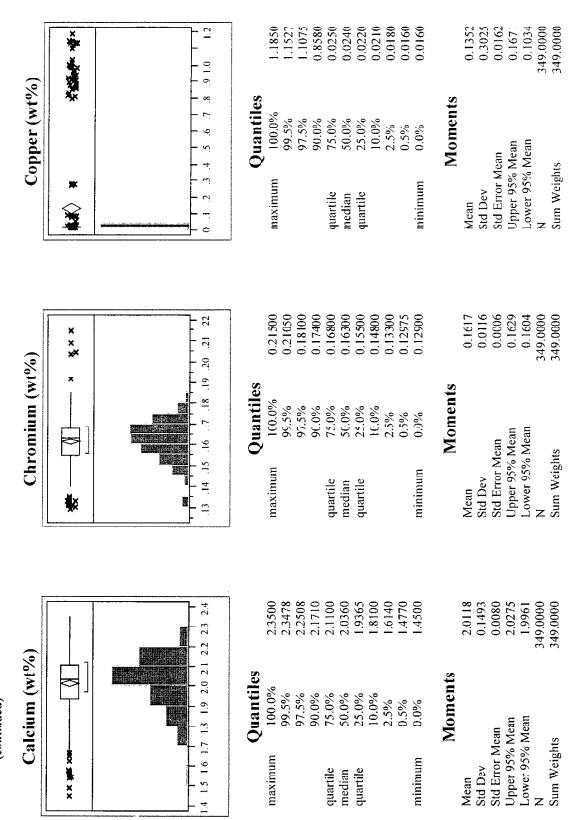


Exhibit 2: Summary Statistics for SRAT Product Measurements (continued)

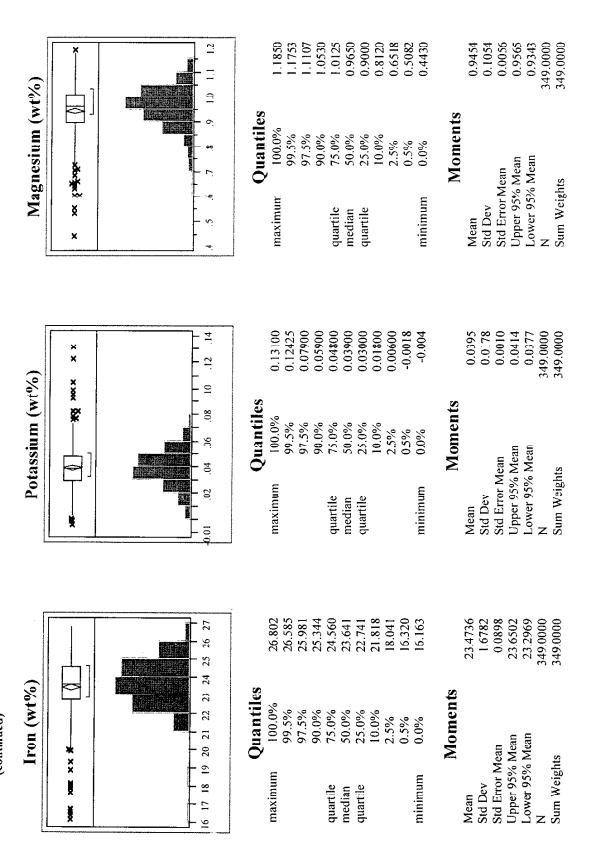


Exhibit 2: Summary Statistics for SRAT Product Measurements (continued)

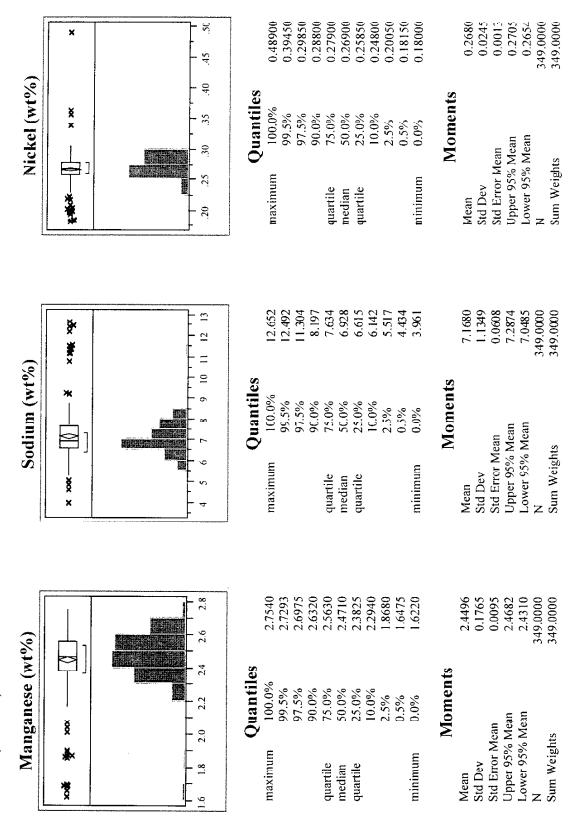


Exhibit 2: Summary Statistics for SRAT Product Measurements (continued)

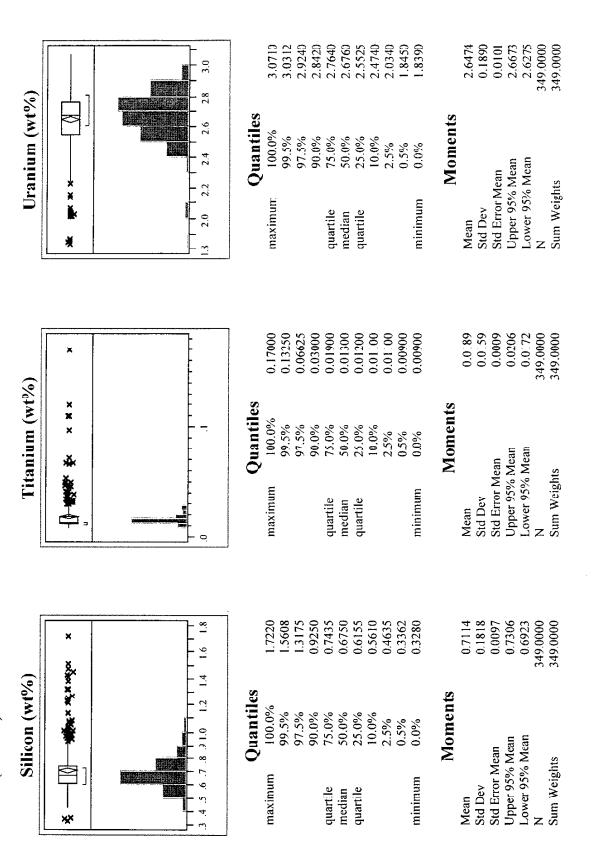


Exhibit 2: Summary Statistics for SRAT Product Measurements (continued)

Fe/AI	× ××× × × × × × × × × × × × × × × × ×		\$	Quantiles			90.0% 5.8625	50.0%	25.0%	10.0% 3.6990	0.5% 3.4802	minimum 0.0% 3.4495	Moments	Mean 3.7809	Std Dev 0.1443	r Mean	Jpper 95% Mean 3.796		34	Sum Weights 349.0000
Mercury (ppm)			101	Quantiles		 00.001 %5.79		20.0%	quartile 25.0% 100.00		%5'0	minimum 0.3% 100.00	Moments	Mean 100.000	Std Dev 0.0000	Std Error Mean 0.0000	Upper 95% Mean 100.0000	Lower 95% Mear. 100.000	0000'9 V	Sum Weights 6.0000
Zirconium (wt%)	x x xxxxx x xxxxx x x x x x x x x x x	Management of the Control of the Con	0. 03 05 07 09 11 13 15	Quantiles	.0	0,000,00 %0,000		50.0%			0.5%	minimum 0.0% 0.01000	Moments			Std Error Mean 0.0007		ower 95% Mean		Sum Weights 349.0000

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Exhibit 3: Summary Statistics for SME Measurements

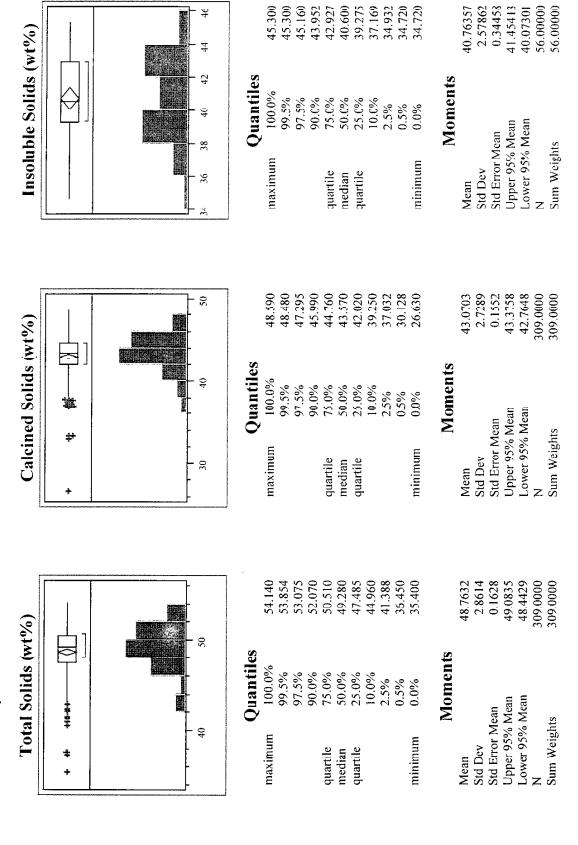
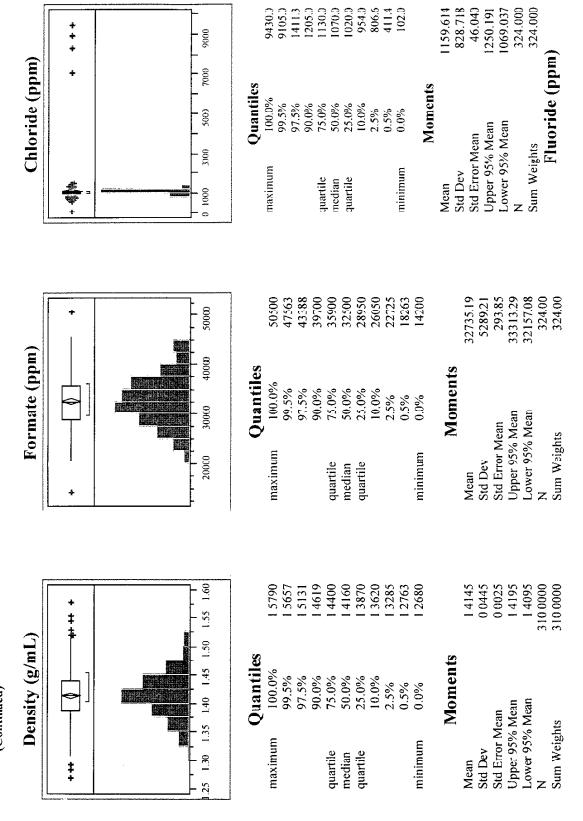
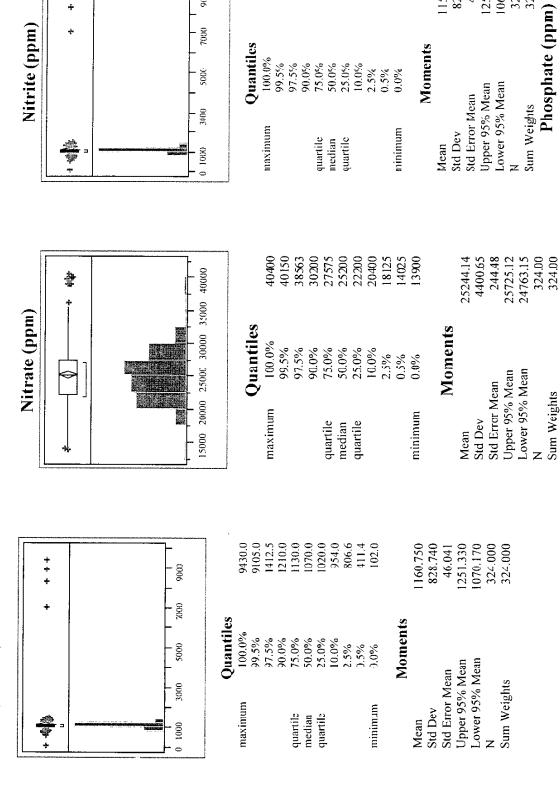


Exhibit 3: Summary Statistics for SME Measurements (Continued)



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Exhibit 3: Summary Statistics for SME Measurements (Continued)



1411.3 1205.0 1130.0 1020.0 1020.0 954.0

9.908 411.4 102.6 46.040

1250.191 1069.037

1159.614 828.718 324.000324.000

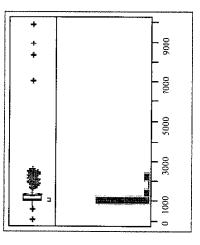
9105.6

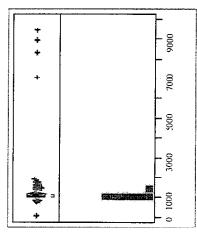
9006

7000

Sum Weights

Exhibit 3: Summary Statistics for SME Measurements (Continued)





*	
* +	2

	9430.0	9105.0	1738.8	1300.0	1167.5	1090.0	1040.0	0.976	884.0	530.1	102.0		1205.448	830.197	46.122	1296.186	1114.709	324.000	324.000
Cuantiles	1(0.0%	96.5%	97.5%	%0:)6	75.0%	\$0.0%	25.0%	10.0%	2.5%	0.5%	0.19%	Moments			ean	Mean	Mean		S
	maximum				quartile	median	quartile				minimum		Mean	Std Dev	Std Error Mean	Upper 95% Mean	Lower 95% Mean	z	Sum Weights

843.1 411.4 102.0

2.5% 0.5% 0.0%

minimum

2.464)

2.1666 1.9237 1.7843 1.6490

90.0% 75.0% 50.0% 25.0% 10.0% 0.5% 0.0%

> quartile median quartile

2115.0 1285.0 1100.0 1050.0 967.0

100.0% 99.5% 97.5% 90.0% 75.0% 50.0% 25.0%

> quartile median quartile

9870.0 9270.0 2483.8

Quantiles

maximum

3.1597 2.8320 2.6848 2.5840

Quantiles

100.0% 99.5% 97.5%

maximum

70

731.0000 731.0000

Sum Weights

2.4445

Moments

1358.256 913.670 50.759

Std Dev

Moments

1458.118 1258.394 324.000 324.000

Std Error Mean Upper 95% Mean Lower 95% Mean

N Sum Weights

Sulfate (ppm)

minimum

0.2211 0.0082 2.4605 2.4284

> Upper 95% Mean Lower 95% Mean

Std Error Mean

Std Dev

Exhibit 3: Summary Statistics for SME Measurements (Continued)

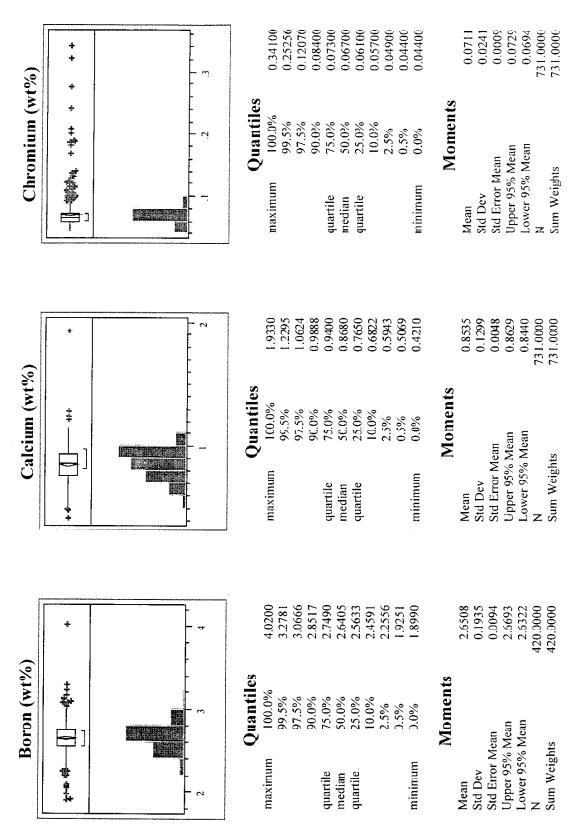


Exhibit 3: Summary Statistics for SME Measurements (Continued)

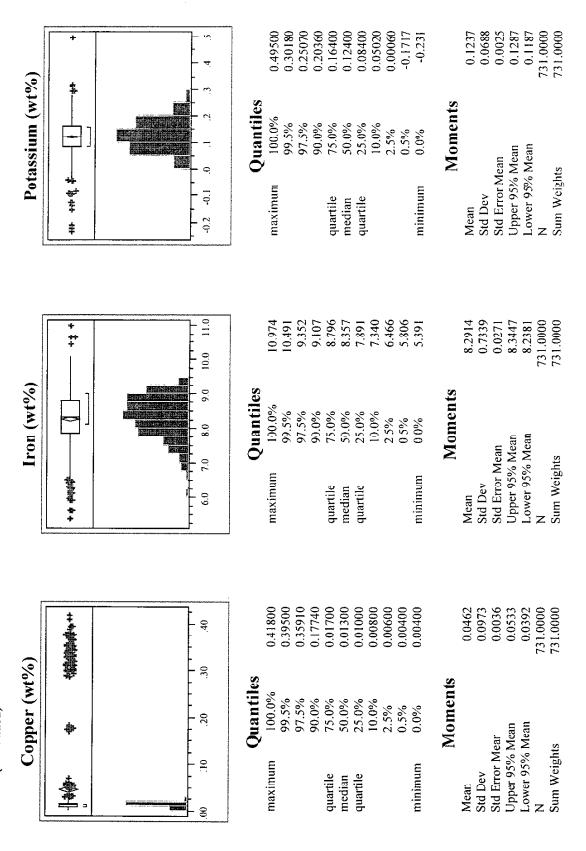


Exhibit 3: Summary Statistics for SME Measurements (Continued)

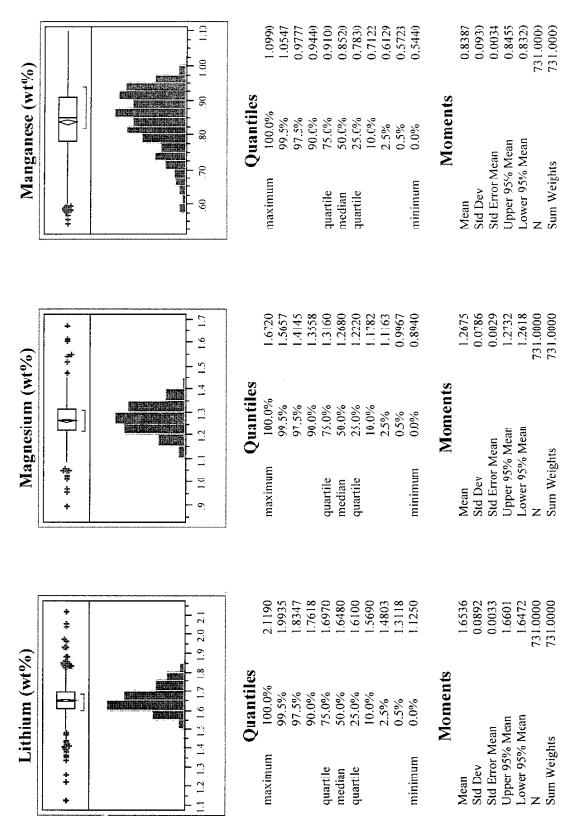


Exhibit 3: Summary Statistics for SME Measurements (Continued)

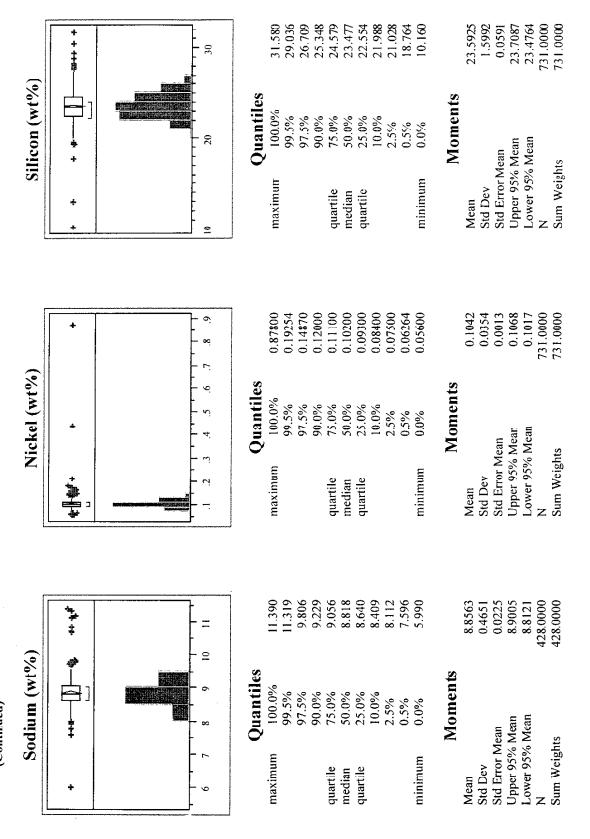


Exhibit 3: Summary Statistics for SME Measurements (Continued)

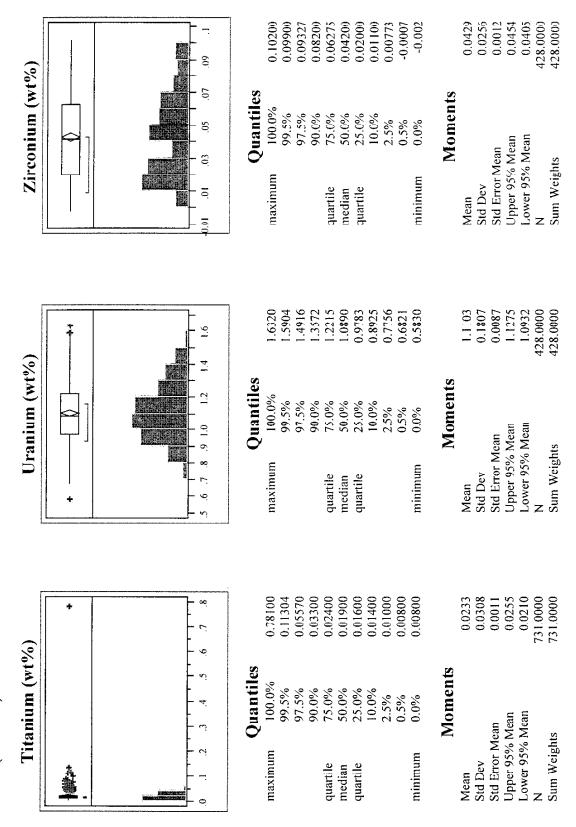


Exhibit 3: Summary Statistics for SME Measurements (Continued)

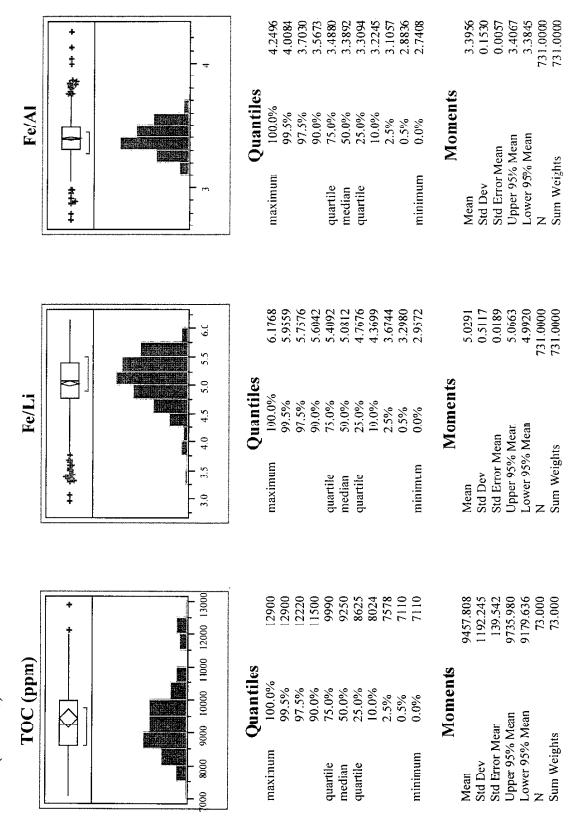


Exhibit 4: Summary Statistics for MFT Measurements

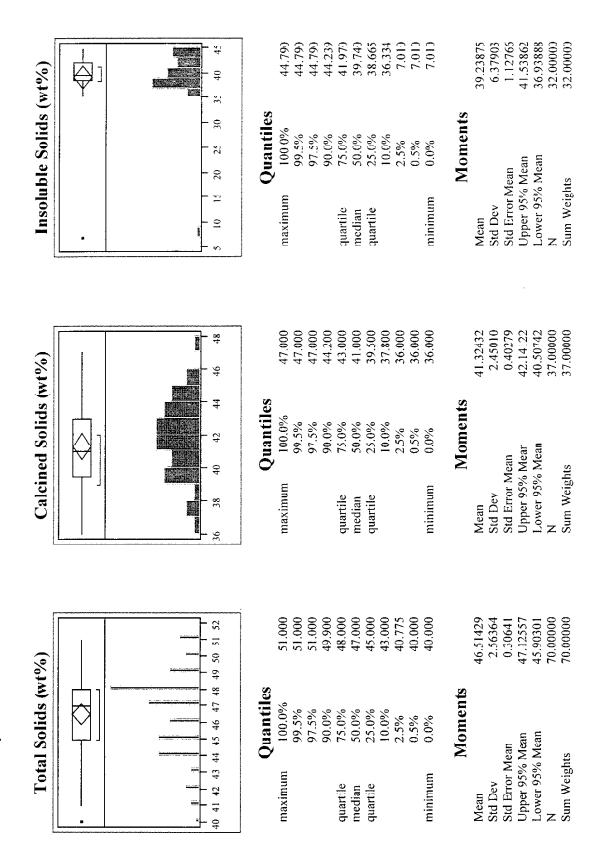


Exhibit 4: Summary Statistics for MFT Measurements (Continued)

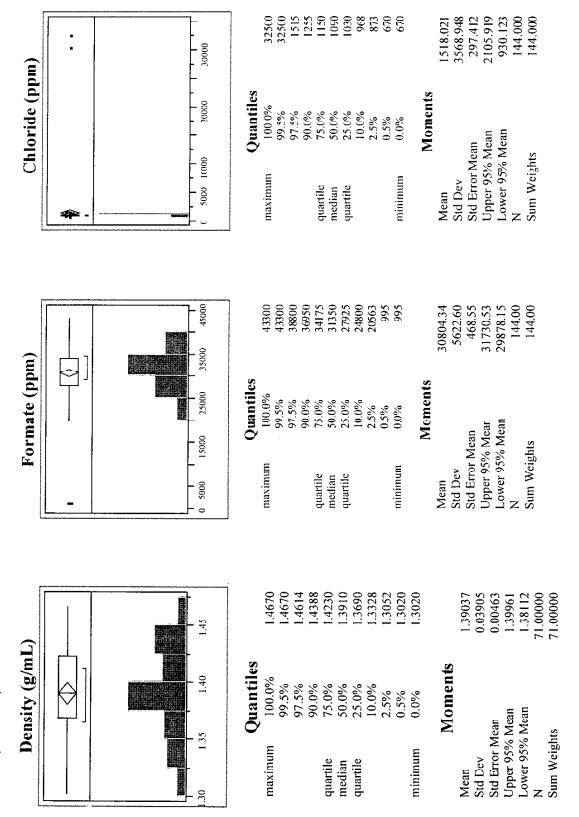
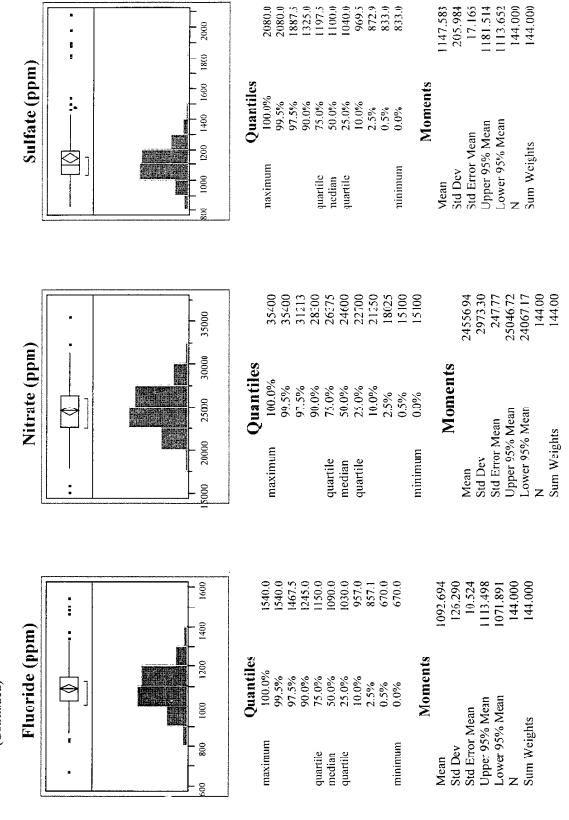


Exhibit 4: Summary Statistics for MFT Measurements (Continued)



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Exhibit 4: Summary Statistics for MFT Measurements (Continued)

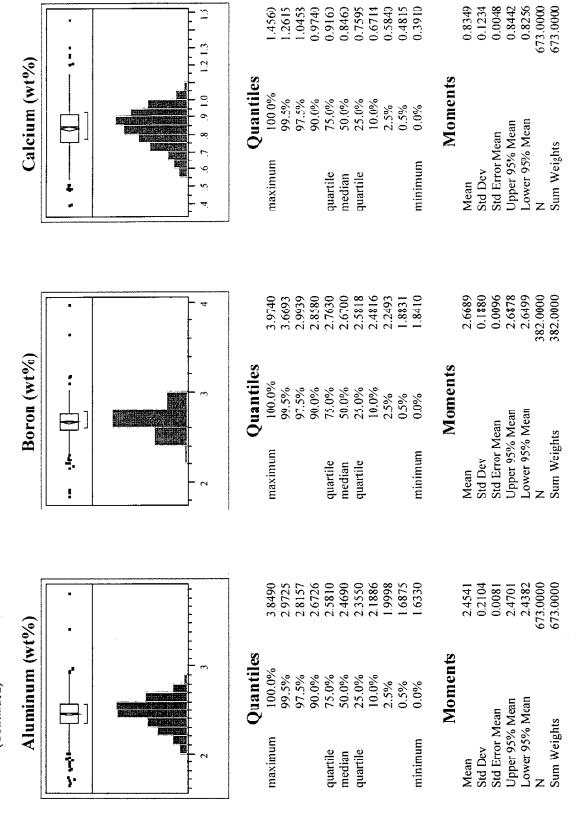
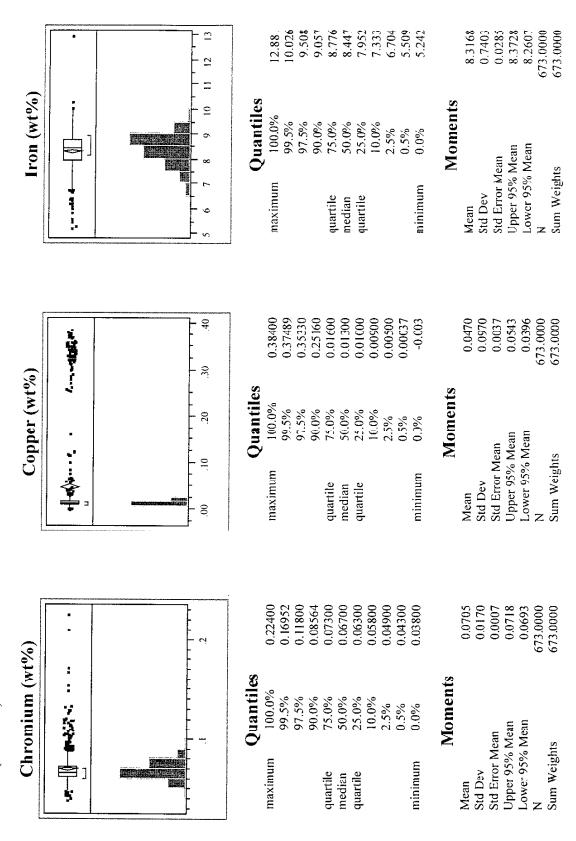


Exhibit 4: Summary Statistics for MFT Measurements (Continued)



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Exhibit 4: Summary Statistics for MFT Measurements (Continued)

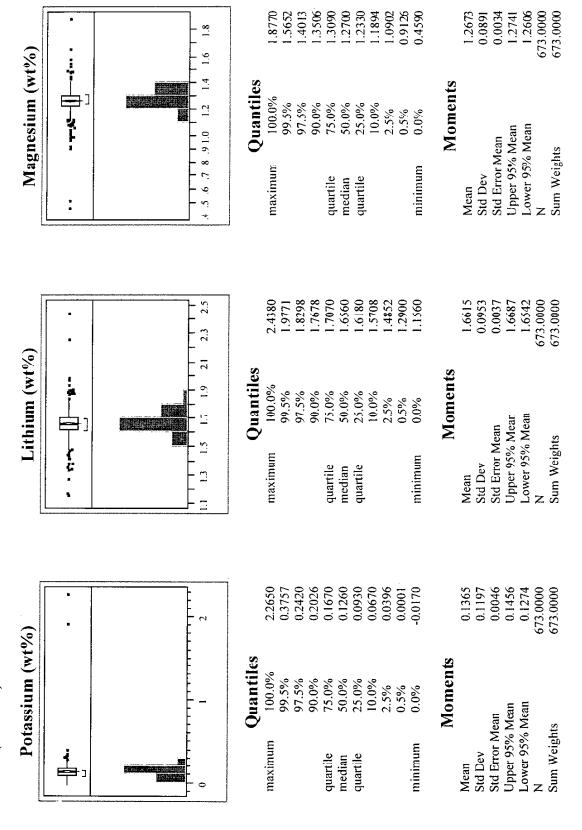


Exhibit 4: Summary Statistics for MFT Measurements (Continued)

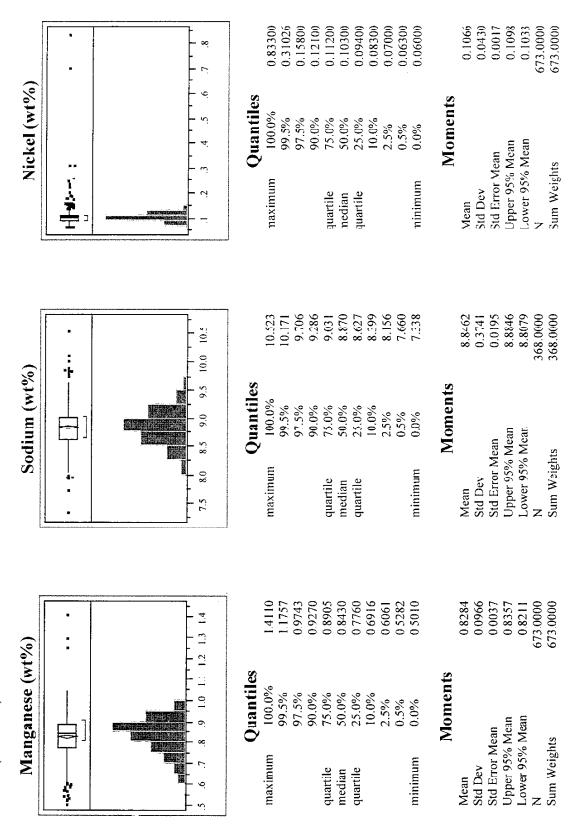


Exhibit 4: Summary Statistics for MFT Measurements (Continued)

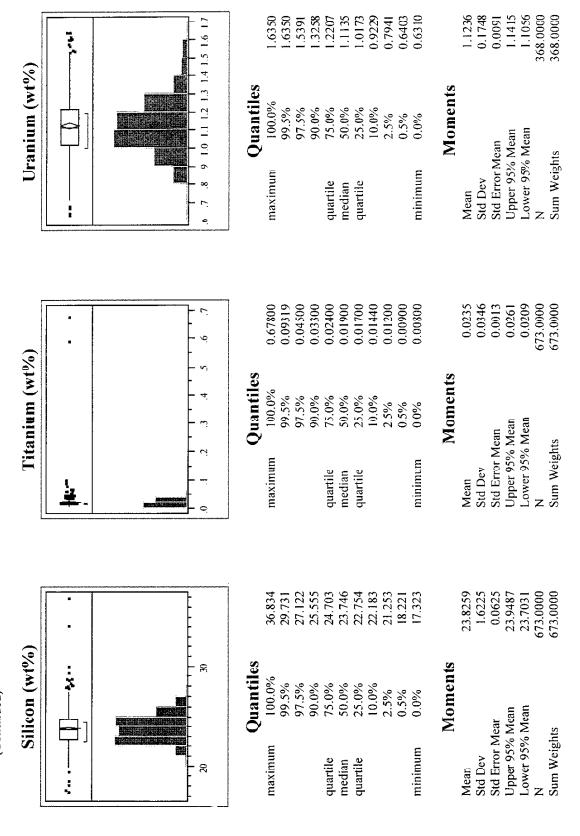
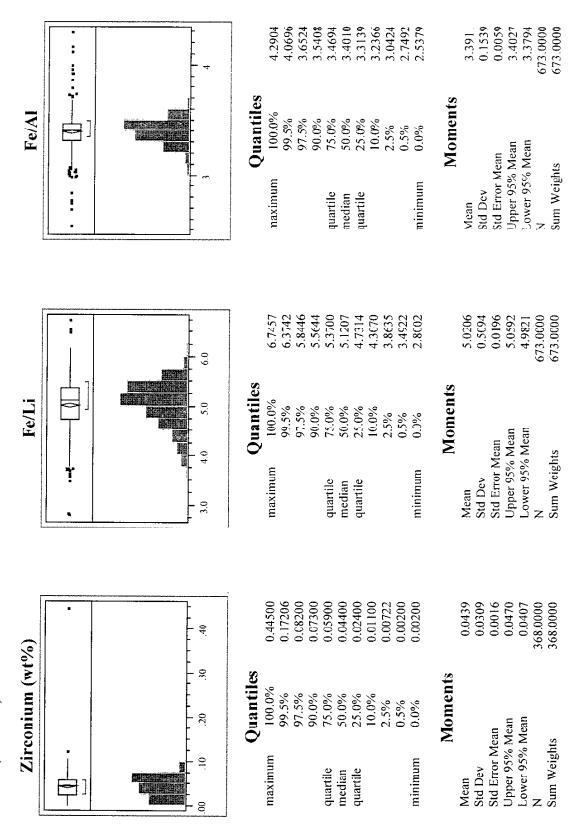


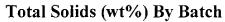
Exhibit 4: Summary Statistics for MFT Measurements (Continued)

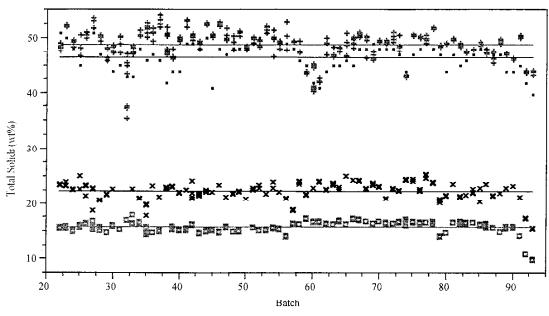


WSRC-RP-2000-00174 Revision 0 Exhibit 4: Summary Statistics for MFT Measurements (Continued)

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Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box – MFT; Plus – SME; Open Box – SRAT Receipt; x's – SRAT Product





Calcined Solids (wt%) By Batch

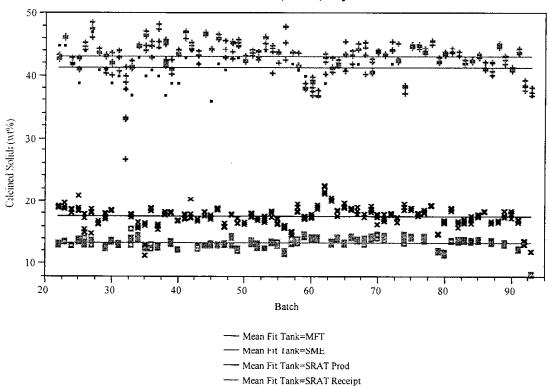
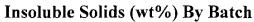
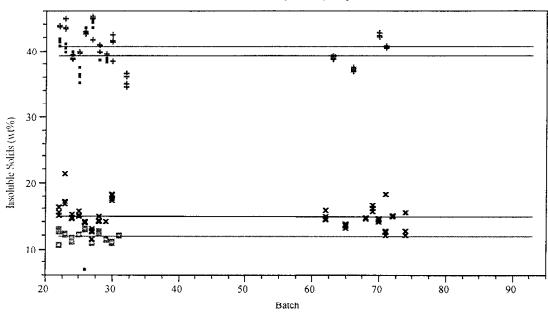


Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box - MFT; Plus - SME; Open Box - SRAT Receipt; x's - SRAT Product
(Continued)





Density (g/mL) By Batch

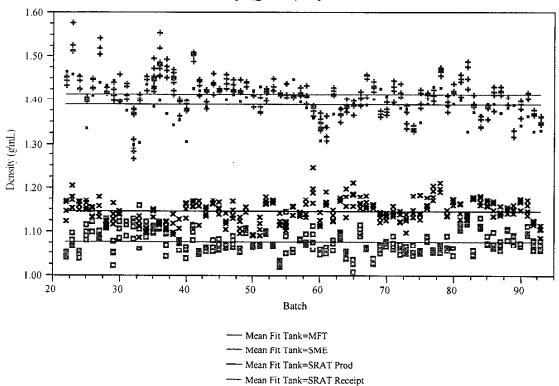
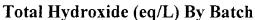
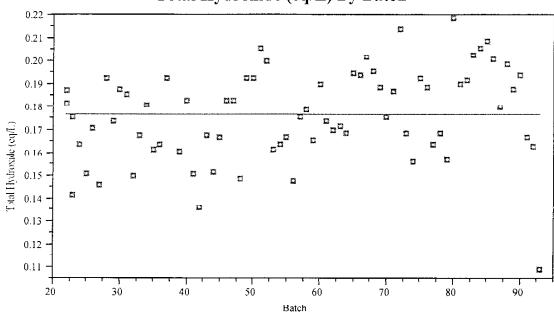
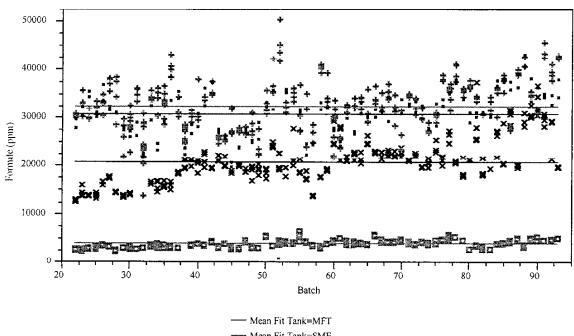


Exhibit 5: Charts of Sample Measurements by Batch by Vessel Small Box - MFT; Plus - SME; Open Box - SRAT Receipt; x's - SRAT Product (Continued)



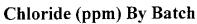


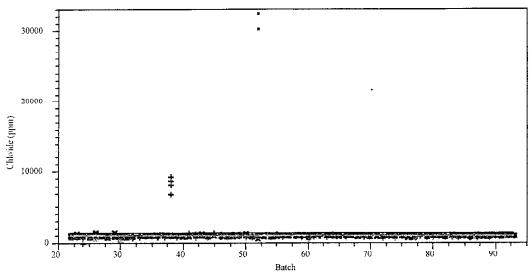
Formate (ppm) By Batch



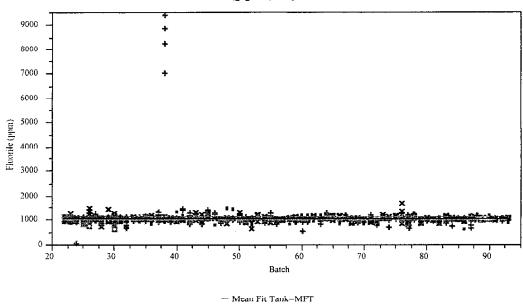
- Mean Fit Tank=SME
- Mean Fit Tank=SRAT Prod
- Mean Fit Tank=SRAT Receipt

Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box - MFT; Plus - SME; Open Box - SRAT Receipt; x's - SRAT Product
(Continued)





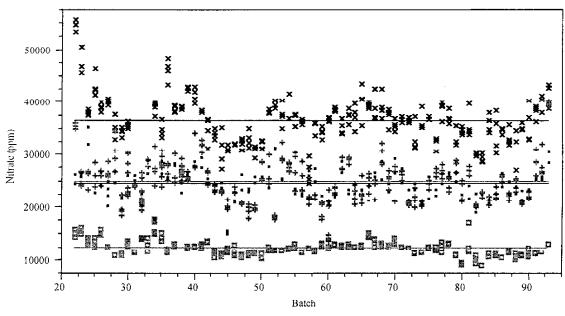
Fluoride (ppm) By Batch



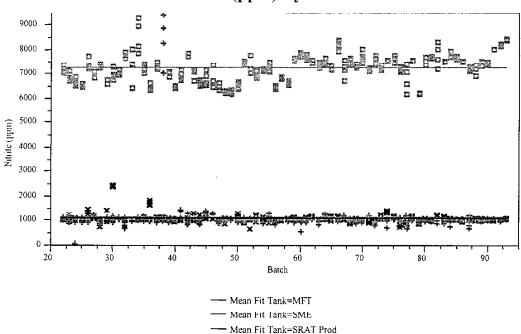
- ---- Mean Fit Tank=SME
- --- Mean Fit Tank=SRAT Prod
- --- Mean Fit Tank=SRAT Receipt

Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box - MFT; Plus - SME; Open Box - SRAT Receipt; x's - SRAT Product
(Continued)

Nitrate (ppm) By Batch



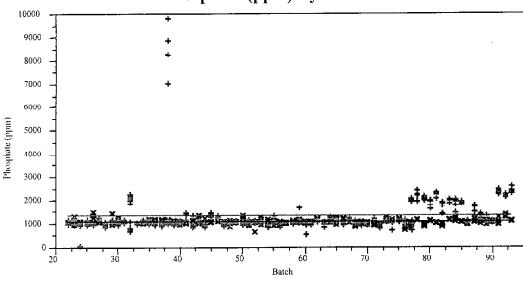
Nitrite (ppm) By Batch



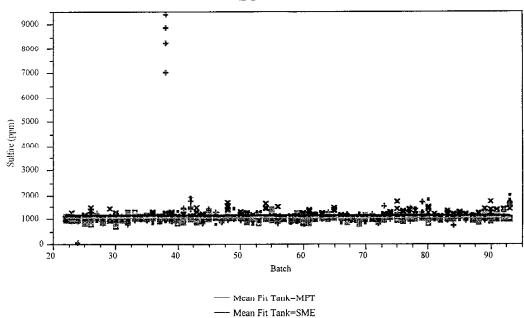
- Mean Fit Tank=SRAT Receipt

Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box - MFT; Plus - SME; Open Box - SRAT Receipt; x's - SRAT Product
(Continued)





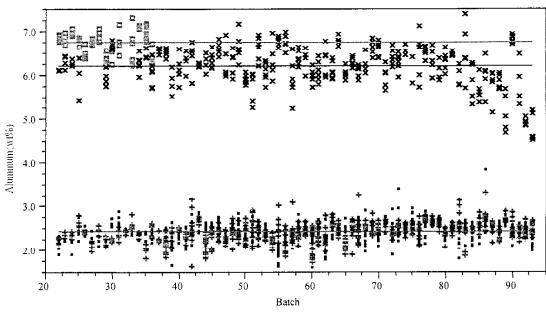
Sulfate (ppm) By Batch



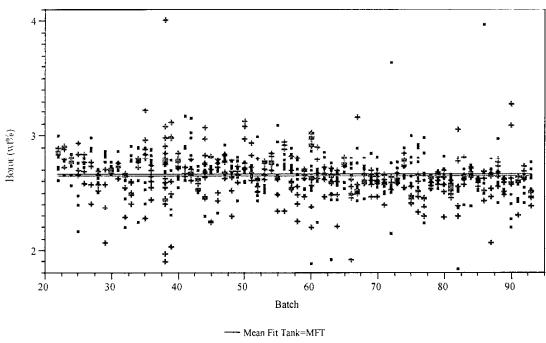
Mean Fit Tank=SRAT ProdMean Fit Tank=SRAT Receipt

Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box - MFT; Plus - SME; Open Box - SRAT Receipt; x's - SRAT Product
(Continued)



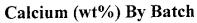


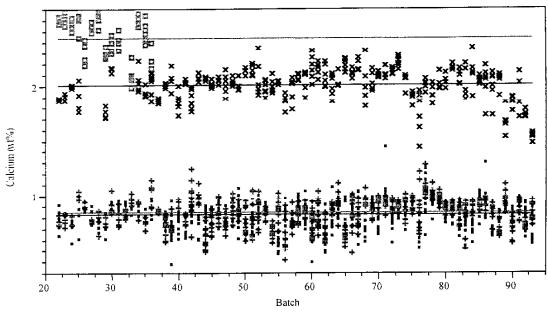
Boron (wt%) By Batch



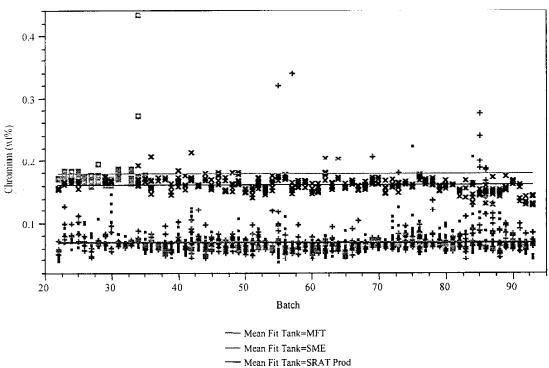
- --- Mean Fit Tank=SME
- Mean Fit Tank=SRAT Prod
- --- Mean Fit Tank=SRAT Receipt

Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box – MFT; Plus – SME; Open Box – SRAT Receipt; x's – SRAT Product
(Continued)





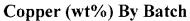
Chromium (wt%) By Batch

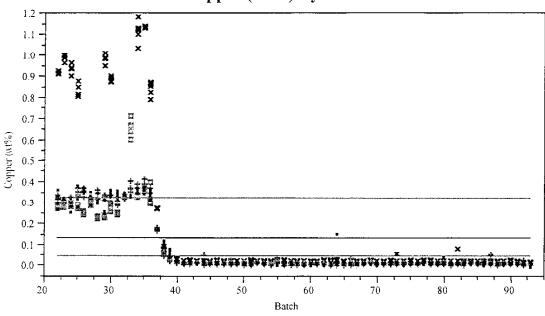


94

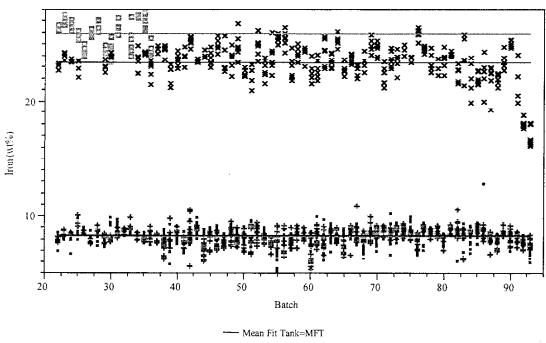
- Mean Fit Tank=SRAT Receipt

Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box - MFT; Plus - SME; Open Box - SRAT Receipt; x's - SRAT Product
(Continued)





Iron (wt%) By Batch

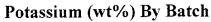


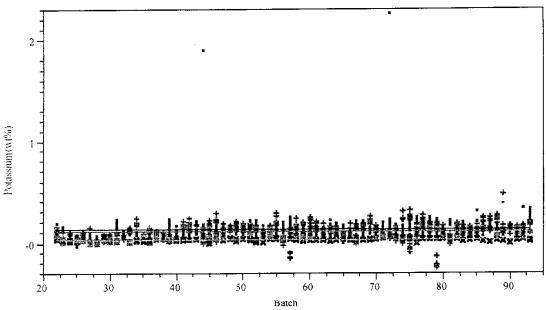
⁻ Mean Fit Tank=SME

⁻⁻⁻ Mean Fit Tank=SRAT Prod

⁻⁻⁻ Mean Fit Tank=SRAT Receipt

Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box - MFT; Plus - SME; Open Box - SRAT Receipt; x's - SRAT Product
(Continued)





Lithium (wt%) By Batch

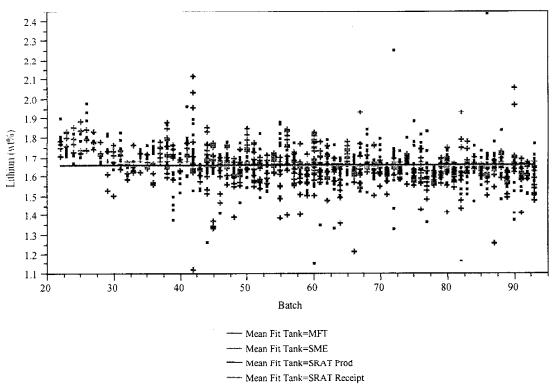
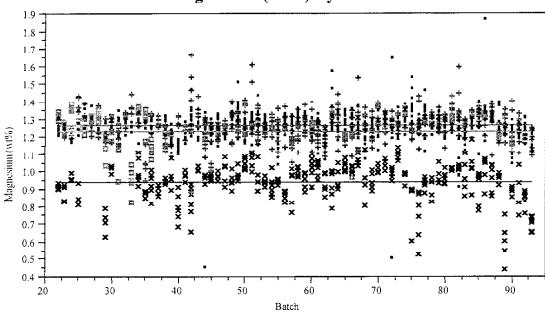
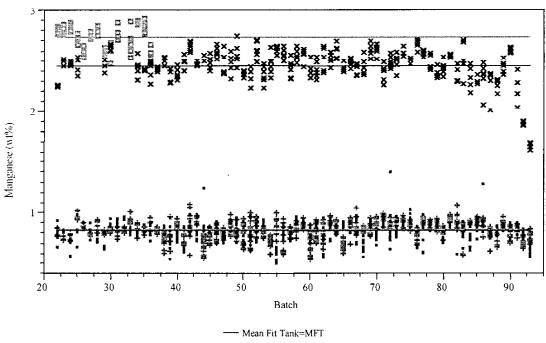


Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box - MFT; Plus - SME; Open Box - SRAT Receipt; x's - SRAT Product
(Continued)





Manganese (wt%) By Batch

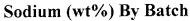


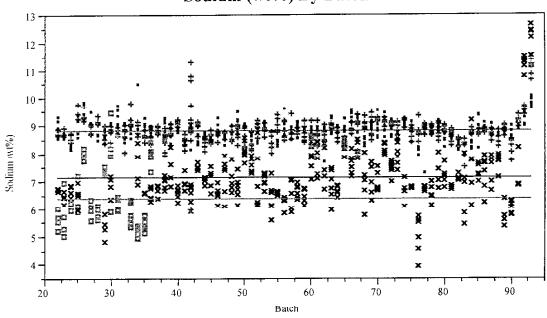
⁻⁻⁻ Mean Fit Tank=SME

⁻⁻ Mean Fit Tank=SRAT Prod

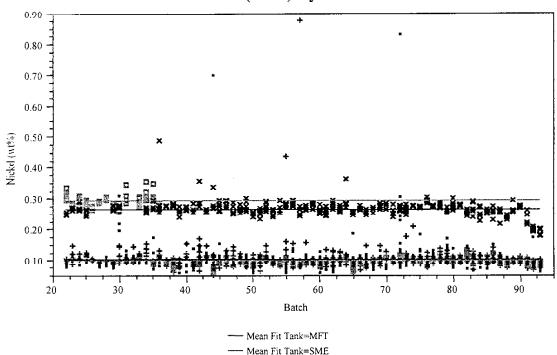
⁻⁻⁻ Mean Fit Tank=SRAT Receipt

Exhibit 5: Charts of Sample Measurements by Batch by Vessel Small Box - MFT; Plus - SME; Open Box - SRAT Receipt; x's - SRAT Product (Continued)





Nickel (wt%) By Batch

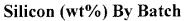


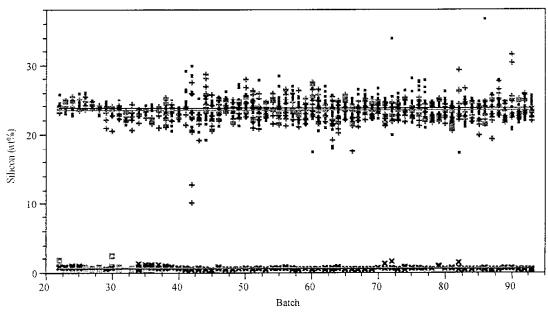
Mean Fit Tank=SME

Mean Fit Tank=SRAT Prod

Mean Fit Tank=SRAT Receipt

Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box - MFT; Plus - SME; Open Box - SRAT Receipt; x's - SRAT Product
(Continued)





Titanium (wt%) By Batch

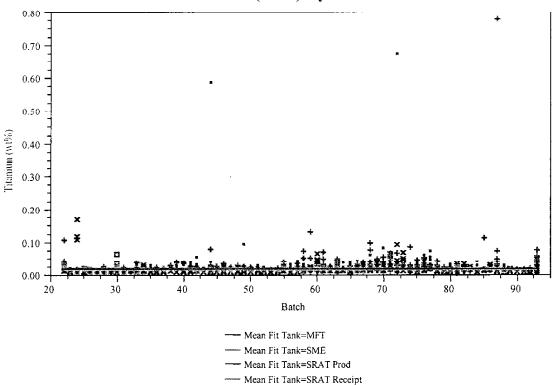
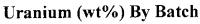
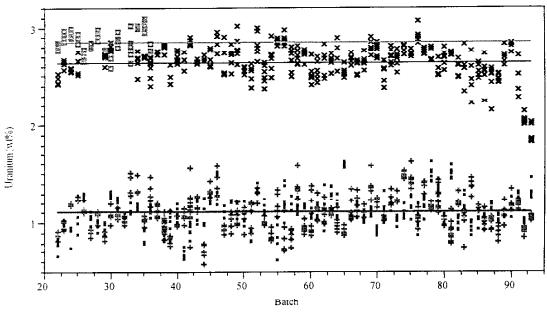
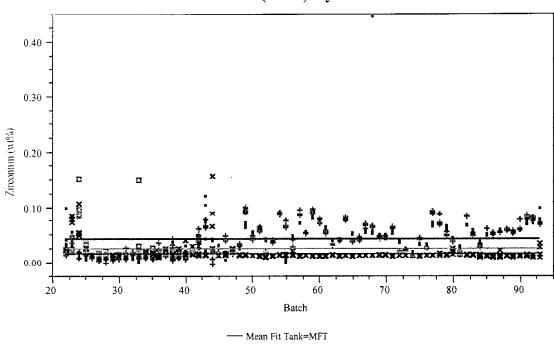


Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box - MFT; Plus - SME; Open Box - SRAT Receipt; x's - SRAT Product
(Continued)



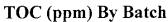


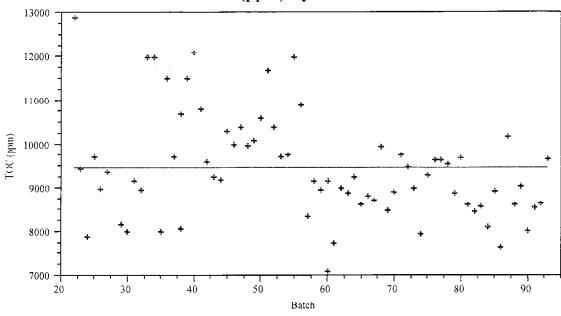
Zirconium (wt%) By Batch



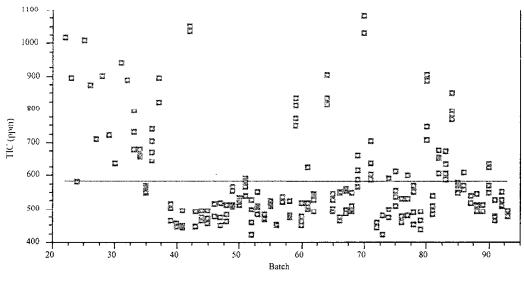
- Mean Fit Tank=SME
- --- Mean Fit Tank=SRAT Prod
- --- Mean Fit Tank=SRAT Receipt

Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box – MFT; Plus – SME; Open Box – SRAT Receipt; x's – SRAT Product
(Continued)



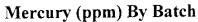


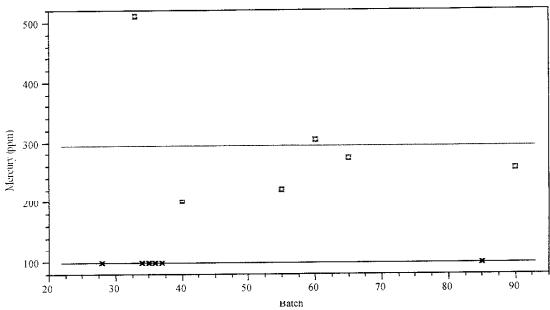
TIC (ppm) By Batch



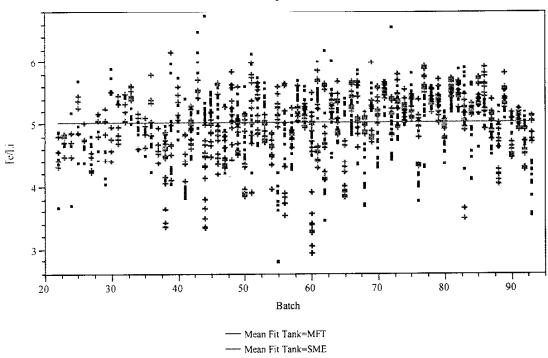
- Mean Fit Tank=MFT
- --- Mean Fit Tank=SME
- --- Mean Fit Tank=SRAT Prod
- --- Mean Fit Tank=SRAT Receipt

Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box – MFT; Plus – SME; Open Box – SRAT Receipt; x's – SRAT Product
(Continued)





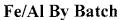
Fe/Li By Batch

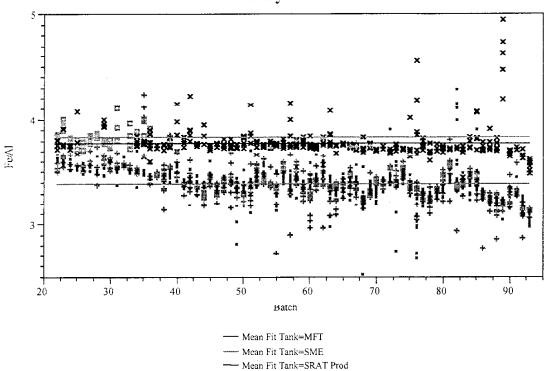


⁻⁻⁻ Mean Fit Tank=SRAT Prod

⁻⁻⁻⁻ Mean Fit Tank=SRAT Receipt

Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box - MFT; Plus - SME; Open Box - SRAT Receipt; x's - SRAT Product
(Continued)





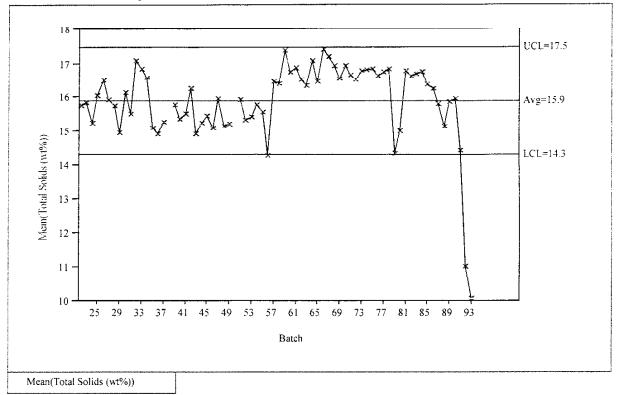
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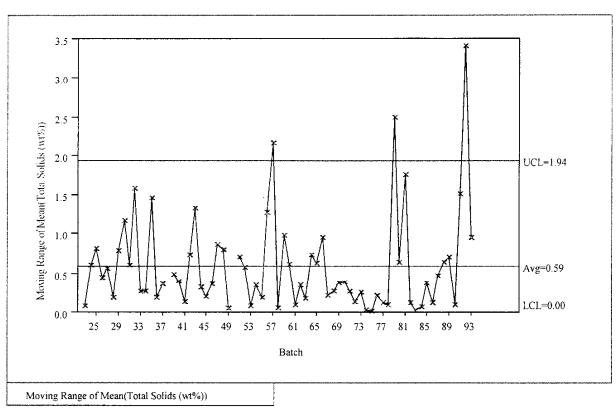
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Exhibit 5: Charts of Sample Measurements by Batch by Vessel
Small Box – MFT; Plus – SME; Open Box – SRAT Receipt; x's – SRAT Product
(Continued)

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Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte

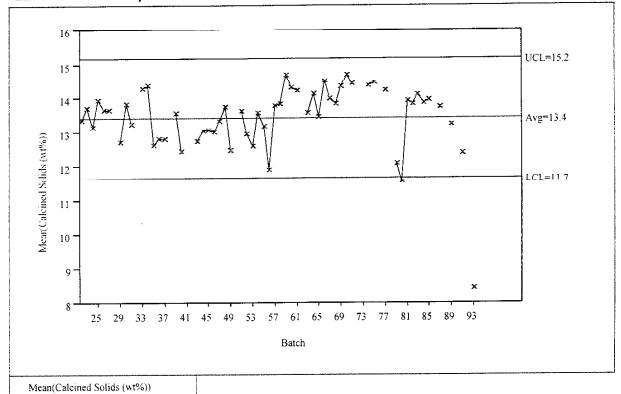




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Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte



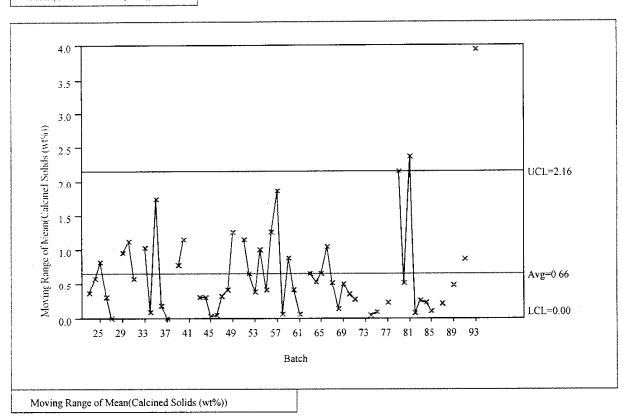
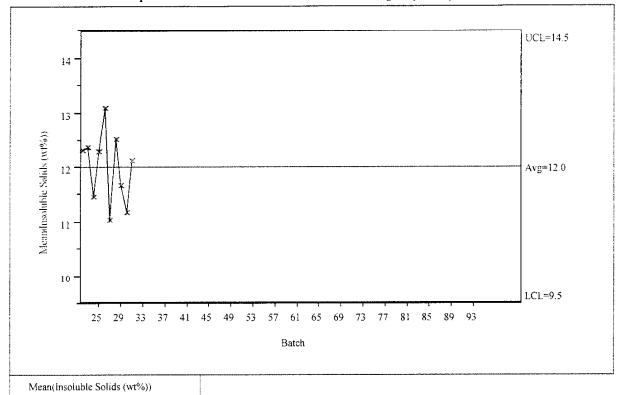
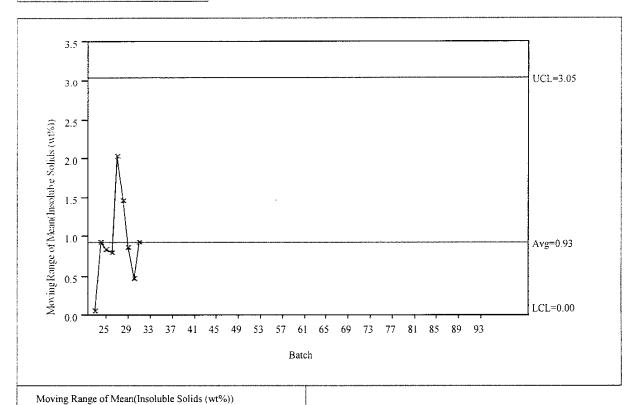


Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte

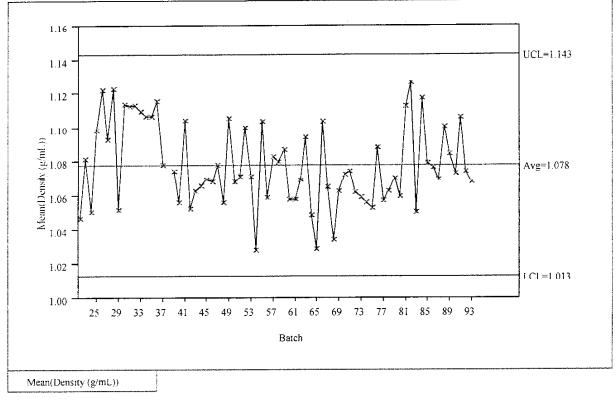




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Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte



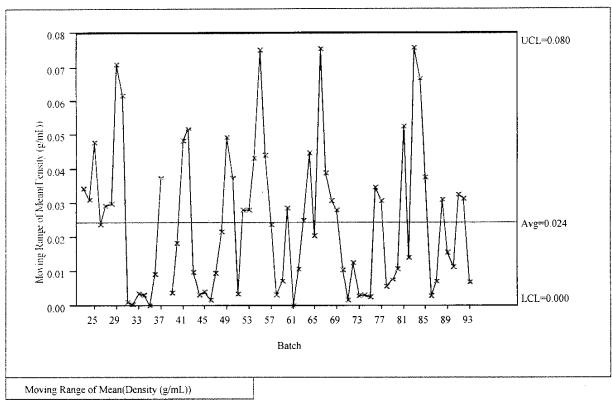
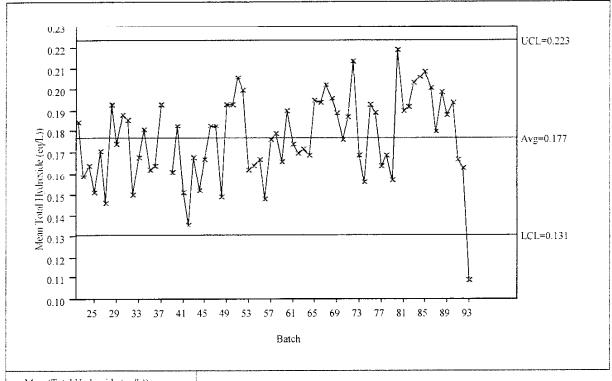
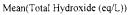


Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte





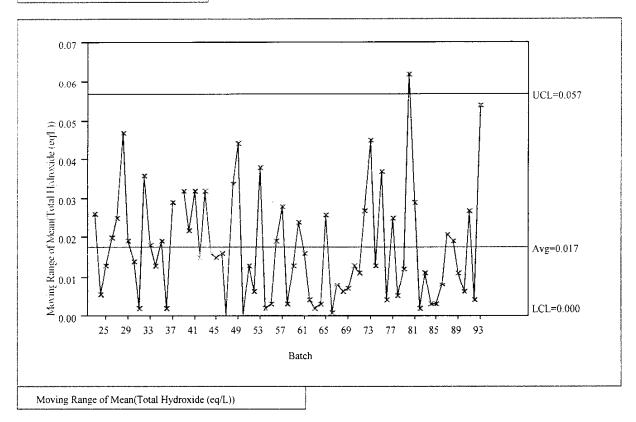
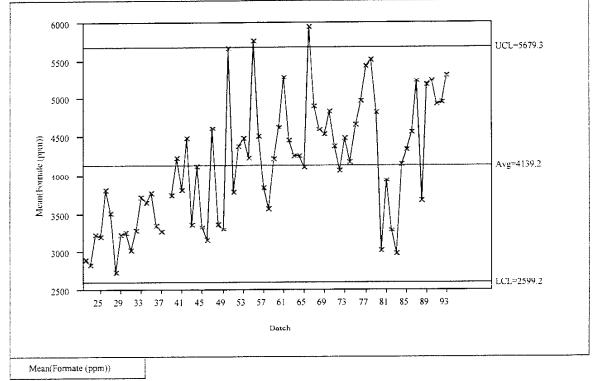


Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte



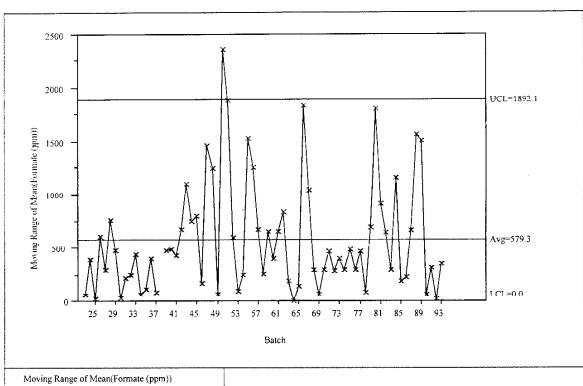
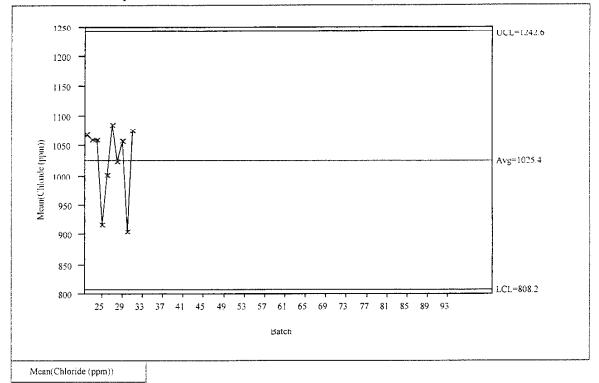


Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte



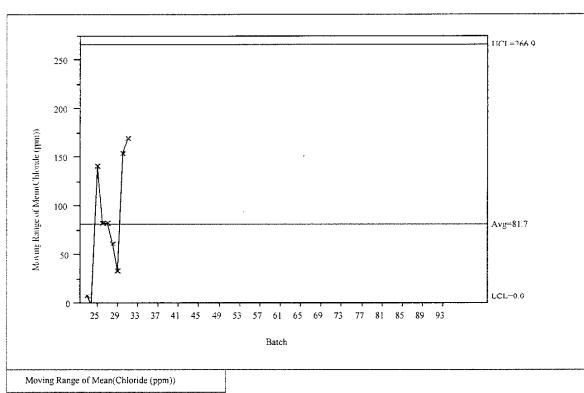
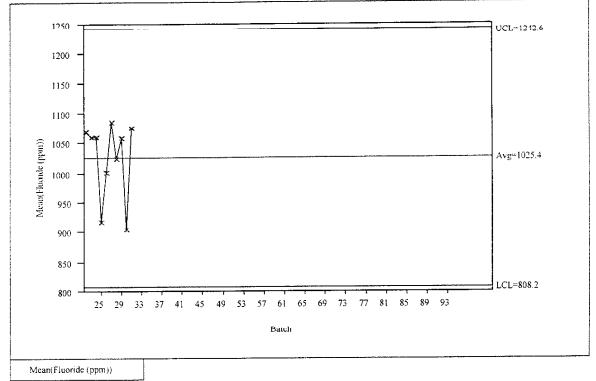


Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte



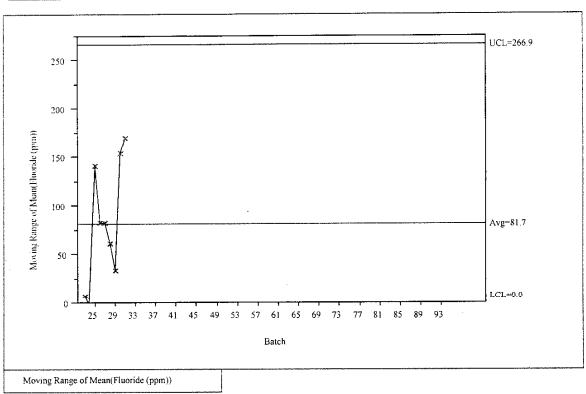
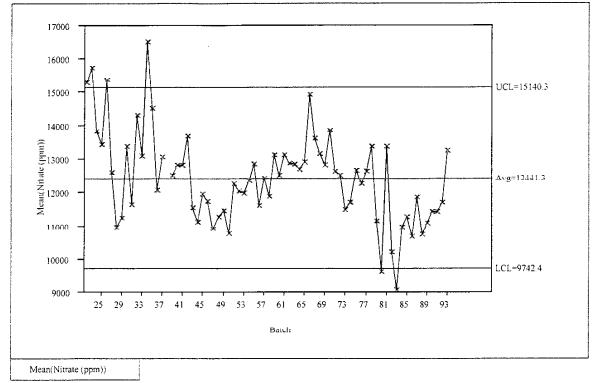


Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte



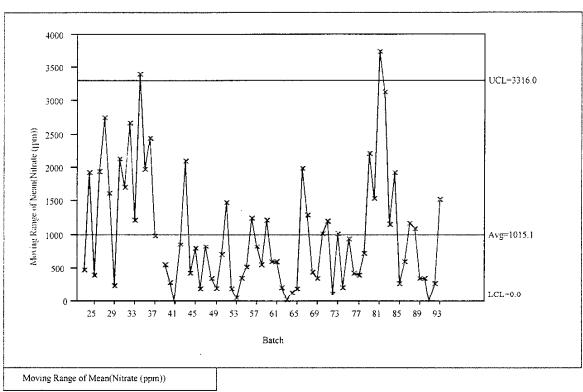
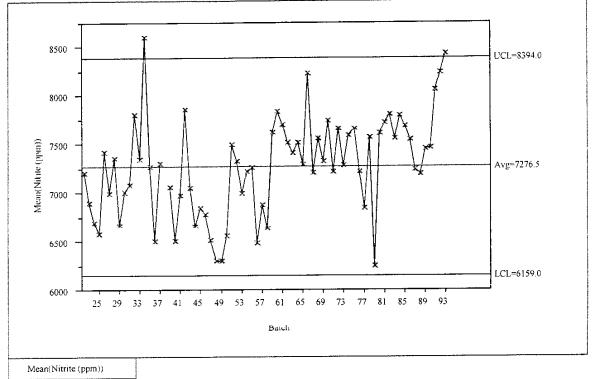


Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte



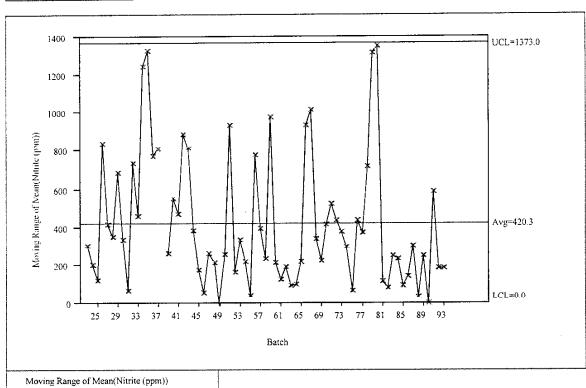
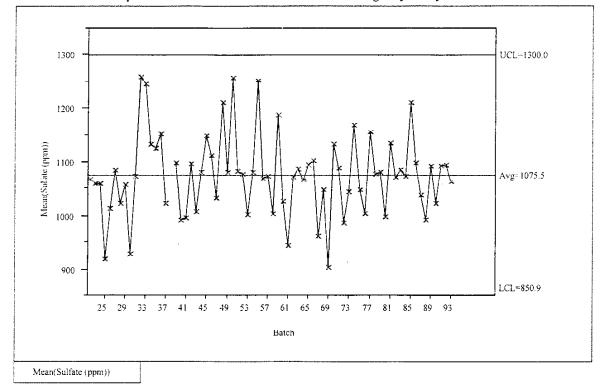
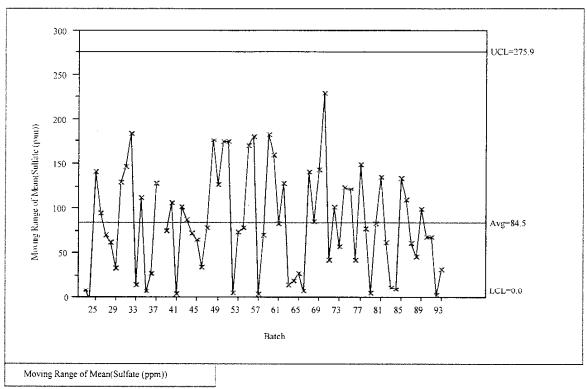


Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte

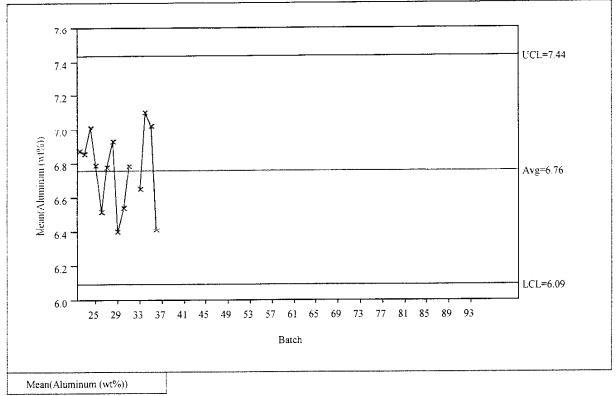




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Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte



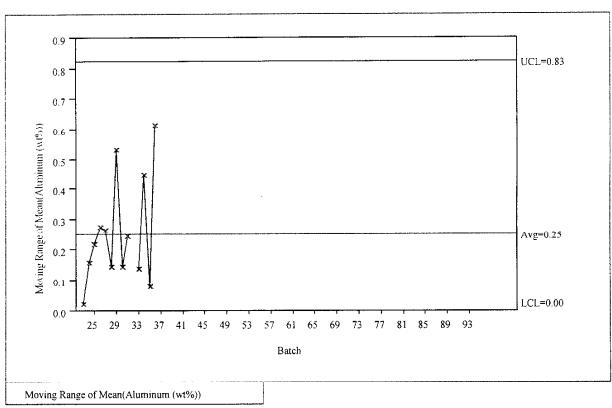
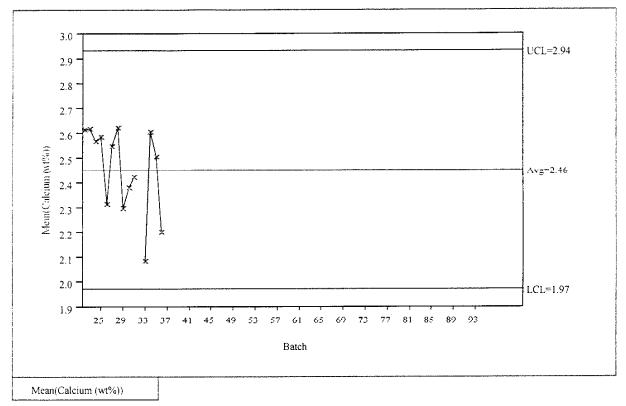
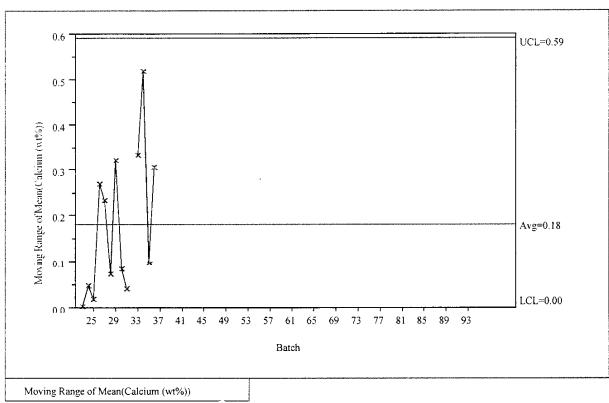


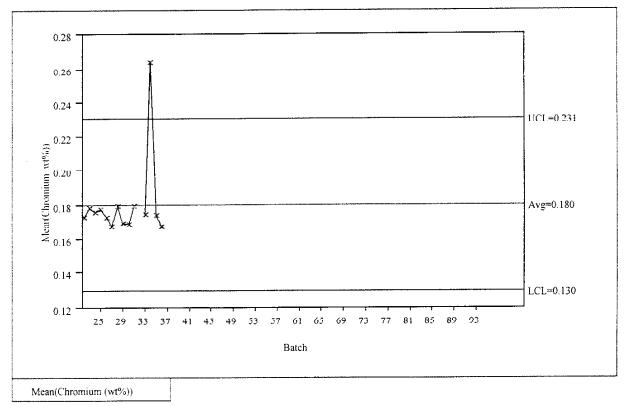
Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte





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Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte



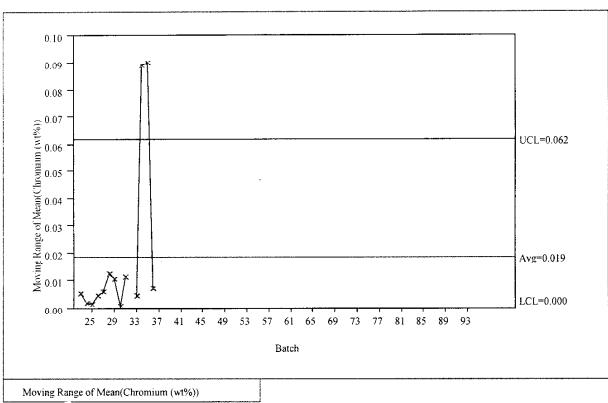
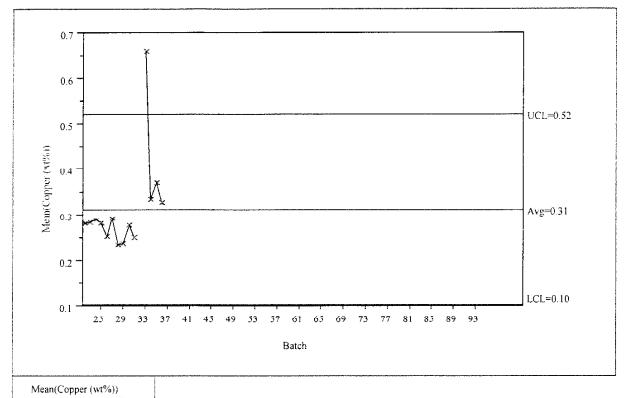
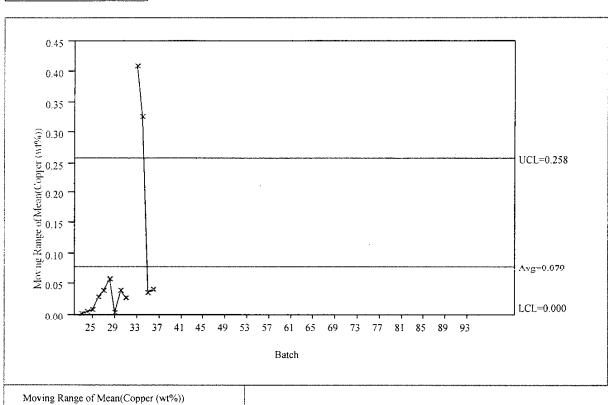


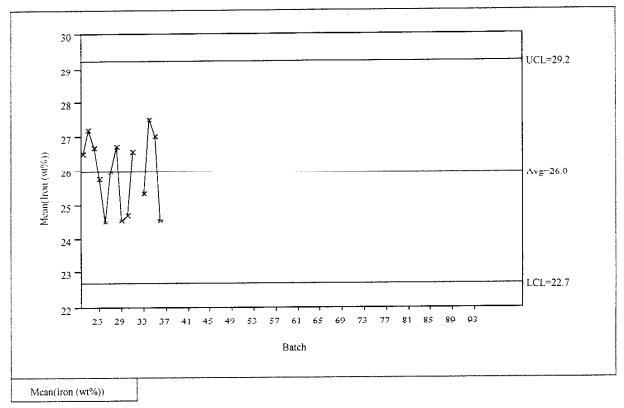
Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte





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Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte



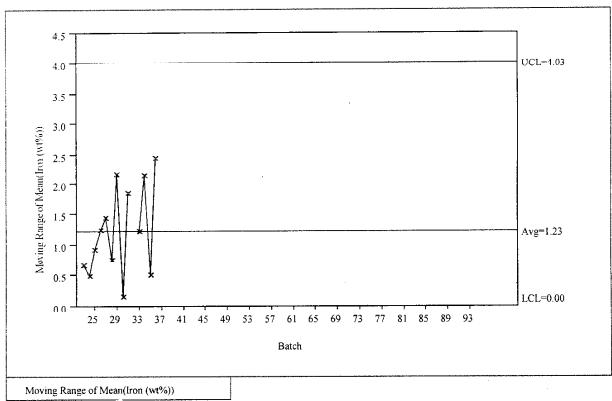
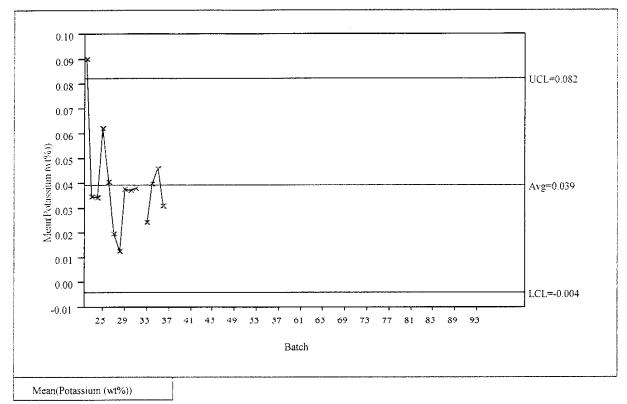
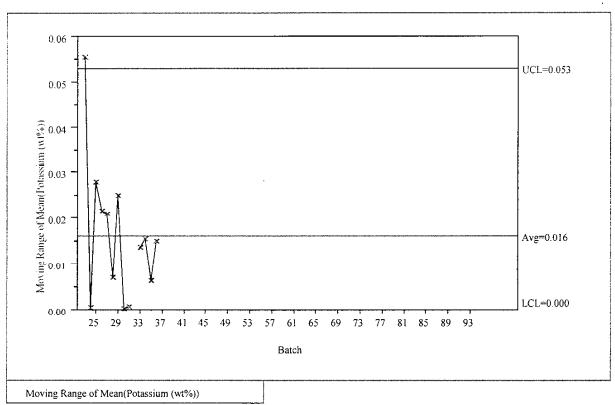
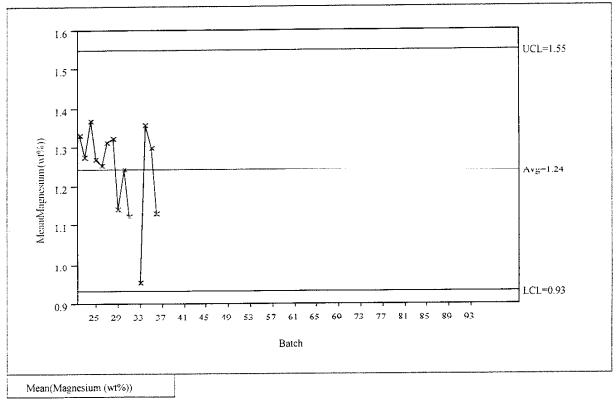


Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte





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Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte



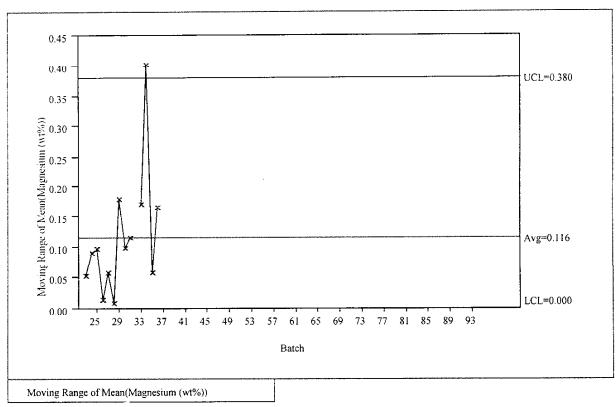
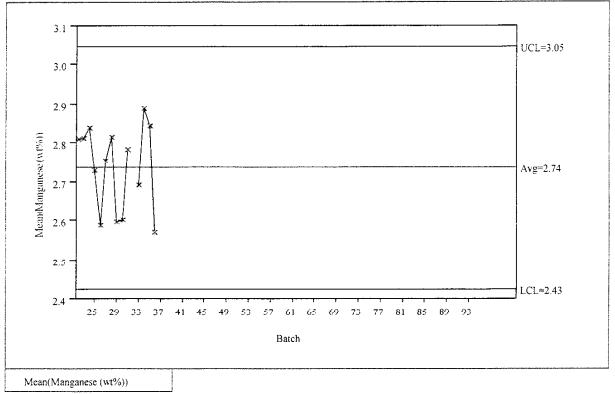
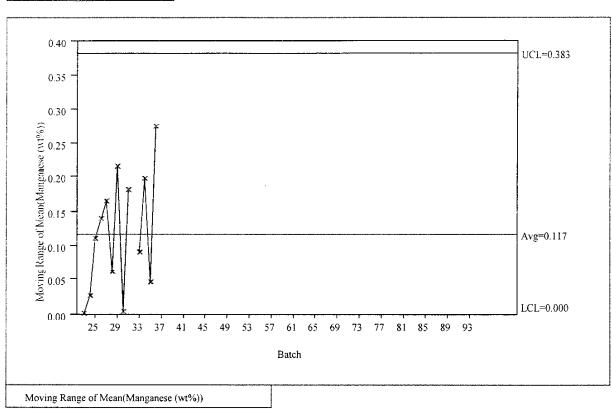


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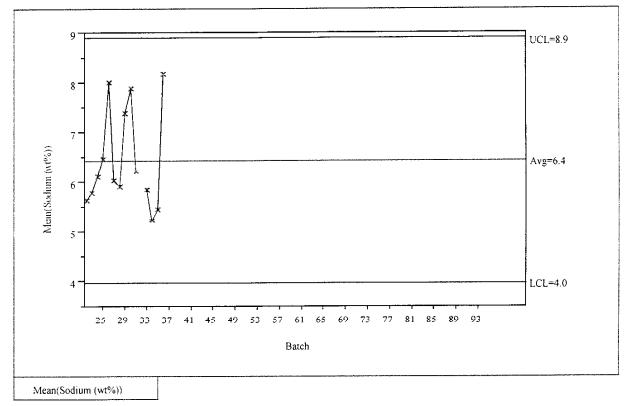




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Exhibit 6: SRAT Receipt Control Charts for Individual Batch Averages by Analyte



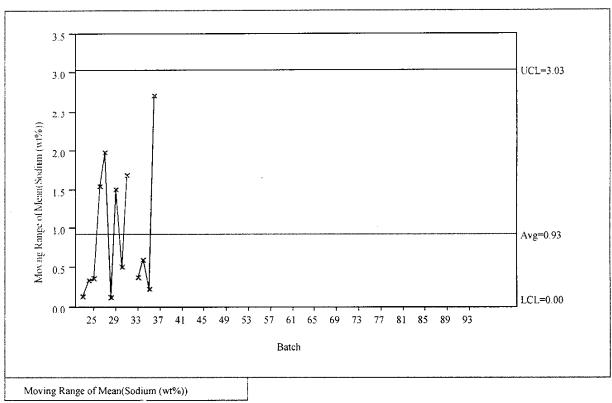
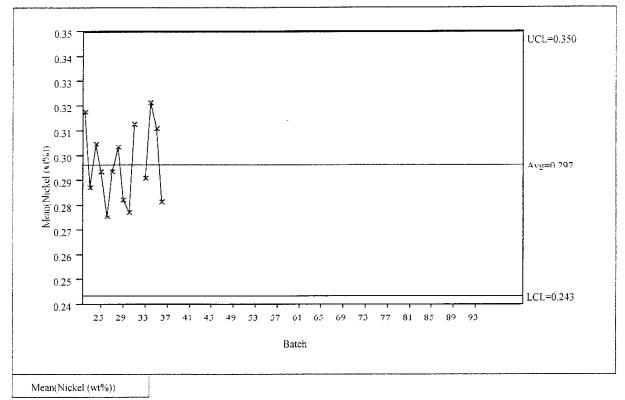
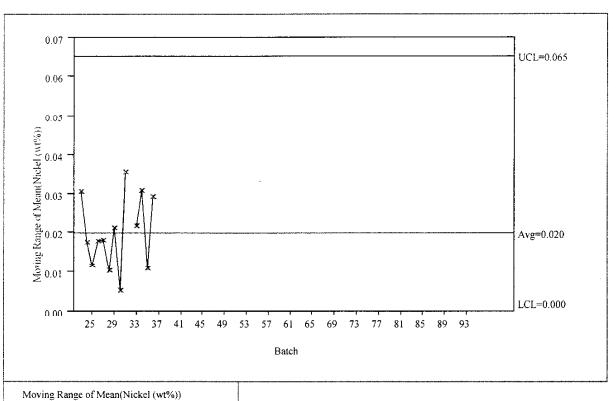


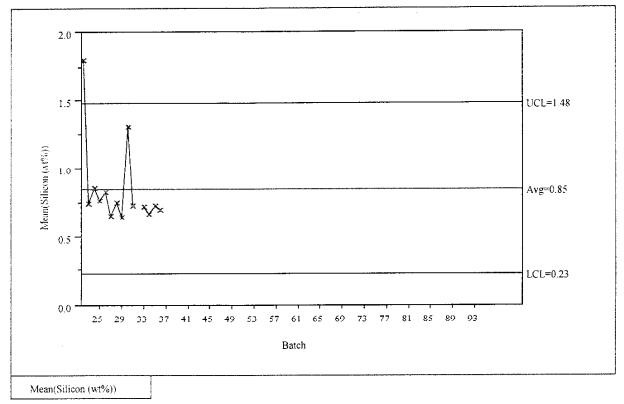
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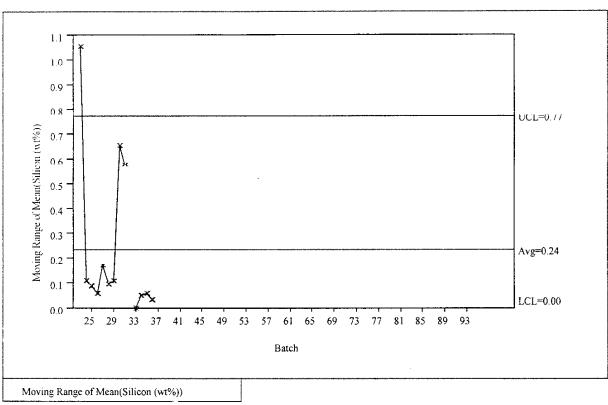
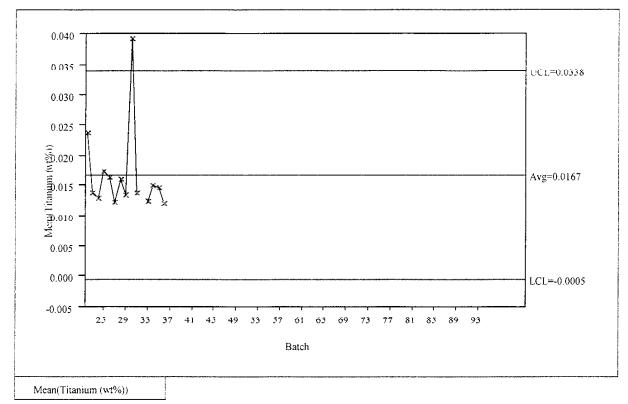
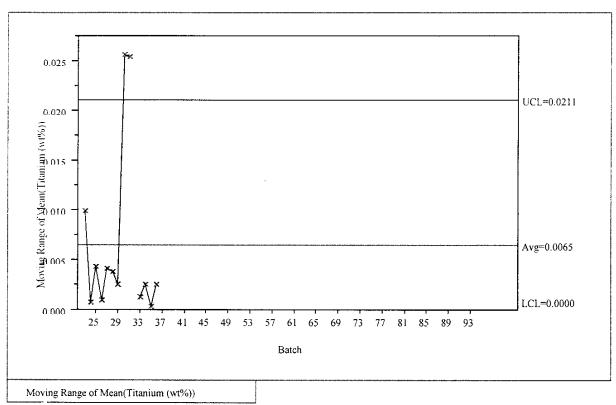


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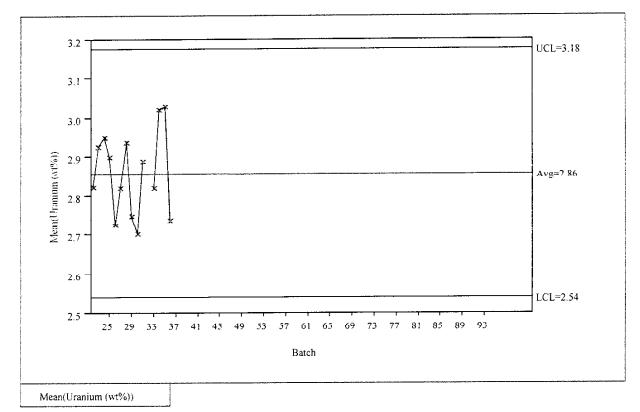




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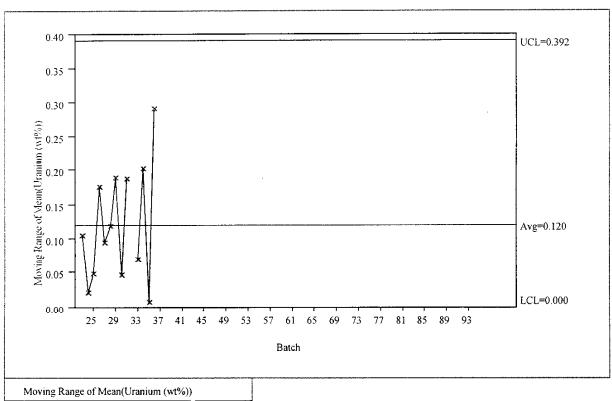
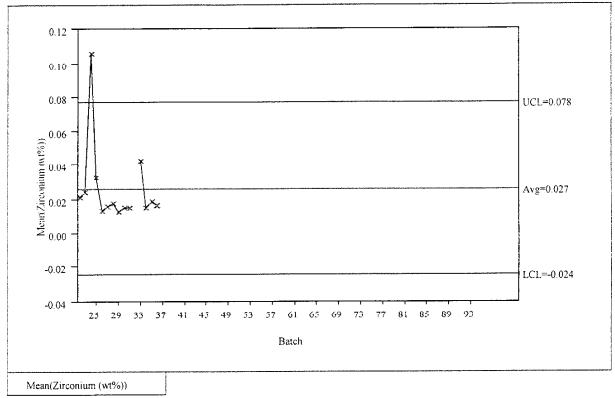


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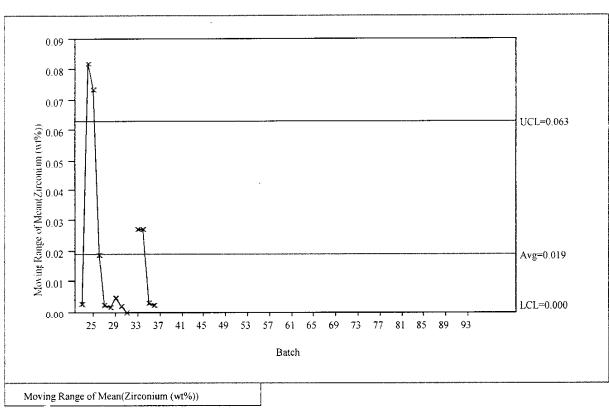
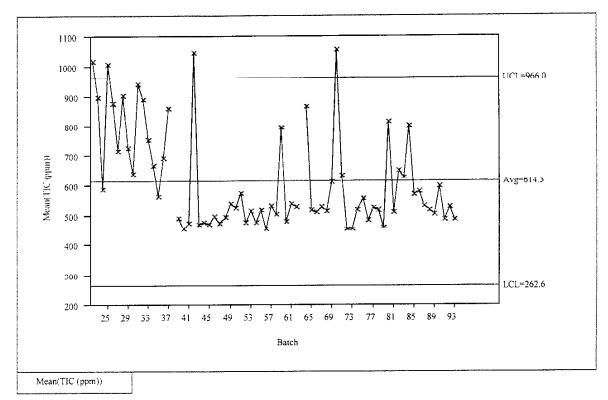


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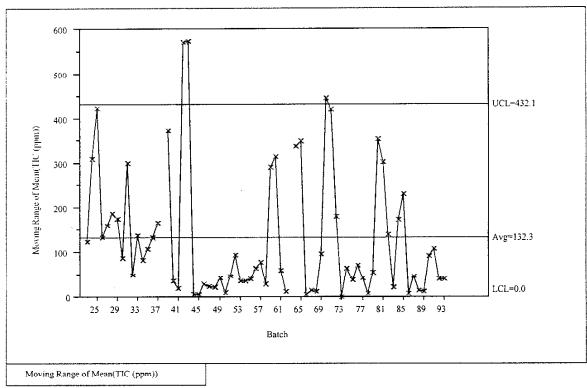
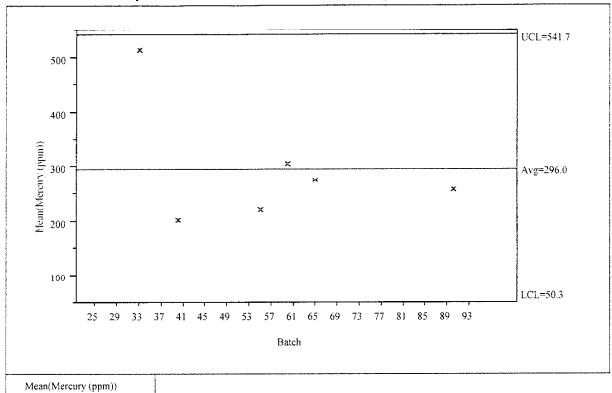


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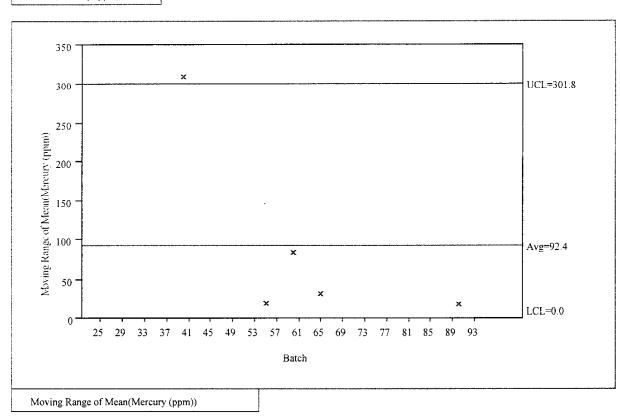
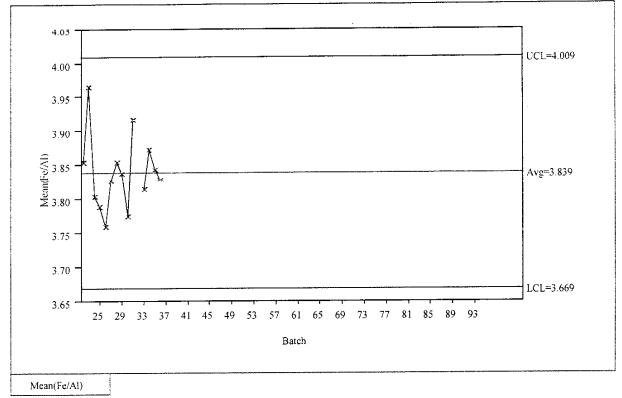


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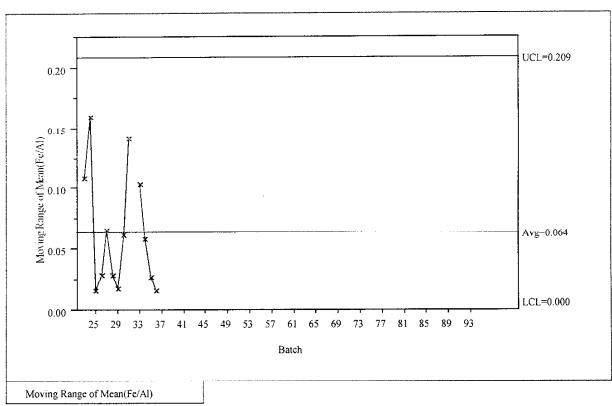
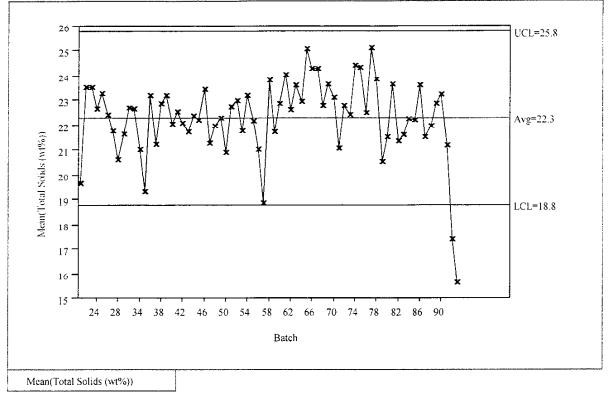


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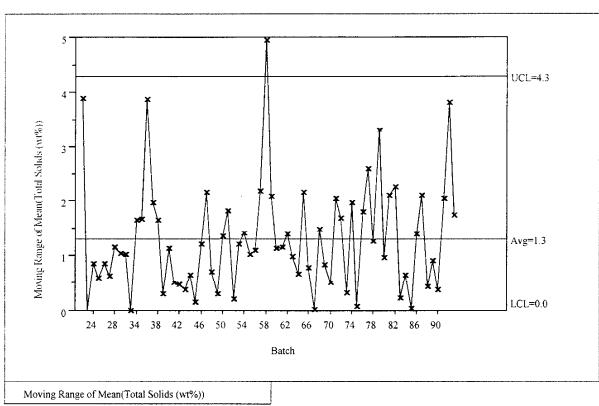
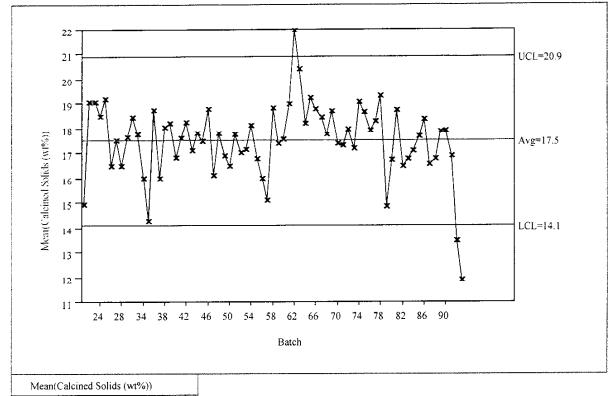


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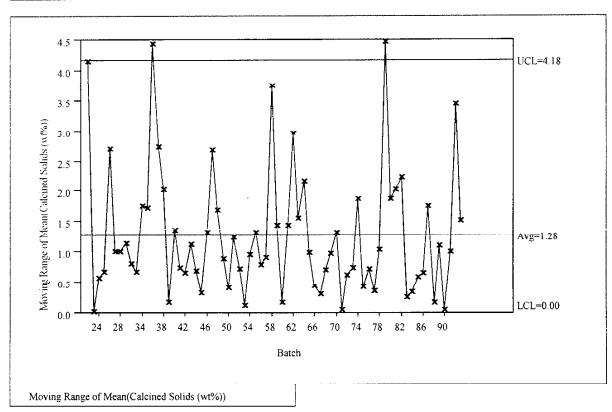
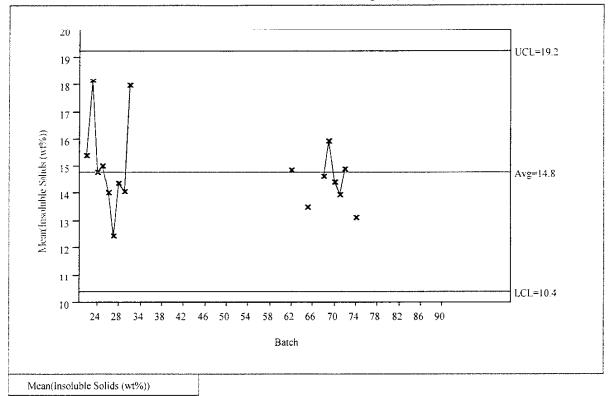


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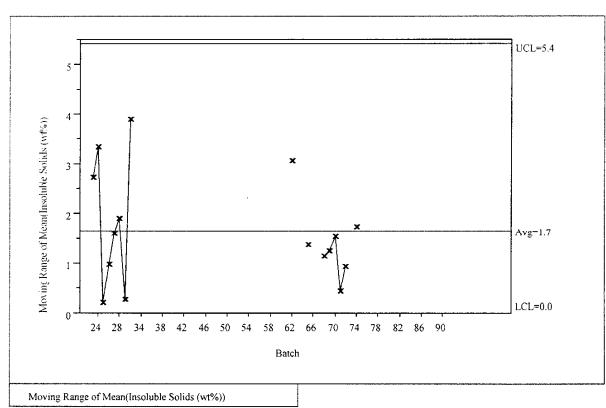
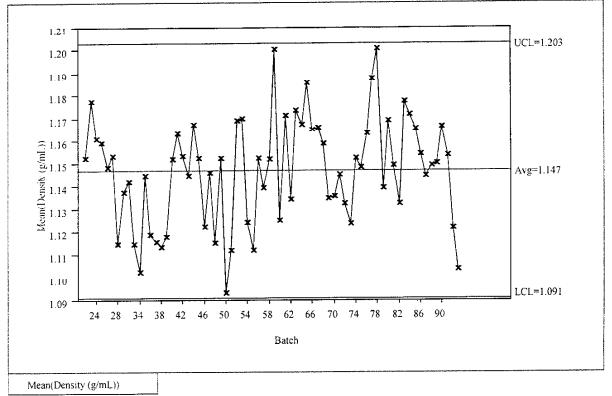


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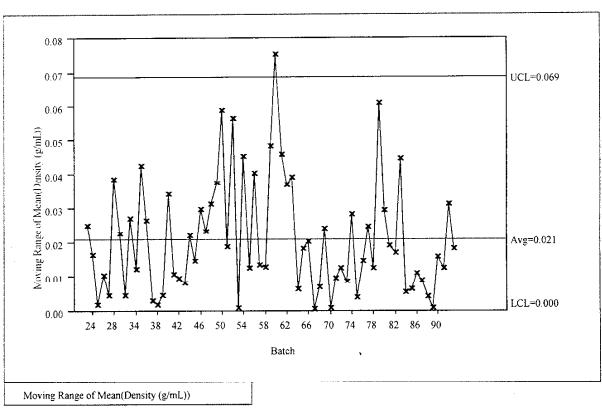
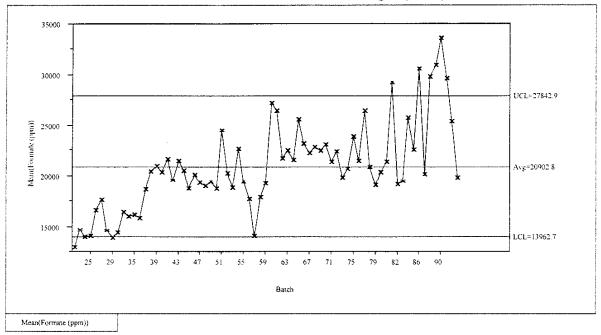
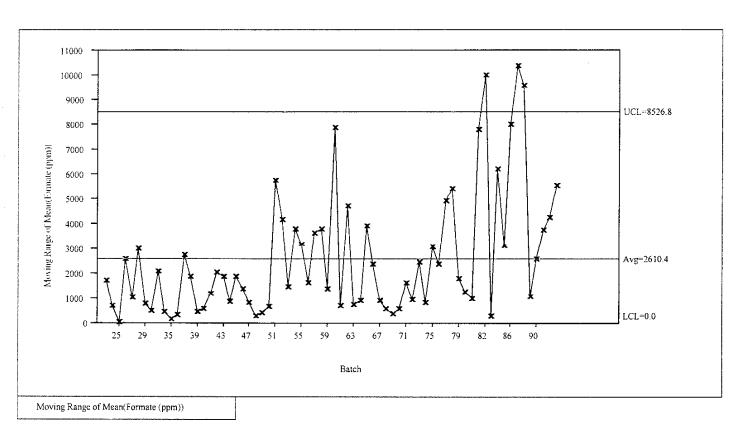


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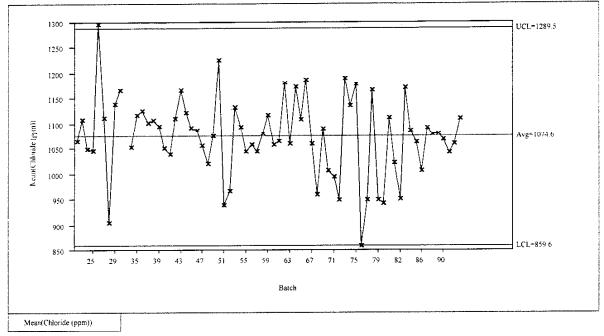




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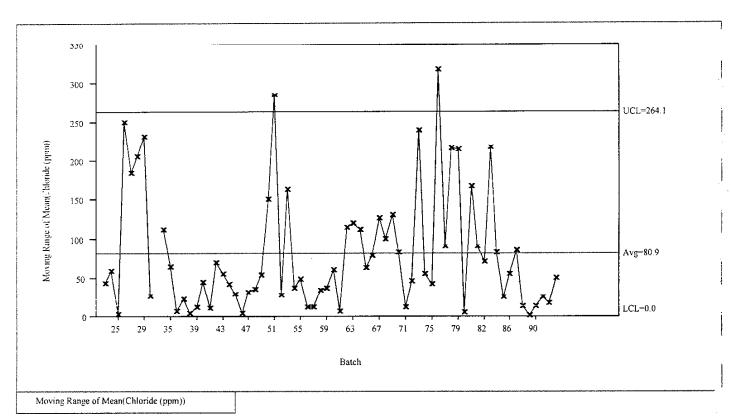
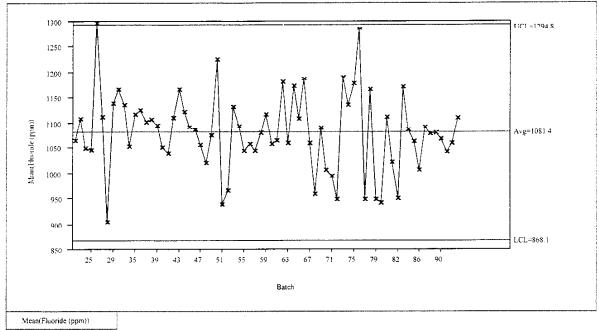
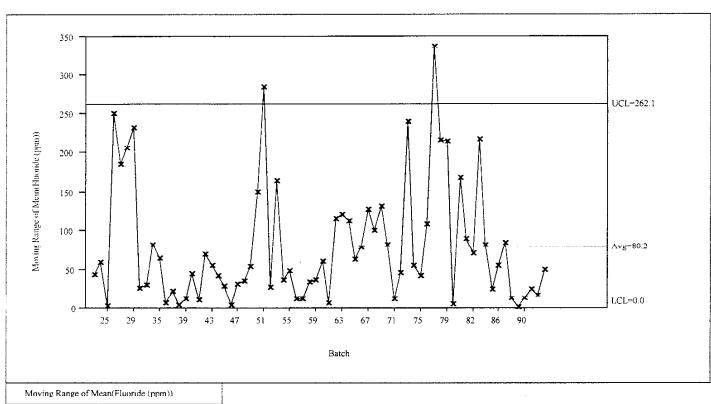


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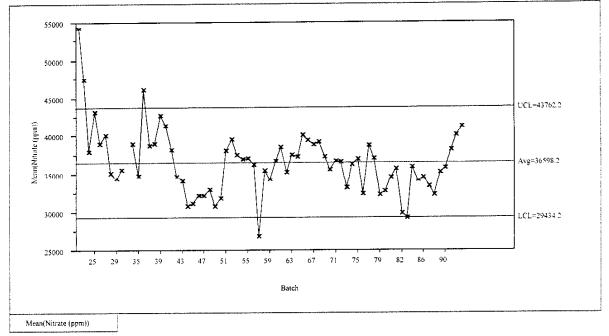




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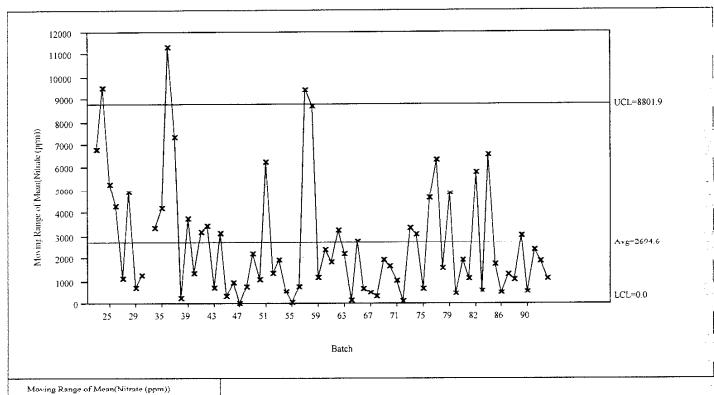
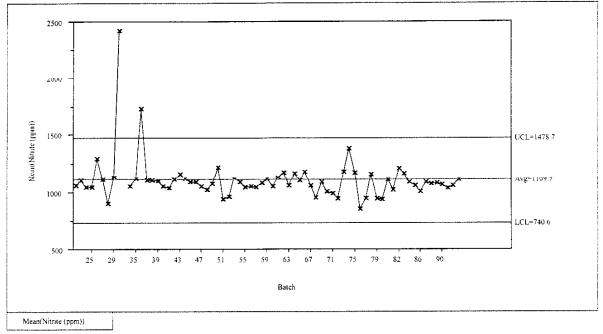
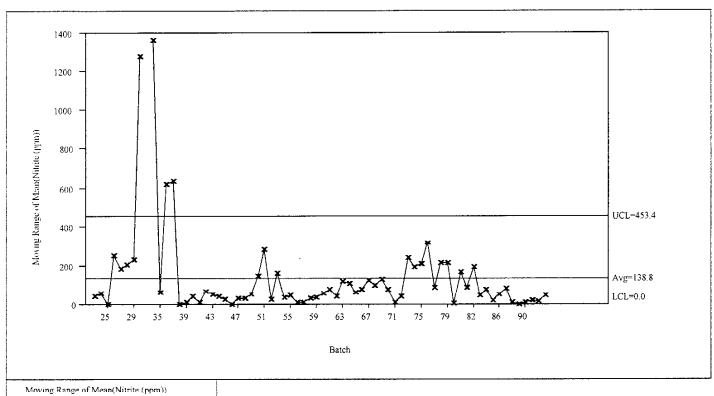


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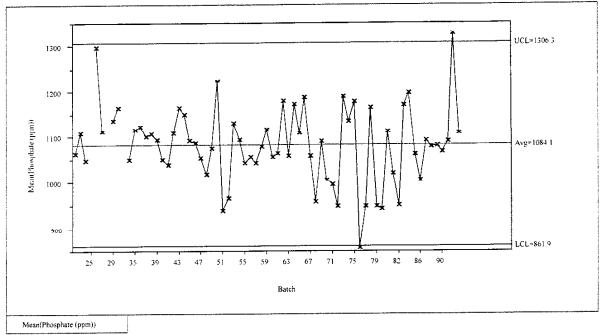




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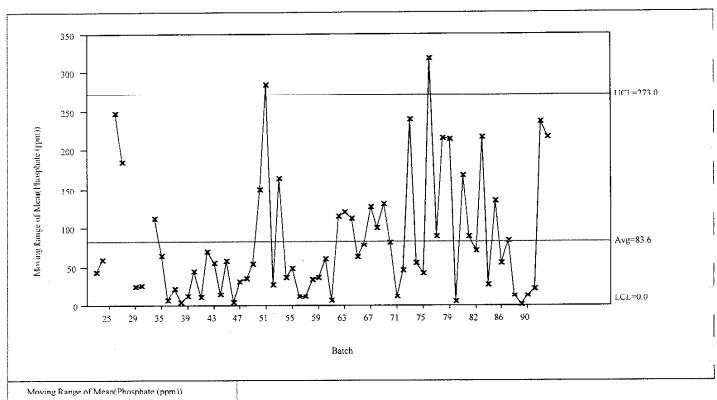
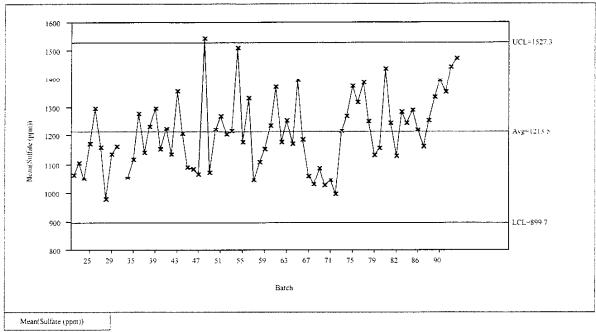


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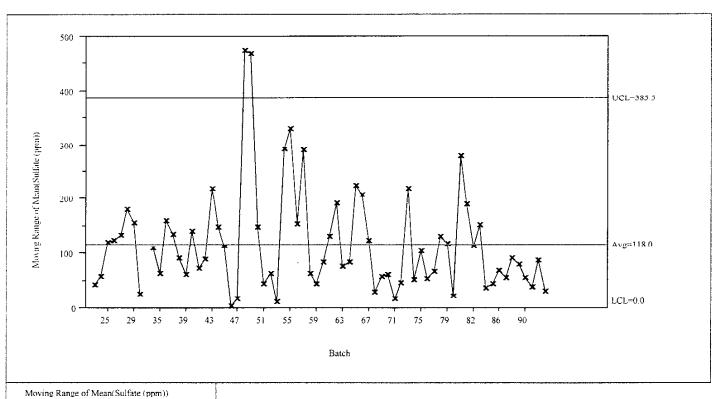
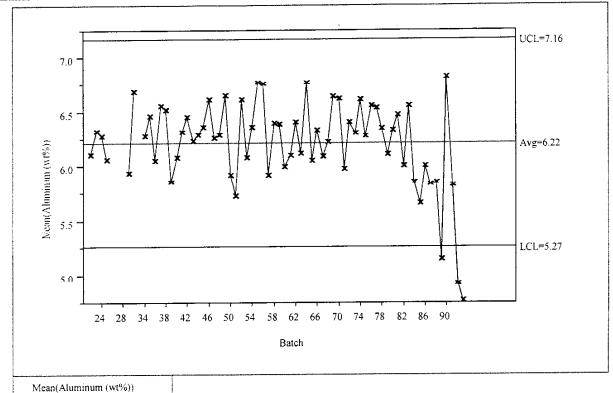


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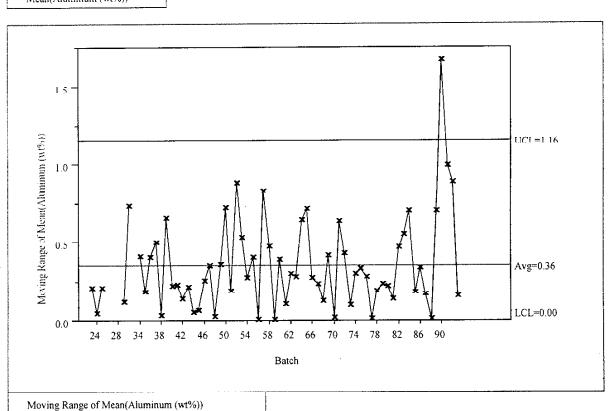
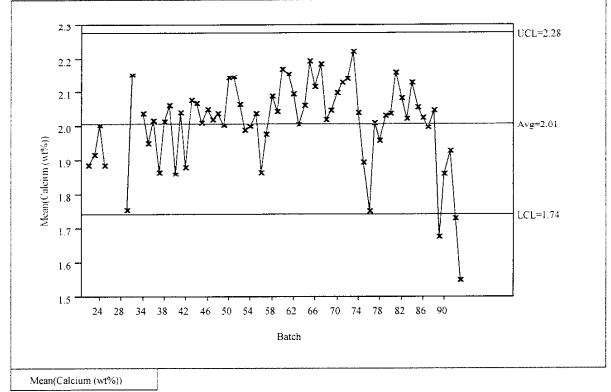


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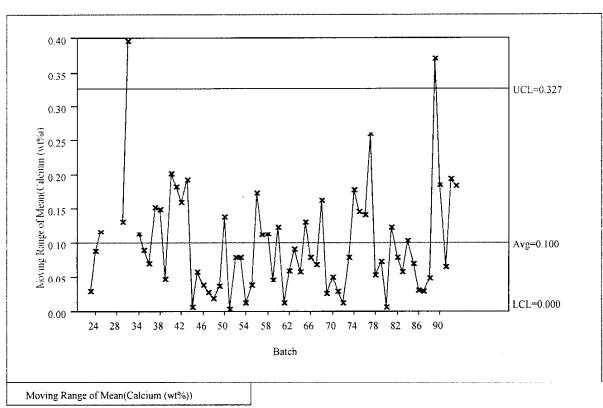
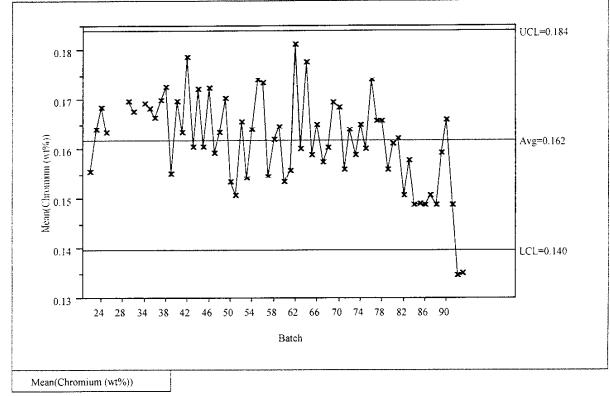


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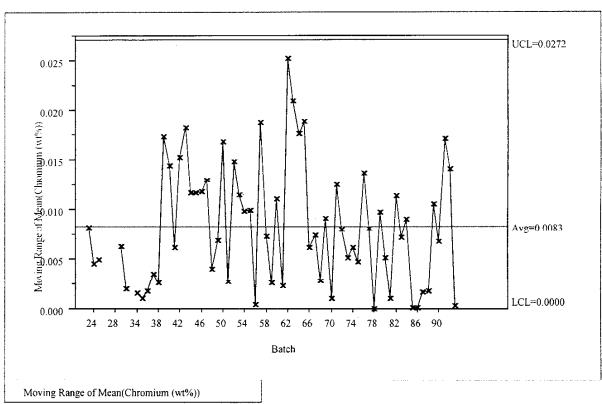
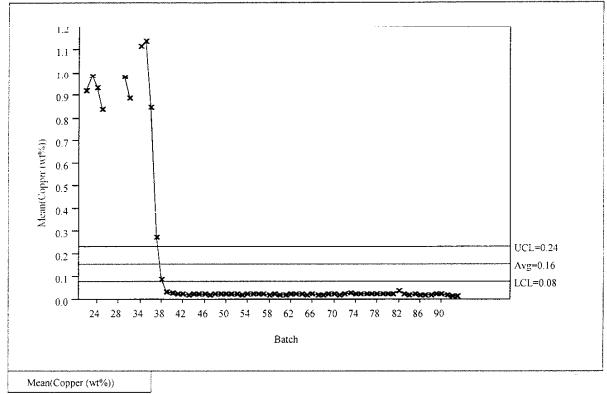


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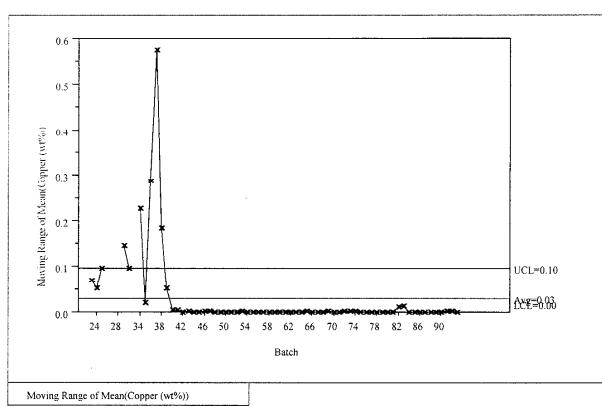
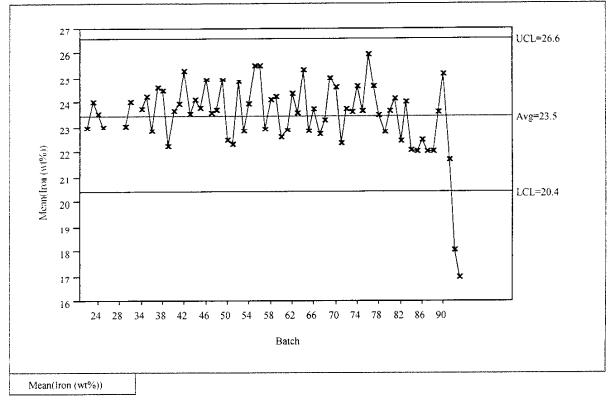


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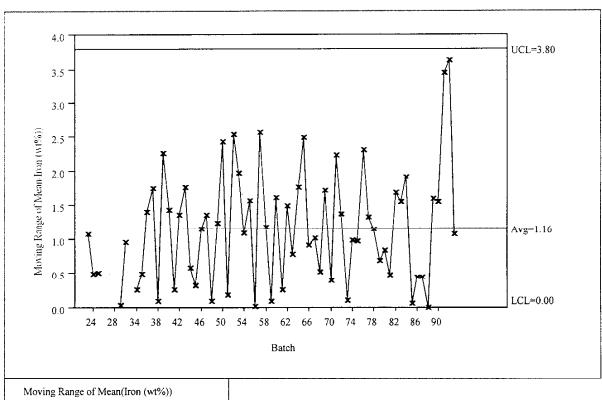
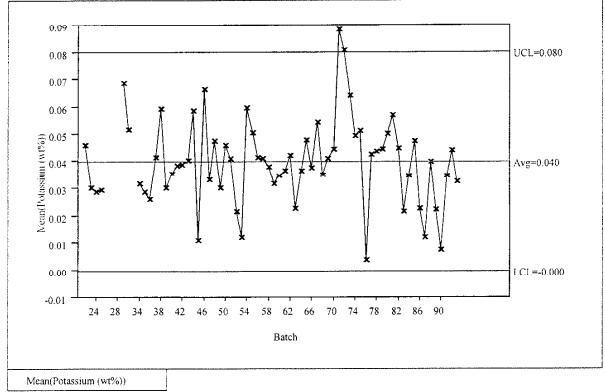


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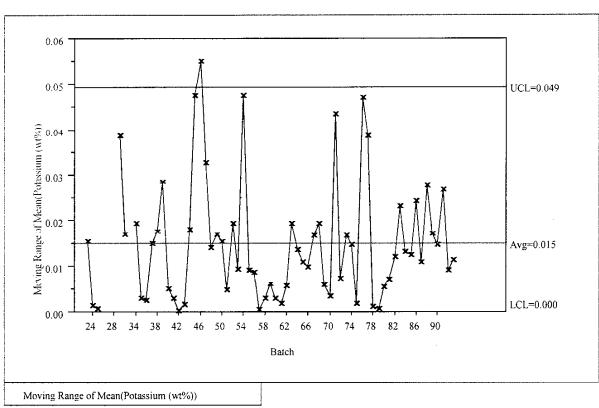
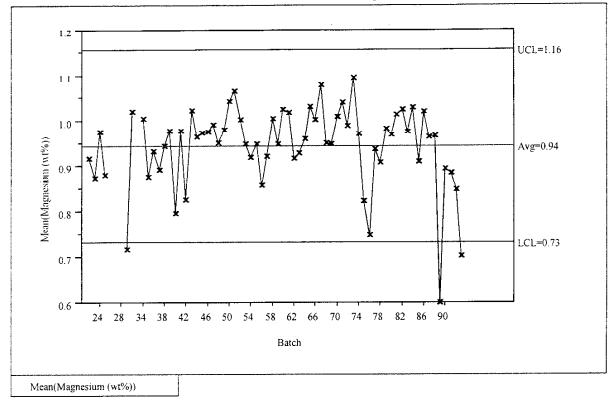


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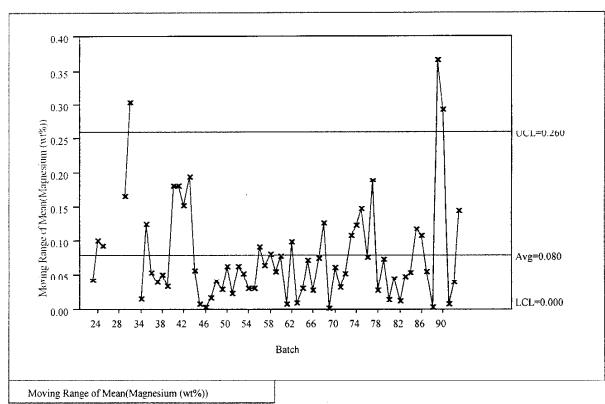
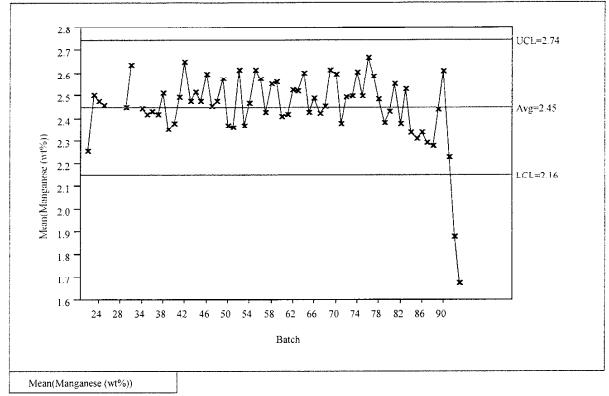


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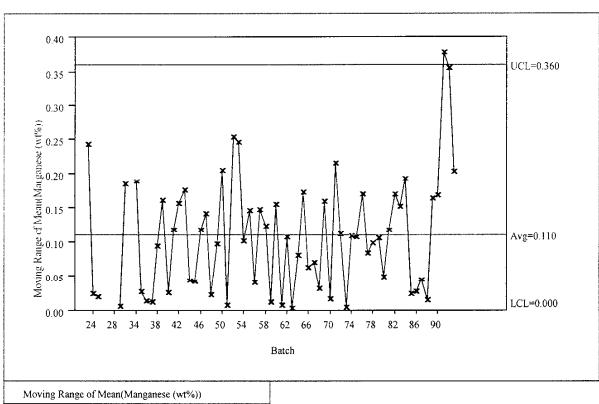
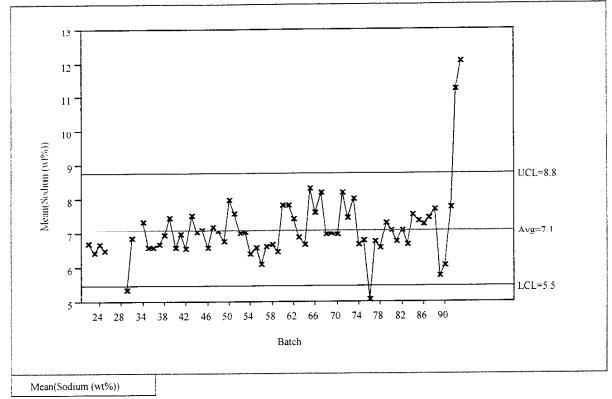


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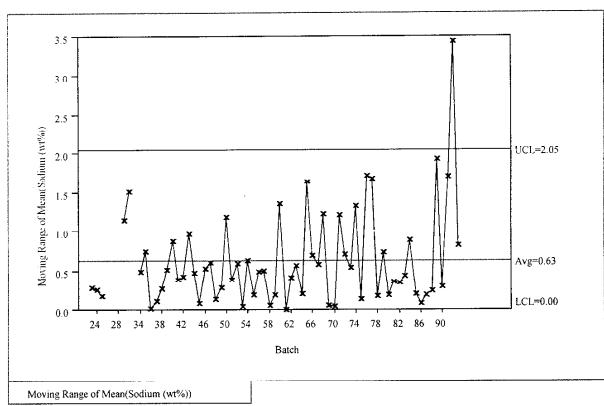
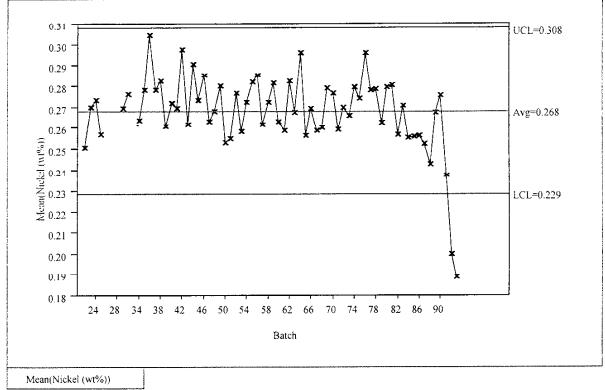


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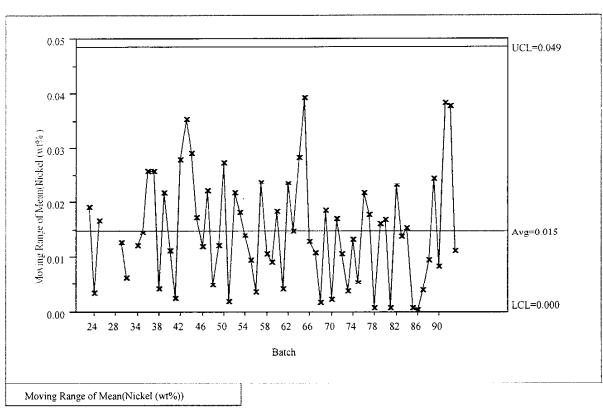
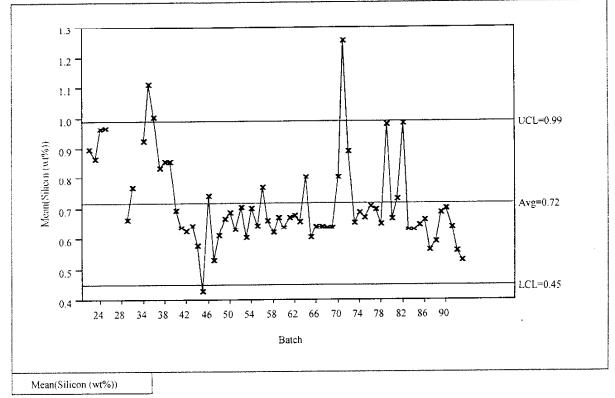


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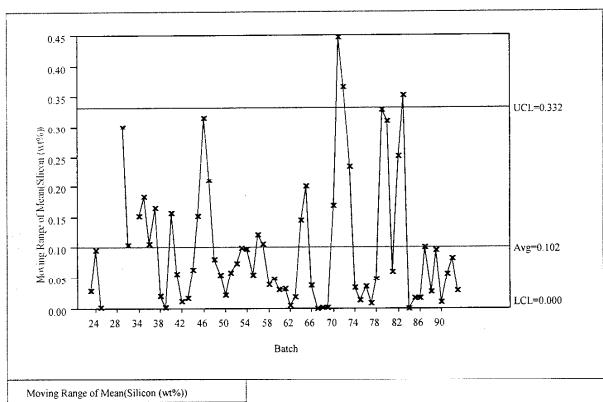
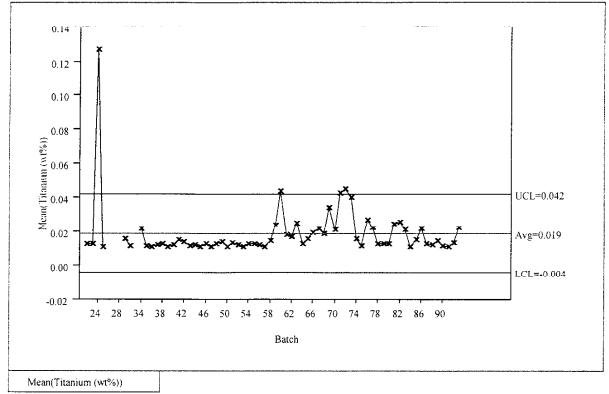


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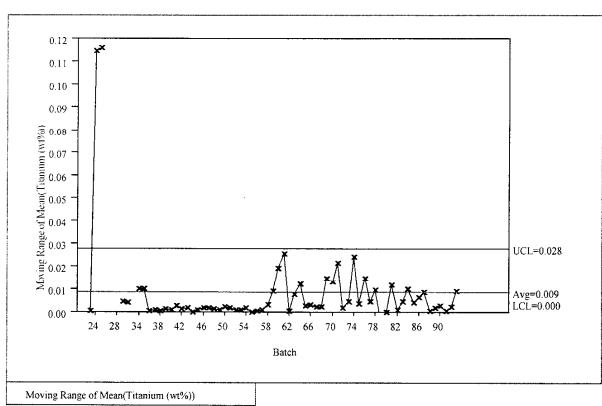
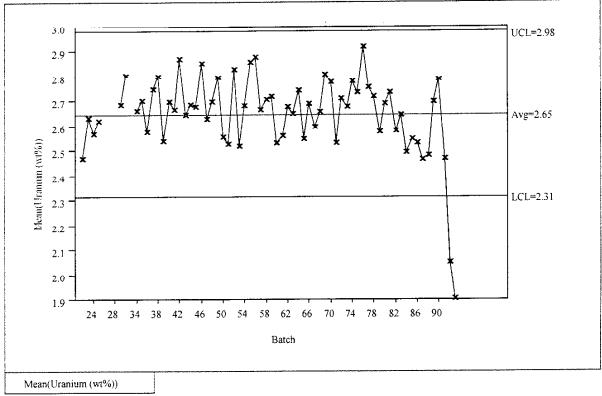


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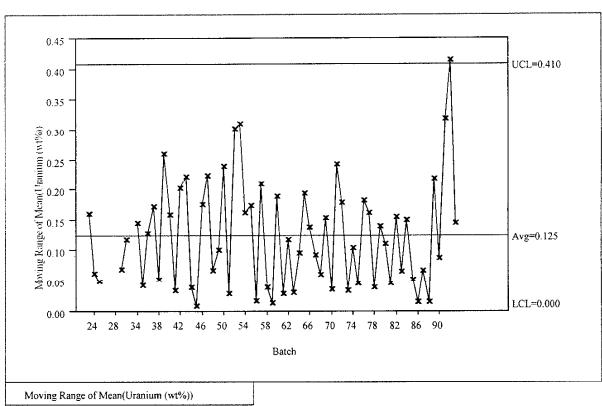
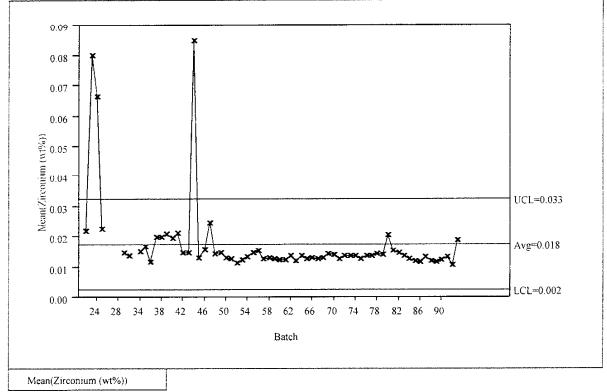


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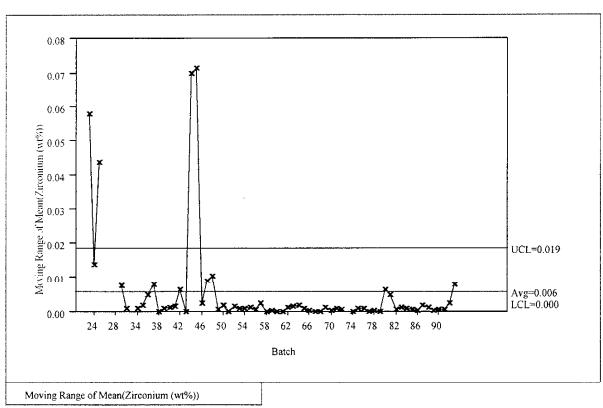
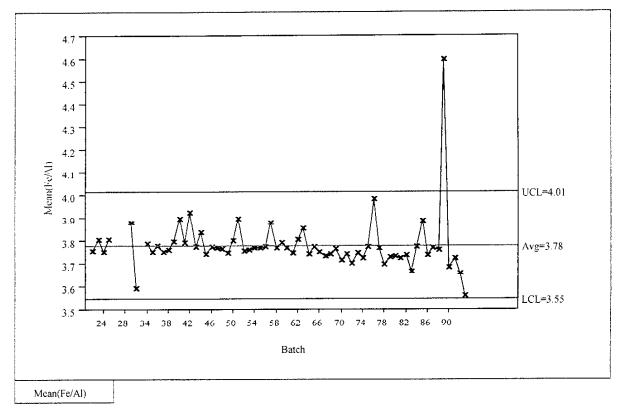


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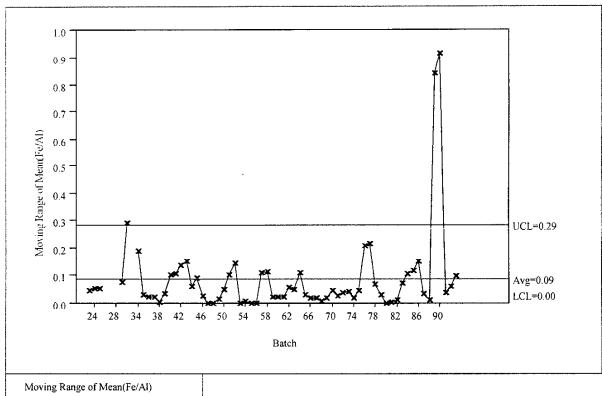
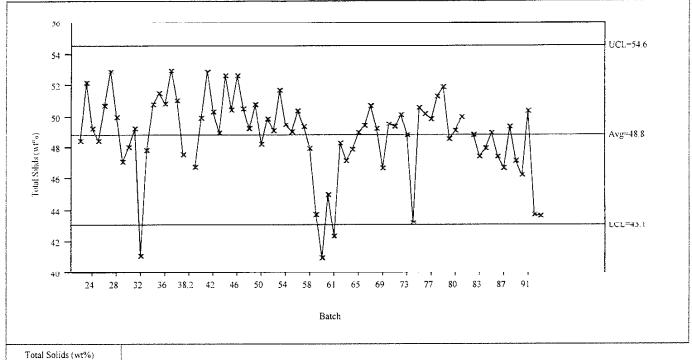
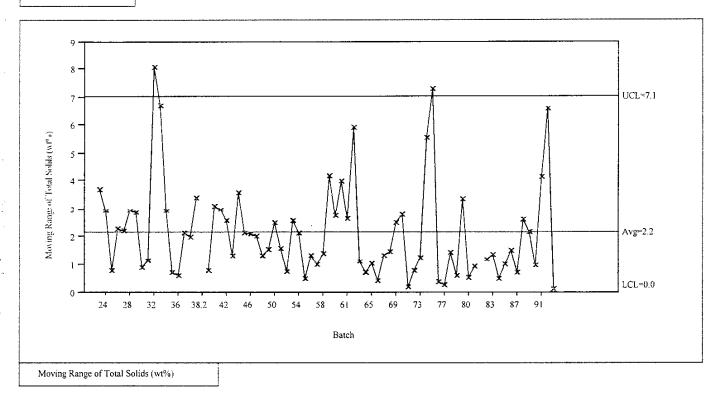


Exhibit 8a: SME Control Charts for Individual Batch Averages for Anions



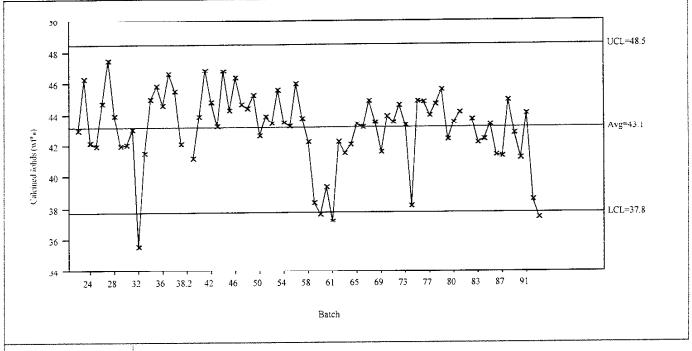




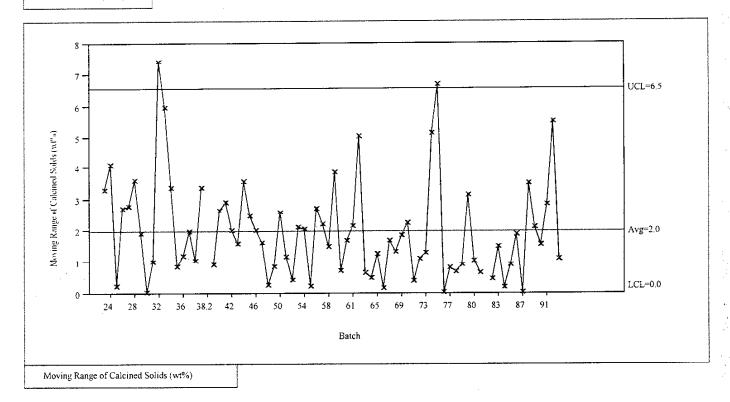
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Exhibit 8a: SME Control Charts for Individual Batch Averages for Anions



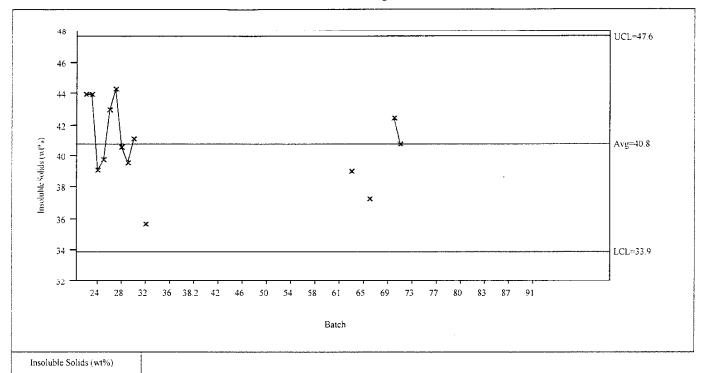
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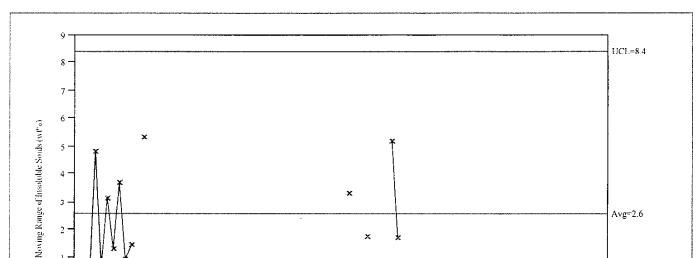


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87 91

Exhibit 8a: SME Control Charts for Individual Batch Averages for Anions





69 73 77 80 83

Moving Range of Insoluble Solids (wt%)

28

32

36 38.2 42

50

54 58 61 65

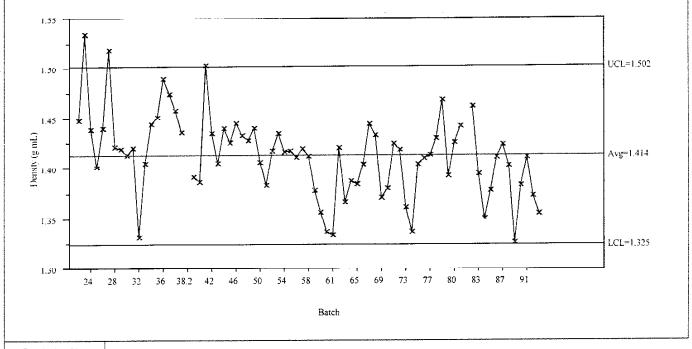
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Batch

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Exhibit 8a: SME Control Charts for Individual Batch Averages for Anions





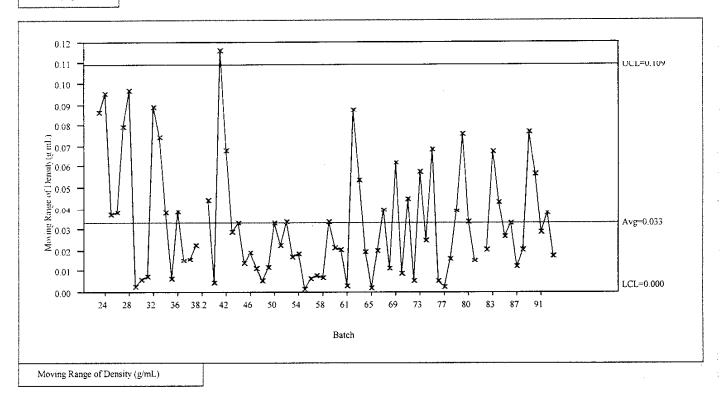
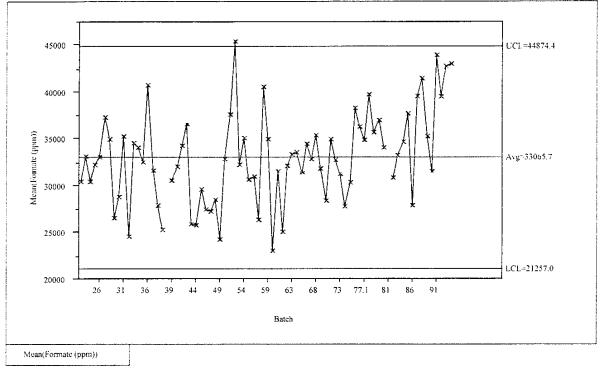
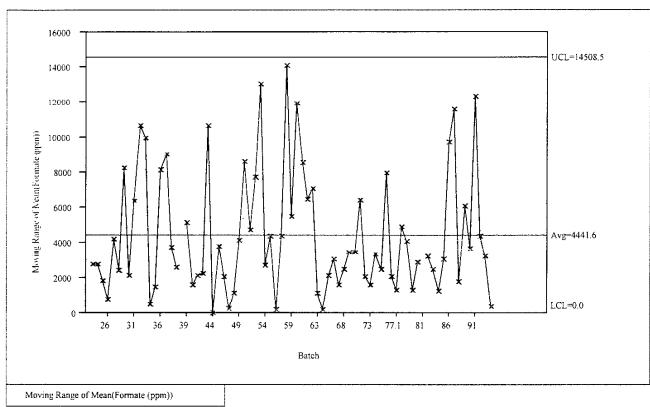


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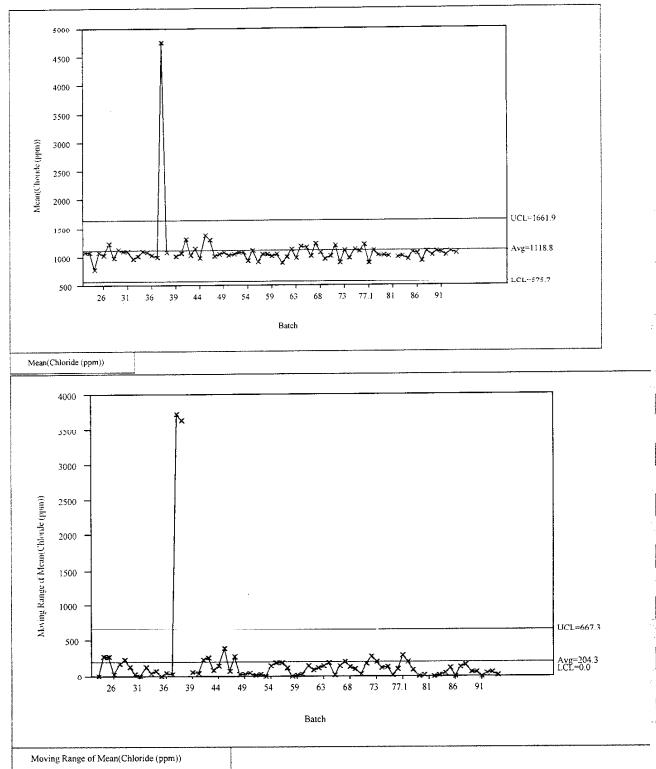
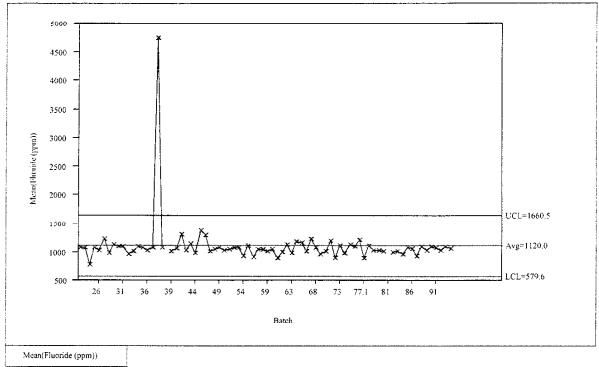
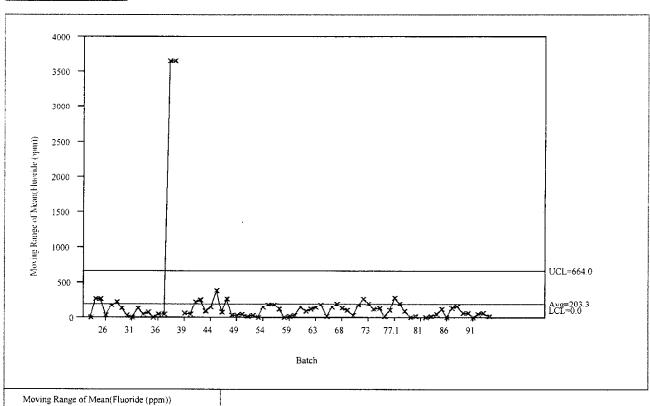


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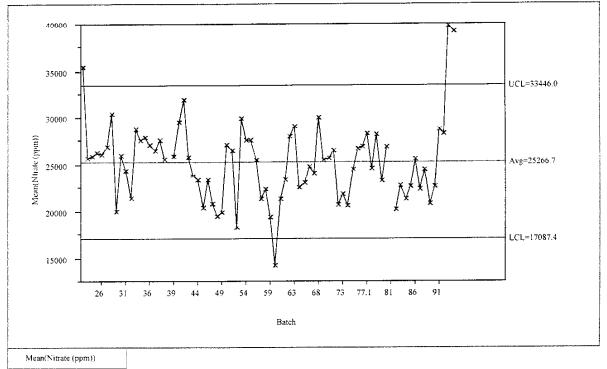




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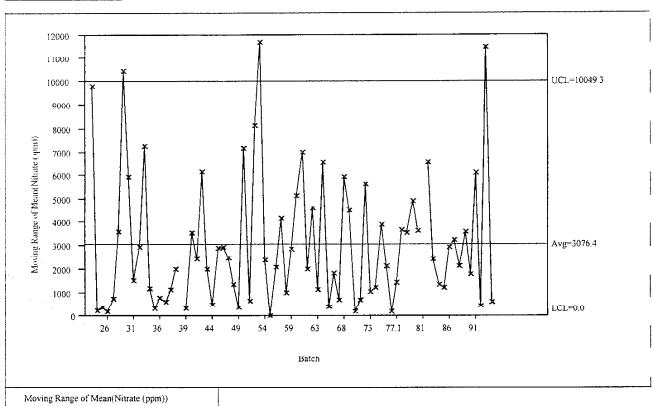
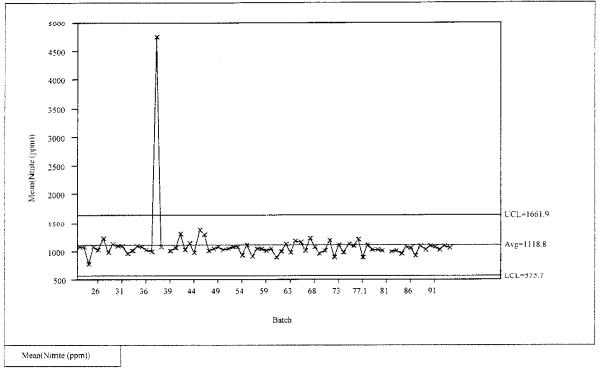
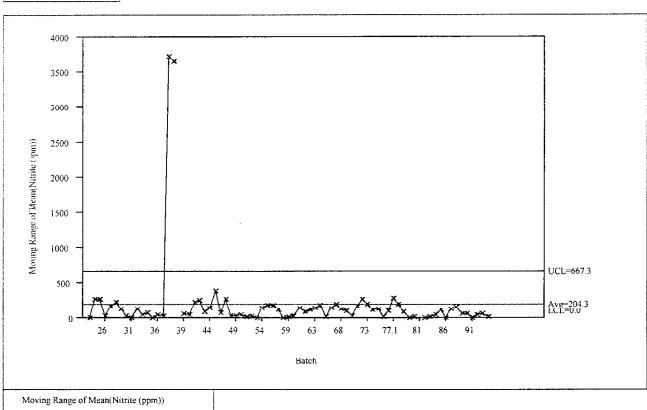


Exhibit 8a: SME Control Charts for Individual Batch Averages for Anions

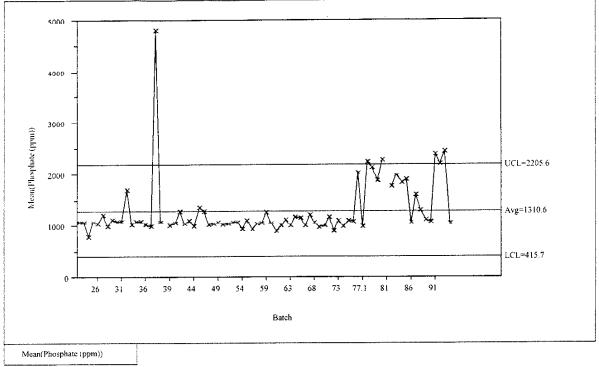




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Exhibit 8a: SME Control Charts for Individual Batch Averages for Anions



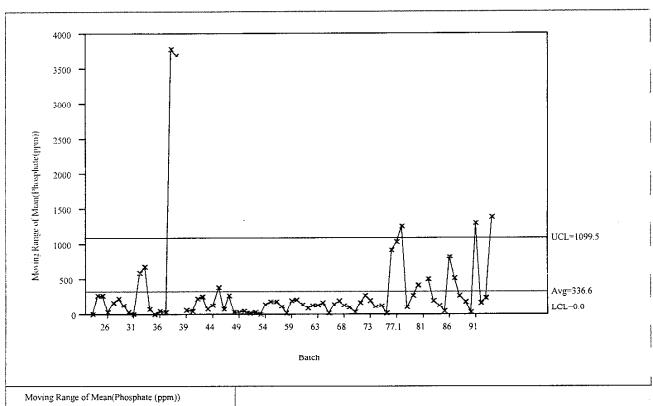
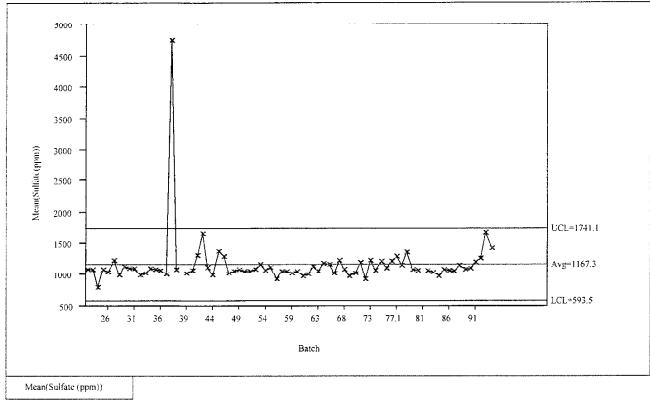
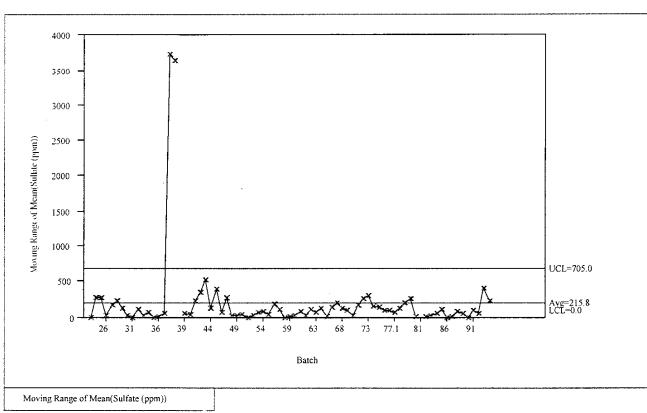
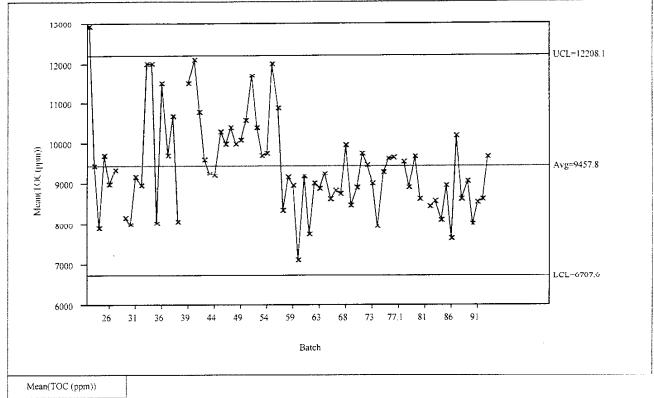


Exhibit 8a: SME Control Charts for Individual Batch Averages for Anions





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Exhibit 8a: SME Control Charts for Individual Batch Averages for Anions



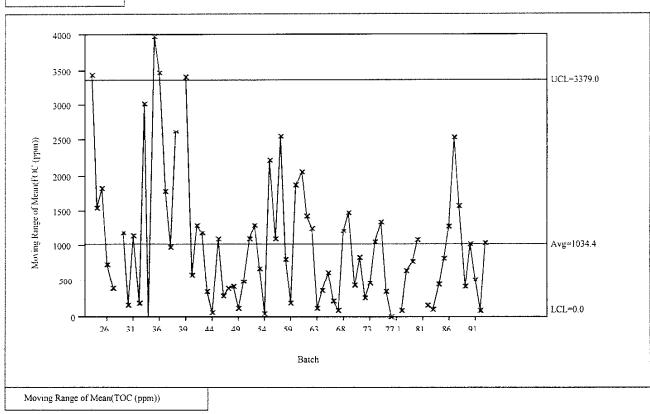
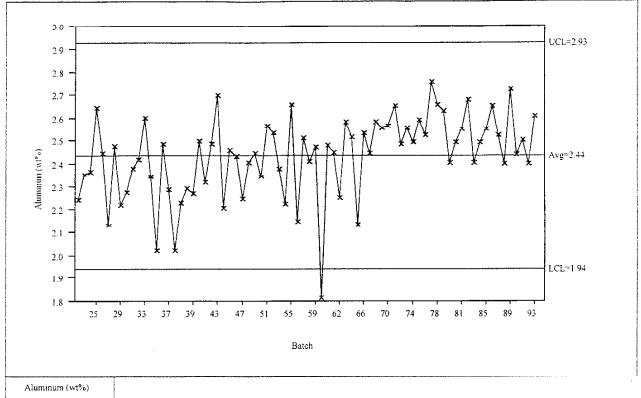
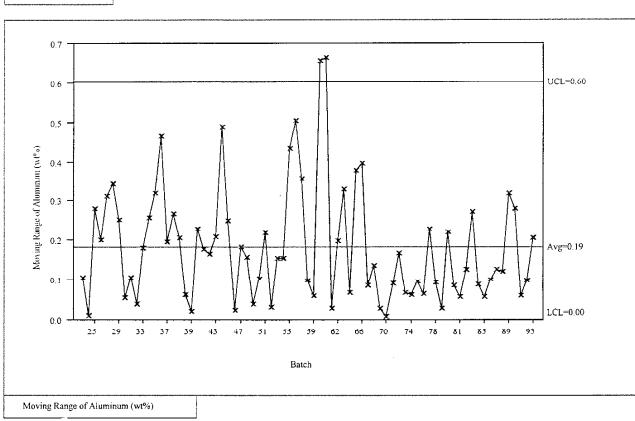
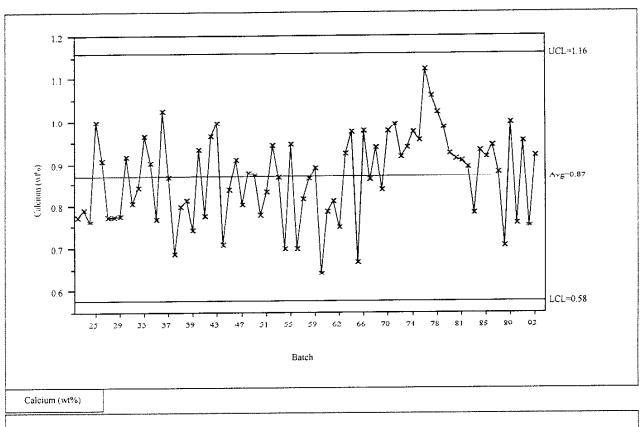


Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte





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Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte



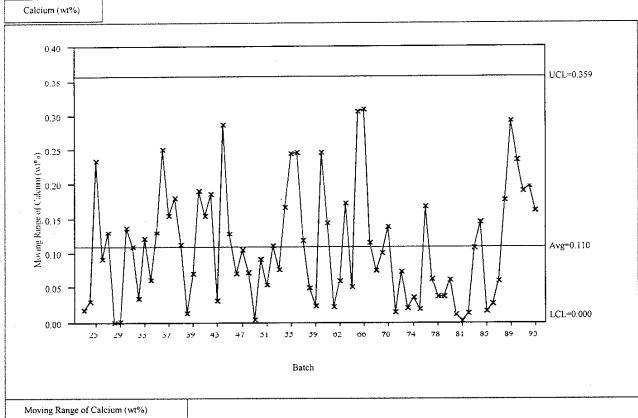
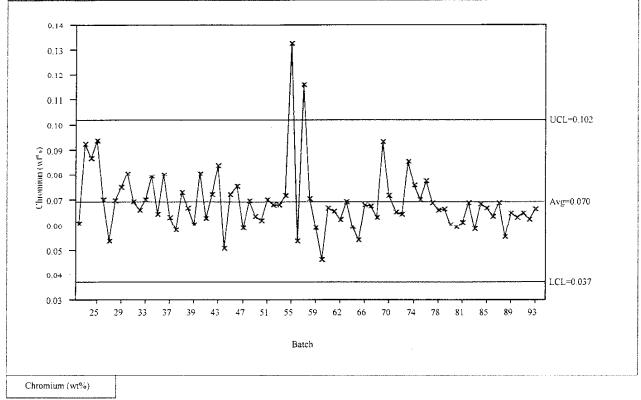
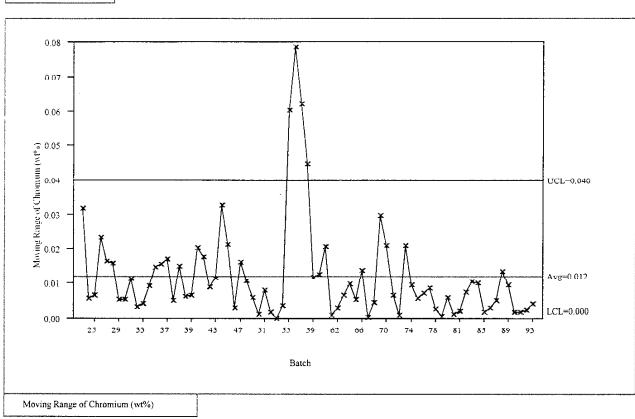


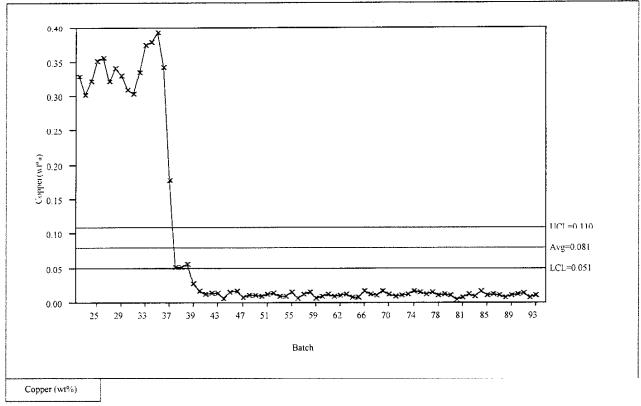
Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte





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Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte



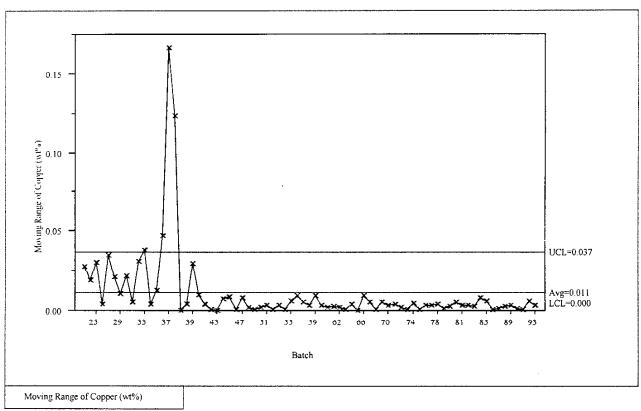
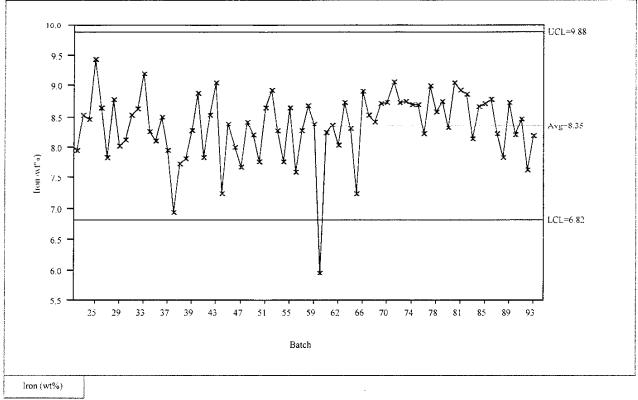
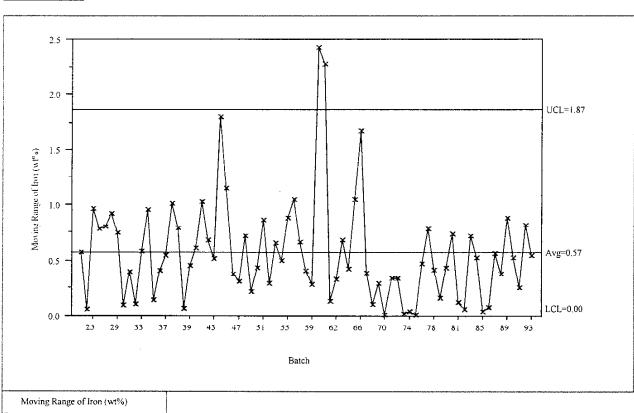


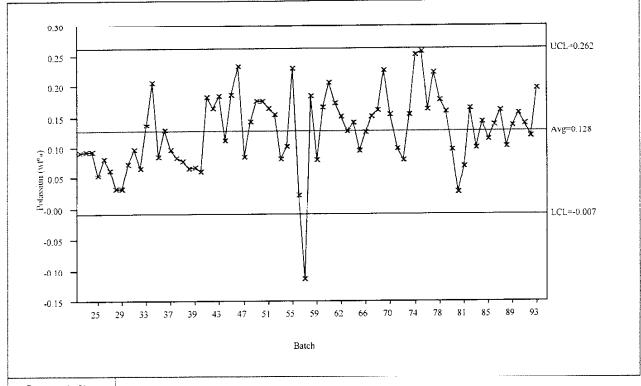
Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte





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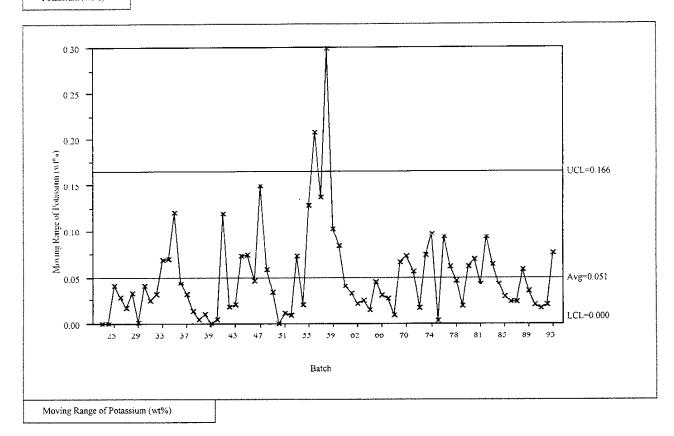
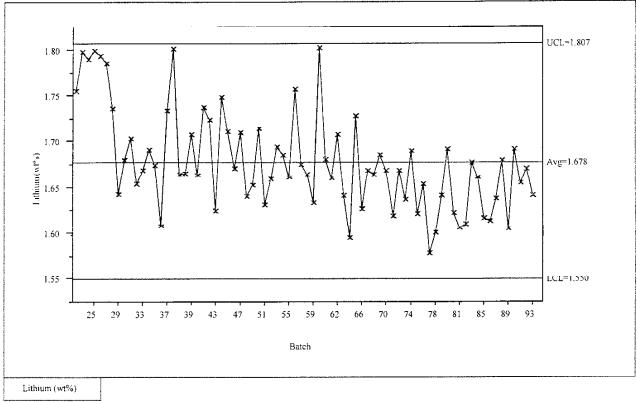
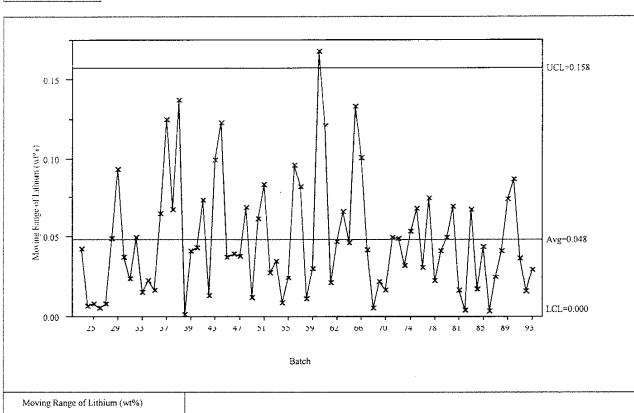


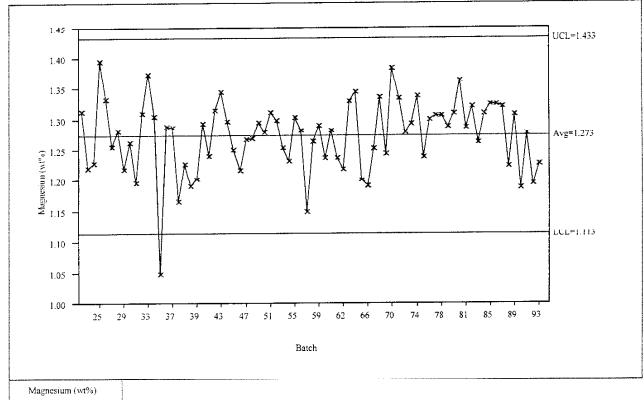
Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte





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Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte



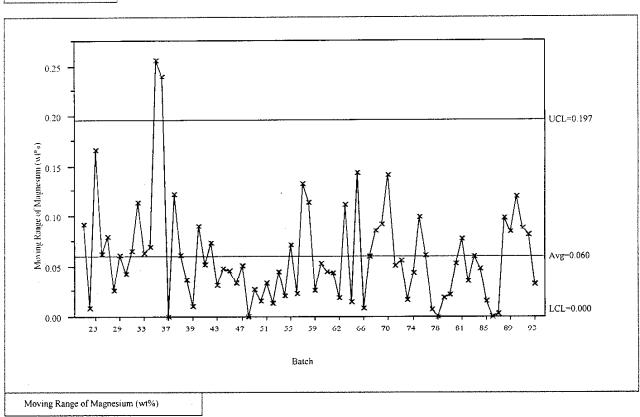
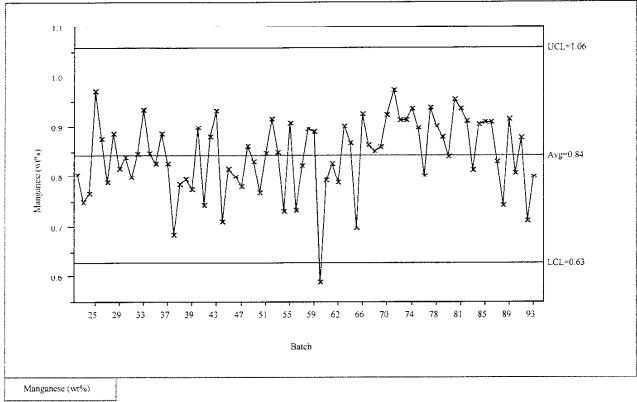
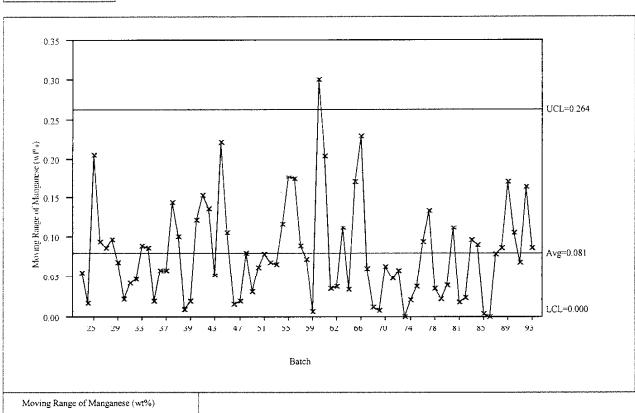


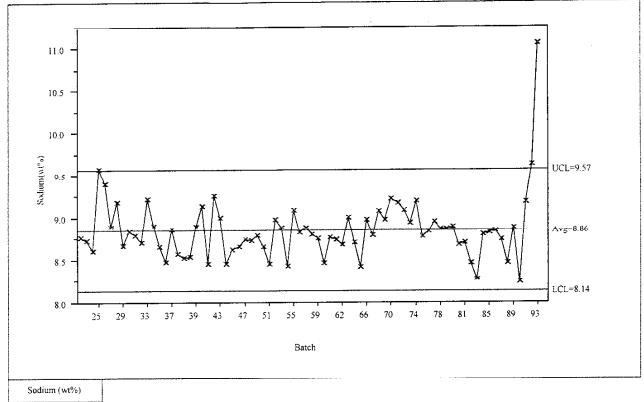
Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte





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Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte



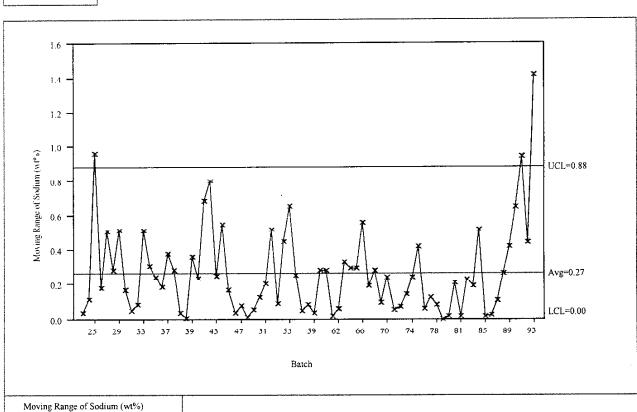
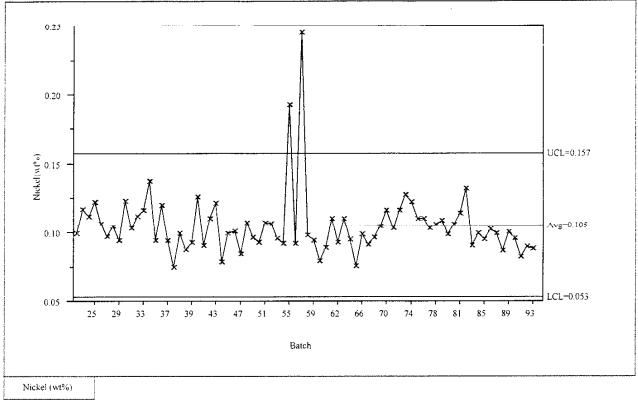
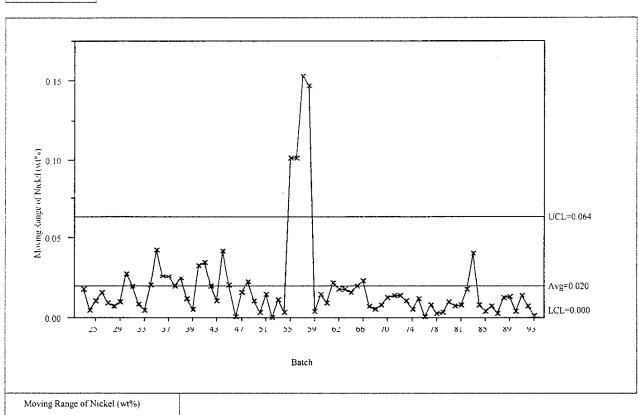


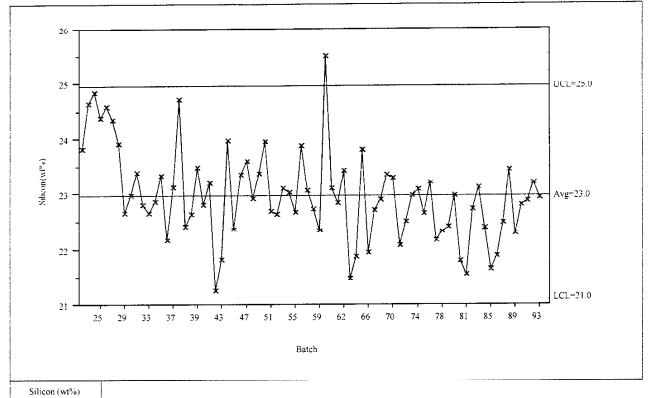
Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte





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Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte



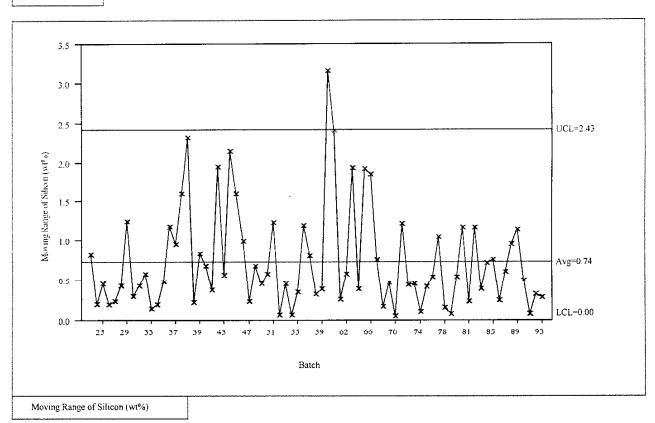
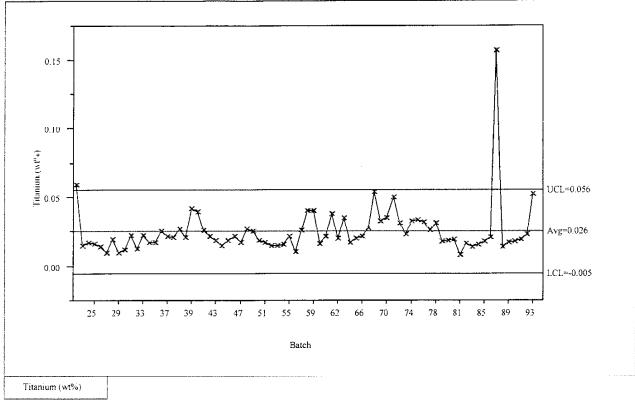
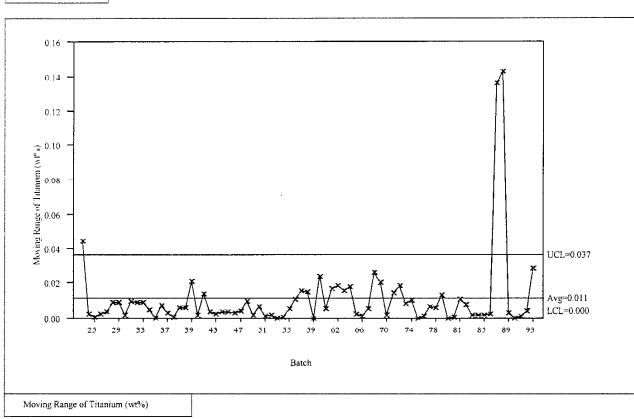


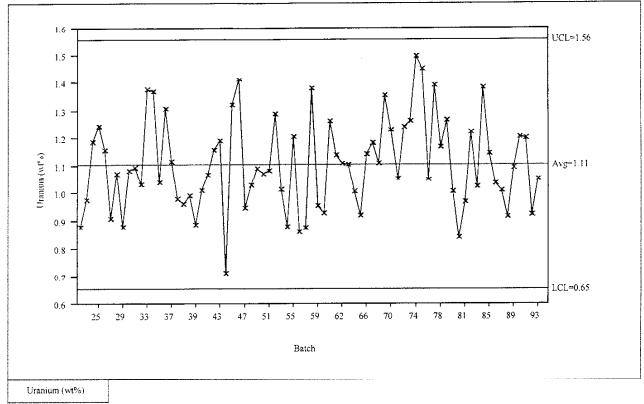
Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte





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Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte



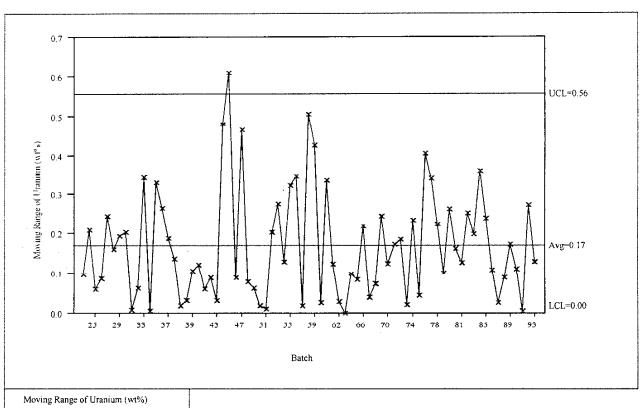
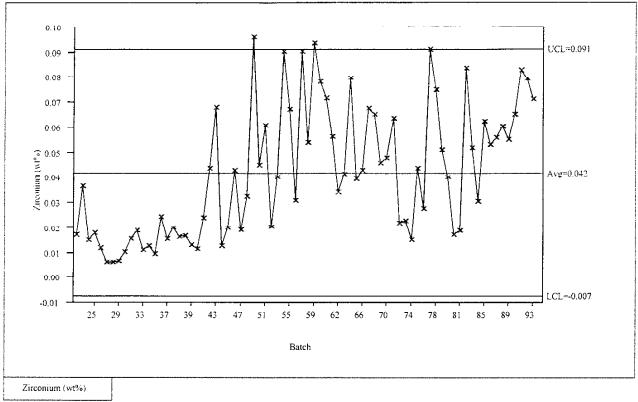
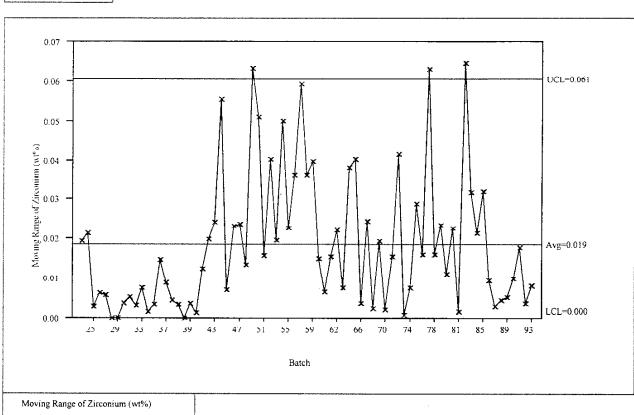


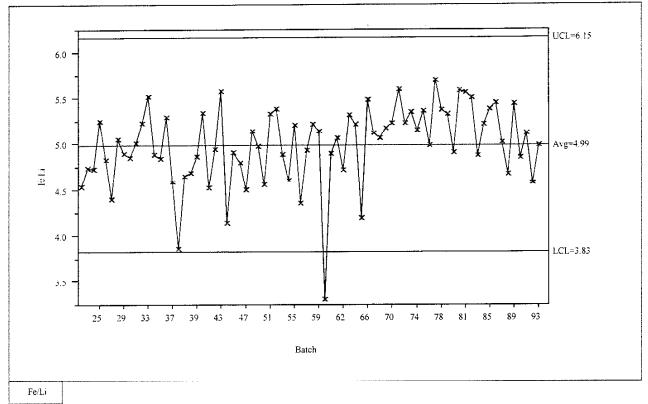
Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte





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Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte



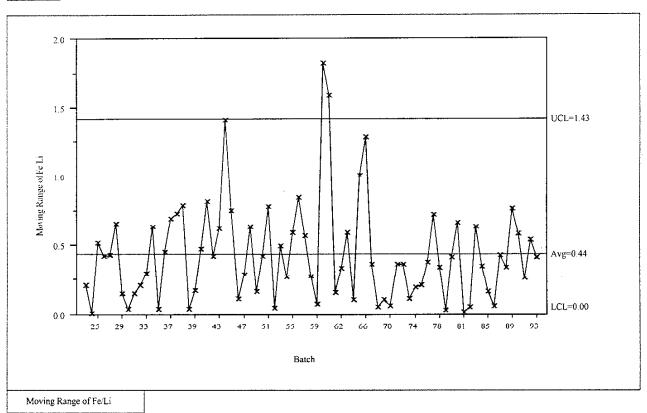
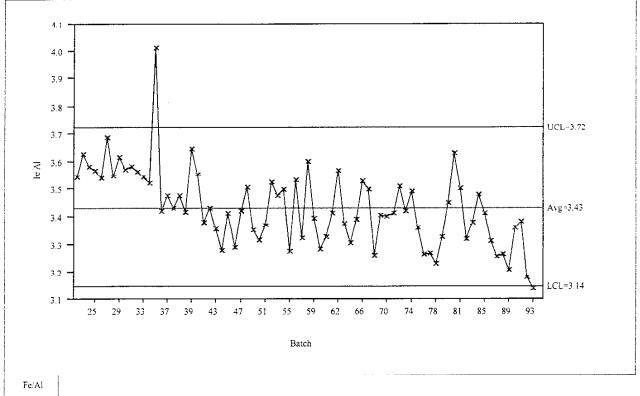
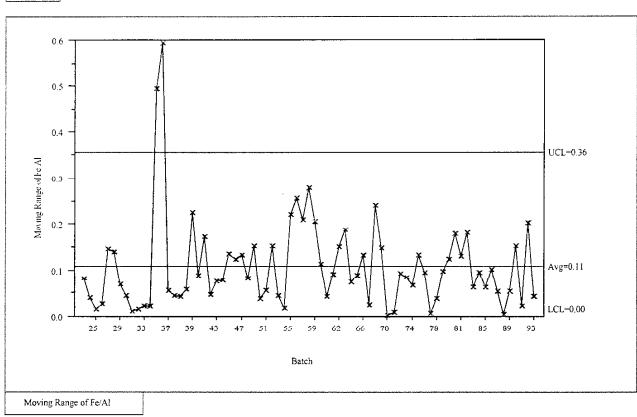


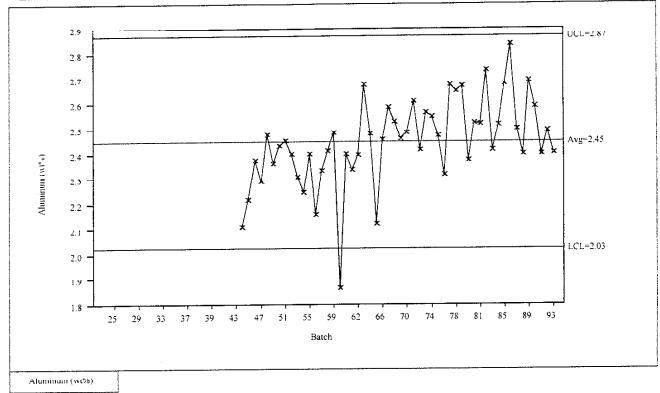
Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte

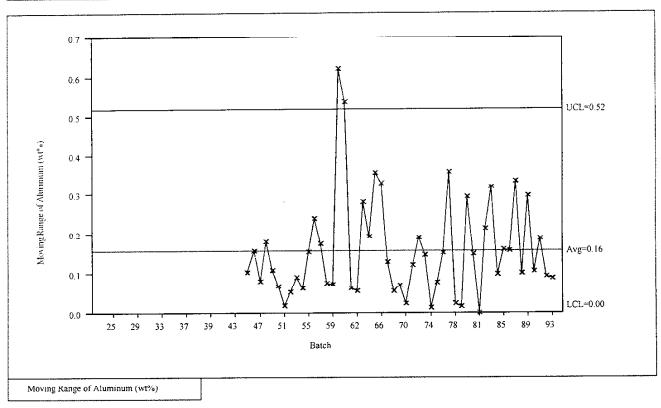




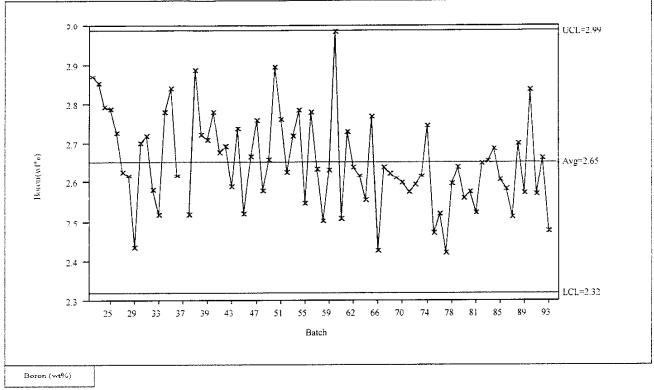
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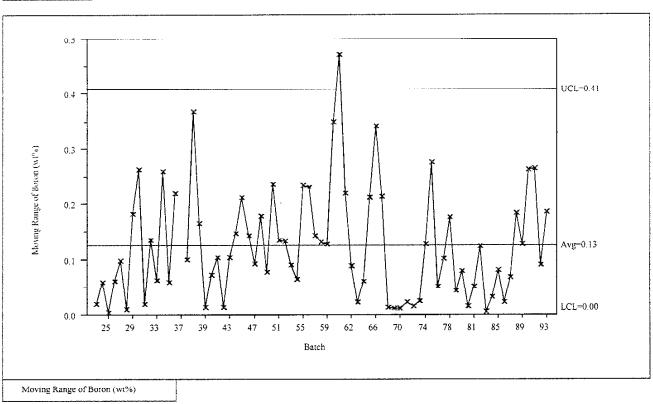
Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte





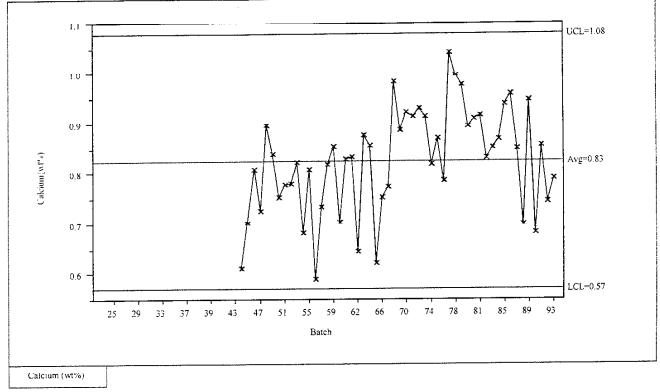
Revision 0
Exhibit 8c: SME Control Charts for Individual Batch Averages for PF Prep by Analyte

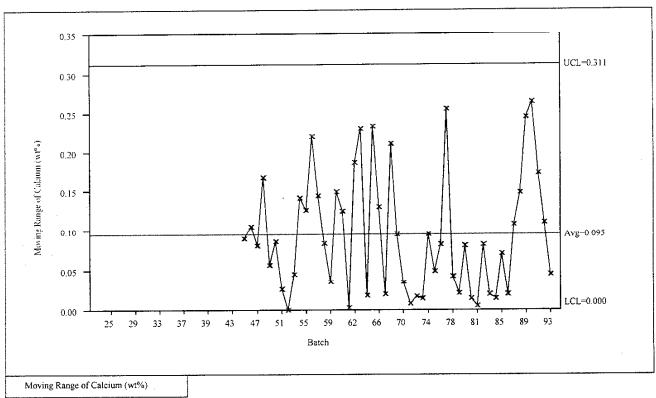




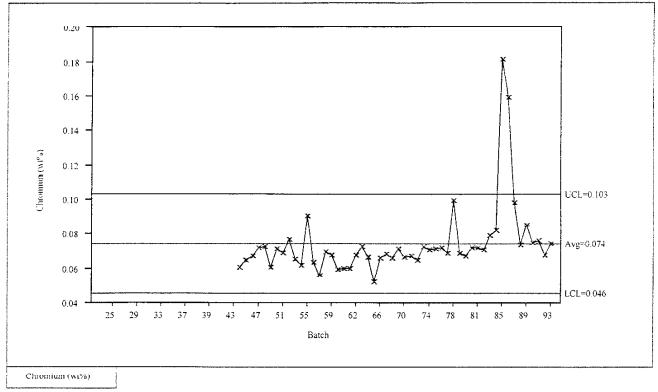
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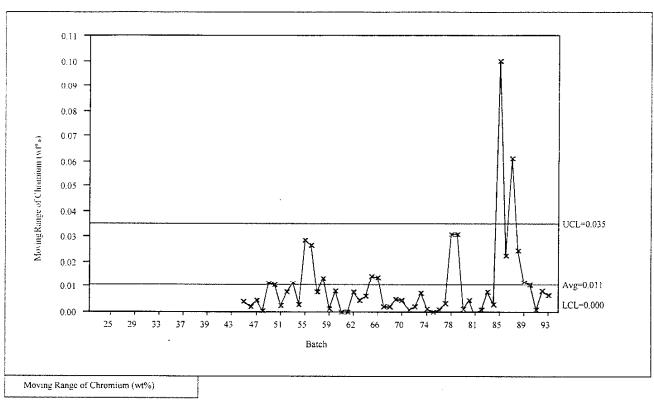
Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte





Revision 0 Exhibit 8c: SME Control Charts for Individual Batch Averages for PF Prep by Analyte

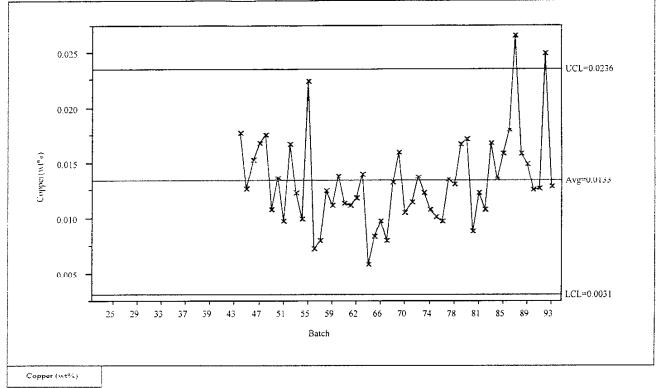


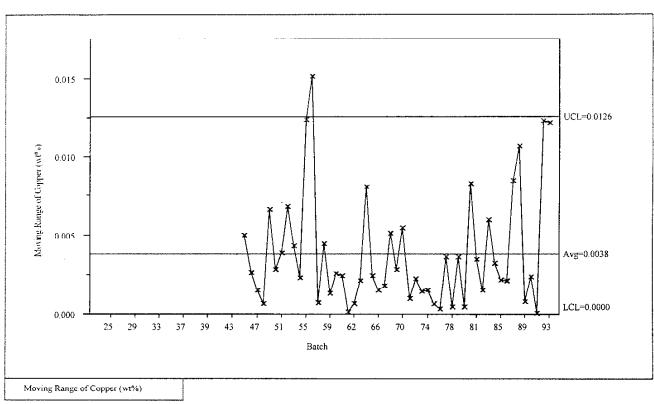


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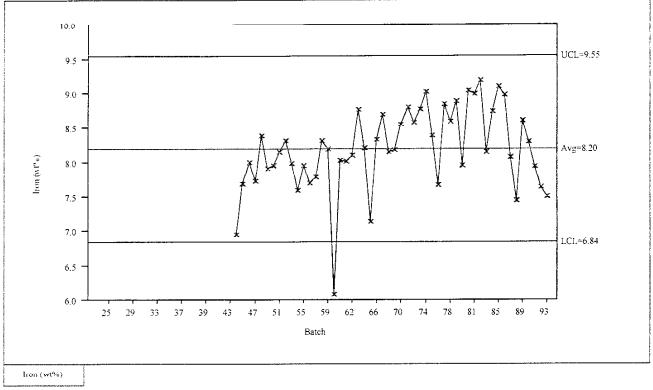
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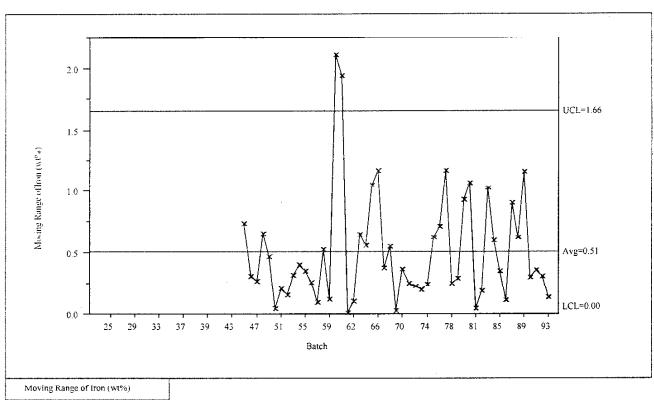
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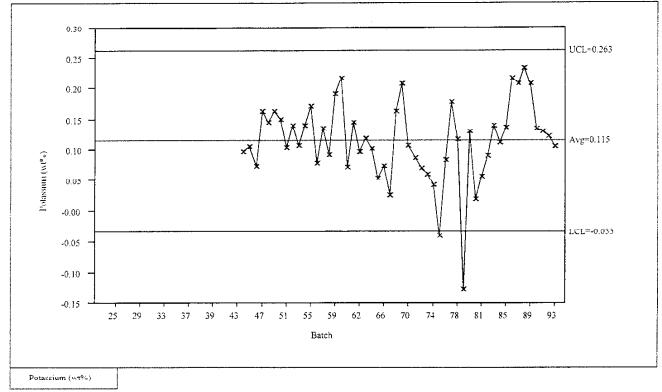
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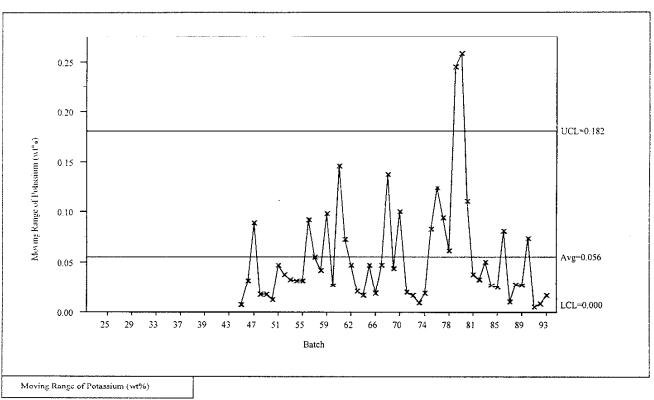




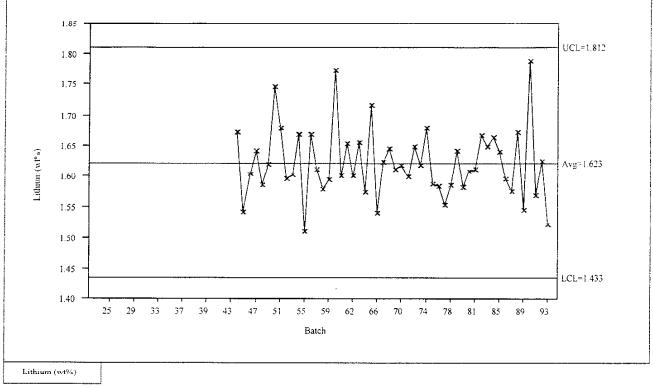
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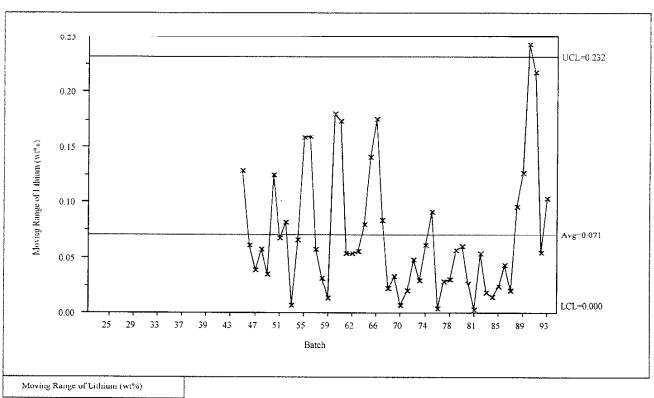
Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte





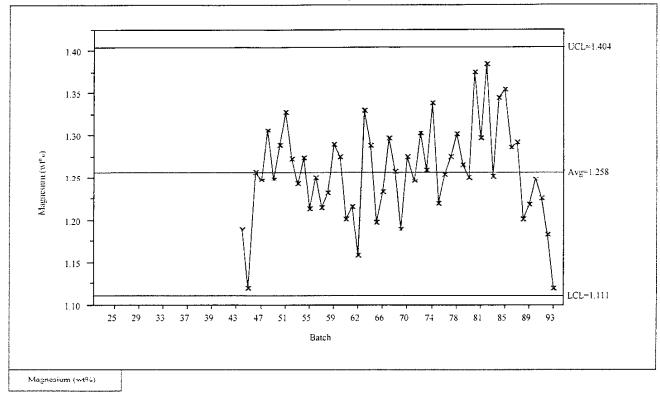
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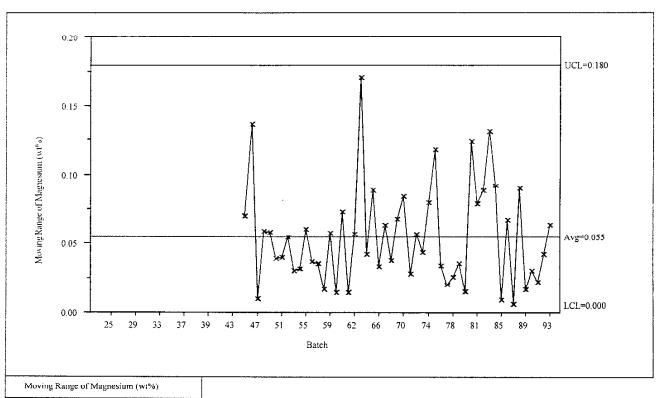




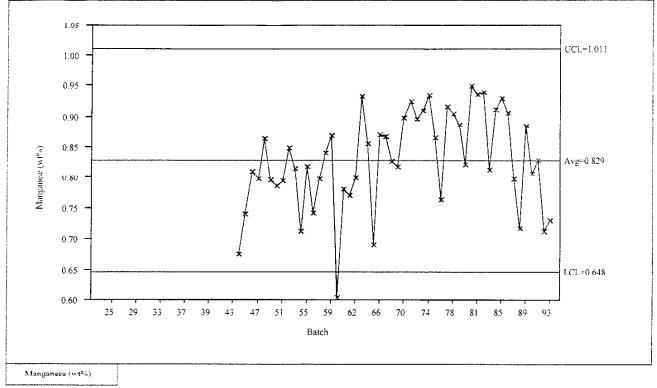
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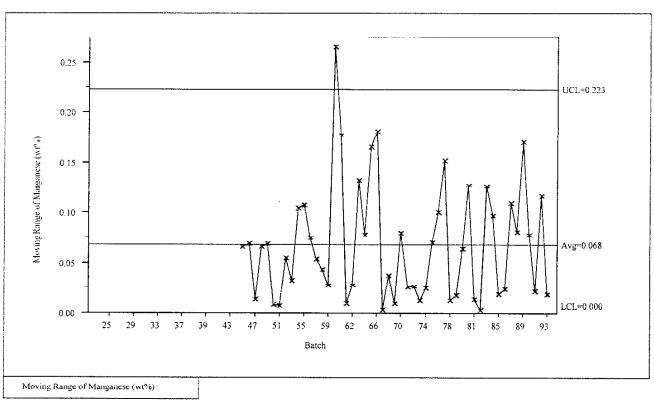
Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte



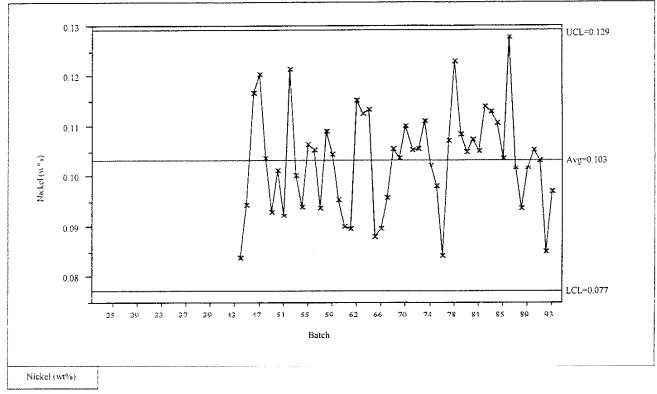


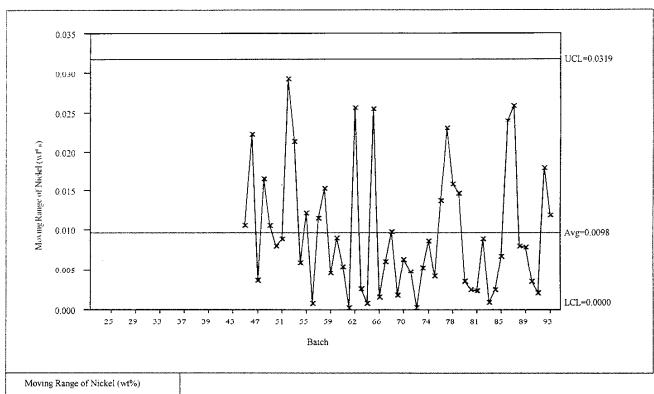
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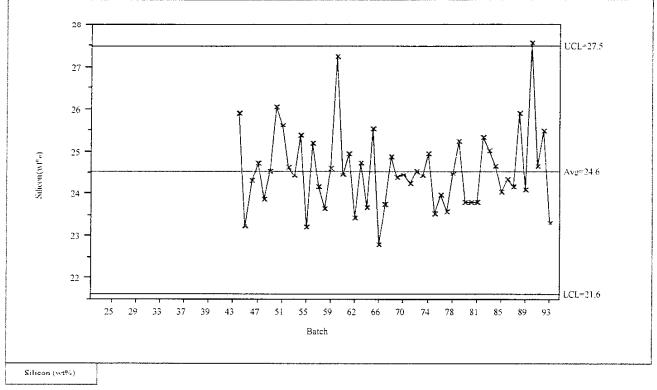


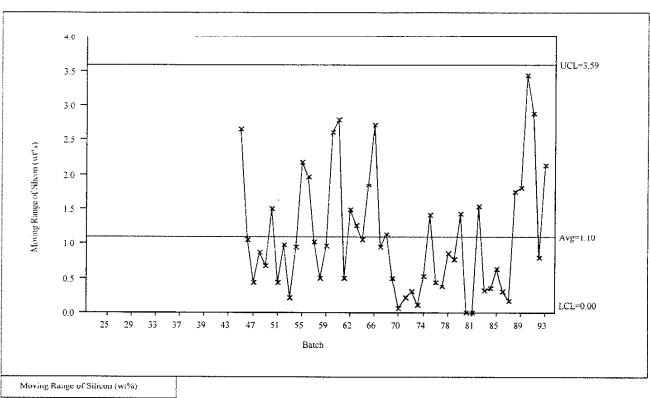
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Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte





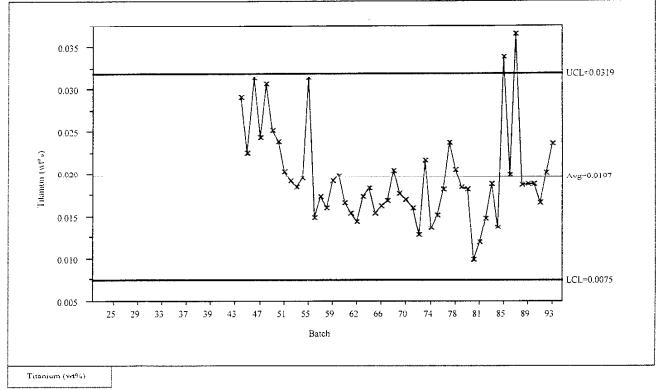
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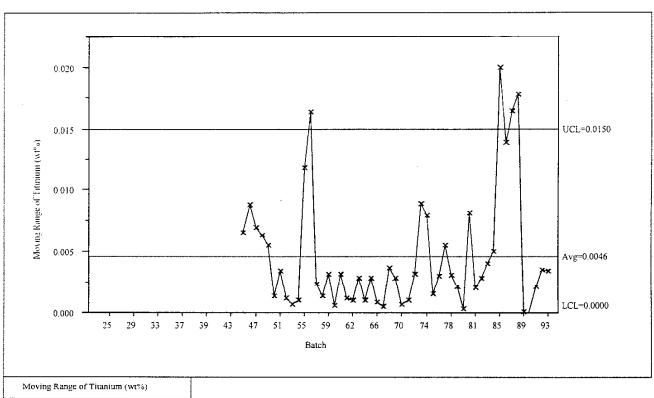




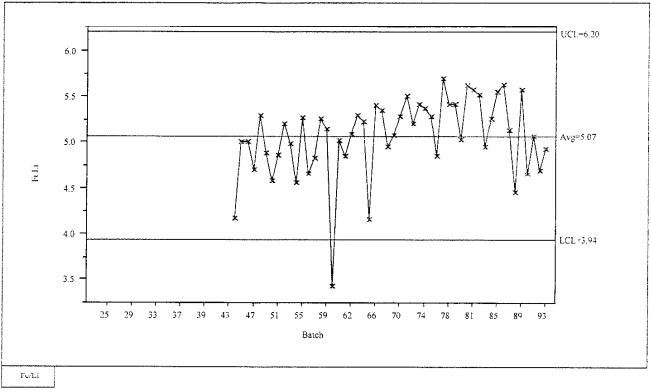
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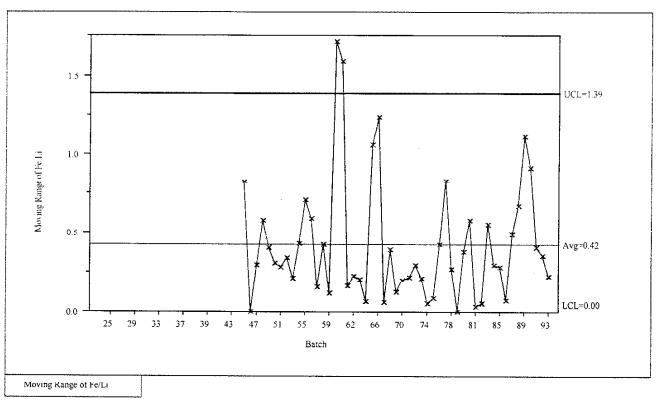
Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte





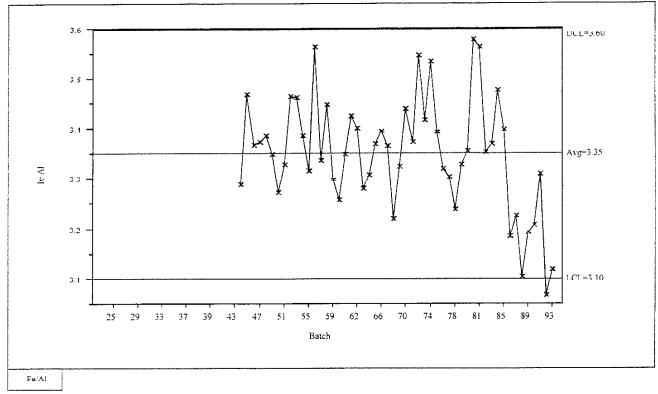
Revision 0 Exhibit 8c: SME Control Charts for Individual Batch Averages for PF Prep by Analyte





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Exhibit 8b: SME Control Charts for Individual Batch Averages for MA Prep by Analyte



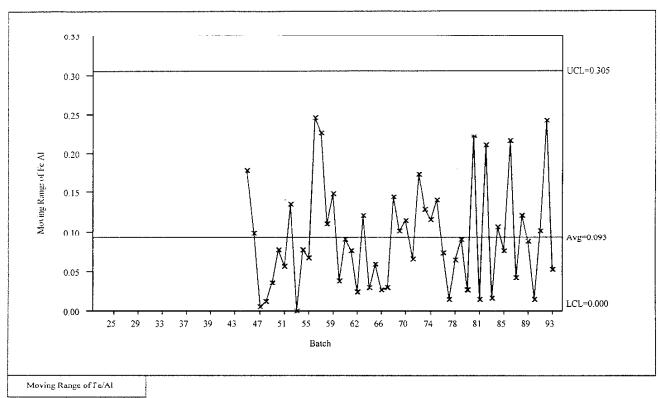
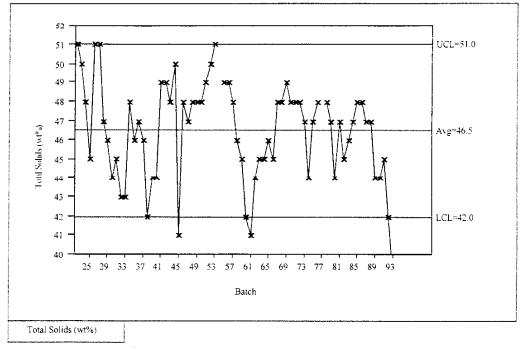


Exhibit 9a: MFT Control Charts for Individual Batch Averages for Anions



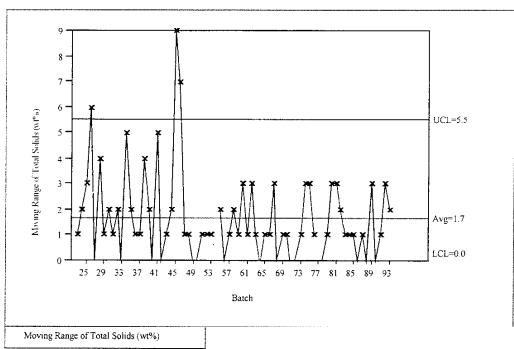
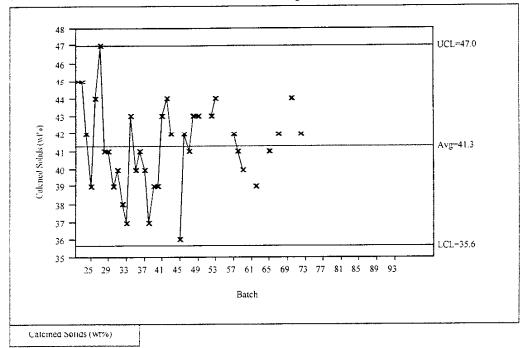
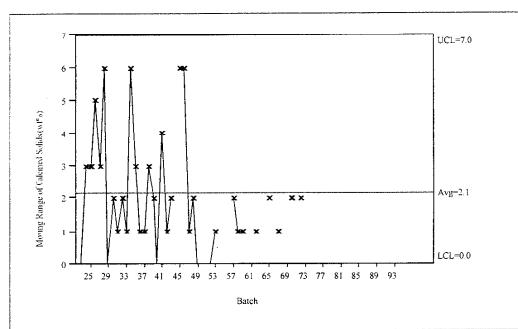


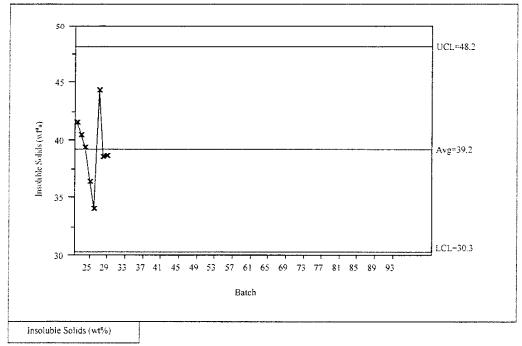
Exhibit 9a: MFT Control Charts for Individual Batch Averages for Anions





Moving Range of Calcined Solids (wt%)

Exhibit 9a: MFT Control Charts for Individual Batch Averages for Anions



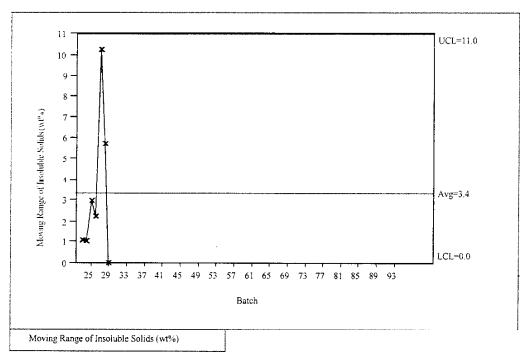
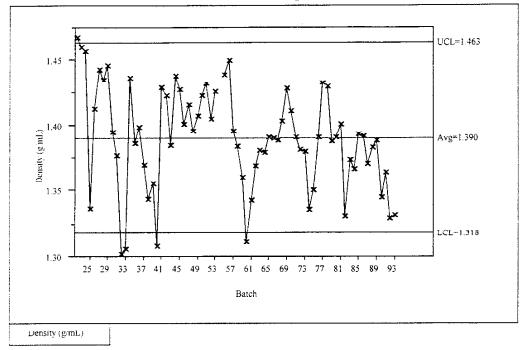


Exhibit 9a: MFT Control Charts for Individual Batch Averages for Anions



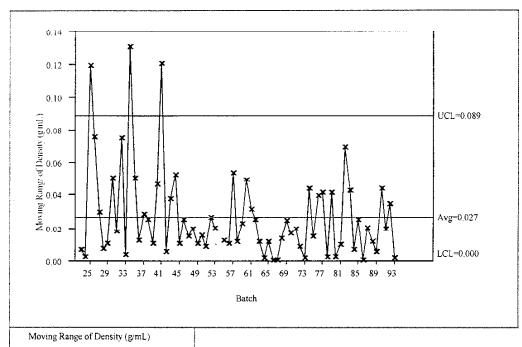
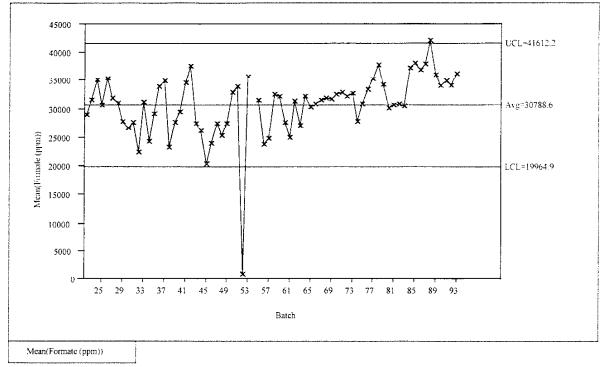


Exhibit 9a: MFT Control Charts for Individual Batch Averages for Anions



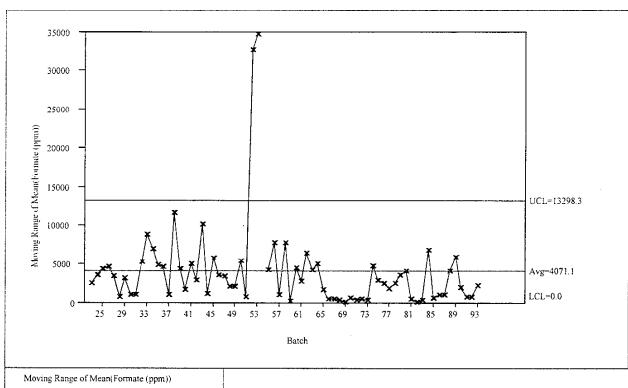
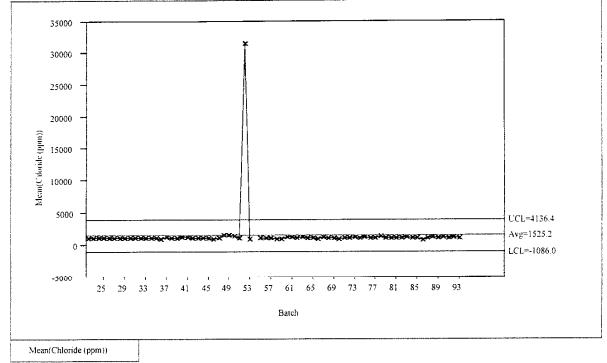


Exhibit 9a: MFT Control Charts for Individual Batch Averages for Anions



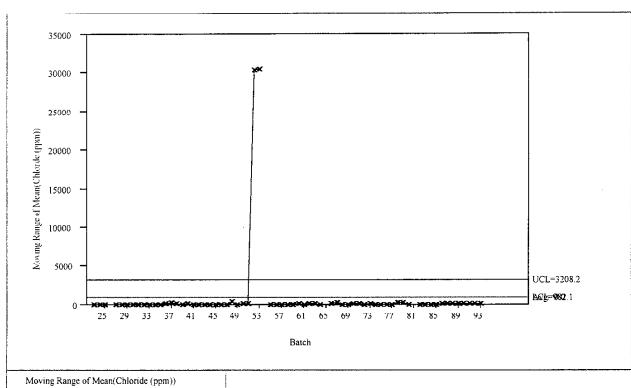
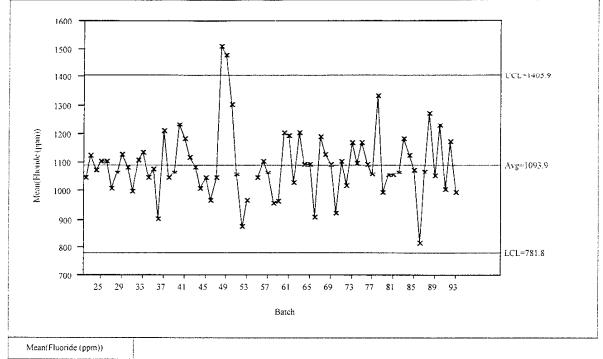


Exhibit 9a: MFT Control Charts for Individual Batch Averages for Anions



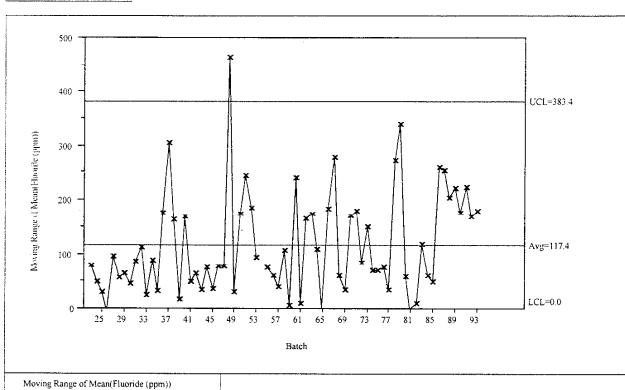
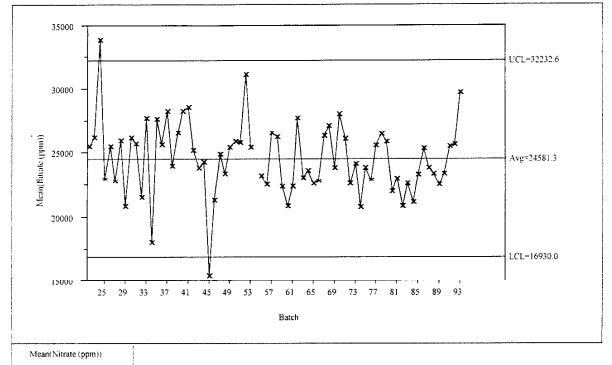


Exhibit 9a: MFT Control Charts for Individual Batch Averages for Anions



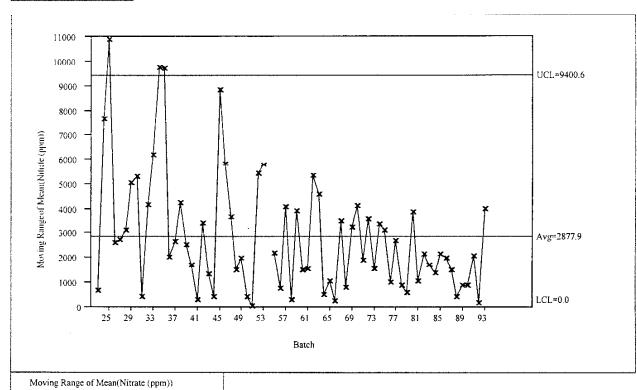
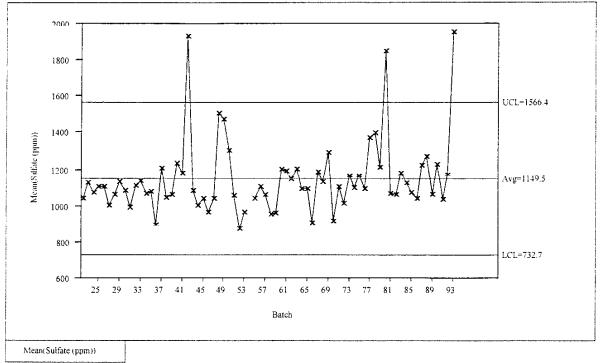
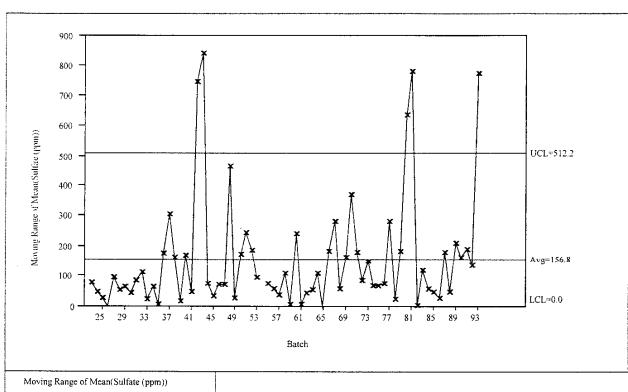


Exhibit 9a: MFT Control Charts for Individual Batch Averages for Anions



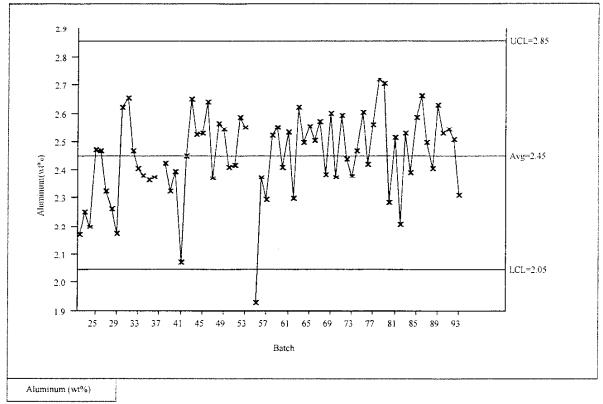


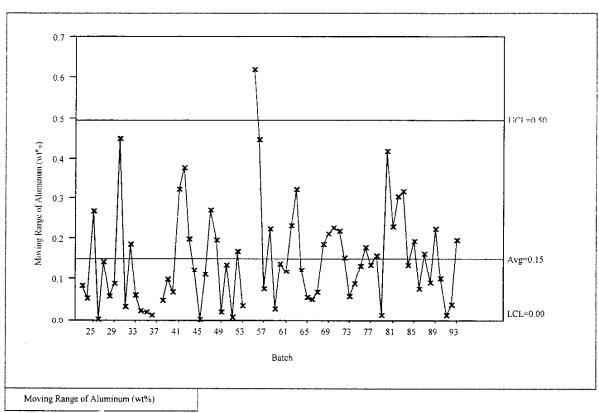
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Exhibit 9a: MFT Control Charts for Individual Batch Averages for Anions

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Exhibit 9b: MFT Control Charts for Individual Batch Averages for MA Prep by Analyte

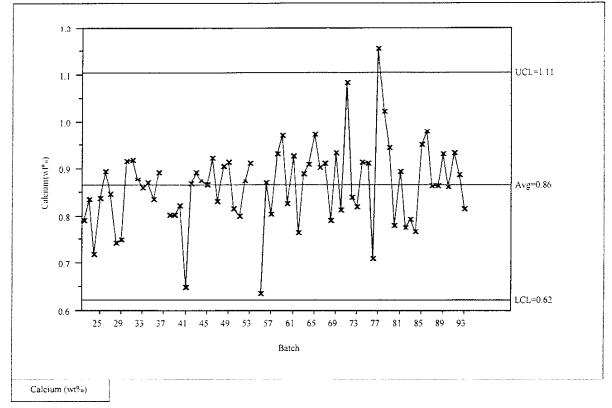




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Exhibit 9b: MFT Control Charts for Individual Batch Averages for MA Prep by Analyte



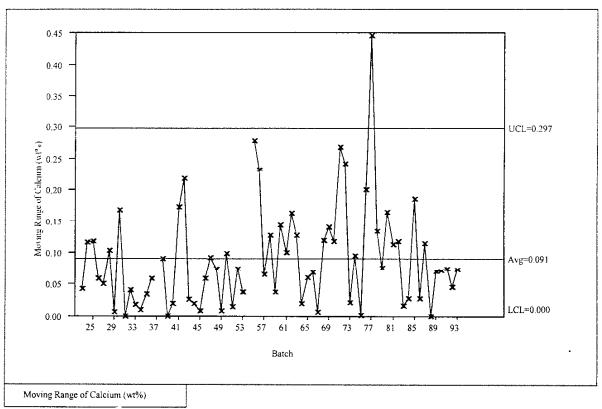
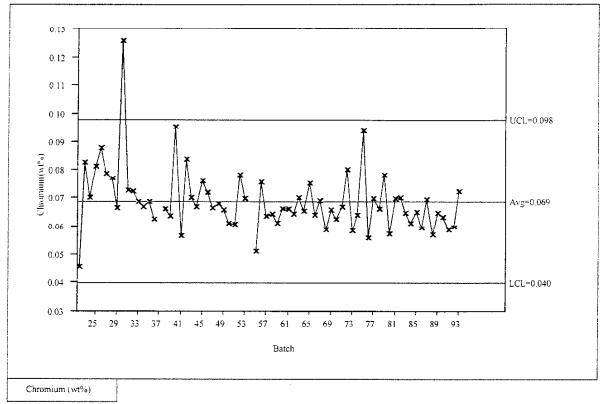
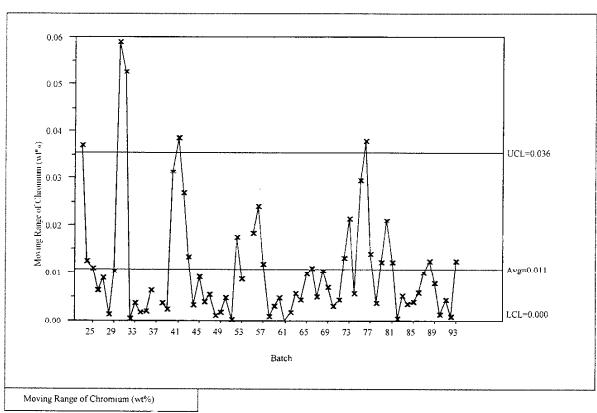


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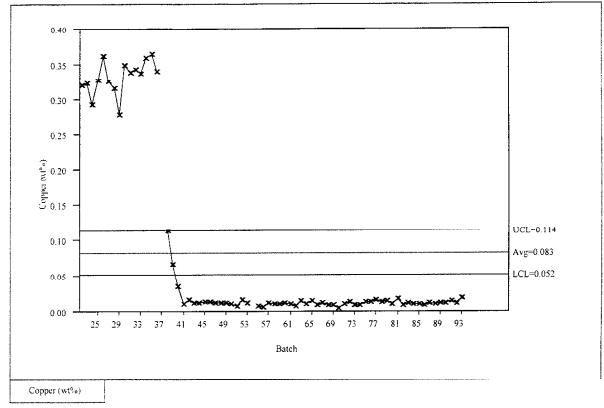




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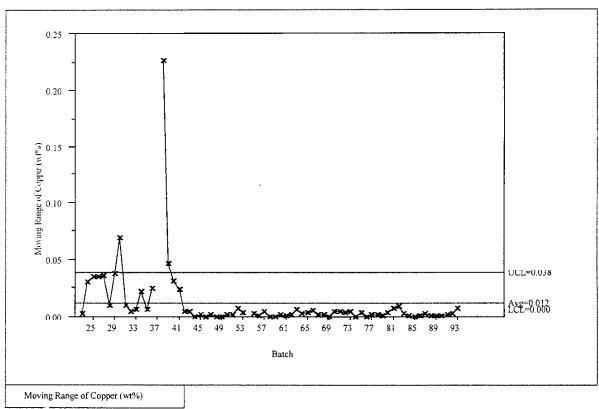
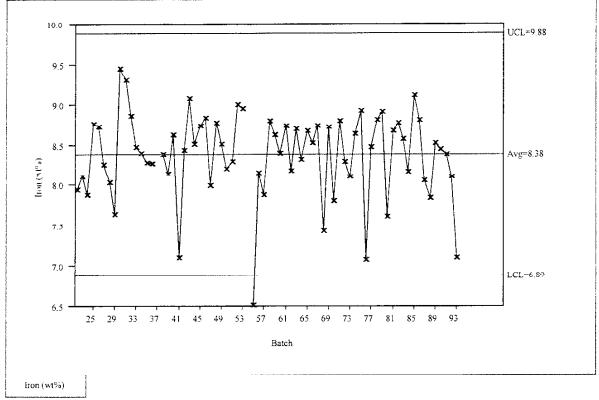
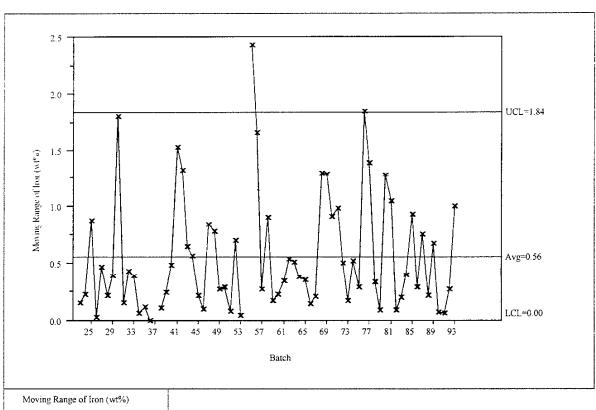


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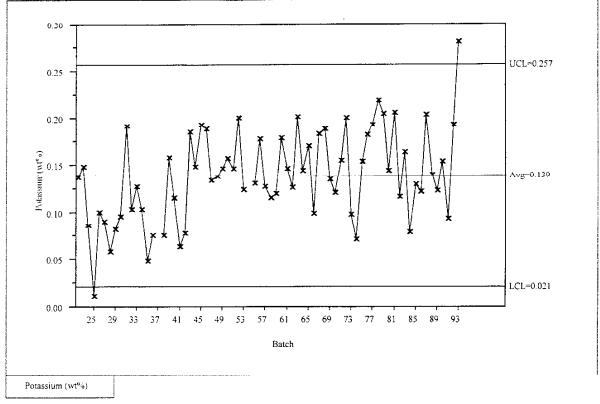




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Exhibit 9b: MFT Control Charts for Individual Batch Averages for MA Prep by Analyte



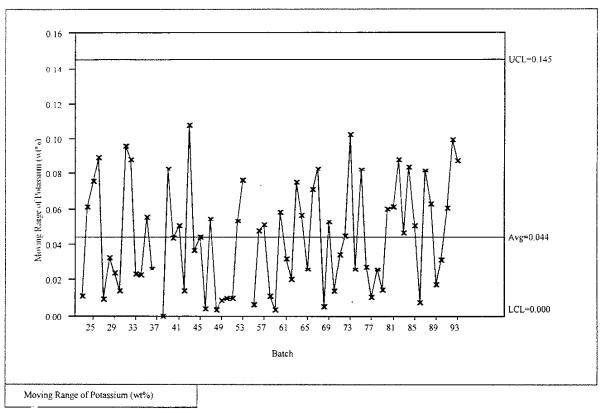
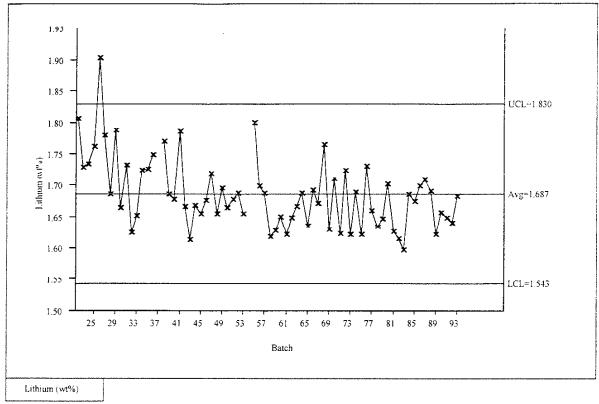
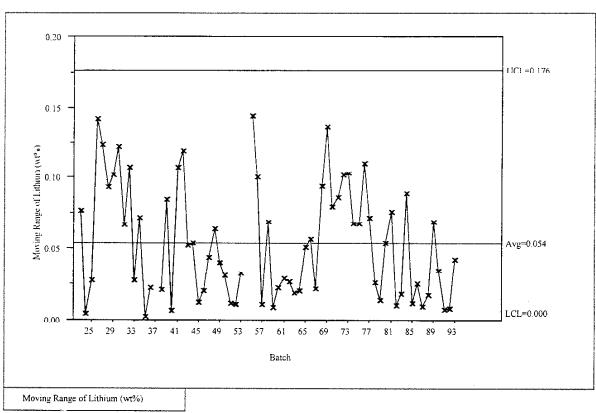


Exhibit 9b: MFT Control Charts for Individual Batch Averages for MA Prep by Analyte

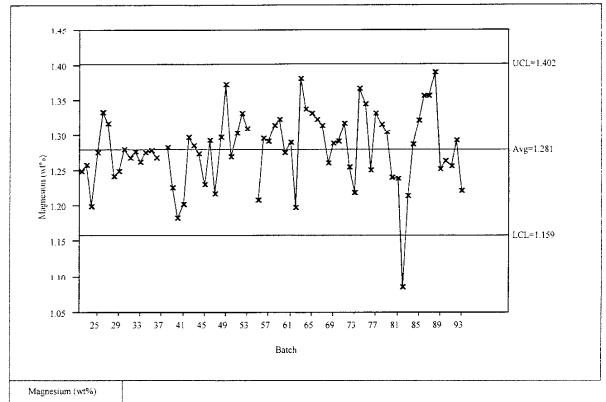




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Exhibit 9b: MFT Control Charts for Individual Batch Averages for MA Prep by Analyte



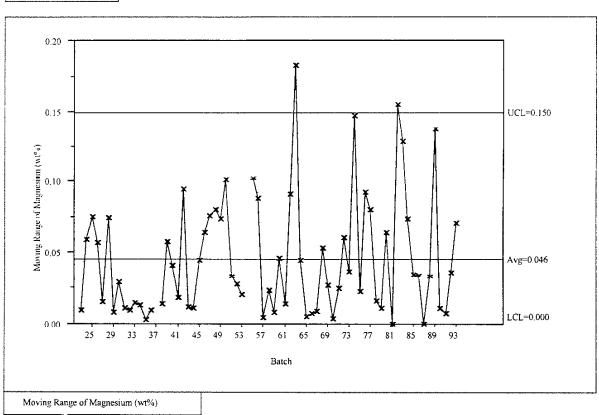
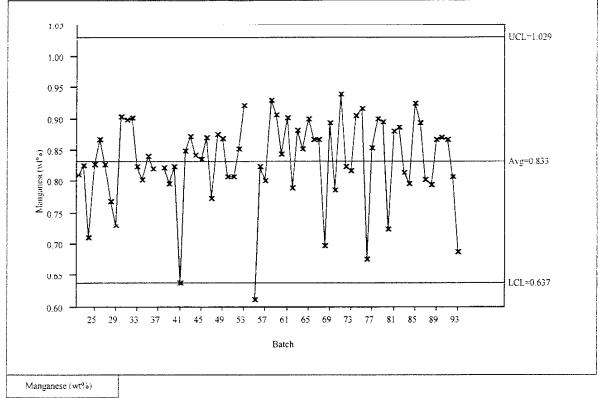
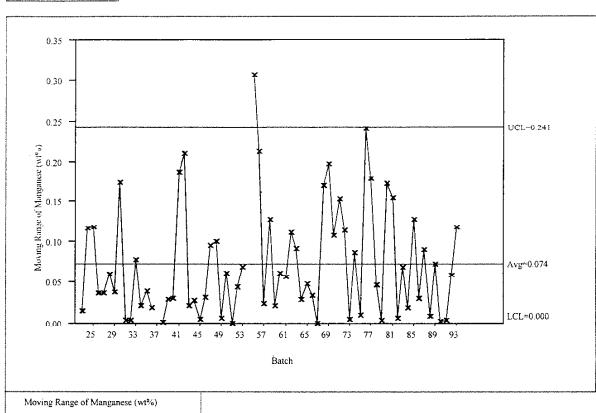


Exhibit 9b: MFT Control Charts for Individual Batch Averages for MA Prep by Analyte

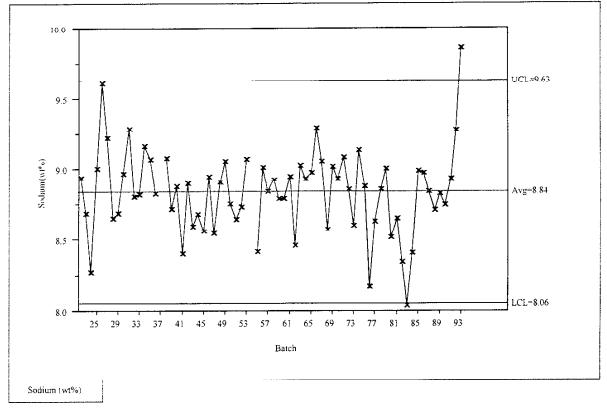




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Exhibit 9b: MFT Control Charts for Individual Batch Averages for MA Prep by Analyte



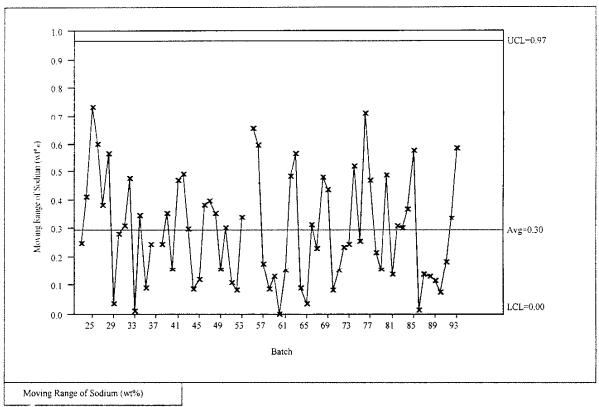
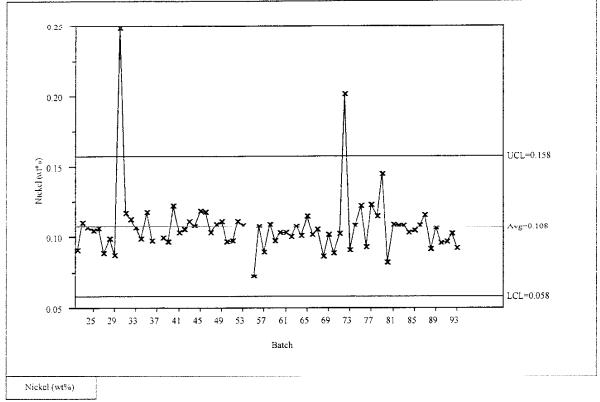
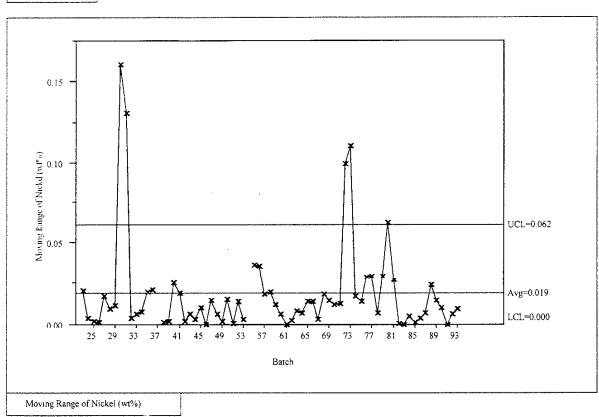


Exhibit 9b: MFT Control Charts for Individual Batch Averages for MA Prep by Analyte

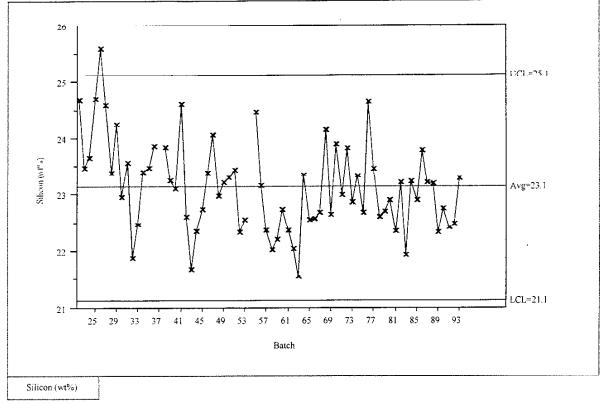




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Exhibit 9b: MFT Control Charts for Individual Batch Averages for MA Prep by Analyte



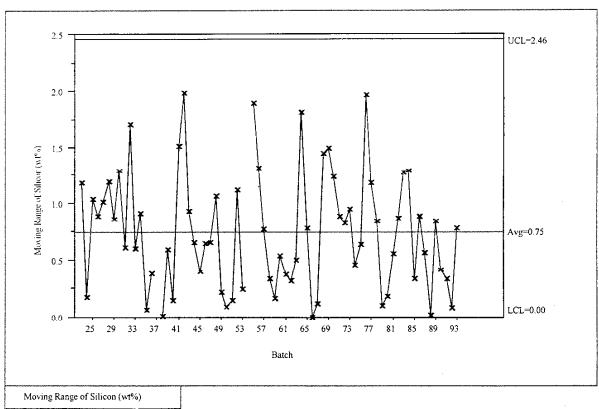
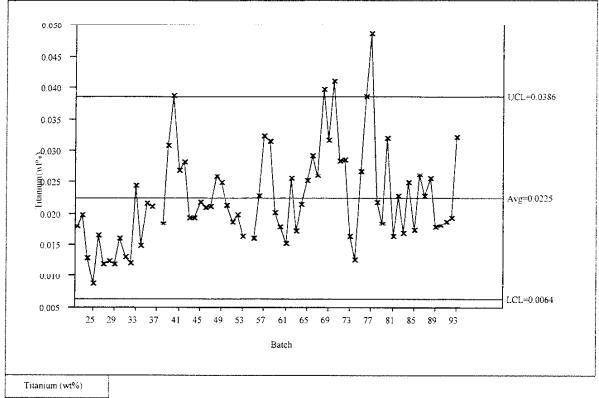
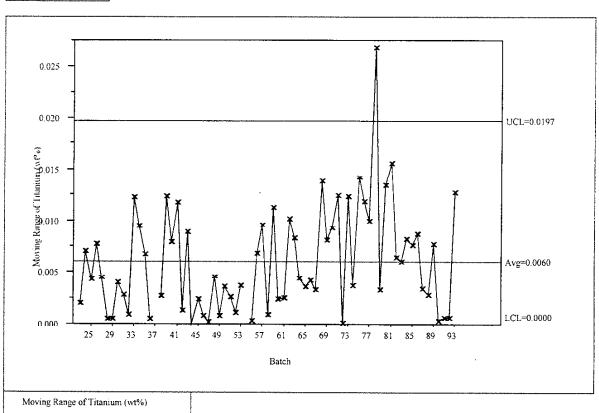


Exhibit 9b: MFT Control Charts for Individual Batch Averages for MA Prep by Analyte

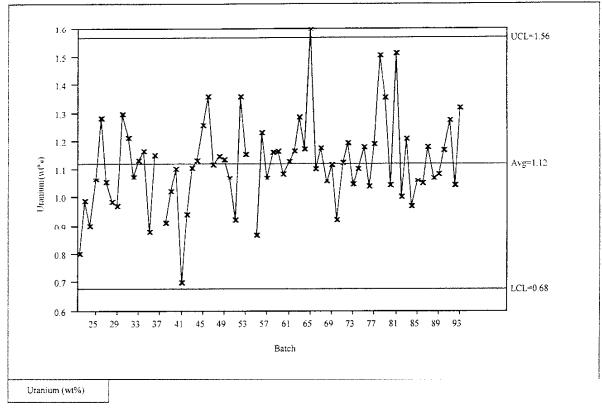




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Exhibit 9b: MFT Control Charts for Individual Batch Averages for MA Prep by Analyte



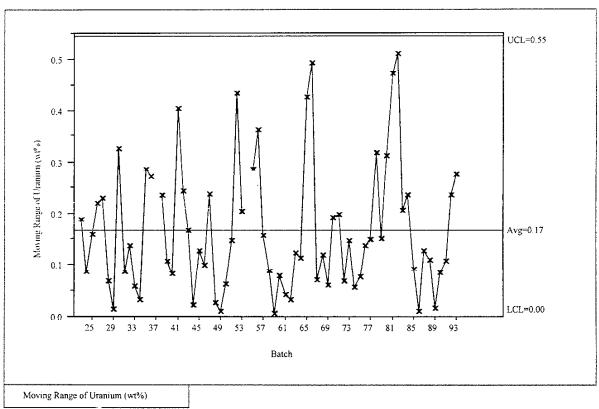
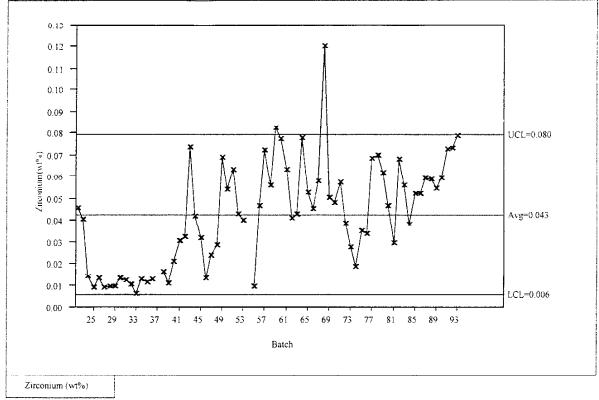
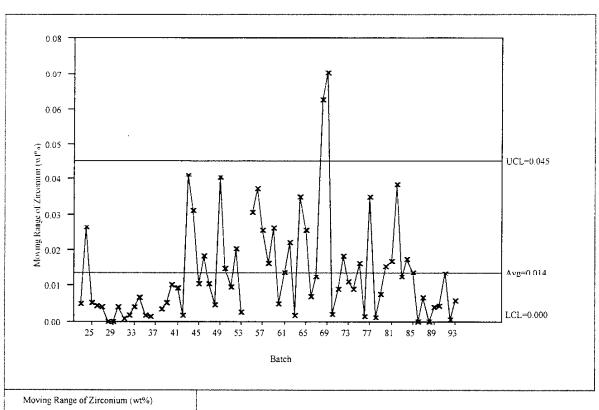


Exhibit 9b: MFT Control Charts for Individual Batch Averages for MA Prep by Analyte

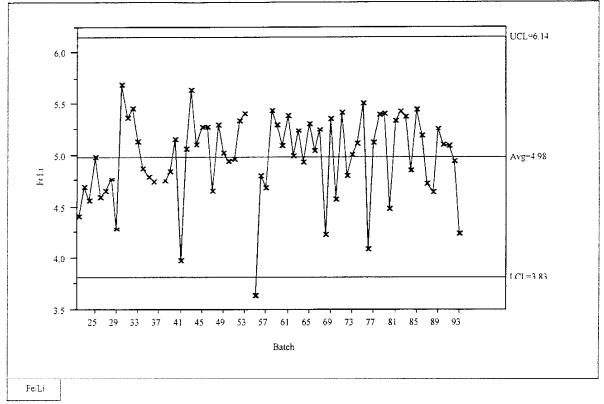




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Exhibit 9b: MFT Control Charts for Individual Batch Averages for MA Prep by Analyte



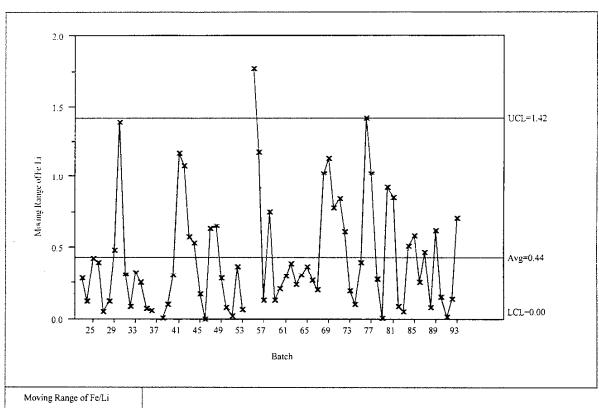
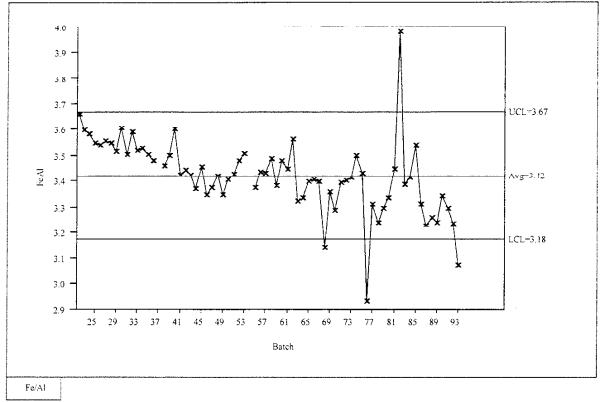


Exhibit 9b: MFT Control Charts for Individual Batch Averages for MA Prep by Analyte



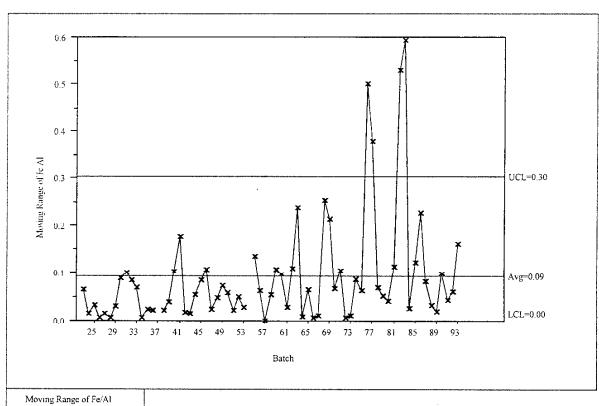
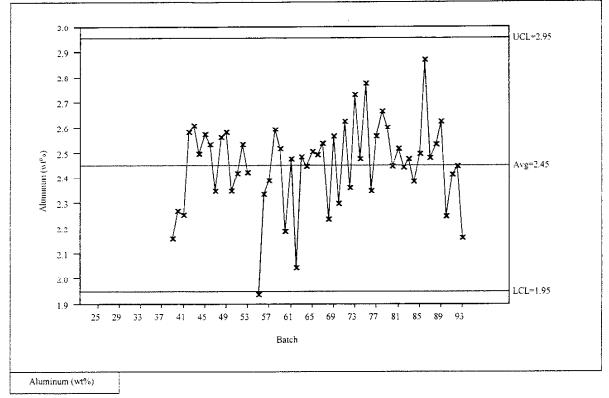


Exhibit 9c: MFT Control Charts for Individual Batch Averages for PF Prep by Analyte



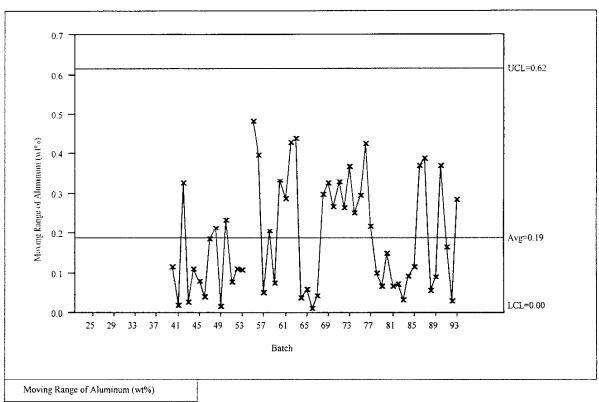
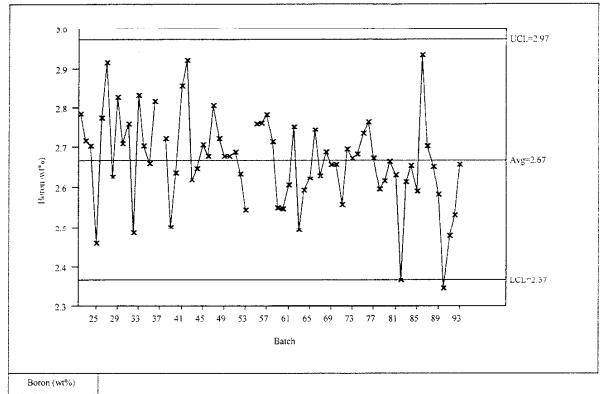
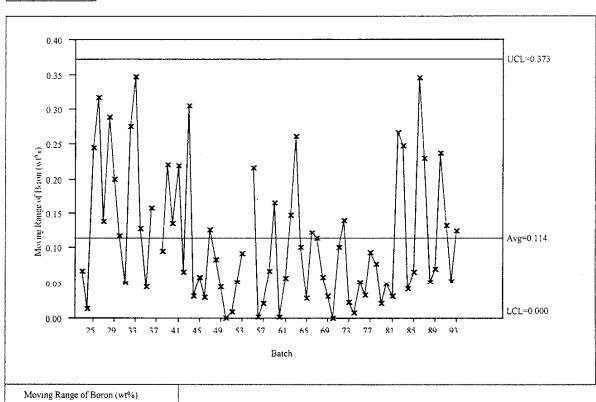


Exhibit 9c: MFT Control Charts for Individual Batch Averages for PF Prep by Analyte

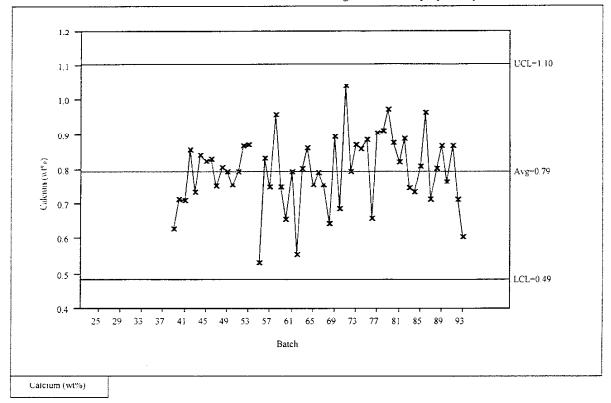




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Exhibit 9c: MFT Control Charts for Individual Batch Averages for PF Prep by Analyte



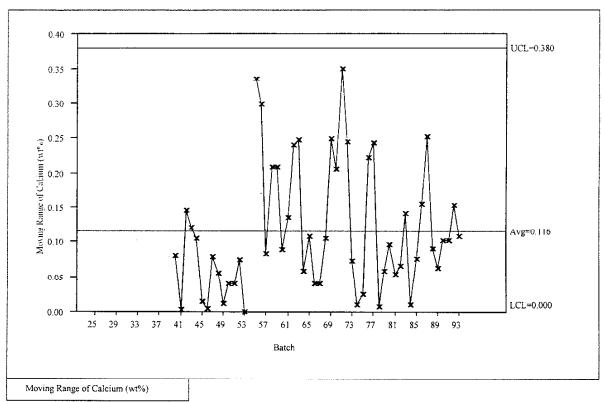
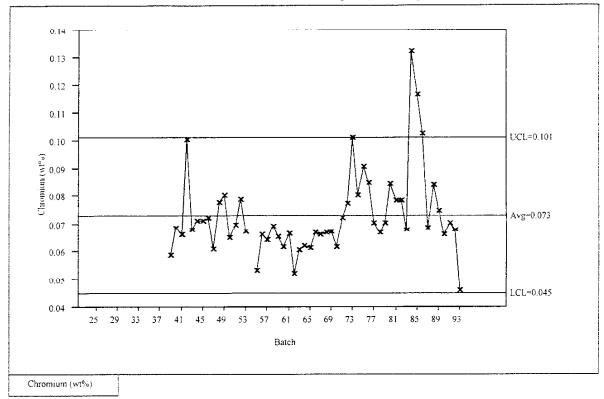
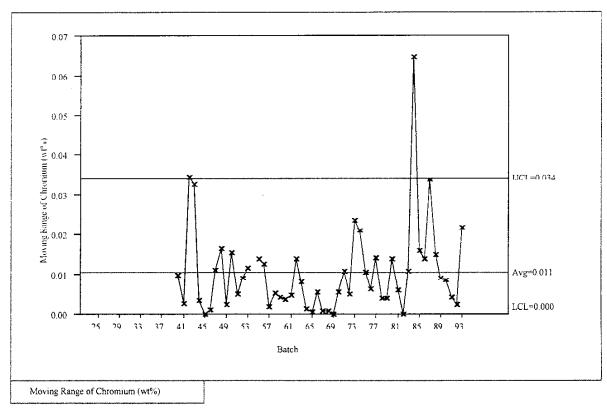


Exhibit 9c: MFT Control Charts for Individual Batch Averages for PF Prep by Analyte

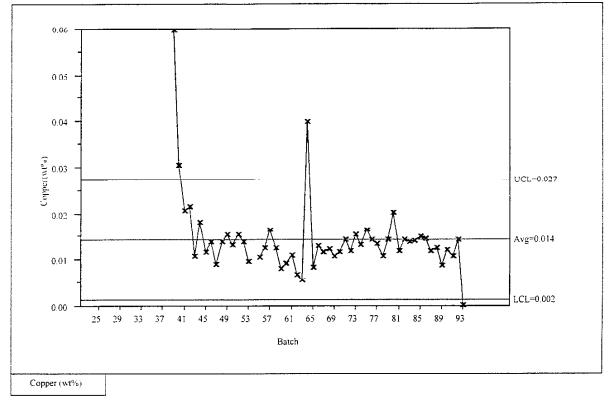




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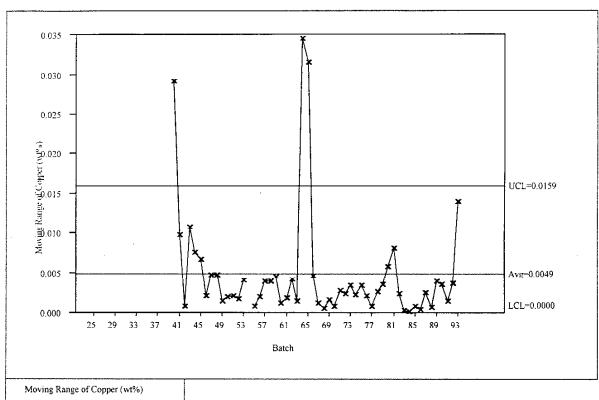
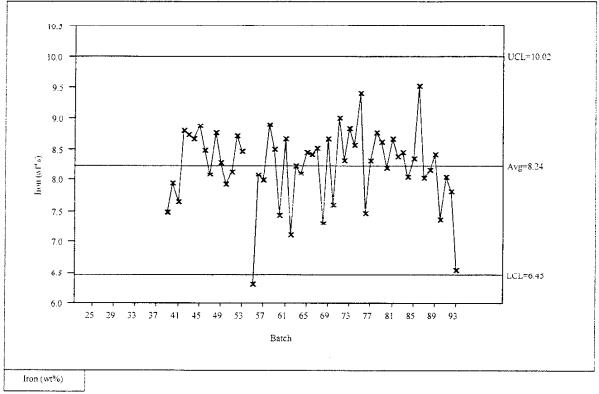
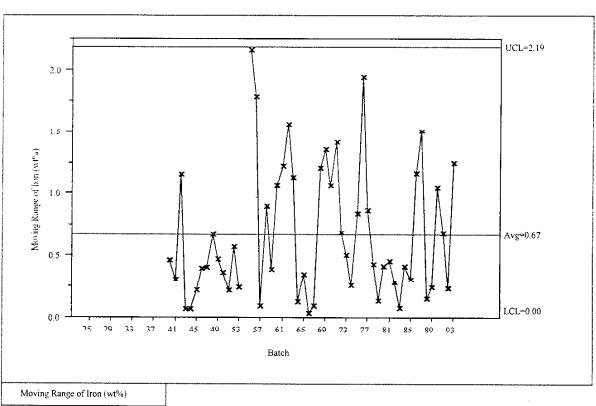


Exhibit 9c: MFT Control Charts for Individual Batch Averages for PF Prep by Analyte

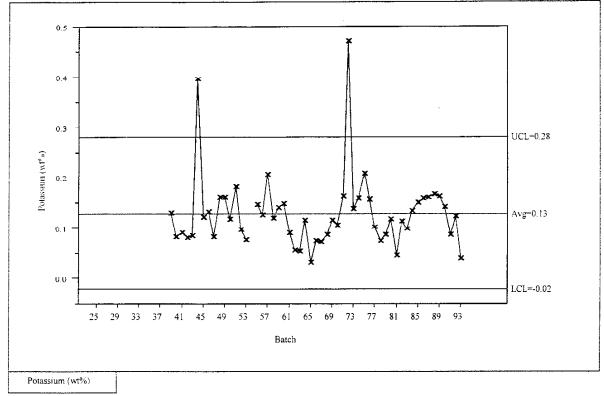




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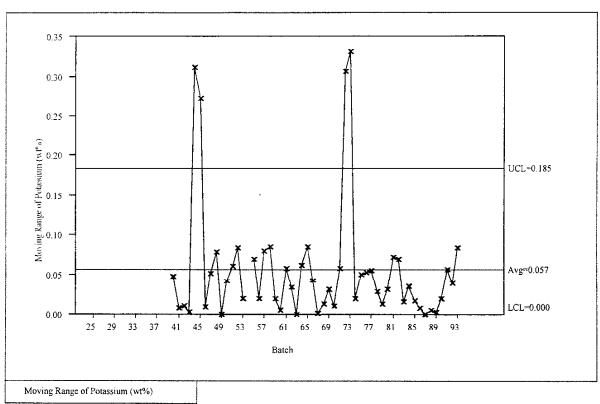
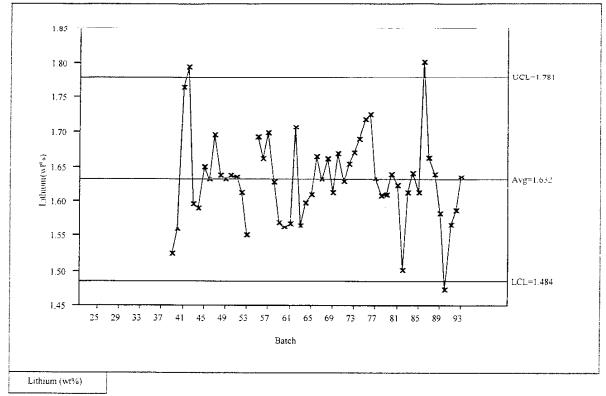
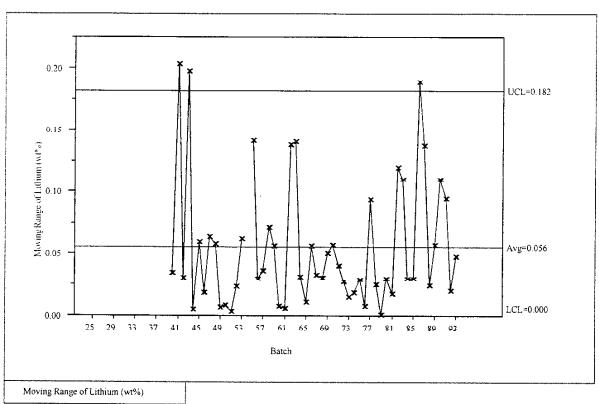


Exhibit 9c: MFT Control Charts for Individual Batch Averages for PF Prep by Analyte

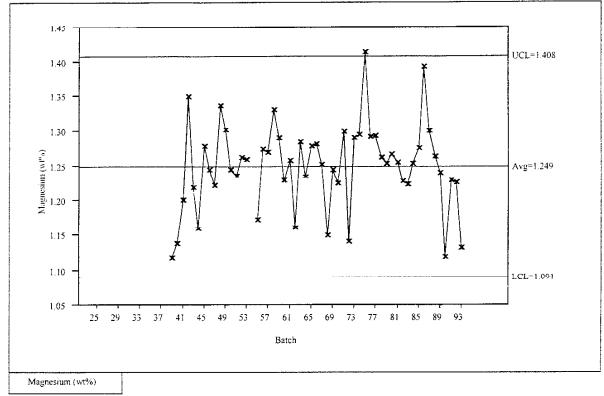




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Exhibit 9c: MFT Control Charts for Individual Batch Averages for PF Prep by Analyte



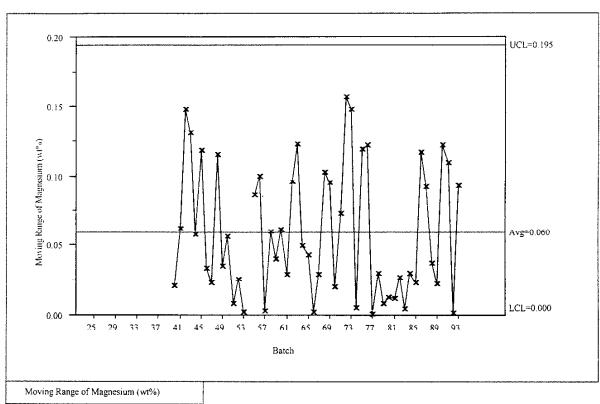
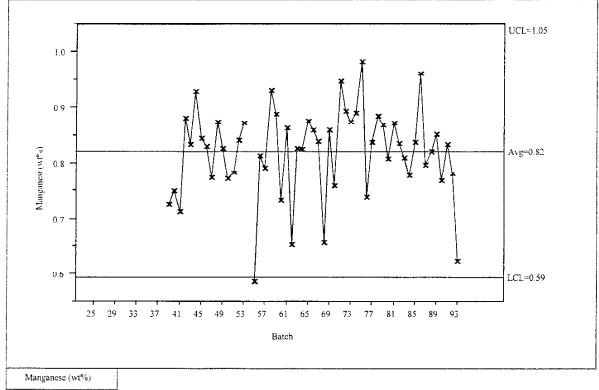
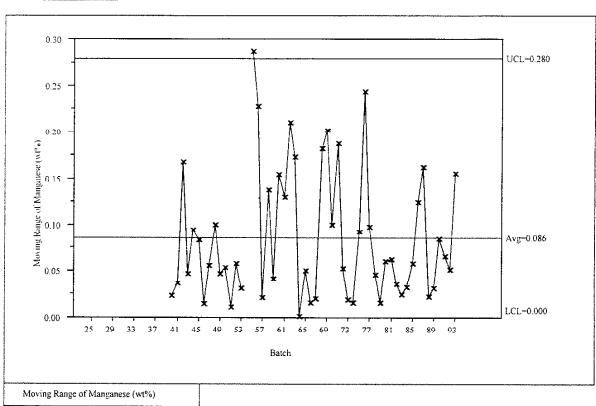


Exhibit 9c: MFT Control Charts for Individual Batch Averages for PF Prep by Analyte

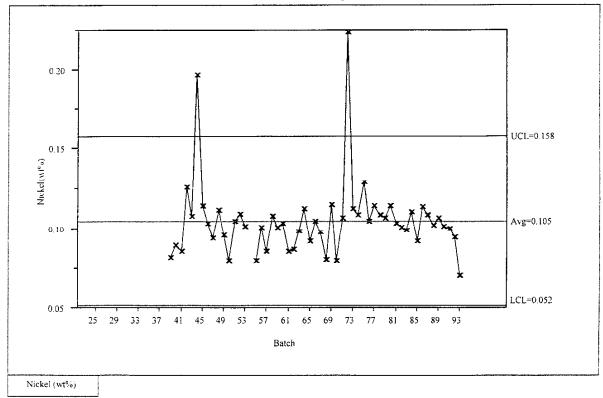




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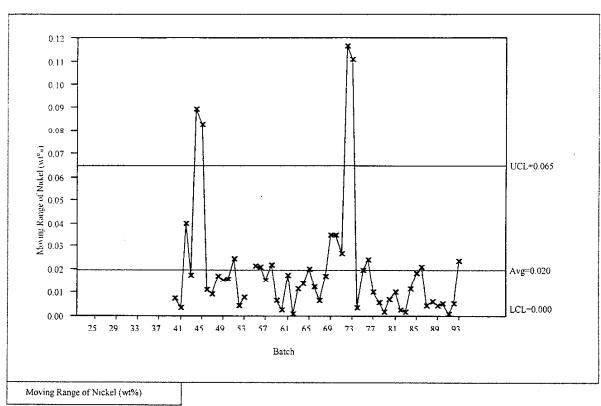
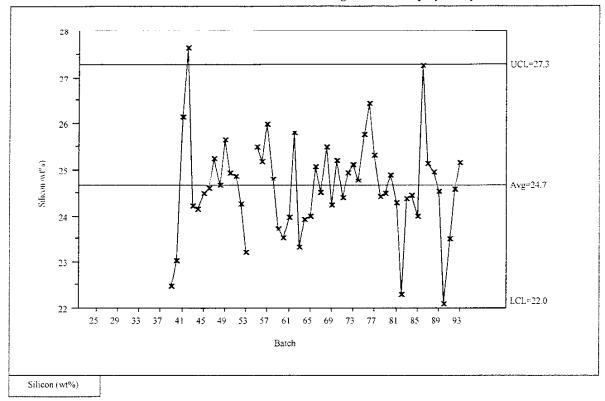
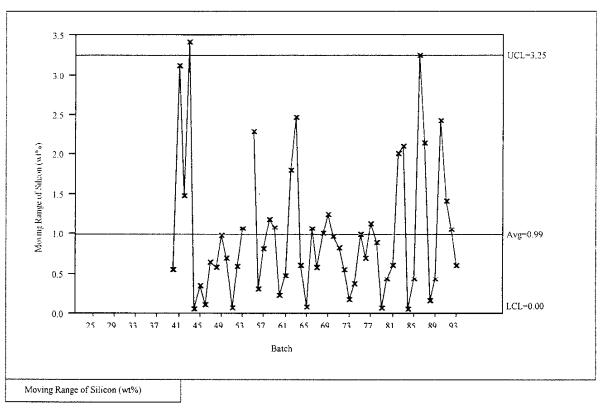


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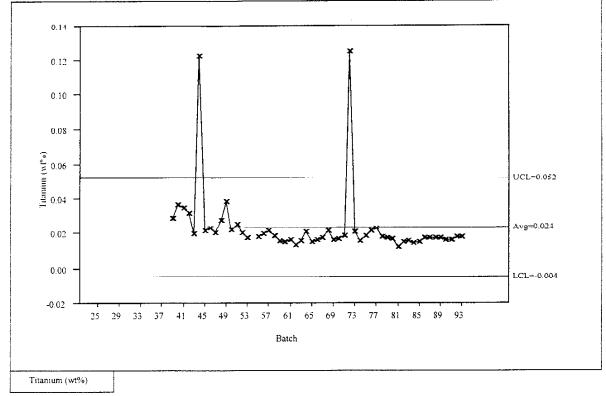




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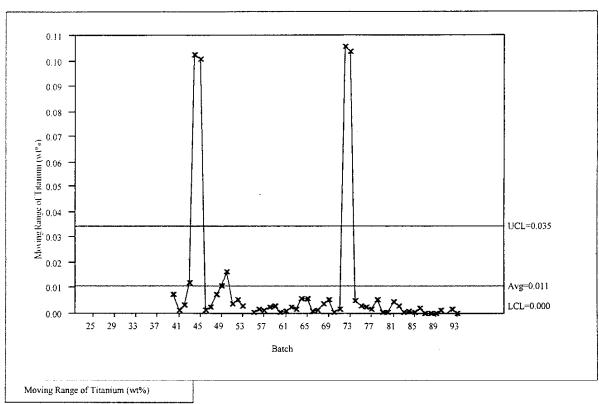
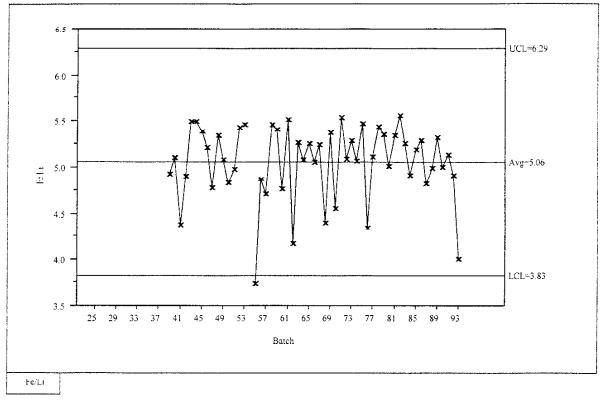
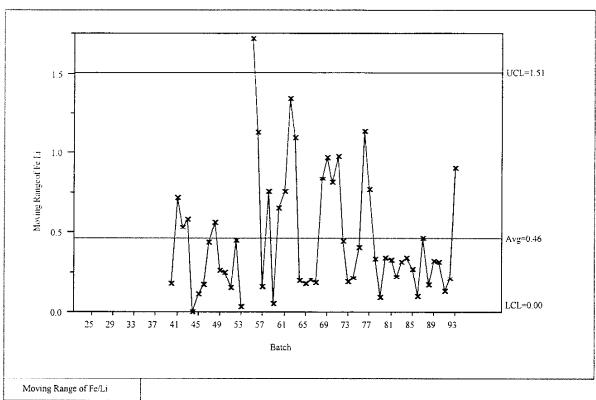


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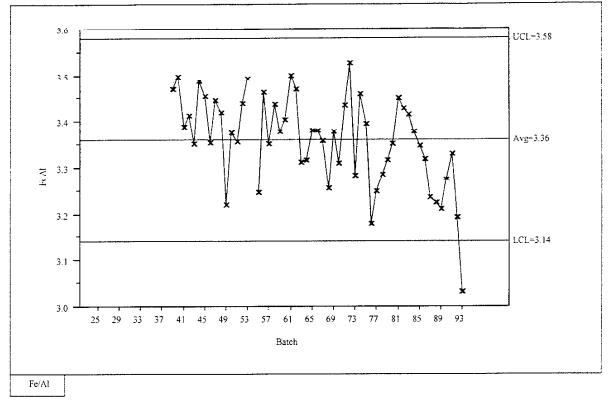




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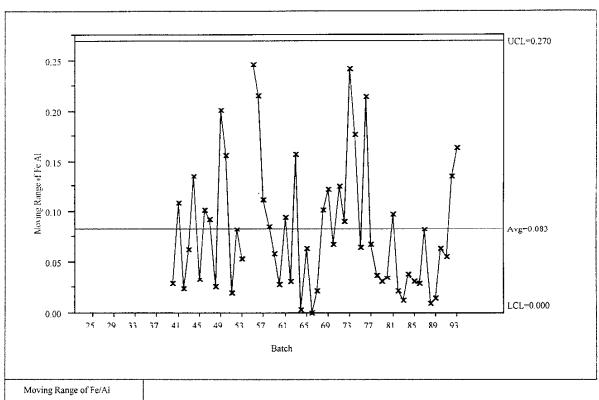
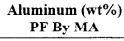
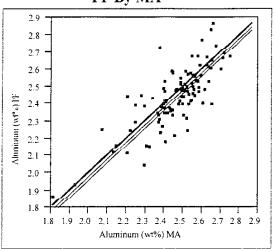


Exhibit 10: Paired Comparisons Between Dissolution Methods for SME and MFT Cations





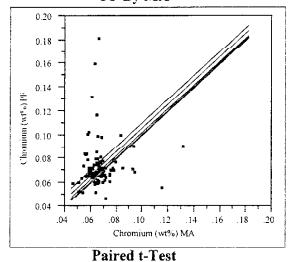
Paired t-Test
Aluminum (wt%) MA - Aluminum (wt%) PF

 Mean Difference
 0.022667
 Prob > |t| 0.0348

 Std Error
 0.010602
 Prob > t 0.0174

 t-Ratio
 2.137933
 Prob < t 0.9826</td>

Chromium (wt%) PF By MA



raneu t-rest

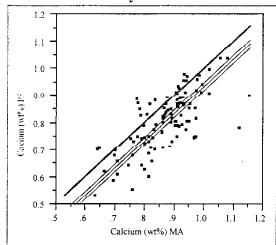
Chromium (wt%) MA - Chromium (wt%) PF

Mean Difference	-0.00592	P(0b > t 0.0051
Std Error	0.002068	Prob > t 0.9975
t-Ratio	-2.86238	$Prob \le t \ 0.0025$
DF	105	

Calcium (wt%) PF By MA

105

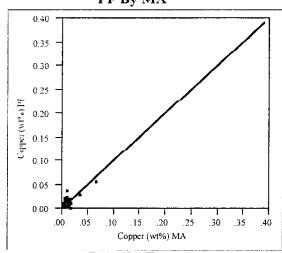
t-Ratio DF



Paired t-Test
Calcium (wt%) MA - Calcium (wt%) PF

Mean Difference	0.065895	Prob > tl <.0001
Std Error	0.00749	Prob > t < .0001
t-Ratio	8.797226	Prob < t 1.0000
DF	105	

Copper (wt%)
PF By MA

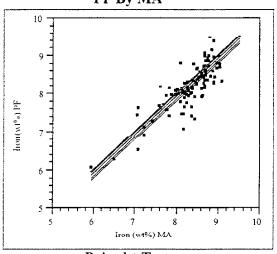


Paired t-Test
Copper (wt%) MA - Copper (wt%) PF

Mean Difference	-0.00139	$Prob \ge \mu 0.0121$
Std Error	0.000545	Prob > t 0.9940
t-Ratio	-2.55488	$Prob < t \ 0.0060$
DE	105	

Exhibit 10: Paired Comparisons Between Dissolution Methods for SME and MFT Cations

Iron (wt%) PF By MA

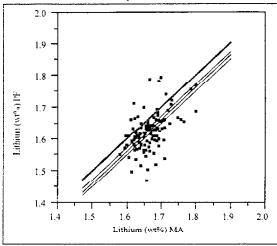


Paired t-Test

Iron (wt%) MA - Iron (wt%) PF

Mean Difference	0.144685	Prob > t < .0001
Std Error	0.033191	Prob > t < .0001
t-Ratio	4.359102	Prob < t 1.0000
DF	CUI	

Lithium (wt%) PF By MA

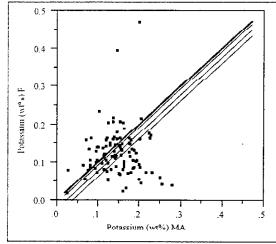


Paired t-Test

Lithium (wt%) MA - Lithium (wt%) PF

Mean Difference	0.038974	Prob > t < .0001
Std Error	0.005241	Prob > t < .0001
t-Ratio	7.435997	Prob < t 1.0000
DF	105	

Potassium (wt%) PF By MA



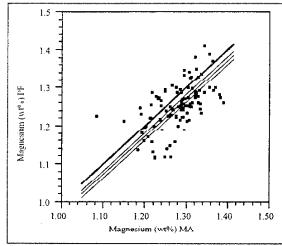
Paired t-Test

Potassium (wt%) MA - Potassium (wt%) PF

Mean Difference	0.022405	Prob > t 0.0036
Std Error	0.007523	Prob > t 0.0018
t-Ratio	2.978064	Prob < t 0.9982
DF	104	

(Negative values excluded.)

Magnesium (wt%) PF By MA



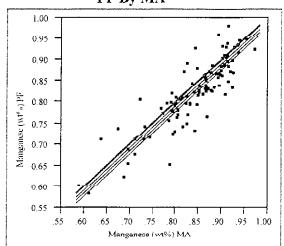
Paired t-Test

Magnesium (wt%) MA - Magnesium (wt%) PF

Mean Difference	0.02753	Prob > t < .0001
Std Error	0.005134	Prob > t < .0001
t-Ratio	5.361954	Prob < t 1.0000
DF	105	

Exhibit 10: Paired Comparisons Between Dissolution Methods for SME and MFT Cations

Manganese (wt%) PF By MA

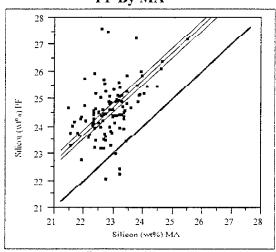


Paired t-Test

Manganese (wt%) MA - Manganese (wt%) PF

Mean Difference	0.017468	Prob > t < .0001
Std Error	0.003807	Prob > t < .0001
t-Ratio	4.587971	$Prob \le t \ 1.0000$
DF	105	

Silicon (wt%) PF By MA

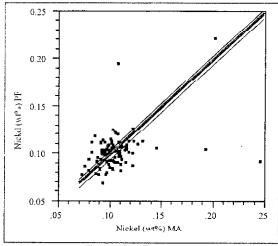


Paired t-Test

Silicon (wt%) MA - Silicon (wt%) PF

Mean Difference	-1.7029	Prob > t < .0001
Std Error	0.090028	$Prob \ge t \ 1.0000$
t-Ratio	-18.9151	$Prob \le t \le .0001$
DF	105	

Nickel (wt%) PF By MA

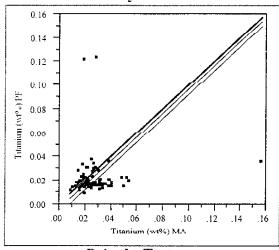


Paired t-Test

Nickel (wt%) MA - Nickel (wt%) PF

Mean Difference	0.001628	Prob > t 0.4726
Std Error	0.002259	Prob > t 0.2363
t-Ratio	0.720846	Prob < t 0.7637
DE	105	

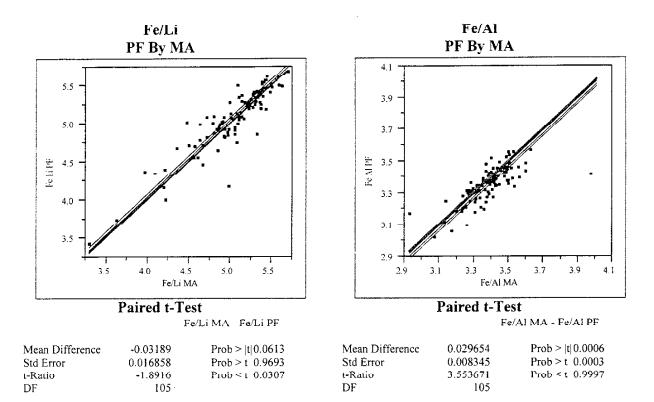
Titanium (wt%) PF By MA



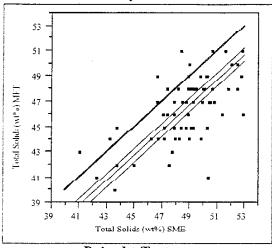
Paired t-Test

Titanium (wt%) MA - Titanium (wt%) PF

Mean Difference	0.003903	Prob > t 0.0564
Std Error	0.002023	Prob \geq t 0.0282
t-Ratio	1.929269	Prob < t 0.9718
DW	105	



Total Solids (wt%) MFT By SME

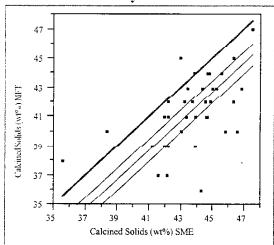


Paired t-Test

Total Solids (wt%) SME - Total Solids (wt%) MFT

Mean Difference	2.327449	Prob > t	<.0001
Std Error	0.260035	Prob > t	<.0001
t-Ratio	8.950517	$Prob \le t$	1.0000
DF	68		

Calcined Solids (wt%) MFT By SME

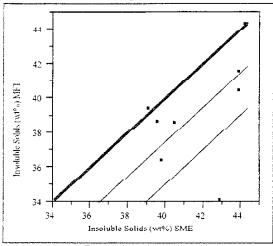


Paired t-Test

Calcined Solids (wt%) SME - Calcined Solids (wt%) MFT

Mean Difference	2.331872	Piob > t	<.0001
Std Error	0.371955	Prob > t	<.0001
t-Ratio	6.269233	$Prob \le t$	1.0000
DF	36		

Insoluble Solids (wt%) MFT By SME

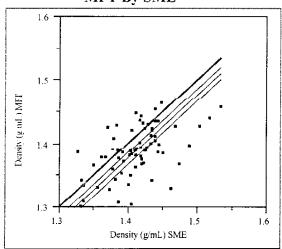


Paired t-Test

Insoluble Solids (wt%) SME - Insoluble Solids (wt%) MFT

Mean Difference	2.541875	$Prob \ge t $	0.0426
Std Error	1.027378	Prob > t	0.0213
t-Ratio	2.474139	$Prob \le t$	0.9787
DE	7		

Density (g/mL) MFT By SME

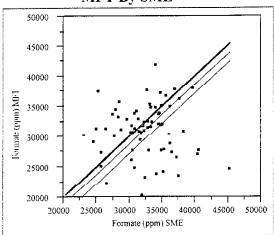


Paired t-Test

Density (g/mL) SME - Density (g/mL) MFT

Mean Difference	0.023029	Prob $\geq \mathfrak{t} $	<.0001
Std Error	0.004618	Prob > t	<.0001
t-Ratio	4.986705	Prob < t	1.0000
DF	69		

Formate (ppm) MFT By SME



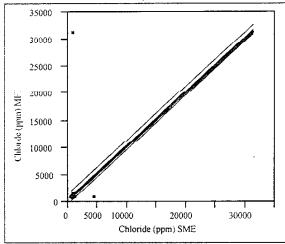
(Excludes results from batch 52)

Paired t-Test

Formate (ppm) SME - Formate (ppm) MFT

Mean Difference	1445.098	Prob > t	0.0537
Std Error	735.8953	Prob > t	0.0269
t-Ratio	1.963728	Prob ≤ t	0.9731
DF	67		

Chloride (ppm) MFT By SME

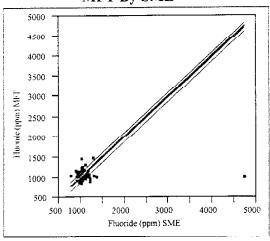


Paired t-Test

Chloride (ppm) SME - Chloride (ppm) MFT

Mean Difference	-416.619	Prob > t	0.3521
Std Error	444.6349	Prob > t	0.8240
t-Ratio	-0.93699	$Prob \le t$	0.1760
DF	68		

Fluoride (ppm) MFT By SME

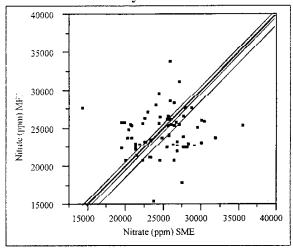


Paired t-Test

Fluoride (ppm) SME - Fluoride (ppm) MFT

Mean Difference	28.53321	$Prob \ge t $	0.6162
Std Error	56.66402	$Prob \ge t$	0.3081
t-Ratio	0.503551	$Prob \le t$	0.6919
DF	68		

Nitrate (ppm) MFT By SME



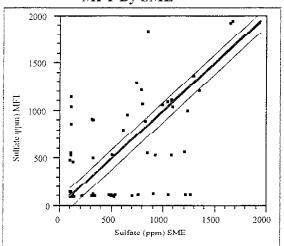
Paired t-Test

Nitrate (ppm) SME - Nitrate (ppm) MFT

Mean Difference	445.5918	Prob > t	0.3934
Std Error	518.7318	Prob > t	0.1967
t-Ratio	0.859002	Prob < t	0.8033
DF	68		

Exhibit 11: Paired Comparisons By Batch Between MFT and SME Anions





Paired t-Test

Sulfate (ppm) SME - Sulfate (ppm) MFT

Mean Difference	19.83274	Prob > t	0.7034
Std Error	51.87768	Prob > t	0.3517
t-Ratio	0.382298	$Prob \le t$	0.6483
DF	69		

WSRC-RP-2000-00174

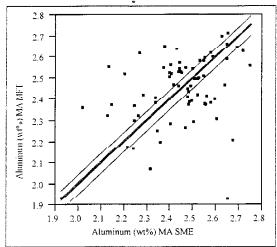
Revision 0

Exhibit 11: Paired Comparisons By Batch Between MFT and SME Anions

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Exhibit 12: Paired Comparisons (by batch) Between the SME and MFT by Dissolution Method

Aluminum (wt%) MA MFT By MA SME

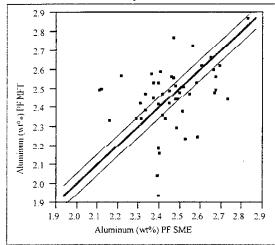


Paired t-Test

Aluminum (wt%) MA SME - Aluminum (wt%) MA MFT

Mean Difference	0.006317	Prob > t	0.7720
Std Error	0.021715	Prob > t	0.3860
t-Ratio	0.290888	$Prob \le t$	0.6140
DE	69		

Aluminum (wt%) PF MFT By PF SME

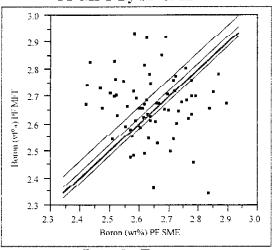


Paired t-Test

Aluminum (wt%) PF SME - Aluminum (wt%) PF MFT

Mean Difference	0.002572	$Prob \ge t $	0.9235
Std Error	0.026631	Prob > t	0.4617
t-Ratio	0.096584	$Prob \le t$	0.5383
DE	18		

Boron (wt%) PF MFT By PF SME

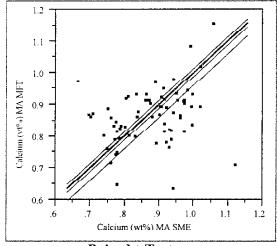


Paired t-Test

Boron (wt%) PF SME - Boron (wt%) PF MFT

Mean Difference	-0.02348	Prob > t	0.2418
Std Error	0.01989	Prob > t	0.8791
t-Ratio	-1.18073	$Prob \le t$	0.1209
DF	69		

Calcium (wt%) MA MFT By MA SME



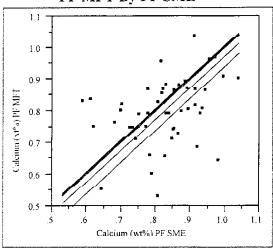
Paired t-Test

Calcium (wt%) MA SME - Calcium (wt%) MA MFT

Mean Difference	0.012809	Prob > t	0.3312
Std Error	0.01309	Prob > t	0.1656
t-Ratio	0.978535	$Prob \le t$	0.8344
DF	69		

Exhibit 12: Paired Comparisons (by batch) Between the SME and MFT by Dissolution Method

Calcium (wt%)
PF MFT By PF SME

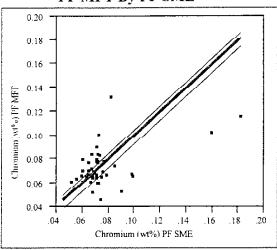


Paired t-Test

Calcium (wt%) PF SME - Calcium (wt%) PF MFT

Mean Difference	0.027354	Prob > t	0.1104
Std Error	0.016818	Prob > t	0.0552
t-Ratio	1.626502	$Prob \le t$	0.9448
DE	48		

Chromium (wt%) PF MFT By PF SME

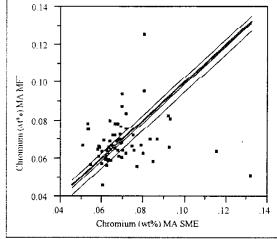


Paired t-Test

Chromium (wt%) PF SME - Chromium (wt%) PF MFT

Mean Difference	0.001902	Prob > t	0.4944
Std Error	0.002762	Prob > t	0.2472
t-Ratio	0.688614	$Prob \le t$	0.7528
DF	48		

Chromium (wt%) MA MFT By MA SME

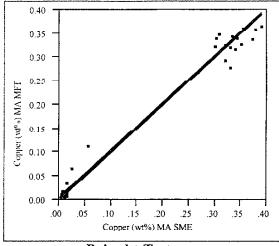


Paired t-Test

Chromium (wt%) MA SME - Chromium (wt%) MA MFT

Mean Difference	0.001151	Prob > t	0.5644
Std Error	0.001988	Prob > t	0.2822
t-Ratio	0.579061	$Prob \le t$	0.7178
DF	69		

Copper (wt%) MA MFT By MA SME



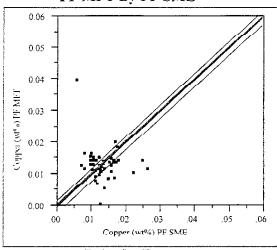
Paired t-Test

Copper (wt%) MA SME - Copper (wt%) MA MFT

Mean Difference	-0.00005	Prob > t	0.9800
Std Error	0.001843	Prob > t	0.5100
t-Ratio	-0.02519	$Prob \le t$	0.4900
DF	69		

Exhibit 12: Paired Comparisons (by batch) Between the SME and MFT by Dissolution Method

Copper (wt%)
PF MFT By PF SME

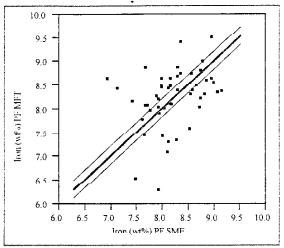


Paired t-Test

Copper (wt%) PF SME - Copper (wt%) PF MFT

Mean Difference	0.000516	$Prob \ge t $	0.6098
Std Error	0.001004	Prob > t	0.3049
t-Ratio	0.513754	$Prob \le t$	0.6951
DF	48		

Iron (wt%) PF MFT By PF SME

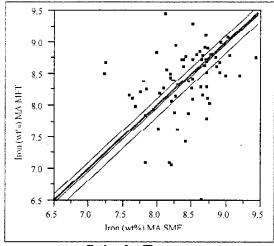


Paired t-Test

Iron (wt%) PF SME - Iron (wt%) PF MFT

Mean Difference	-0.01428	Prob > t	0.8801
Std Error	0.094098	Prob > t	0.5600
t-Ratio	-0.1517	$Prob \le t$	0.4400
DF	48		

Iron (wt%) MA MFT By MA SME

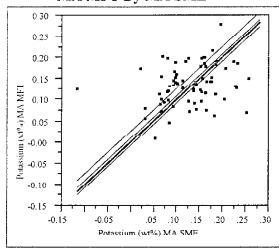


Paired t-Test

Iron (wt%) MA SME - Iron (wt%) MA MFT

Mean Difference	0.035477	Prob > t	0.6141
Std Error	0.070046	Prob > t	0.3071
t-Ratio	0.506475	$Prob \le t$	0.6929
DF	69		

Potassium (wt%) MA MFT By MA SME

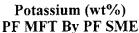


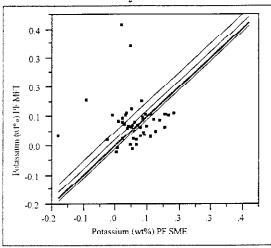
Paired t-Test

Potassium (wt%) MA SME - Potassium (wt%) MA MFT

Mean Difference	-0.00831	Prob > t	0.3107
Std Error	0.008134	Prob > t	0.8446
t-Ratio	-1.02125	Prob < t	0.1554
DF	69		

Exhibit 12: Paired Comparisons (by batch) Between the SME and MFT by Dissolution Method



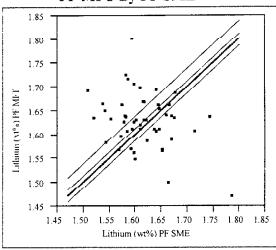


Paired t-Test

Potassium (wt%) PF SME - Potassium (wt%) PF MFT

Mean Difference	-0.01915	Prob > t	0.1796
Std Error	0.01406	Prob > t	0.9102
t-Ratio	-1.36181	Prob < t	0.0898
DF	48		

Lithium (wt%) PF MFT By PF SME

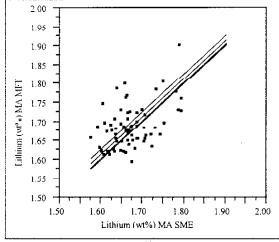


Paired t-Test

Lithium (wt%) PF SME - Lithium (wt%) PF MFT

Mean Difference	-0.01212	Prob > t	0.3481
Std Error	0.01279	Prob > t	0.8260
t-Ratio	-0.94758	$Prob \le t$	0.1740
DF	48		

Lithium (wt%) MA MFT By MA SME

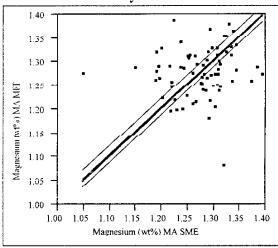


Paired t-Test

Lithium (wt%) MA SME - Lithium (wt%) MA MFT

Mean Difference	-0.01198	Prob > t	0.0759
Std Error	0.006648	Prob > t	0.9621
t-Ratio	-1.80237	$Prob \le t$	0.0379
DF	69		

Magnesium (wt%) MA MFT By MA SME



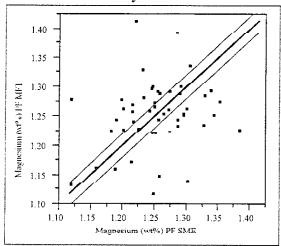
Paired t-Test

Magnesium (wt%) MA SME - Magnesium (wt%) MA MFT

Mean Difference	-0.00563	Prob > t	0.5252
Std Error	0.008811	Prob > t	0.7374
t-Ratio	-0.63866	$Prob \le t$	0.2626
DF	69		

Exhibit 12: Paired Comparisons (by batch) Between the SME and MFT by Dissolution Method

Magnesium (wt%) PF MFT By PF SME

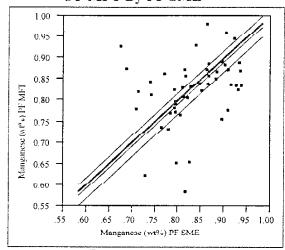


Paired t-Test

Magnesium (wt%) PF SME - Magnesium (wt%) PF MFT

Mean Difference	0.000833	Prob > t	0.9347
Std Error	0.01011	Prob > t	0.4673
t-Ratio	0.082393	$Prob \le t$	0.5327
DF	48		

Manganese (wt%) PF MFT By PF SME

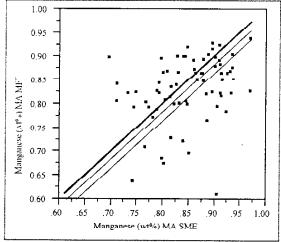


Paired t-Test

Manganese (wt%) PF SME - Manganese (wt%) PF MFT

Mean Difference	0.009557	Prob > t	0.4527
Std Error	0.012625	Prob > t	0.2264
t-Ratio	0.757	$Prob \le t$	0.7736
DF	48		

Manganese (wt%) MA MFT By MA SME

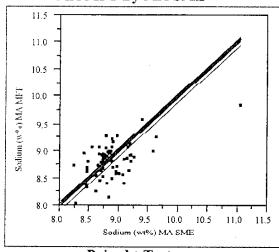


Paired t-Test

Manganese (wt%) MA SME - Manganese (wt%) MA MFT

Mean Difference	0.017395	Prob > t	0.0685
Std Error	0.009398	Prob > t	0.0342
t-Ratio	1.85096	$Prob \le t$	0.9658
DF	69		

Sodium (wt%) MA MFT By MA SME



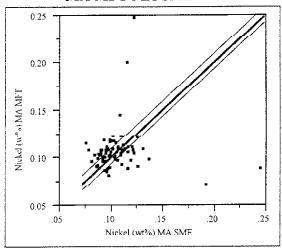
Paired t-Test

Sodium (wt%) MA SME - Sodium (wt%) MA MFT

Mean Difference	0.036285	Prob > t	0.3544
Std Error	0.038916	Prob > t	0.1772
t-Ratio	0.932402	$Prob \le t$	0.8228
DF	69		

Exhibit 12: Paired Comparisons (by batch) Between the SME and MFT by Dissolution Method

Nickel (wt%) MA MFT MA SME

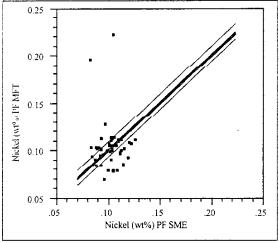


Paired t-Test

Nickel (wt%) MA SME - Nickel (wt%) MA MFT

Mean Difference	-0.00136	Prob > t	0.7338
Std Error	0.00399	Prob > t	0.6331
τ-Ratio	-0.34152	Prob ≤ ι	0.3669
DE	69		

Nickel (wt%) PF MFT By PF SME

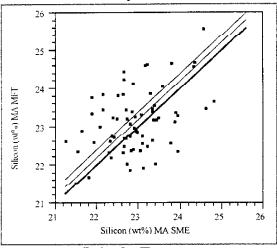


Paired t-Test

Nickel (wt%) PF SME Nickel (wt%) PF MFT

Mean Difference	-0.00194	Prob > t	0.6222
Std Error	0.003917	Prob > t	0.6889
t-Ratio	-0.496	Prob≤t	0.3111
DE	40		

Silicon (wt%) MA MFT By MA SME

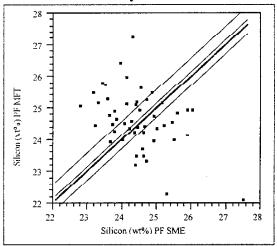


Paired t-Test

Silicon (wt%) MA SME - Silicon (wt%) MA MFT

Mean Difference	-0.19288	Prob > t	0.0582
Std Error	0.100152	Prob > t	0.9709
t-Ratio	-1.92588	$Prob \le t$	0.0291
DF	69		

Silicon (wt%) PF MFT By PF SME

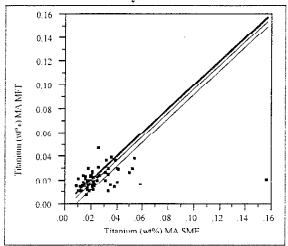


Paired t-Test

Silicon (wt%) PF SME - Silicon (wt%) PF MFT

Mean Difference	-0.14783	Prob > t	0.4983
Std Error	0.216645	Prob > t	0.7509
t-Ratio	-0.68238	$Prob \le t$	0.2491
DF	48		

Titanium (wt%) MA MFT By MA SME

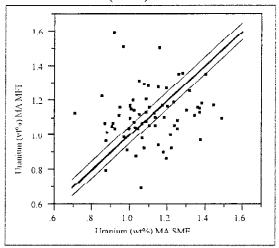


Paired t-Test

Titanium (wt%) MA SME - Titanium (wt%) MA MFT

Mean Difference	0.003444	Prob > t	0.1282
Std Error	0.002237	Prob > t	0.0641
t-Ratio	1.539819	Prob < t	0.9359
DF	69		

Uranium (wt%) MA MFT By Uranium (wt%) MA SME

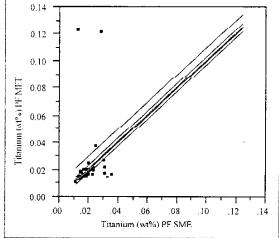


Paired t-Test

Uranium (wt%) MA SME - Uranium (wt%) MA MFT

Mean Difference	-0.00146	Prob > t	0.9544
Std Error	0.025434	Prob > t	0.5228
t-Ratio	-0.05745	$Prob \le t$	0.4772
DE	ń9		

Titanium (wt%) PF MFT By PF SME

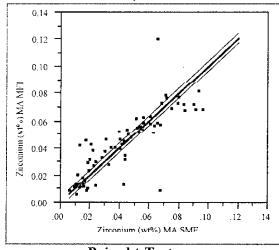


Paired t-Test

Titanium (wt%) PF SME - Titanium (wt%) PF MFT

Mean Difference	-0.00327	Prob > t	0.2925
Std Error	0.003071	Prob > t	0.8538
t-Ratio	-1.06435	$Prob \le t$	0.1462
DF	48		

Zirconium (wt%) MA MFT By MA SME



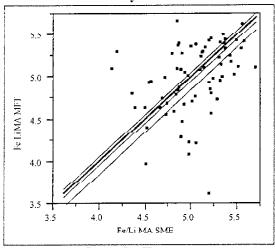
Paired t-Test

Zirconium (wt%) MA SME - Zirconium (wt%) MA MFT

Mean Difference	-0.00056	Prob > t	0.7472
Std Error	0.001719	Prob > t	0.6264
t-Ratio	-0.32359	Prob < t	0.3736
DF	69		

Exhibit 12: Paired Comparisons (by batch) Between the SME and MFT by Dissolution Method

Fe/Li MA MFT By MA SME

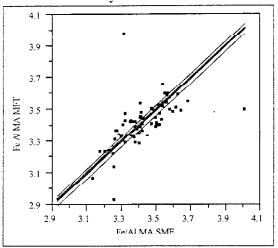


Paired t-Test

Fe/Li MA SME - Fe/Li MA MFT

Mean Difference	0.054631	$Prob \ge t $	0.2940
Std Error	0.051664	Prob > t	0.1470
t-Ratio	1.057421	Prob < t	0.8530
Dir	69		

Fe/Al MA MFT By Fe/Al MA SME

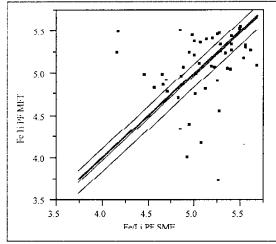


Paired t-Test

Fe/Al MA SME - Fe/Al MA MFT

Mean Difference	0.008503	Prob > t	0.5802
Std Error	0.0153	Prob > t	0.2901
t-Ratio	0.555721	$Prob \le t$	0.7099
DF	69		

Fe/Li PF MFT By PF SME

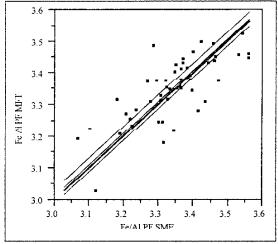


Paired t-Test

Fe/Li PF SME - Fe/Li PF MFT

Mean Difference	0.028678	Prob > t	0.6783
Std Error	0.068718	Prob > t	0.3392
t-Ratio	0.41732	$Prob \le t$	0.6608
DF	48		

Fe/Al PF MFT PF SME



Paired t-Test

Fe/Al PF SME - Fe/Al PF MFT

Mean Difference	-0.00682	Prob > t	0.5339
Std Error	0.010887	Prob > t	0.7331
t-Ratio	-0.62666	Prob < t	0.2669
DF	48		

Response: Total Solids (wt%) Summary of Fit

0.988969
0.166579
15.81092
284

Variance Component Estimates Component Var Comp Est

Component	vai Comp Est
Batch	1.895215
Residual	0.027749

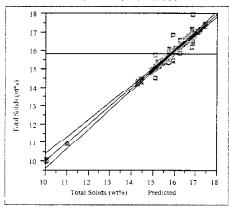
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio Prob>F

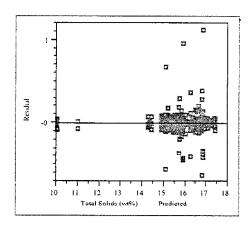
 Batch
 532.361
 7.71538
 69
 278.0458
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Меан Ѕquare	F Ratio
Model	69	532.36136	7.71538	278.0458
Error	214	5.93820	0.02775	Prob>F
C Total	283	538,29956		< 0001



Response: Calcined Solids (wt%) Summary of Fit

RSquare	0.931004
Root Mean Square Error	0.311313
Mean of Response	13.43221
Observations (or Sum Wgts)	226

Variance Component Estimates Component Var Comp Est

Component	vai Comp Est
Batch	0.970964
Residual	0.096916

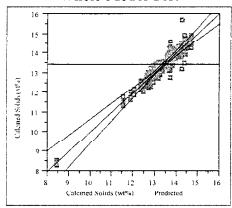
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

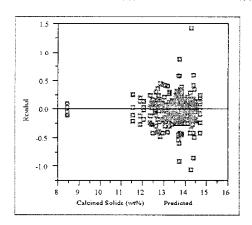
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 221.007
 3.94656
 56
 40.7216
 <.0001</td>

Whole-Model Test



in the state of th				
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	56	221.00715	3.94656	40.7216
Error	169	16.37874	0.09692	Prob>F
C Total	225	237.38589		<.0001



Response: Insoluble Solids (wt%) Summary of Fit

RSquare	0.810236
Root Mean Square Error	0.343496
Mean of Response	12.01125
Observations (or Sum Wgts)	40

Variance Component Estimates Component Var Comp Est

Batch	0.390318
Residual	0.117989

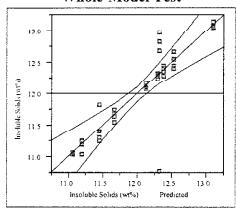
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

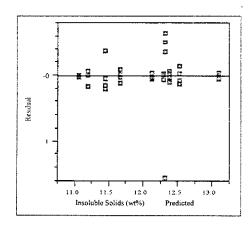
 Batch
 15.1134
 1.67926
 9
 14.2323
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	9	15.113363	1.67926	14.2323
Error	30	3.539675	0.11799	Prob>F
C Total	39	18.653037		<.0001



Response: Density (g/mL) Summary of Fit

RSquare	0.822276
Root Mean Square Error	0.01273
Mean of Response	1.07822
Observations (or Sum Wgts)	286

Variance Component Estimates Component Var Comp Est

Component	vai Comp Lst
Batch	0.000532
Residual	0.000162

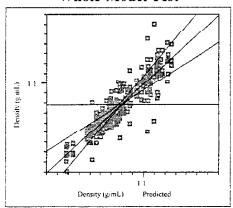
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

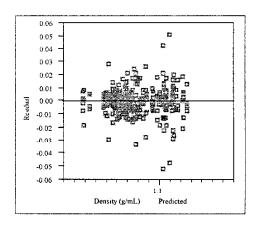
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 0.16121
 0.0023
 70
 14.2106
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	70	0.16121304	0.002303	14.2106
Error	215	0.03484408	0.000162	Prob>F
C Total	285	0.19605712		<.0001



Response: Total Hydroxide (eq/L) Summary of Fit

RSquare	0.979344
Root Mean Square Error	0.017305
Mean of Response	0.176852
Observations (or Sum Wgts)	73

Variance Component Estimates Component Var Comp Est

Component	var Comp est
Batch	0.000103
Residual	0.000299

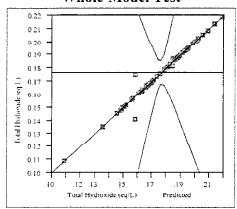
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

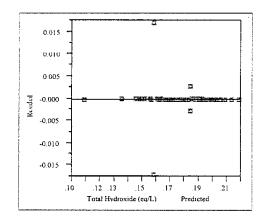
 Batch
 0.0284
 0.00041
 70
 1.3546
 0.5183

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	70	0.02839540	0.000406	1.3546
Error	2	0.00059891	0.000299	Prob>F
C Total	72	0.02899431		0.5183



Response: Formate (ppm) Summary of Fit

RSquare	0.957516
Root Mean Square Error	192.4118
Mean of Response	4139.225
Observations (or Sum Wgts)	284

Variance Component Estimates Component Var Comp Est

Component	var comp Est
Batch	625491.9
Residual	37022.3

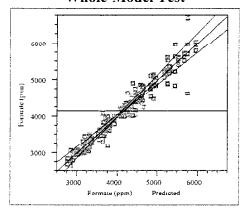
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

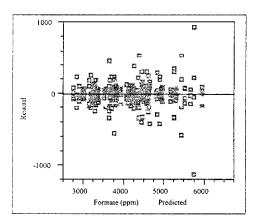
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 1.777e8
 2538990
 70
 68.5800
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	70	177729280	2538990	68.5800
Error	213	7885750	37022	Prob>F
C Total	283	185615030		<.0001



Response: Chloride (ppm) Summary of Fit

RSquare	0.383333
Root Mean Square Error	90.14784
Mean of Response	1025.4
Observations (or Sum Wgts)	40

Variance Component Estimates Component Var Comp Est

2178.081
8126.633

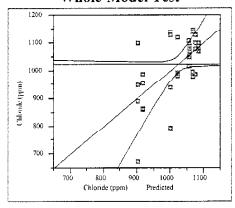
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

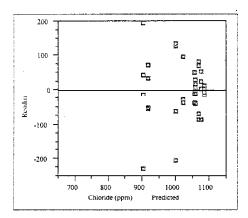
 Batch
 151551
 16839
 9
 2.0721
 0.0652

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	9	151550.60	16839.0	2.0721
Error	30	243799.00	8126.6	Prob>F
C Total	39	395349 60		0.0652



Response: Fluoride (ppm) Summary of Fit

RSquare	0.383333
Root Mean Square Error	90.14784
Mean of Response	1025.4
Observations (or Sum Wgts)	40

Variance Component Estimates Component Var Comp Est

Component	Var Comp Es
Batch	2178.08
Residual	8126.633

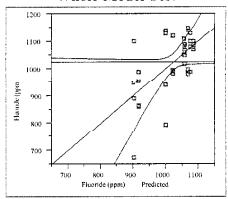
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 151551
 16839
 9
 2.0721
 0.0652

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	9	151550.60	16839.0	2.0721
Error	30	243799.00	8126.6	Prob>F
C Total	39	395349.60		0.0652

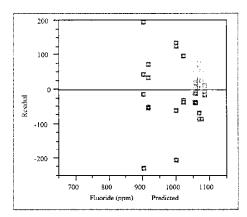


Exhibit 13: Random Effects Study for SRAT Receipt by Analyte

Response: Nitrate (ppm) Summary of Fit

RSquare	0.904372
Root Mean Square Error	508.7749
Mean of Response	12441.34
Observations (or Sum Wgts)	284

Variance Component Estimates

Component	Var Comp Est
Batch	1797529
Residual	258851.9

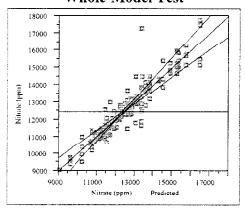
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

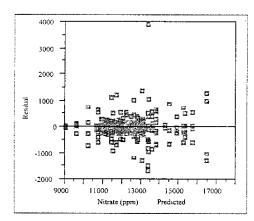
 Batch
 5.214e8
 7448969
 70
 28.7770
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	70	521427842	7448969	28.7770
Error	213	55135450	258852	Prob>F
C Total	283	576563292		<.0001



Response: Nitrite (ppm) Summary of Fit

RSquare	0.899566
Root Mean Square Error	195.4416
Mean of Response	7276.549
Observations (or Sum Wgts)	284

Variance Component Estimates Component Var Comp Est

Component	vai Comp Est
Batch	250709.8
Residual	38197.42

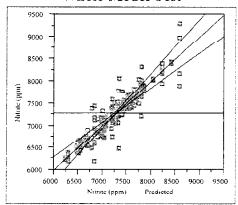
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

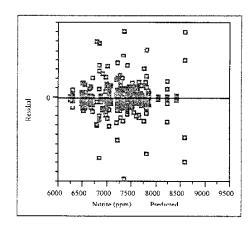
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 7.287e7
 1041037
 70
 27.2541
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	70	72872568	1041037	27.2541
Error	213	8136050	38197	Prob>F
C Total	283	81008618		<.0001



Response: Sulfate (ppm) Summary of Fit

RSquare	0.642159
Root Mean Square Error	64.79314
Mean of Response	1075.482
Observations (or Sum Wgts)	284

Variance Component Estimates

Component	var Comp Est
Batch	4681.479
Residual	4198.151

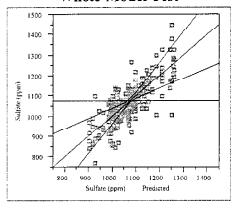
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

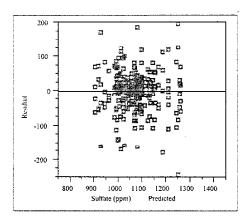
 Batch
 1604685
 22924.1
 70
 5.4605
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares		F Ratio
Model	70	1604684.7	22924.1	
Error	213	894206.2	4198.2	Prob>F
C Total	283	2498890.9		<.0001



Response: Aluminum (wt%) Summary of Fit

·•	
RSquare	0.622141
Root Mean Square Error	0.196362
Mean of Response	6.763656
Observations (or Sum Wgts)	61

Variance Component Estimates Component Var Comp Est

Component	,	- Cump 250
Batch		0.04392
Residual		0.038558

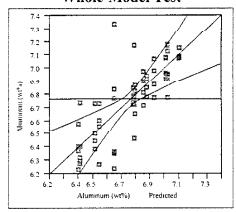
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

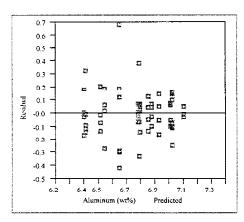
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 2.98382
 0.22952
 13
 5.9527
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	13	2.9838164	0.229524	5.9527
Error	47	1.8122314	0.038558	Prob>F
C I otal	60	4.7960478		<.0001



Response: Calcium (wt%) Summary of Fit

0.85995
0.081225
2.440852
61

Variance Component Estimates Component Var Comp Est

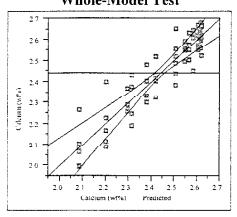
Batch	0.032167
Residual	0.006598

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

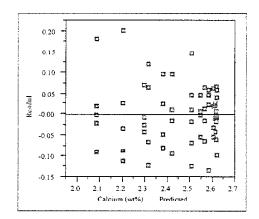
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	1.90401	0.14646	13	22,1996	<.0001

Whole-Model Test



Analysis of Variance

,					
Source	DF	Sum of Squares	Mean Square	F Ratio	
Model	13	1.9040148	0.146463	22.1996	
Error	47	0.3100849	0.006598	Prob>F	
C Total	60	2.2140997		<.0001	



Response: Chromium (wt%) Summary of Fit

RSquare	0.405309
Root Mean Square Error	0.031417
Mean of Response	0.179803
Observations (or Sum Wgts)	61

Variance Component Estimates Component Var Comp Est

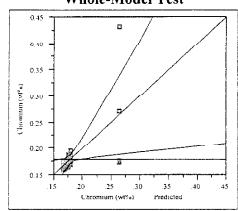
Component	vai Comp Est
Batch	0.000332
Residual	0.000987

These estimates based on equating Mean Squares to Expected Value.

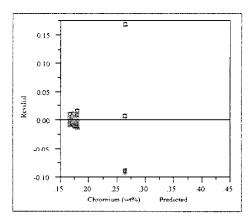
Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.03162	0.00243	13	2.4641	0.0121

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	13	0.03161722	0.002432	2.4641
Error	47	0.04639042	0.000987	Prob>F
C Total	60	0.07800764		0.0121



Response: Copper (wt%) Summary of Fit

RSquare	0.981833
Root Mean Square Error	0.018165
Mean of Response	0.326459
Observations (or Sum Wgts)	61

Variance Component Estimates Component Var Comp Est

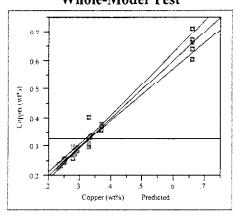
Batch	0.014752
Residual	0.00033

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

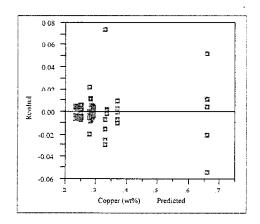
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.83816	0.06447	13	195.3930	<.0001

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	13	0.83815661	0.064474	195.393
Error	47	0.01550853	0.000330	Prob>F
C Total	60	0.85366515		<.0001



Response: Iron (wt%) Summary of Fit

RSquare	0.784033
Root Mean Square Error	0.612254
Mean of Response	25.9583
Observations (or Sum Wgts)	61

Variance Component Estimates Component Var Comp Est

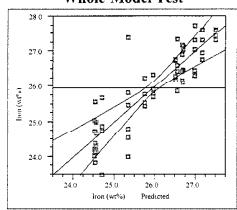
Component	vai Comp Est
Batch	1.045333
Residual	0.374855

These estimates based on equating Mean Squares to Expected Value.

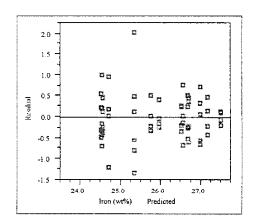
Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	63.9602	4.92001	13	13.1251	<.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	13	63.960162	4.92001	13.1251
Error	47	17.618199	0.37486	Prob>F
C Lotal	60	81.578361		<.0001



Response: Potassium (wt%) Summary of Fit

RSquare	0.72516
Root Mean Square Error	0.012448
Mean of Response	0.03877
Observations (or Sum Wets)	61

Variance Component Estimates Component Var Comp Est

Batch 0.000304 Residual 0.000155

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.01922	0.00148	13	9.5391	<.0001

Response: Magnesium (wt%) Summary of Fit

•	
RSquare	0.858126
Root Mean Square Error	0.055191
Mean of Response	1.232672
Observations (or Sum Wgts)	61

Variance Component Estimates Component Var Comp Est

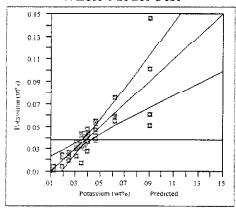
1	
Batch	0.014619
Residual	0.003046

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

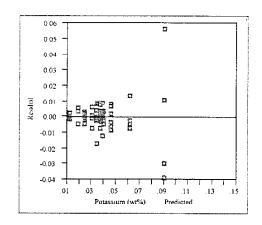
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.86593	0.06661	13	21.8676	<.0001

Whole-Model Test

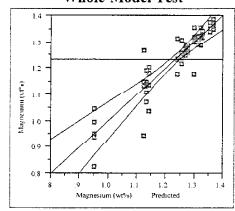


Analysis of Variance

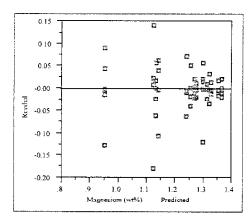
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	13	0.01921587	0.001478	9.5391
Error	47	0.00728292	0.000155	Prob>F
C Total	60	0.02649879		< 0001



Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	13	0.8659273	0.066610	21.8676
Error	47	0.1431642	0.003046	Prob>F
C Total	60	1.0090914		<.0001



Response: Manganese (wt%) Summary of Fit

RSquare	0.78666
Root Mean Square Error	0.062417
Mean of Response	2.736852
Observations (or Sum Wgts)	61

Variance Component Estimates Var Comp Est Component

0.011049 Batch 0.003896 Residual

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.67518	0.05194	13	13.3312	<.0001

b>F	
0001	

These estimates based on equating Mean Squares to Expected Value.

Variance Component Estimates

Response: Sodium (wt%) **Summary of Fit**

RSquare

Batch

Residual

Root Mean Square Error

Observations (or Sum Wgts)

Mean of Response

Component

0.811398

0.533121

6.412754

0.951348

0.284218

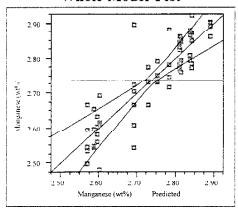
Var Comp Est

61

Tests wrt Random Effects

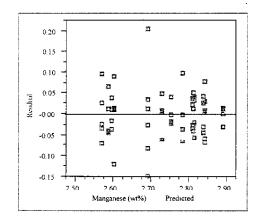
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	57.4694	4.42072	13	15.5540	<.0001

Whole-Model Test



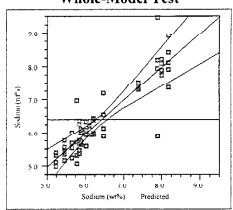
Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	13	0.67518189	0.051937	13.3312
Error	47	0.18310778	0.003896	Prob>F
C Total	60	0.85828967		<.0001

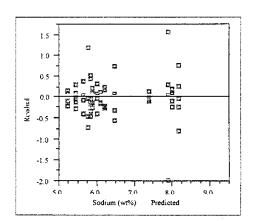


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Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	13	57.469372	4.42072	15.5540
Error	47	13.358231	0.28422	Prob>F
C Total	60	70.827603		<.0001



Response: Nickel (wt%) Summary of Fit

RSquare	0.586071
RSquare Adj	0.47158
Root Mean Square Error	0.013921
Mean of Response	0.296721
Observations (or Sum Wgts)	61

Variance Component Estimates Component Var Comp Est

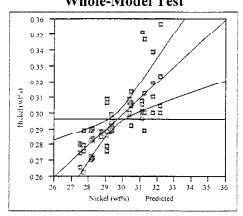
Component	var comp bs
Batch	0.000184
Residual	0.000194

These estimates based on equating Mean Squares to Expected Value

Tests wrt Random Effects

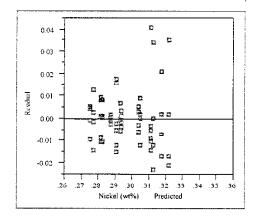
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.0129	0.00099	13	5 1189	< 0001

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	13	0.01289606	0.000992	5.1189
Error	47	0.00910820	0.000194	Prob>F
C Total	60	0.02200426		<.0001



Response: Silicon (wt%) Summary of Fit

RSquare	0.702015
Root Mean Square Error	0.219834
Mean of Response	0.842754
Observations (or Sum Wgts)	61

Variance

Variance Component Estimates Component Var Comp Est Batch 0.083553

 Batch
 0.083553

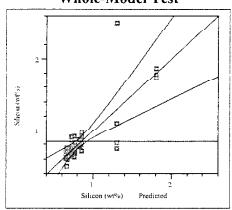
 Residual
 0.048327

These estimates based on equating Mean Squares to Expected Value

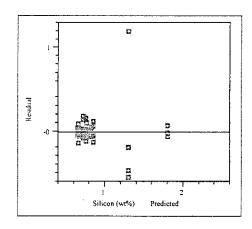
Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	5.35108	0.41162	13	8.5174	<.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	13	5.3510793	0.411621	8.5174
Error	47	2.2713780	0.048327	Prob>F
C Total	60	7.6224573		<.0001



Response: Titanium (wt%) Summary of Fit

•	
RSquare	0.655627
Root Mean Square Error	0.005512
Mean of Response	0.016377
Observations (or Sum Wgts)	61

Variance Component Estimates Component Var Comp Est

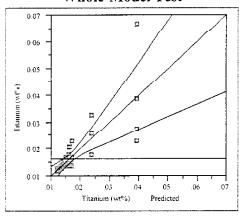
Batch 0.000041 Residual 0.00003

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

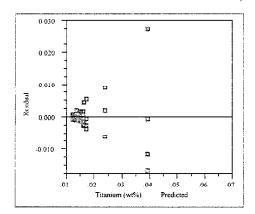
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.00272	0.00021	13	6.8831	<.0001

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	13	0.00271844	0.000209	6.8831
Error	47	0.00142788	0.000030	Prob>F
C Total	60	0.00414633		<.0001



Response: Uranium (wt%) Summary of Fit

Dumming Office	
RSquare	0.776258
Root Mean Square Error	0.064672
Mean of Response	2.861197
Observations (or Sum Wgts)	61

Variance Component Estimates Component Var Comp Est

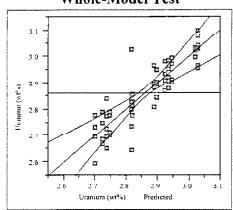
Component	·
Batch	0.011104
Residual	0.004182

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.68201	0.05246	13	12.5433	<.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	13	0.68200901	0.052462	12.5433
Error	47	0.19657663	0.004182	Prob>F
C Total	60	0.87858564		<.0001

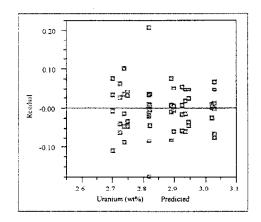


Exhibit 13: Random Effects Study for SRAT Receipt by Analyte

Response: Zirconium (wt%) Summary of Fit

RSquare	0.642673
Root Mean Square Error	0.019339
Mean of Response	0.026738
Observations (or Sum Wets)	61

Variance Component Estimates Component Var Comp Est

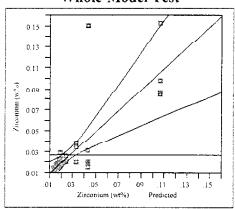
1	· · · · · · · · · · · · · · · · · · ·
Batch	0.000473
Residual	0.000374

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

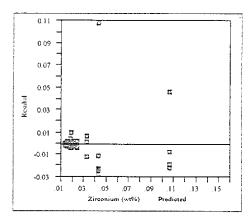
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.03162	0.00243	13	6.5025	<.0001

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Katio
Model	13	0.03161552	0.002432	6.5025
Error	47	0.01757828	0.000374	Prob>F
C Total	60	0.04919380		<.0001



Response: TIC (ppm) Summary of Fit

RSquare	0.963122
Root Mean Square Error	33 98965
Mean of Response	584.6057
Observations (or Sum Wgts)	247

Variance Component Estimates

Component	var Comp est
Batch	21637.49
Residual	1155.296

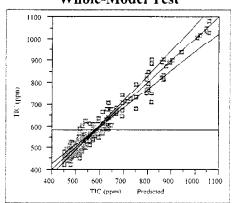
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 5340516
 77398.8
 69
 66.9947
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	5340516.5	77398.8	66.9947
Error	177	204487.5	1155.3	Prob>F
C Total	246	5545003.9		< 0001

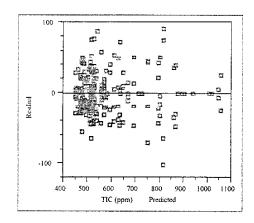


Exhibit 13: Random Effects Study for SRAT Receipt by Analyte

Response: Fe/Al Summary of Fit

RSquare	0.436641
Root Mean Square Error	0.064888
Mean of Response	3.838125
Observations (or Sum Wgts)	61

Variance Component Estimates Component Var Comp Est

Component	, at Comp 200
Batch	0.001745
Residual	0.00421

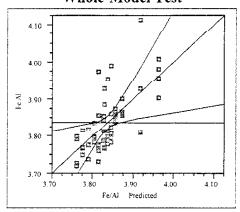
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

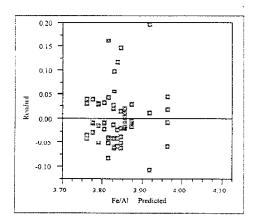
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 0.15338
 0.0118
 13
 2.8022
 0.0049

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	13	0.15337914	0.011798	2.8022
Error	47	0.19789168	0.004210	Prob>F
C Total	60	0.35127081		0.0049



Response: Total Solids (wt%) Summary of Fit

RSquare	0.946867
Root Mean Square Error	0.425524
Mean of Response	22.33421
Observations (or Sum Wgts)	280

Variance Component Estimates Component Var Comp Est

1	
Batch	2.409923
Residual	0.181071

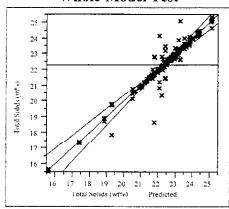
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

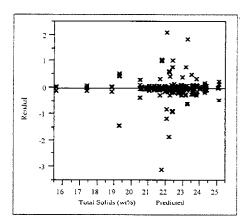
 Batch
 677.633
 9.82076
 69
 54.2372
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	677.63258	9.82076	54.2372
Error	210	38.02485	0.18107	Prob>F
C Total	279	715.65743		<.0001



Response: Calcined Solids (wt%) Summary of Fit

.	
RSquare	0.905599
Root Mean Square Error	0.553193
Mean of Response	17.55246
Observations (or Sum Wgts)	280

Variance Component Estimates

Component	var Comp Est
Batch	2.157191
Residual	0.306023

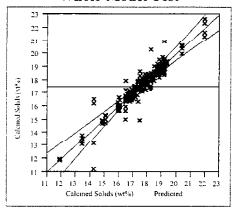
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

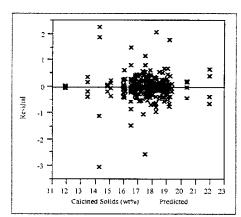
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 616.5
 8.93479
 69
 29.1965
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	616.50027	8.93479	29.1965
Error	210	64.26473	0.30602	Prob>F
C Total	279	680.76500		<.0001



Response: Insoluble Solids (wt%) Summary of Fit

RSquare	0.724617
Root Mean Square Error	1.026023
Mean of Response	14.80941
Observations (or Sum Wgts)	68

Variance Component Estimates

Сотровен	var Comp Est
Batch	1.944196
Residual	1.052723

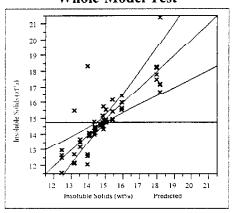
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

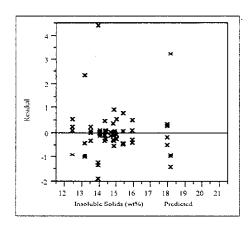
 Batch
 141.272
 8.82951
 16
 8.3873
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	16	141.27213	8.82951	8.3873
Error	51	53.68885	1.05272	Prob>F
C Total	67	194.96098		<.0001



Response: Density (g/mL) Summary of Fit

RSquare	0.788787
Root Mean Square Error	0.013858
Mean of Response	1.147143
Observations (or Sum Wgts)	280

Variance Component Estimates

Component	Var Comp Est
Batch	0.000498
Residual	0.000192

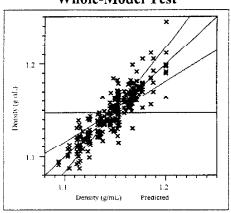
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

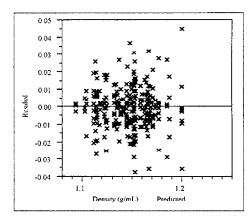
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 0.15061
 0.00218
 69
 11.3660
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	0.15061429	0.002183	11.3660
Error	210	0.04033000	0.000192	Prob>F
C Total	279	0.19094429		<.0001



Response: Formate (ppm) Summary of Fit

RSquare	0.916156
Root Mean Square Error	1529.721
Mean of Response	20902.82
Observations (or Sum Wgts)	284

Variance Component Estimates Component Var Comp Est

oomponen.	· ar comp ist
Batch	18866087
Residual	2340047

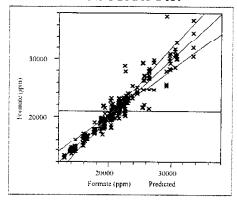
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

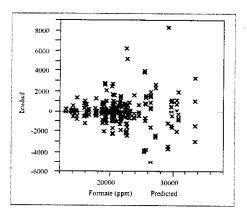
 Batch
 5.446e9
 7.78e+7
 70
 33.2491
 <.0001</td>

Whole-Model Test



Analysis of Variance

		•		
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	70	5446307746	77804396	33.2491
Error	213	498430000	2340047	Prob>F
C Total	283	5944737746		<.0001



Response: Chloride (ppm) Summary of Fit

•	
RSquare	0.590718
Root Mean Square Error	74 53958
Mean of Response	1074.568
Observations (or Sum Wgts)	280

Variance Component Estimates Component Var Comp Est

Component	, 41	Comp Lst
Batch		4712.526
Residual		5556.149

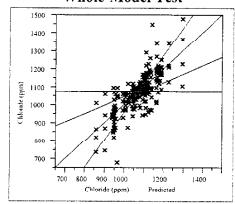
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 1684031
 24406.3
 69
 4.3927
 <.0001</td>

Whole-Model Test



		₩		
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	1684031.5	24406.3	4.3927
Error	210	1166791.2	5556.1	Prob>F
C Total	279	2850822.7		< 0001

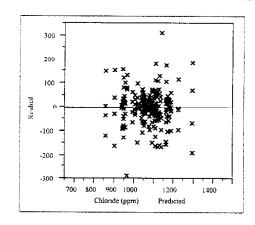


Exhibit 14: Random Effects Study for SRAT Product by Analyte

Response: Fluoride (ppm) Summary of Fit

RSquare	0.532694
Root Mean Square Error	83.14685
Mean of Response	1081.437
Observations (or Sum Wets)	284

Variance Component Estimates

Component	var Comp Est
Batch	4266.65
Residual	6913.399

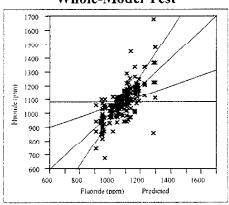
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

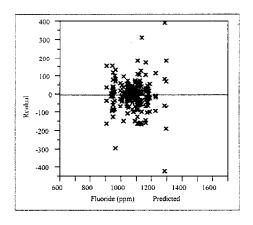
 Batch
 1678600
 23980
 70
 3.4686
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	70	1678599.9	23980.0	3.4686
Error	213	1472554.0	6913.4	Prob>F
C Total	283	3151153.9		<.0001



Response: Nitrate (ppm) Summary of Fit

RSquare	0.878485
Root Mean Square Error	1823.468
Mean of Response	36598.21
Observations (or Sum Wgts)	280

Variance Component Estimates

Component	var Comp Est
Batch	17458638
Residual	3325036

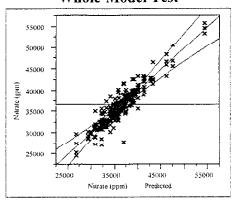
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

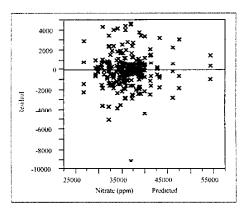
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 5.048e9
 7.316e7
 69
 22.0026
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	5048011607	73159589	22.0026
Error	210	698257500	3325036	Prob>F
C Total	279	5746269107		<.0001



Response: Nitrite (ppm) Summary of Fit

RSquare	0.904073
Root Mean Square Error	73.51017
Mean of Response	1109.686
Observations (or Sum Wots)	280

Variance Component Estimates

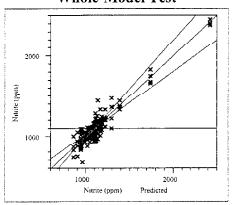
Component	Var Comp Est
Batch	37398.53
Residual	5403.745

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

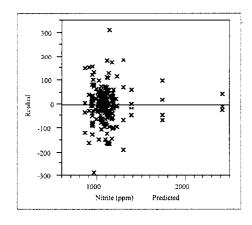
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	1.069e7	154998	69	28.6834	<.0001

Whole-Model Test



Analysis of Variance

		Sum of Squares	Mean Square	
Model	69	10694854	154998	28.6834
Error	210	1134786	5404	Prob>F
C Total	279	11829640		<.0001



Response: Phosphate (ppm) Summary of Fit

RSquare	0.621752
Root Mean Square Error	74.63105
Mean of Response	1084.11
Observations (or Sum Wgts)	272

Variance Component Estimates Component Var Comp Est

Component	vai Comp Esc
Batch	5576.621
Residual	5569.794

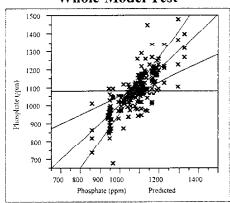
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

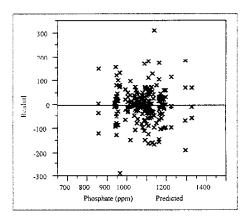
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 1867711
 27876.3
 67
 5.0049
 <.0001</td>

Whole-Model Test



		Sum of Squares	Mean Square	
Model	67	1867710.7	27876.3	5.0049
Error	204	1136238.0	5569.8	Prob>F
C Total	271	3003948.7		<.0001



Response: Sulfate (ppm) Summary of Fit

RSquare	0.778744
Root Mean Square Error	78.3595
Mean of Response	1213.521
Observations (or Sum Wgts)	280

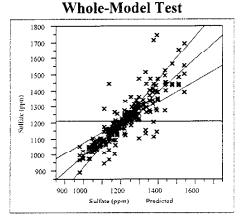
Variance Component Estimates

Component	var Comp Est
Batch	14908.39
Residual	6140.212

These estimates based on equating Mean Squares to Expected Value.

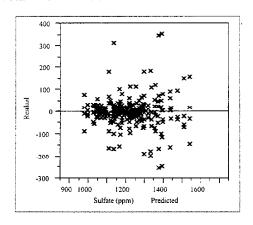
Tests wrt Random Effects

Source SS MS Num DF Num F Ratio Prob>F 4538389 65773.8 69 10.7120 <.0001 Batch



Analysis of Variance

indivision variable					
Source	DF	Sum of Squares	Mean Square	F Ratio	
Model	69	4538389.4	65773.8	10.7120	
Error	210	1289444.5	6140.2	Prob>F	
C Total	279	5827833.9		<.0001	



Response: Aluminum (wt%) **Summary of Fit**

RSquare	0.738289
Root Mean Square Error	0.26669
Mean of Response	6.214109
Observations (or Sum Wgts)	349

Variance Component Estimates

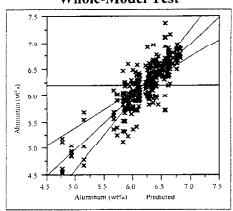
Component	Var Comp Est
Batch	0.151807
Residual	0.071123

These estimates based on equating Mean Squares to Expected Value.

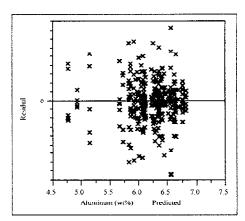
Tests wrt Random Effects

MS Num DF Num F Ratio Prob>F Source 56.7811 0.87356 12.2823 <.0001 Batch 65

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	65	56.781139	0.873556	12.2823
Error	283	20.127916	0.071123	Prob>F
C Total	348	76.909056		<.0001



Response: Calcium (wt%) Summary of Fit

RSquare	0.73568
Root Mean Square Error	0.085118
Mean of Response	2.011817
Observations (or Sum Wgts)	349

Variance Component Estimates Component Var Comp Est

Batch	0.015239
Residual	0.007245

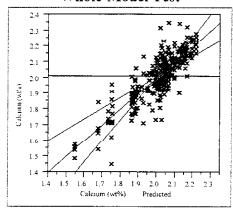
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

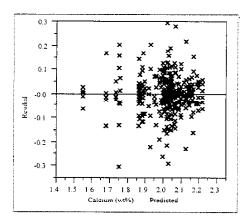
 Batch
 5.70675
 0.0878
 65
 12.1180 < .0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Katio
Model	65	5.7067480	0.087796	12.1180
Error	283	2.0503603	0.007245	Prob>F
C Total	348	7.7571083		<.0001



Response: Chromium (wt%) Summary of Fit

•	
RSquare	0.654056
Root Mean Square Error	0.007582
Mean of Response	0.161665
Observations (or Sum Wgts)	349

Variance Component Estimates Component Var Comp Est

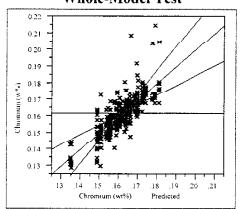
component	 Comp Lot
Batch	0.000079
Residual	0.000057

These estimates based on equating Mean Squares to Expected Value.

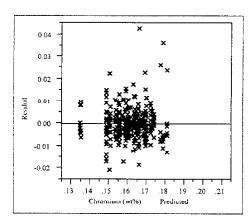
Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.03076	0.00047	65	8.2316	<.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	65	0.03075879	0.000473	8.2316
Error	283	0.01626898	0.000057	Prob>F
C Total	348	0.04702778		<.0001



Response: Copper (wt%) Summary of Fit

RSquare	0.999078
Root Mean Square Error	0.010187
Mean of Response	0.135232
Observations (or Sum Wgts)	349

Variance Component Estimates Component Var Comp Est

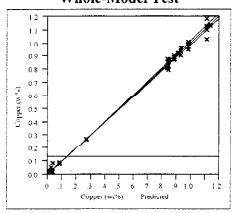
Component	var comp Est
Batch	0.092565
Residual	0.000104

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

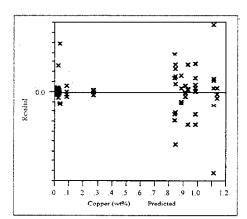
Source	SS	MS Num	DF Num	· F Ratio	Prob>F
Batch	31.8105	0.48939	65	4715.87	0.0000

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	65	31.810484	0.489392	
Error	283	0.029368	0.000104	Prob>F
C Total	348	31.839852		0.0000



Response: Iron (wt%) Summary of Fit

RSquare	0.810669
Root Mean Square Error	0.809755
Mean of Response	23.47355
Observations (or Sum Wgts)	349

Variance Component Estimates Component Var Comp Est

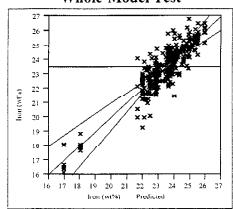
component	
Batch	2.188467
Residual	0.655703

These estimates based on equating Mean Squares to Expected Value.

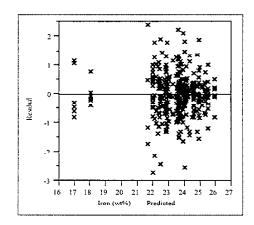
Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	794.538	12.2237	65	18.6421	<.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	65	794.53790	12.2237	18.6421
Error	283	185.56409	0.6557	Prob>F
C Total	348	980.10198		<.0001



Response: Potassium (wt%) Summary of Fit

RSquare	0.80374
Root Mean Square Error	0.008721
Mean of Response	0.039521
Observations (or Sum Wets)	349

Variance Component Estimates Component Var Comp Est

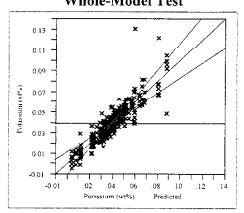
	· · · · · · · · · · · · · · · · · · ·
Batch	0.000242
Residual	0.000076

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

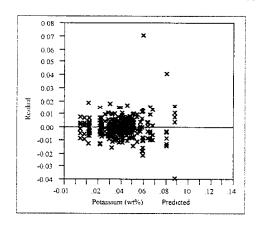
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.08815	0.00136	65	17.8303	< 0001

Whole-Model Test



Analysis of Variance

		₩		
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	65	0.08815191	0.001356	17.8303
Error	283	0.02152518	0.000076	Prob>F
C Total	348	0.10967709		< 0001



Response: Magnesium (wt%) Summary of Fit

RSquare	0.71246
Root Mean Square Error	0.062692
Mean of Response	0.945433
Observations (or Sum Wgts)	349

Variance Component Estimates Component Var Comp Est

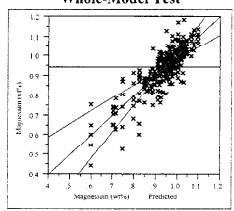
Component	var comp Est
Batch	0.007278
Residual	0.00393

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	2.75593	0.0424	65	10.7879	<.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	65	2.7559287	0.042399	10.7879
Error	283	1.1122590	0.003930	Prob>F
C Total	348	3.8681877		<.0001

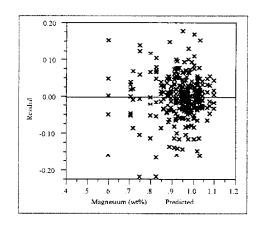


Exhibit 14: Random Effects Study for SRAT Product by Analyte

Response: Manganese (wt%) Summary of Fit

RSquare	0.853185
Root Mean Square Error	0.075014
Mean of Response	2.449582
Observations (or Sum Wots)	349

Variance Component Estimates Component Var Comp Est

Component	, 50 mp 250
Batch	0.02587
Residual	0.005627

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	9.25437	0.14237	65	25.3014	<.0001

Response: Sodium (wt%) Summary of Fit

RSquare	0.860009
Root Mean Square Error	0.470886
Mean of Response	7.16796
Observations (or Sum Wgts)	349

Variance Component Estimates Component Var Comp Est

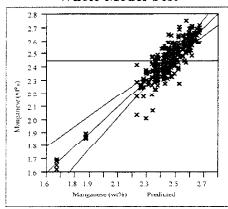
Component	var Comp Est
Batch	1.080043
Residual	0.221734

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

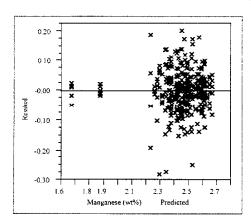
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	385.496	5.9307	65	26.7470	<.0001

Whole-Model Test

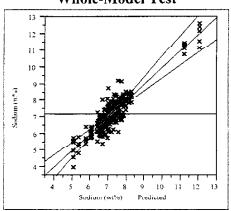


Analysis of Variance

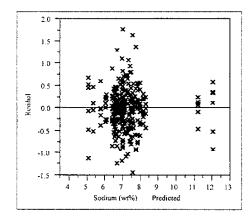
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	65	9.254374	0.142375	25.3014
Error	283	1.592483	0.005627	Prob>F
C Total	348	10.846857		<.0001



Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	65	385.49575	5.93070	26.7470
Error	283	62.75059	0.22173	Prob>F
C Total	348	448,24634		<.0001



Response: Nickel (wt%) Summary of Fit

RSquare	0.598769
Root Mean Square Error	0.017243
Mean of Response	0.26796
Observations (or Sum Wets)	349

Variance Component Estimates Component Var Comp Est

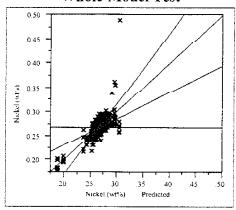
	1
Batch	0.000309
Residual	0.000297

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

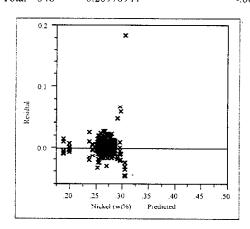
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.12557	0.00193	65	6.4974	< 0001

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	65	0.12556756	0.001932	
Error	283	0.08414188	0.000297	
C Total	348	0.20970944	0.000=,,	< 0001



Response: Silicon (wt%) Summary of Fit

RSquare	0.603223
Root Mean Square Error	0.127012
Mean of Response	0.711444
Observations (or Sum Wgts)	349

Variance Component Estimates Component Var Comp Est

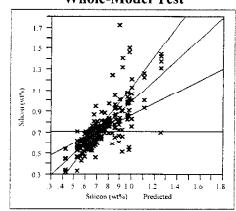
Component	vai Comp Est
Batch	0.017149
Residual	0.016132

These estimates based on equating Mean Squares to Expected Value.

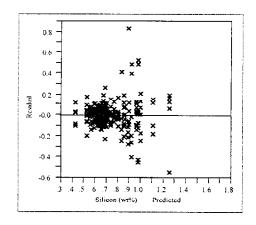
Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	6.94081	0.10678	65	6.6192	<.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	65	6.940815	0.106782	6.6192
Error	283	4.565402	0.016132	Prob>F
C Total	348	11.506216		<.0001



Response: Titanium (wt%) Summary of Fit

RSquare	0.812203
Root Mean Square Error	0.007657
Mean of Response	0.01888
Observations (or Sum Wets)	349

Variance Component Estimates Component Var Comp Est

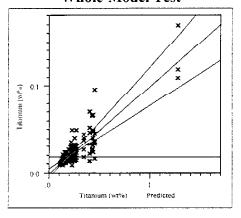
Batch	0.000198
Residual	0.000059

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

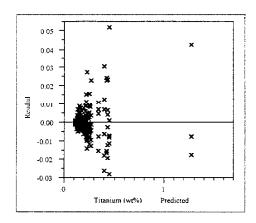
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.07176	0.0011	65	18.8299	< .0001

Whole-Model Test



Analysis of Variance

		•		
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	65	0.07175565	0.001104	18.8299
Error	283	0.01659130	0.000059	Prob>F
C Total	348	0.08834695		<.0001



Response: Uranium (wt%) Summary of Fit

RSquare	0.797285
Root Mean Square Error	0.094388
Mean of Response	2.647381
Observations (or Sum Wgts)	349

Variance Component Estimates Component Var Comp Est

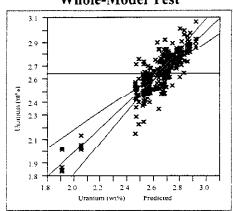
Component	var comp 250
Batch	0.027176
Residual	0.008909

These estimates based on equating Mean Squares to Expected Value.

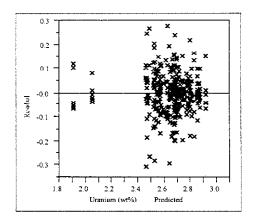
Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	9.91621	0.15256	65	17.1238	<.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	65	9.916211	0.152557	
Error	283	2.521264	0.008909	Prob>F
C Total	348	12.437474		<.0001



Response: Zirconium (wt%) Summary of Fit

RSquare	0.790974
Root Mean Square Error	0.00676
Mean of Response	0.016771
Observations (or Sum Wgts)	349

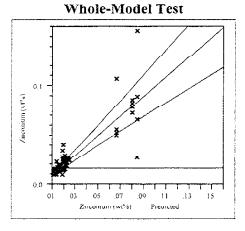
Variance Component Estimates Component Var Comp Est

Batch	0.000134
Residual	0.000046

These estimates based on equating Mean Squares to Expected Value.

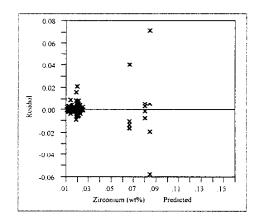
Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.04893	0.00075	65	16.4753	<.0001



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	65	0.04893095	0.000753	16.4753
Error	283	0.01293072	0.000046	Prob>F
C Total	348	0.06186166		<.0001



Response: Fe/Al Summary of Fit

RSquare	0.694407
Root Mean Square Error	0.088482
Mean of Response	3.78092
Observations (or Sum Wgts)	349

Variance Component Estimates Component Var Comp Est

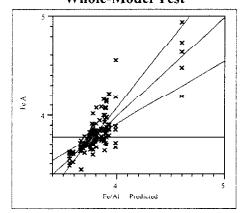
Batch	0.013172
Residual	0.007829

These estimates based on equating Mean Squares to Expected Value.

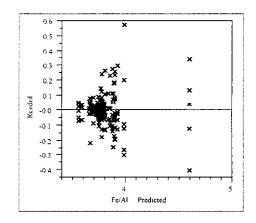
Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	5.0346	0.07746	65	9.8933	<.0001

Whole-Model Test



Source	DΓ	Sum of Squares	Mean Square	Γ Ratio
Model	65	5.0345986	0.077455	9.8933
Error	283	2.2156195	0.007829	Prob>F
C Total	348	7.2502181		<.0001



WSRC-RP-2000-00174 Revision 0 Exhibit 14: Random Effects Study for SRAT Product by Analyte

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Response: Total Solids (wt%) Summary of Fit

RSquare	0.876352
Root Mean Square Error	1.112606
Mean of Response	48.82135
Observations (or Sum Wgts)	297

Variance Component Estimates Component Var Comp Est

Batch	6.442512
Residual	1.237893

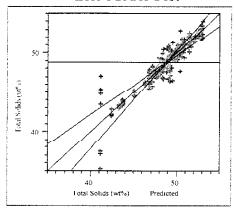
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

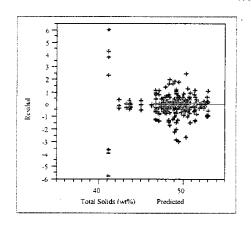
 Batch
 1974.05
 27.8035
 71
 22.4604
 <.0001</td>

Whole-Model Test



Analysis of Variance

in any one or it at taken to				
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	71	1974.0498	27.8035	22.4604
Error	225	278.5259	1.2379	Prob>F
C Total	296	2252,5757		< 0001



Response: Calcined Solids (wt%) Summary of Fit

RSquare	0.838115
Root Mean Square Error	1.24286
Mean of Response	43.09811
Observations (or Sum Wets)	297

Variance Component Estimates Component Var Comp Est

1 1	· · · · · · · · · · · · · · · · · · ·
Batch	5.771507
Residual	1.544701

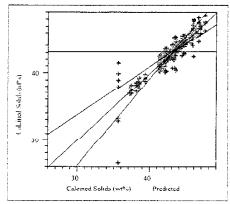
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

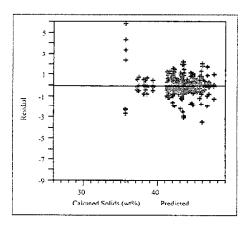
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 1799.38
 25.3434
 71
 16.4067
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	71	1799.3845	25.3434	16.4067
Error	225	347.5576	1.5447	Prob>F
C Total	296	2146.9421		<.0001



Response: Insoluble Solids (wt%) Summary of Fit

RSquare	0.934941
Root Mean Square Error	0.752659
Mean of Response	40.76357
Observations (or Sum Wets)	56

Variance Component Estimates Component Var Comp Est

Batch	6.433689
Residual	0.566495

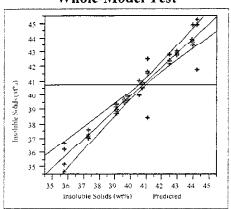
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

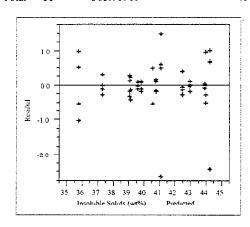
 Batch
 341.916
 26.3013
 13
 46.4280
 <.0001</td>

Whole-Model Test



Analysis of Variance

2 *************************************				
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	13	341.91629	26.3013	46.4280
Error	42	23.79280	0.5665	Prob>F
C Total	55	365.70909		<.0001



Response: Density (g/mL) Summary of Fit

RSquare	0.872605
Root Mean Square Error	0.018226
Mean of Response	1.414685
Observations (or Sum Wgts)	298

Variance Component Estimates Component Var Comp Est

Component	· mr comp Est
Batch	0.001671
Residual	0.000332

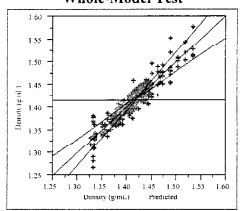
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

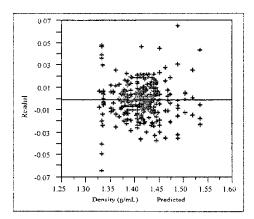
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 0.51425
 0.00724
 71
 21.8030
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	71	0.51425085	0.007243	21.8030
Error	226	0.07507750	0.000332	Prob>F
C Total	297	0.58932835		<.0001



Response: Formate (ppm) Summary of Fit

RSquare	0.871203
Root Mean Square Error	2166.301
Mean of Response	32735.19
Observations (or Sum Wgts)	324

Variance Component Estimates Component Var Comp Est

•	
Batch	23544805
Residual	4692860

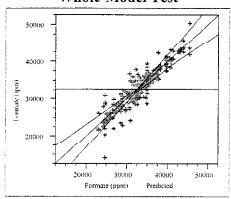
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

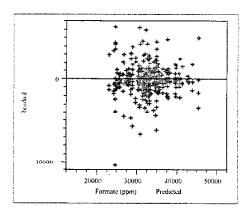
 Batch
 7.872e9
 1.05e+8
 75
 22.3669
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	75	7872349722	1.0496e8	22.3669
Error	248	1163829167	4692860	Prob>F
C Total	323	9036178889		<.0001



Response: Chloride (ppm) Summary of Fit

RSquare	0.486327
Root Mean Square Error	677.8373
Mean of Response	1159.614
Observations (or Sum Wgts)	324

Variance Component Estimates Component Var Comp Est

1	- I - I
Batch	229866.8
Residual	459463.4

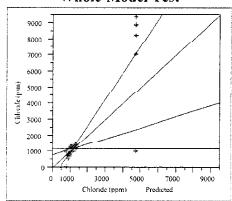
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 1.079e8
 1438412
 75
 3.1306
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	75	107880907	1438412	3.1306
Error	248	113946936	459463	Prob>F
C Total	323	221827843		<.0001

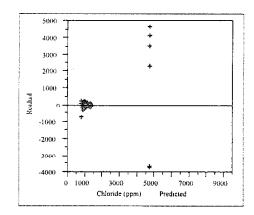


Exhibit 15: Random Effects Study for SME by Anion

Response: Fluoride (ppm) Summary of Fit

RSquare	0.485941
Root Mean Square Error	678.1098
Mean of Response	1160.75
Observations (or Sum Wgts)	324

Variance Component Estimates Component Var Comp Est

- + F	
Batch	229529.6
Residual	459832.9

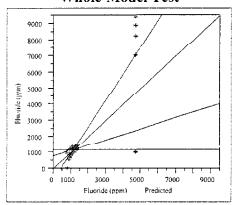
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

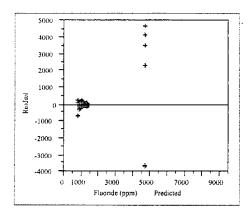
 Batch
 1.078e8
 1437346
 75
 3.1258
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source		Sum of Squares	Mean Square	
Model	75	107800917	1437346	3.1258
Error	248	114038568	459833	Prob>F
C Total	323	221839485		<.0001



Response: Nitrate (ppm) Summary of Fit

RSquare	0.878834
Root Mean Square Error	1748.168
Mean of Response	25244.14
Observations (or Sum Wgts)	324

Variance Component Estimates Component Var Comp Est

Component	var comp Est
Batch	16493110
Residual	3056090

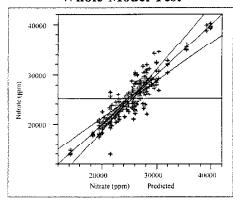
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 5.497e9
 7.33e+7
 75
 23.9837
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	75	549/228441	/32963/9	23.983/
Error	248	757910417	3056090	Prob>F
C Total	323	6255138858		<.0001

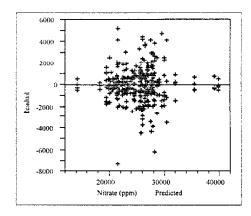


Exhibit 15: Random Effects Study for SME by Anion Response: Nitrite (ppm)

Summary of Fit

RSquare	0.486327
Root Mean Square Error	677.8373
Mean of Response	1159.614
Observations (or Sum Wgts)	324

Variance Component Estimates

Component	Var Comp Est
Batch	229866.8
Residual	459463.4

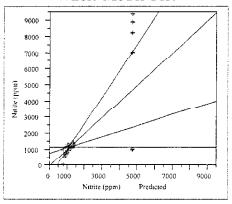
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

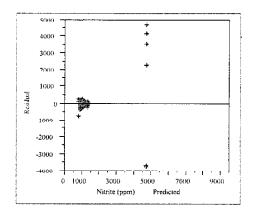
 Batch
 1.079e8
 1438412
 75
 3.1306
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	75	107880907	1438412	3.1306
Error	248	113946936	459463 I	Prob>F
C Total	323	221827843		<.0001



Response: Phosphate (ppm) Summary of Fit

RSquare	0.54196
Root Mean Square Error	705.6939
Mean of Response	1358.256
Observations (or Sum Wgts)	324

Variance Component Estimates Component Var Comp Est

-	-
Batch	340577.3
Residual	498003.9

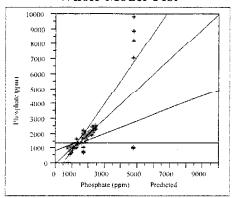
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

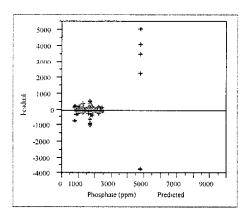
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 1.461e8
 1948443
 75
 3.9125
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	75	146133196	1948443	3.9125
Error	248	123504956	498004	Prob>F
C Total	323	269638152		<.0001



Response: Sulfate (ppm) Summary of Fit

RSquare	0.487503
Root Mean Square Error	678.2695
Mean of Response	1205.448
Observations (or Sum Wgts)	324

Variance Component Estimates

Component	Var Comp Est
Batch	231755.2
Residual	460049.6

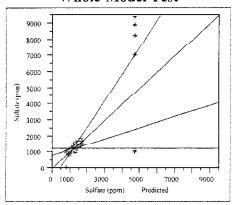
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 1.085e8
 1447041
 75
 3.1454
 <.0001</td>

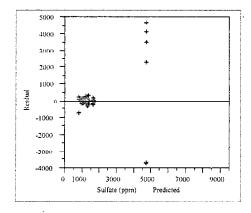
Whole-Model Test



Analysis of Variance

Source DFSum of SquaresMean SquareF Ratio

Model	75	108528054	1447041	3.1454
Error	248	114092296	460050	Prob>F
C Total	323	222620350		<.0001



Response: Aluminum (wt%) Summary of Fit

RSquare	0.508153
Root Mean Square Error	0.168259
Mean of Response	2.452694
Observations (or Sum Wgts)	291

Variance Component Estimates Component Var Comp Est

	I
Batch	0.019861
Residual	0.028311

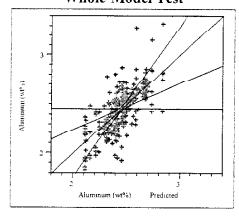
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

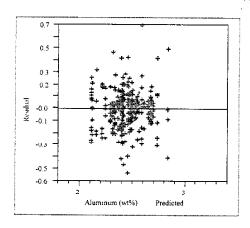
 Batch
 7.04919
 0.14386
 49
 5.0814
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	49	7.049195	0.143861	5.0814
Error	241	6.823007	0.028311	Prob>F
C Total	290	13.872202		<.0001



Response: Boron (wt%) Summary of Fit

RSquare	0.39372
Root Mean Square Error	0.147044
Mean of Response	2.645247
Observations (or Sum Wgts)	396

Variance Component Estimates Component Var Comp Est

Component	, 41	Complese
Batch		0.007815
Residual		0.021622

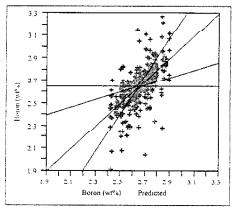
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

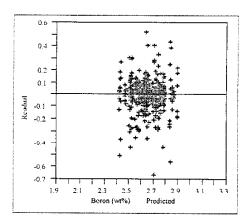
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 4.56342
 0.06519
 70
 3.0151
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	70	4.563415	0.065192	3.0151
Error	325	7.027099	0.021622	Prob>F
C Total	3 <i>95</i>	11.590514		<.0001



Response: Calcium (wt%) Summary of Fit

RSquare	0.64744
Root Mean Square Error	0.084267
Mean of Response	0.823467
Observations (or Sum Wgts)	291

Variance Component Estimates Component Var Comp Est

	· = /
Batch	0.009803
Residual	0.007101

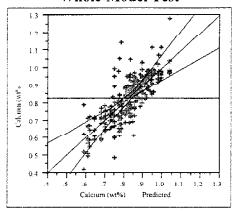
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

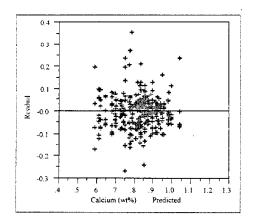
 Batch
 3.14266
 0.06414
 49
 9.0321
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares		F Ratio
Model	49	3.1426627	0.064136	9.0321
Error	241	1.7113238	0.007101	Prob>F
C Total	290	4.8539864		<.0001



Response: Chromium (wt%) Summary of Fit

~	
RSquare	0.698584
Root Mean Square Error	0.01541
Mean of Response	0.07421
Observations (or Sum Wgts)	291

Variance Component Estimates

Component	Var Comp Est
Batch	0.000424
Residual	0.000237

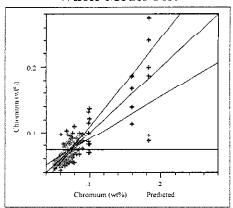
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

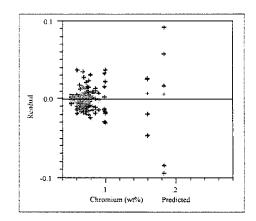
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 0.13264
 0.00271
 49
 11.3992
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	49	0.13264308	0.002707	11.3992
Error	241	0.05723113	0.000237	Prob>F
C Total	290	0.18987421		<.0001



Response: Copper (wt%) Summary of Fit

RSquare	0.51593
Root Mean Square Error	0.004266
Mean of Response	0.01346
Observations (or Sum Wgts)	291

Variance Component Estimates Component Var Comp Est

A	
Batch	0.000013
Residual	0.000018

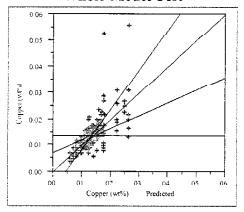
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

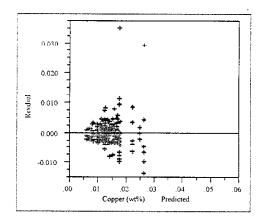
 Batch
 0.00467
 0.0001
 49
 5.2421
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	49	0.00467448	0.000095	5.2421
Error	241	0.00438582	0.000018	Prob>F
C Total	290	0.00906030		<.0001



Response: Iron (wt%) Summary of Fit

RSquare	0.519779
Root Mean Square Error	0.556147
Mean of Response	8.205206
Observations (or Sum Wgts)	291

Variance Component Estimates Component Var Comp Est

Component	vai Comp Est
Batch	0.229851
Residual	0.3093

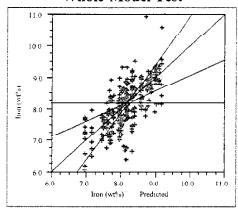
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

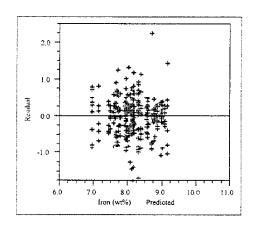
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 80.6814
 1.64656
 49
 5.3235
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	49	80.68143	1.64656	5.3235
Error	241	74.54120	0.30930	Prob>F
C Total	290	155,22264		<.0001



Response: Potassium (wt%) Summary of Fit

RSquare	0.75105
Root Mean Square Error	0.039752
Mean of Response	0.113787
Observations (or Sum Wgts)	291

Variance Component Estimates Component Var Comp Est

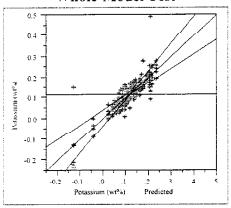
Component	,
Batch	0.003759
Kesidual	0.00158

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

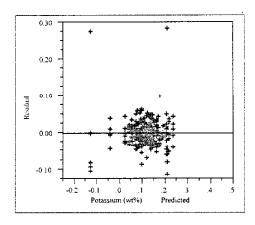
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	1.14894	0.02345	49	14.8381	<.0001

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	49	1.1489390	0.023448	14.8381
Error	241	0.3808378	0.001580	Prob>F
C Total	290	1.5297768		< 0001



Response: Lithium (wt%) Summary of Fit

0.299168
0.088108
1.620354
291

Variance Component Estimates Component Var Comp Est

Component	vai Comp Esi
Batch	0.001467
Residual	0.007763

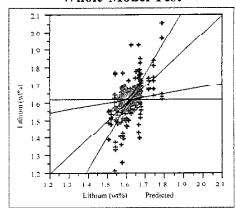
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

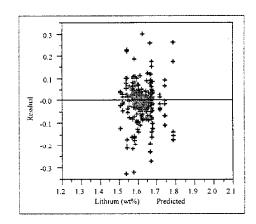
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 0.79864
 0.0163
 49
 2.0995
 0.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	49	0.7986440	0.016299	2.0995
Error	241	1.8709066	0.007763	Prob>F
C Total	200	2.6695505		0.0001



Response: Magnesium (wt%) Summary of Fit

RSquare	0.450908
Root Mean Square Error	0.065718
Mean of Response	1.253945
Observations (or Sum Wgts)	291

Variance Component Estimates Component Var Comp Est

	L L
Batch	0.002256
Residual	0.004319

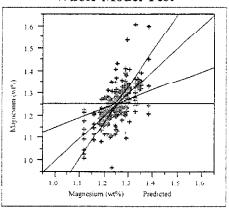
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

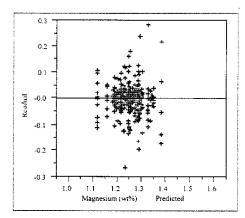
 Batch
 0.85474
 0.01744
 49
 4.0389
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	49	0.8547422	0.017444	4.0389
Error	241	1.0408589	0.004319	Prob>F
C Total	290	1.8956011		<.0001



Response: Manganese (wt%) Summary of Fit

RSquare	0.616109
Root Mean Square Error	0.062832
Mean of Response	0.829694
Observations (or Sum Wgts)	291

Variance Component Estimates Component Var Comp Est

Batch	0.004678
Residual	0.003948

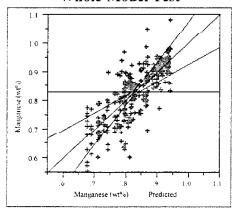
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

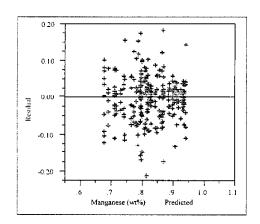
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 1.52695
 0.03116
 49
 7.8935
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	49	1.5269544	0.031162	7.8935
Error	241	0.9514293	0.003948	Prob>F
C Total	220	2.4783838		< 0001



Response: Nickel (wt%) Summary of Fit

RSquare	0.450566
Root Mean Square Error	0.012523
Mean of Response	0.103031
Observations (or Sum Wgts)	291

Variance Component Estimates Component Var Comp Est

Component	vai Comp Est
Batch	0.000082
Residual	0.000157

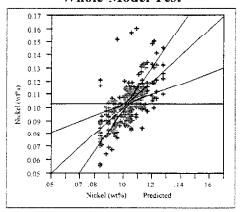
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

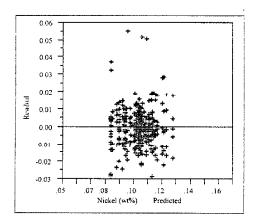
 Batch
 0.03099
 0.00063
 49
 4.0333
 <.0001</td>

Whole-Model Test



Analysis of Variance

illuly 515 Of Variance				
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	49	0.03099385	0.000633	4.0333
Error	241	0.03779487	0.000157	Prob>F
C Total	290	0.06878872		<.0001



Response: Silicon (wt%) Summary of Fit

RSquare	0.359443
Root Mean Square Error	1.262315
Mean of Response	24.52288
Observations (or Sum Wgts)	291

Variance Component Estimates Component Var Comp Est

Component	vai Comp Est
Batch	0.482006
Residual	1.593438

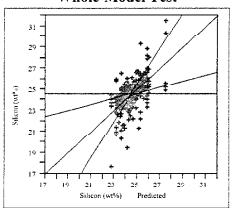
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

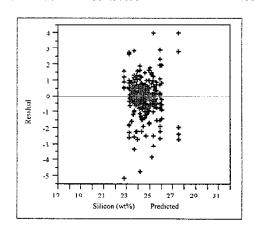
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 215.488
 4.39772
 49
 2.7599
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	49	215.48841	4.39772	2.7599
Error	241	384.01854	1.59344	Prob>F
C Total	200	599 50695		< 0001



Response: Titanium (wt%) Summary of Fit

RSquare	0.351959
Root Mean Square Error	0.008266
Mean of Response	0.020048
Observations (or Sum Wgts)	291

Variance Component Estimates Component Var Comp Est

I	
Batch	0.00002
Residual	0.000068

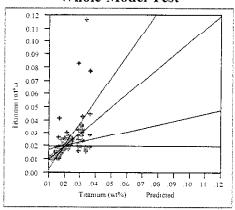
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

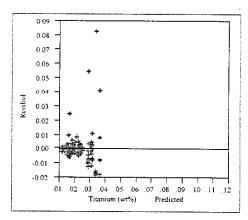
 Batch
 0.00894
 0.00018
 49
 2.6712
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	49	0.00894233	0.000182	2.6712
Error	241	0.01646500	0.000068	Prob>F
C Total	290	0.02540733		<.0001



Response: Fe/Li Summary of Fit

RSquare	0.591548
Root Mean Square Error	0.333371
Mean of Response	5.076177
Observations (or Sum Wgts)	291

Variance Component Estimates Component Var Comp Est

Batch	0.116966
Residual	0.111136

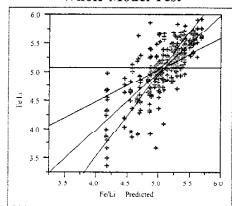
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

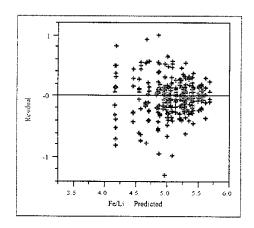
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 38.7902
 0.79164
 49
 7.1231
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	49	38.790164	0.791636	7.1231
Error	241	26.783880	0.111136	Prob>F
C Total	290	65.574044		<.0001



Response: Fe/Al Summary of Fit

RSquare	0.696765
Root Mean Square Error	0.076233
Mean of Response	3.347665
Observations (or Sum Wgts)	291

Variance Component Estimates Component Var Comp Est

Component	var Comp Est
Batch	0.01029
Residual	0.005812

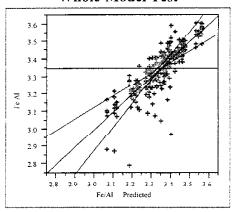
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

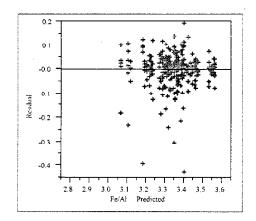
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 3.2182
 0.06568
 49
 11.3013
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	49	3.2181994	0.065678	11.3013
Error	241	1.4005740	0.005812	Prob>F
C Total	290	4.6187734		<.0001



Response: Aluminum (wt%) Summary of Fit

RSquare	0.594097
Root Mean Square Error	0.144757
Mean of Response	2.45187
Observations (or Sum Wgts)	424

Variance Component Estimates Component Var Comp Est

Batch	0.022025
Residual	0.020955

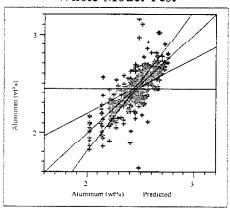
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

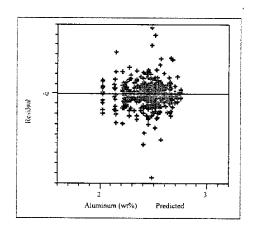
 Batch
 10.7345
 0.14705
 73
 7.0175
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DΓ	Sum of Squares	Mean Square	F Ratio
Model	73	10.734486	0.147048	7.0175
Error	350	7.334094	0.020955	Prob>F
C Total	423	18.068580		< 0001



Response: Calcium (wt%) Summary of Fit

D Causes	0.625426
RSquare	0.625436
Root Mean Square Error	0.084108
Mean of Response	0.877323
Observations (or Sum Wgts)	424

Variance Component Estimates Component Var Comp Est

	· • • P == •
Batch	0.008657
Residual	0.007074

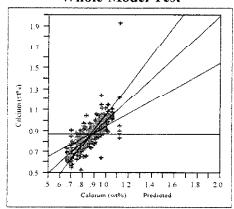
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 4.13425
 0.05663
 73
 8.0058
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	73	4.1342470	0.056634	8.0058
Error	350	2.4759337	0.007074	Prob>F
C Total	423	6.6101807		<.0001

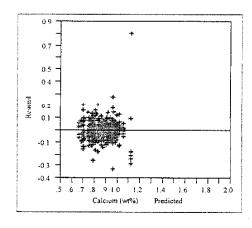


Exhibit 17: Random Effects Study for SME by Cation from MA Dissolution Method

Response: Chromium (wt%) Summary of Fit

RSquare	0.274965
Root Mean Square Error	0.021682
Mean of Response	0.069401
Observations (or Sum Wgts)	424

Variance Component Estimates Component Var Comp Est

Batch 0.000067 Residual 0.00047

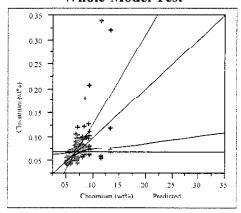
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

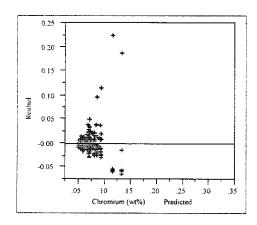
 Batch
 0.0624
 0.00085
 73
 1.8183
 0.0002

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	73	0.06240153	0.000855	1.8183
Error	350	0.16454231	0.000470	Prob>F
C Total	423	0.22694384		0.0002



Response: Copper (wt%) Summary of Fit

RSquare	0.997409
Root Mean Square Error	0.006848
Mean of Response	0.070059
Observations (or Sum Wgts)	424

Variance Component Estimates Component Var Comp Est

•	•
Batch	0.015106
Residual	0.000047

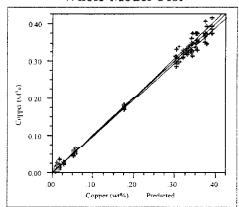
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 6.31659
 0.08653
 73
 1845.325
 0.0000

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	73	6.3165898	0.086529	1845.325
Error	350	0.0164118	0.000047	Prob>F
C Total	423	6.3330015		0.0000

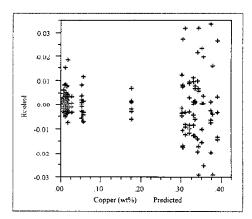


Exhibit 17: Random Effects Study for SME by Cation from MA Dissolution Method

Response: Iron (wt%) Summary of Fit

RSquare	0.539515
Root Mean Square Error	0.480534
Mean of Response	8.393351
Observations (or Sum Wets)	424

Variance Component Estimates Component Var Comp Est

Batch	0.186238
Residual	0.230913

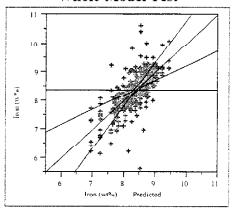
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

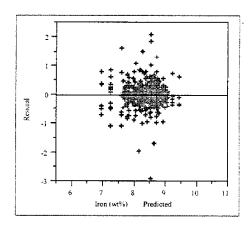
 Batch
 94.6902
 1.29713
 73
 5.6174
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	73	94.69018	1.29713	5.6174
Error	350	80.81949	0.23091	Prob>F
C Total	423	175 50967		< 0001



Response: Potassium (wt%) Summary of Fit

RSquare	0.872747
Root Mean Square Error	0.025156
Mean of Response	0.130248
Observations (or Sum Wgts)	424

Variance Component Estimates Component Var Comp Est

~ · · · · · · · · · · · · · · · · · · ·	
Batch	0.003524
Residual	0.000633

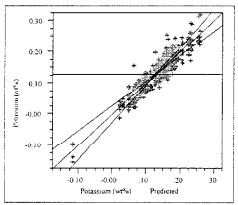
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 1.519
 0.02081
 73
 32.8824
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	73	1.5190006	0.020808	32.8824
Error	350	0.2214824	0.000633	Prob>F
C Total	423	1.7404830		<.0001

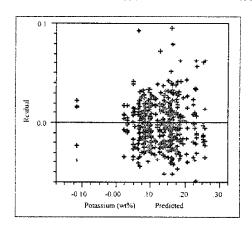


Exhibit 17: Random Effects Study for SME by Cation from MA Dissolution Method

Response: Lithium (wt%) Summary of Fit

RSquare	0.446526
Root Mean Square Error	0.062227
Mean of Response	1.6/3986
Observations (or Sum Wgts)	424

Variance Component Estimates Component Var Comp Est

Batch	0.00194
Residual	0.003872

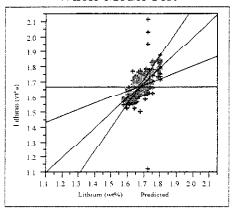
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

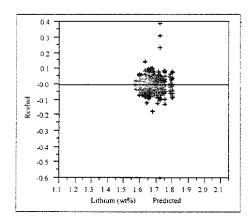
 Batch
 1.0934
 0.01498
 73
 3.8681
 <.0001</td>

Whole-Model Test



Analysis of Variance

- ,					
Source	DF	Sum of Squares	Mean Square	F Ratio	
Model	73	1.0933993	0.014978	3.8681	
Error	350	1.3552806	0.003872	Prob>F	
C Total	423	2 4486799		< 0001	



Response: Magnesium (wt%) Summary of Fit

RSquare	0.551646
Root Mean Square Error	0.056143
Mean of Response	1.275392
Observations (or Sum Wgts)	424

Variance Component Estimates Component Var Comp Est

Component	· wi comp ass
Batch	0.002697
Residual	0.003152

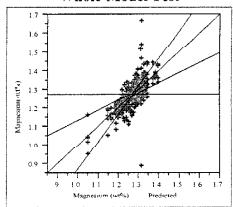
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 1.35736
 0.01859
 73
 5.8991
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	73	1.3573584	0.018594	5.8991
Error	350	1.1032026	0.003152	Prob>F
C Total	423	2.4605610		<.0001

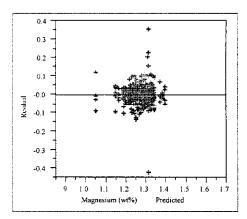


Exhibit 17: Random Effects Study for SME by Cation from MA Dissolution Method

Response: Manganese (wt%) Summary of Fit

RSquare	0.639825
Root Mean Square Error	0.05651
Mean of Response	0.849042
Observations (or Sum Wots)	424

Variance Component Estimates Component Var Comp Est

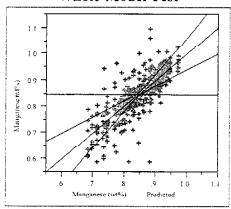
Batch	0.004193
Residual	0.003193

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

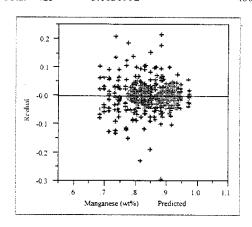
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	1.98551	0.0272	73	8.5171	<.0001

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	73	1.9855051	0.027199	8.5171
Error	350	1.1176941	0.003193	Prob>F
C Total	423	3 1031992		< 0001



Response: Sodium (wt%) Summary of Fit

RSquare	0.586534
Root Mean Square Error	0.329169
Mean of Response	8.859892
Observations (or Sum Wgts)	424

Variance Component Estimates Component Var Comp Est

I	
Batch	0.109799
Residual	0.108352

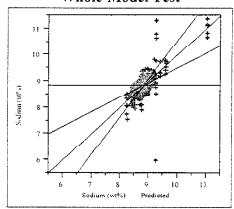
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 53.7973
 0.73695
 73
 6.8014
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	73	53.797305	0.736949	6.8014
Error	350	37.923358	0.108352	Prob>F
C Total	423	91.720663		<.0001

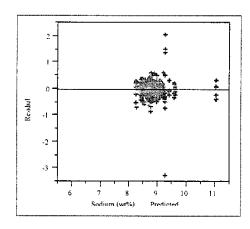


Exhibit 17: Random Effects Study for SME by Cation from MA Dissolution Method

Response: Nickel (wt%) Summary of Fit

RSquare	0.243632
Root Mean Square Error	0.042652
Mean of Response	0.105375
Observations (or Sum Wgts)	424

Variance Component Estimates Component Var Comp Est

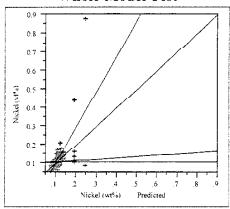
1	1
Batch	0.000173
Residual	0.001819

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

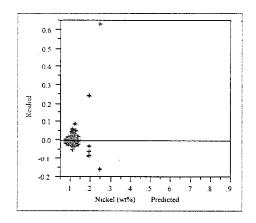
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.20509	0.00281	73	1.5443	0.0056

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	73	0.20509139	0.002809	1.5443
Error	350	0.63671798	0.001819	Prob>F
C Total	423	0.84180938		0.0056



Response: Silicon (wt%) Summary of Fit

0.359626
1.134884
22.88123
424

Variance Component Estimates Component Var Comp Est

Component	var Comp Est
Batch	0.380773
Residual	1.287962

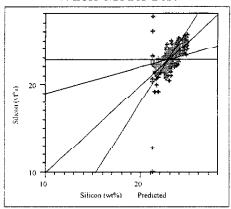
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

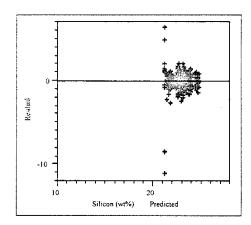
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 253.156
 3.46789
 73
 2.6925
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	73	253.15570	3.46789	2.6925
Error	350	450.78680	1.28796	Prob>F
C Total	423	703.94250		<.0001



Response: Titanium (wt%) Summary of Fit

RSquare	0.227526
Root Mean Square Error	0.038109
Mean of Response	0.025748
Observations (or Sum Wgts)	424

Variance Component Estimates Component Var Comp Est

Batch	0.000105
Residual	0.001452

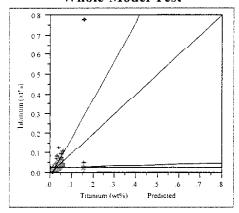
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

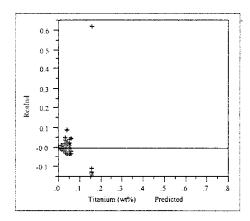
 Batch
 0.14971
 0.00205
 73
 1.4122
 0.0225

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	73	0.14971352	0.002051	1.4122
Error	350	0.50829248	0.001452	Prob>F
C Total	423	0.65800600		0.0225



Response: Uranium (wt%) Summary of Fit

RSquare	0.816597
Root Mean Square Error	0.08506
Mean of Response	1.112059
Observations (or Sum Wgts)	424

Variance Component Estimates Component Var Comp Est

	· · · · · · · · · · · · · · · · · · ·
Batch	0.025715
Residual	0.007235

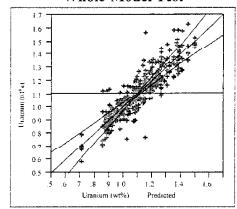
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 11.2751
 0.15445
 73
 21.3475
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	73	11.275085	0.154453	21.3475
Error	350	2.532318	0.007235	Prob>F
C Total	423	13.807404		<.0001

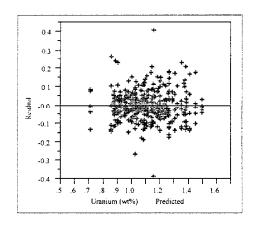


Exhibit 17: Random Effects Study for SME by Cation from MA Dissolution Method

Response: Zirconium (wt%) Summary of Fit

RSquare	0.975409
Root Mean Square Error	0.004393
Mean of Response	0.042587
Observations (or Sum Wgts)	424

Variance Component Estimates Component Var Comp Est

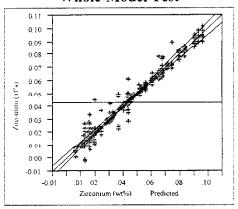
Batch	0.000638
Residual	0.000019

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

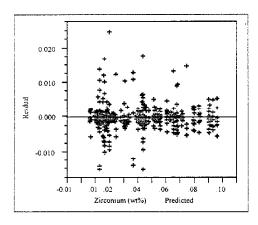
Source	SS	MS Num	DF Num	F Ratio Prob>F
Batch	0.26796	0.00367	73	190.1731 < .0001

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	73	0.26795916	0.003671	190.1731
Error	350	0.00675561	0.000019	Prob>F
C Total	423	0.27471477		<.0001



Response: Fe/Li Summary of Fit

RSquare	0.622096
Root Mean Square Error	0.32035
Mean of Response	5.027451
Observations (or Sum Wgts)	424

Variance Component Estimates Component Var Comp Est

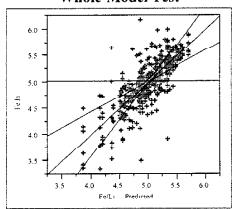
Component	·
Batch	0.123555
Residual	0.102624

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	59.1281	0.80997	73	7.8926	<.0001

Whole-Model Test



	Source	DF	Sum of Squares	Mean Square	F Ratio
	Model	73	59.128092	0.809974	7.8926
	Error	350	35.918522	0.102624	Prob>F
	C Total	423	95 046613		< 0001

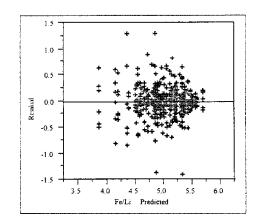


Exhibit 17: Random Effects Study for SME by Cation from MA Dissolution Method

Response: Fe/Al Summary of Fit

RSquare	0.694769
Root Mean Square Error	0.097551
Mean of Response	3.428974
Observations (or Sum Wgts)	424

Variance Component Estimates

Сошронент	var Comp Est
Batch	0.016478
Residual	0.009516

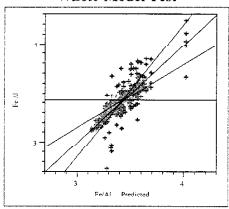
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

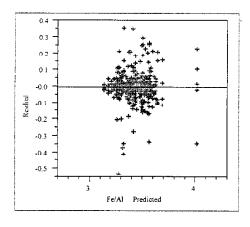
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 7.58126
 0.10385
 73
 10.9133
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	73	7.581262	0.103853	10.9133
Error	350	3.330659	0.009516	Prob>F
C Total	423	10.911921		<.0001



Response: Insoluble Solids (wt%) Summary of Fit

RSquare	0.21648
Root Mean Square Error	6.417342
Mean of Response	39.23875
Observations (or Sum Wgts)	32

Variance Component Estimates Component Var Comp Est

Batch	-0.54274
Residual	41.18227

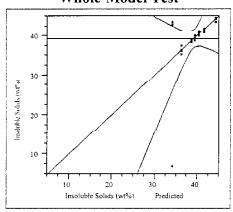
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

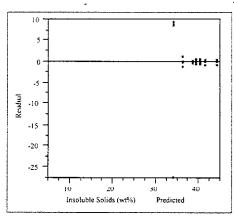
 Batch
 273.079
 39.0113
 7
 0.9473
 0.4899

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	7	273.0792	39.0113	0.9473
Error	24	988.3745	41.1823	Prob>F
C Total	31	1261.4537		0.4899



Response: Formate (ppm) Summary of Fit

RSquare	0.968743
Root Mean Square Error	1391.28
Mean of Response	30804.34
Observations (or Sum Wgts)	144

Variance Component Estimates Component Var Comp Est

201111	
Batch	29898662
Residual	1935659

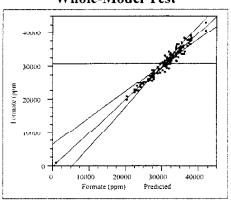
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

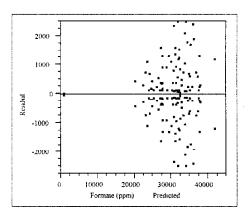
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 4.379e9
 6.256e7
 70
 32.3215
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	70	4379445100	62563501	32.3215
Еггог	73	141303112	1935659	Prob>F
C Total	143	4520748212		<.0001



Response: Chloride (ppm) Summary of Fit

RSquare	0.998624
Root Mean Square Error	185.2788
Mean of Response	1518.021
Observations (or Sum Wgts)	144

Variance Component Estimates Component Var Comp Est

ovpo	 Comp Est
Batch	12797524
Residual	34328.24

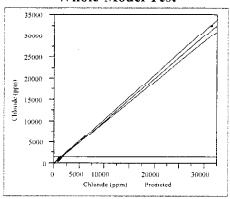
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio Prob>F

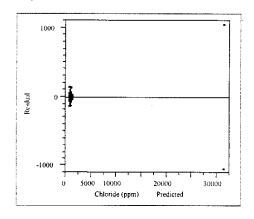
 Batch
 1.819e9
 2.598e7
 70
 756.9529 < .0001</td>

Whole-Model Test



Analysis of Variance

		, 0.0 01 .		
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	70	1818940379	25984863	756.9529
Error	73	2505961.75	34328.24	Prob>F
C Total	143	1821446341		< 0001



Response: Fluoride (ppm) Summary of Fit

RSquare	0.861403
Root Mean Square Error	65.80401
Mean of Response	1092.694
Observations (or Sum Wgts)	144

Variance Component Estimates Component Var Comp Est

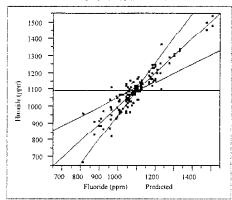
Component	vai Comp Est
Batch	11705.36
Residual	4330.168

These estimates based on equating Mean Squares to Expected Value.

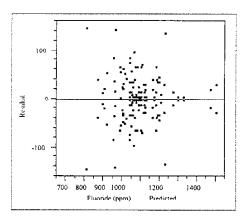
Tests wrt Random Effects

Source SS MS Num DF Num F Ratio Prob>F Batch 1964622 28066 70 6.4815 < .0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	r Ratio
Model	70	1964622.3	28066.0	6.4815
Error	73	316102.3	4330.2	Prob>F
C Total	143	2280724.6		<.0001



Response: Nitrate (ppm) Summary of Fit

RSquare	0.904087
Root Mean Square Error	1288.795
Mean of Response	24556.94
Observations (or Sum Wgts)	144

Variance Component Estimates Component Var Comp Est

Component	vai Comp Esi
Batch	7232907
Residual	1660 99 3

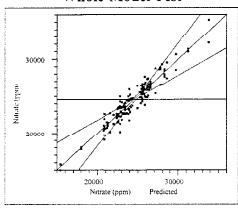
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

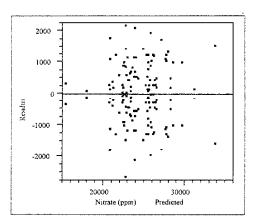
 Batch
 1.143e9
 1.633e7
 70
 9.8301
 <.0001</td>

Whole-Model Test



Analysis of Variance

Analysis of variance				
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	70	1142940556	16327722	9.8301
Error	73	121252500	1660993	Prob>F
C Total	143	1264193056		<.0001



Response: Sulfate (ppm) Summary of Fit

0.941765
69.57181
1147.583
144

Variance Component Estimates Component Var Comp Est

Component	var Comp Est
Batch	37868.8
Residual	4840.236

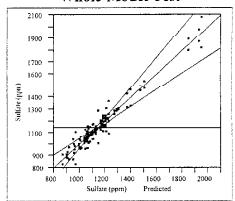
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

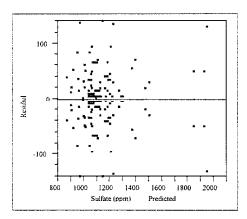
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 5714082
 81629.7
 70
 16.8648
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	70	5714081.8	81629.7	16.8648
Error	73	353337.2	4840.2	Prob>F
C Total	143	6067419.0		<.0001



Response: Aluminum (wt%) Summary of Fit

RSquare	0.510778
Root Mean Square Error	0.181292
Mean of Response	2.449732
Observations (or Sum Wgts)	306

Variance Component Estimates Component Var Comp Est

Batch 0.022772 Residual 0.032867

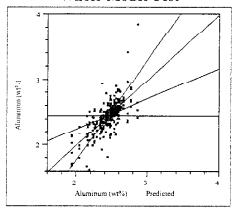
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

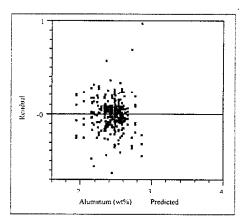
 Batch
 8.61305
 0.1595
 54
 4.8530
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	54	8.613049	0.159501	4.8530
Error	251	8.249543	0.032867	Prob>F
C Total	305	16.862592		<.0001



Response: Boron (wt%) Summary of Fit

RSquare	0.352013
Root Mean Square Error	0.167208
Mean of Response	2.668859
Observations (or Sum Wgts)	382

Variance Component Estimates Component Var Comp Est

Component	vai Comp Est
Batch	0.007464
Residual	0.027959

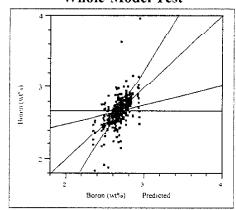
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

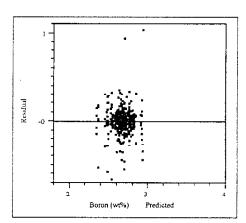
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 4.73873
 0.06868
 69
 2.4564
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	4.738726	0.068677	2.4564
Error	312	8.723061	0.027959	Prob>F
C Total	381	13.461786		<.0001



Response: Calcium (wt%) Summary of Fit

RSquare	0.630832
Root Mean Square Error	0.08519
Mean of Response	0.794614
Observations (or Sum Wgts)	306

Variance Component Estimates Component Var Comp Est

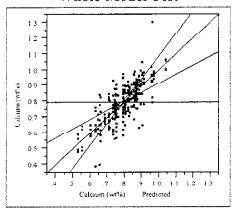
Component	,	Comp 25
Batch		0.009061
Residual		0.007257

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

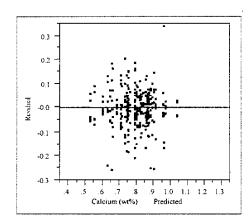
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	3.11271	0.05764	54	7.9427	<.0001

Whole-Model Test



Analysis of Variance

in in the interest of the inte				
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	54	3.1127105	0.057643	7.9427
Error	251	1.8215860	0.007257	Prob>F
C Total	305	4.9342965		<.0001



Response: Chromium (wt%) Summary of Fit

RSquare	0.649932
Root Mean Square Error	0.012132
Mean of Response	0.072771
Observations (or Sum Wgts)	306

Variance Component Estimates Component Var Comp Est

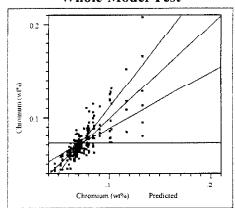
Component	var Comp Esi
Batch	0.000202
Residual	0.000147

These estimates based on equating Mean Squares to Expected Value.

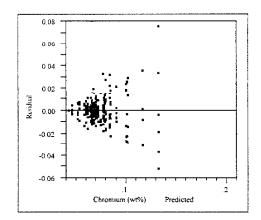
Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.06859	0.00127	54	8.6297	<.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	54	0.06858994	0.001270	8.6297
Error	251	0.03694405	0.000147	Prob>F
C Total	305	0.10553399		<.0001



Response: Copper (wt%) Summary of Fit

•	
RSquare	0.852581
Root Mean Square Error	0.009016
Mean of Response	0.01548
Observations (or Sum Wgts)	306

Variance Component Estimates Component Var Comp Est

Batch 0.000378 Residual 0.000081

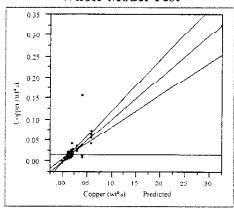
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

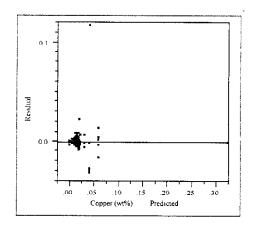
 Batch
 0.118
 0.00219
 54
 26.8820
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	54	0.11800090	0.002185	26.8820
Error	251	0.02040348	0.000081	Prob>F
C Total	305	0.13840438		< .0001



Response: Iron (wt%) Summary of Fit

RSquare	0.536781
Root Mean Square Error	0.624242
Mean of Response	8.233895
Observations (or Sum Wgts)	306

Variance Component Estimates Component Var Comp Est

Component	var Comp Est
Batch	0.307364
Residual	0.389678

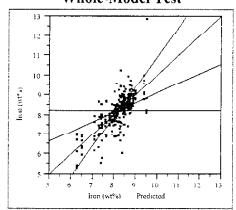
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

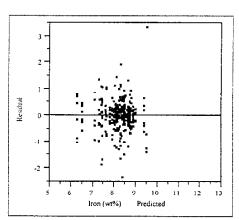
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 113.342
 2.09893
 54
 5.3863
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	54	113.34221	2.09893	5.3863
Error	251	97.80928	0.38968	Prob>F
C Total	305	211.15149		<.0001



Response: Potassium (wt%) Summary of Fit

RSquare	0.194681
Root Mean Square Error	0.165301
Mean of Response	0.131118
Observations (or Sum Wgts)	306

Variance Component Estimates Component Var Comp Est

Compositor	· · · · · · · · · · · · · · · · · · ·
Batch	0.000608
Residual	0.027325

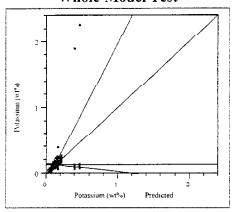
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

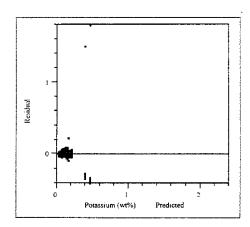
 Batch
 1.65799
 0.0307
 54
 1.1237
 0.2739

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio		
Model	54	1.6579924	0.030704	1.1237		
Error	251	6.8584613	0.027325	Prob>F		
C Total	305	8.5164538		0.2739		



Response: Lithium (wt%) Summary of Fit

RSquare	0.289054
Root Mean Square Error	0.107588
Mean of Response	1.633748
Observations (or Sum Wgts)	306

Variance Component Estimates Component Var Comp Est

Component	vai Comp Est
Batch	0.001852
Residual	0.011575

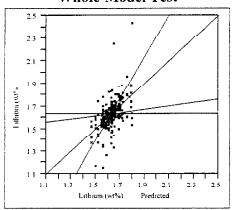
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

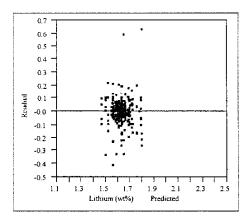
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 1.18126
 0.02188
 54
 1.8898
 0.0006

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	54	1.1812605	0.021875	1.8898
Error	251	2.9053891	0.011575	Prob>F
C Total	305	4.0866496		0.0006



Response: Magnesium (wt%) Summary of Fit

RSquare	0.309995
Root Mean Square Error	0.099327
Mean of Response	1.250141
Observations (or Sum Wgts)	306

Variance Component Estimates Component Var Comp Est

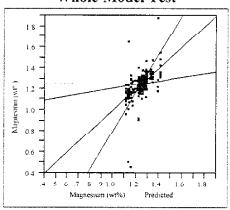
*	
Batch	0.001931
Residual	0.009866

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

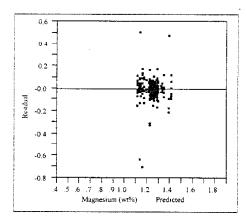
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	1.11253	0.0206	54	2.0883	<.0001

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	54	1.1125281	0.020602	2.0883
Error	251	2.4763248	0.009866	Prob>F
C Total	305	3.5888530		<.0001



Response: Manganese (wt%) Summary of Fit

RSquare	0.529869
Root Mean Square Error	0.081934
Mean of Response	0.820255
Observations (or Sum Wgts)	306

Variance Component Estimates Component Var Comp Est

Power	· · · · · · · · · · · · · · · · · · ·	-
Batch	0.00511	7
Residual	0.00671	5

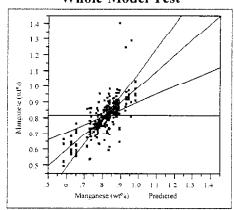
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

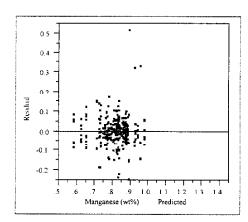
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 1.89913
 0.03517
 54
 5.2388
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	54	1.8991332	0.035169	5.2388
Error	251	1.6850230	0.006713	Prob>F
C Total	305	3.5841561		<.0001



Response: Nickel (wt%) Summary of Fit

RSquare	0.190659
Root Mean Square Error	0.055926
Mean of Response	0.105052
Observations (or Sum Wgts)	306

Variance Component Estimates Component Var Comp Est

Component	var comp zot
Batch	0.000053
Residual	0.003128

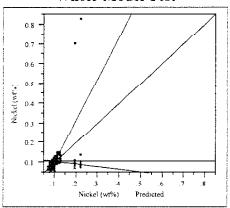
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

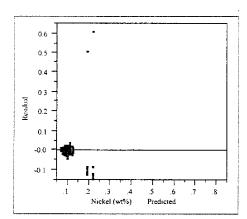
 Batch
 0.18494
 0.00342
 54
 1.0950
 0.3168

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	54	0.18493908	0.003425	1.0950
Error	251	0.78506208	0.003128	Prob>F
C Total	305	0.97000116		0.3168



Response: Silicon (wt%) Summary of Fit

RSquare	0.31817
Root Mean Square Error	1.662353
Mean of Response	24.66783
Observations (or Sum Wgts)	306

Variance Component Estimates

Component	var Comp Est
Batch	0.580915
Residual	2.763416

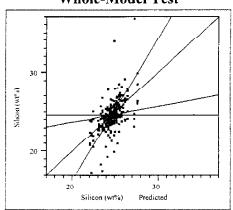
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

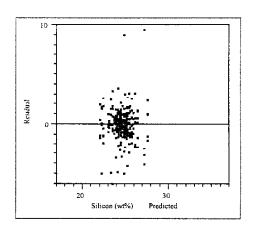
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 323.67
 5.99389
 54
 2.1690
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	54	323.6699	5.99389	2.1690
Error	251	693.6174	2.76342	Prob>F
C Total	305	1017.2873		<.0001



Response: Titanium (wt%) Summary of Fit

RSquare	0.173731
Root Mean Square Error	0.050291
Mean of Response	0.024105
Observations (or Sum Wgts)	306

Variance Component Estimates Component Var Comp Est

Batch -0.00001 Residual 0.002529

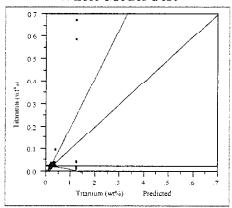
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

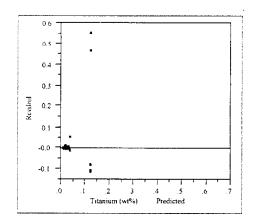
 Batch
 0.13348
 0.00247
 54
 0.9773
 0.5247

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	54	0.13347727	0.002472	0.9773
Error	251	0.63482138	0.002529	Prob>F
C Total	305	0.76829865		0.5247



Response: Fe/Li Summary of Fit

RSquare	0.59703
Root Mean Square Error	0.366973
Mean of Response	5.054695
Observations (or Sum Wgts)	306

Variance Component Estimates Component Var Comp Est

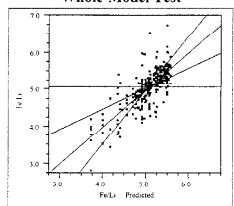
Component	vai Comp Est
Batch	0.142554
Residual	0.134669

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	50.0802	0.92741	54	6.8866	<.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	54	50.080151	0.927410	6.8866
Error	251	33.801950	0.134669	Prob>F
C Total	305	83.882101		<.0001

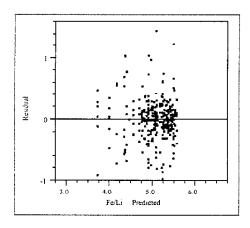


Exhibit 19: Random Effects Study for MFT by Cation from PF Dissolution Method

Response: Fe/Al Summary of Fit

RSquare	0.572785
Root Mean Square Error	0.094897
Mean of Response	3.361595
Observations (or Sum Wgts)	306

Variance Component Estimates

var Comp Est
0.008473
0.009005

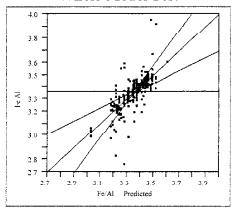
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

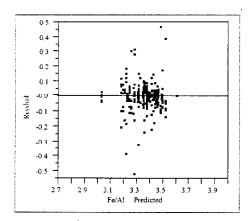
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 3.03058
 0.05612
 54
 6.2320
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	54	3.0305841	0.056122	6.2320
Error	251	2.2603762	0.009005	Prob>F
C Total	305	5.2909603		<.0001



Response: Aluminum (wt%) Summary of Fit

RSquare	0.638798
Root Mean Square Error	0.125203
Mean of Response	2.457095
Observations (or Sum Wets)	368

Variance Component Estimates Component Var Comp Est

-	•
Batch	0.0198
Residual	0.013676

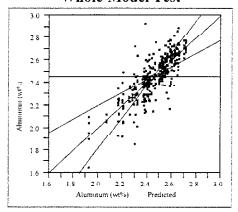
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

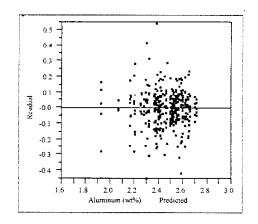
 Batch
 8.26153
 0.11973
 69
 7.6380
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	8.261527	0.119732	7.6380
Error	298	4.671394	0.015676	Prob>F
C Total	367	12.932922		<.0001



Response: Calcium (wt%) Summary of Fit

RSquare	0.64151
Root Mean Square Error	0.072726
Mean of Response	0.868302
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

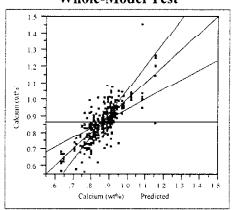
Component	vai Comp Est
Batch	0.006772
Residual	0.005289

These estimates based on equating Mean Squares to Expected Value.

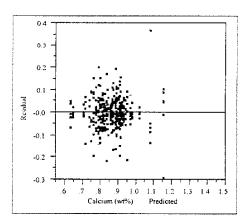
Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	2.82049	0.04088	69	7.7285	<.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	2.8204945	0.040877	7.7285
Error	298	1.5761550	0.005289	Prob>F
C Total	367	4.3966495		<.0001



Response: Chromium (wt%) Summary of Fit

RSquare	0.480233
Root Mean Square Error	0.01228
Mean of Response	0.068614
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

Batch 0.000086 Residual 0.000151

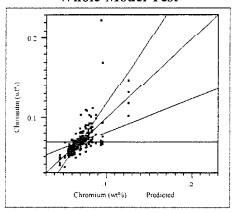
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

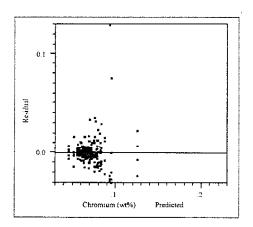
 Batch
 0.04152
 0.0006
 69
 3.9903
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	0.04151929	0.000602	3.9903
Error	298	0.04493721	0.000151	Prob>F
C Total	367	0.08645649		<.0001



Response: Copper (wt%) Summary of Fit

RSquare	0.994807
Root Mean Square Error	0.009962
Mean of Response	0.073929
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

component	, an Comp Est
Batch	0.015603
Residual	0.000099

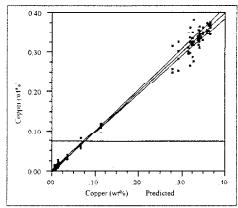
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

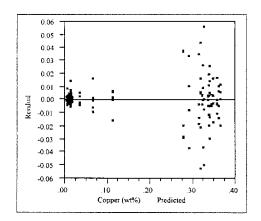
 Source
 SS
 MS Num
 DF Num
 F Ratio Prob>F

 Batch
 5.66491
 0.0821
 69
 827.3561 < .0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	5.6649071	0.082100	827.356
Error	298	0.0295711	0.000099	Prob>F
C Total	367	5.6944782		<.0001



Response: Iron (wt%) Summary of Fit

RSquare	0.675789
Root Mean Square Error	0.408587
Mean of Response	8.384696
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

Batch 0.254201 Residual 0.166943

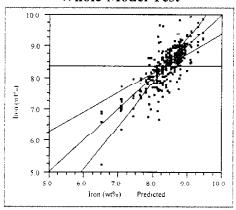
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

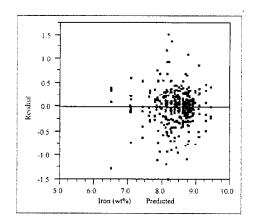
 Batch
 103.697
 1.50286
 69
 9.0022
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	103.69735		9.0022
Error	298	49.74903	0.16694	Prob>F
C Total	367	153,44638		<.0001



Response: Potassium (wt%) Summary of Fit

RSquare	0.753301
Root Mean Square Error	0.030226
Mean of Response	0.141128
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

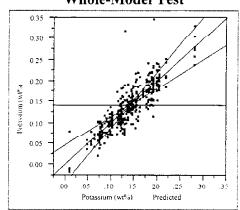
Component	7 44 4	Comp Lst
Batch		0.002119
Residual		0.000914

These estimates based on equating Mean Squares to Expected Value.

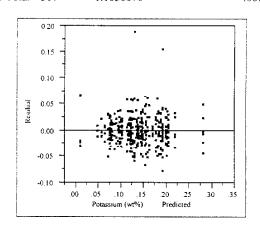
Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.83135	0.01205	69	13.1877	<.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	0.8313500	0.012049	13.1877
Error	298	0.2722590	0.000914	Prob>F
C Total	367	1.1036090		< 0001



Response: Lithium (wt%) Summary of Fit

RSquare	0.694447
KSquare Adj	0.623698
Root Mean Square Error	0.040458
Mean of Response	1.684823
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

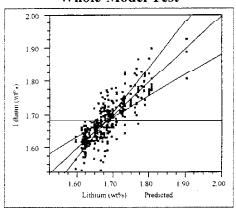
	-
Batch	0.002746
Residual	0.001637

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

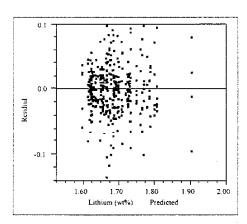
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Ratch	1.10858	0.01607	69	9.8157	<.0001

Whole-Model Test



Analysis of Variance

/ xixusy sas of variance				
Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	1.1085838	0.016066	9.8157
Error	298	0.4877717	0.001637	Prob>F
C Total	367	1.5963555		<.0001



Response: Magnesium (wt%) Summary of Fit

RSquare	0.637698
Root Mean Square Error	0.04388
Mean of Response	1.281552
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

Component	var Comp Est
Batch	0.002419
Residual	0.001925

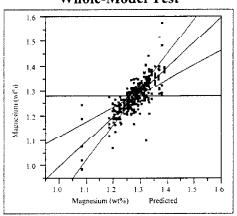
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

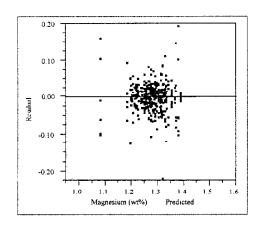
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 1.00992
 0.01464
 69
 7.6017
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	1.0099239	0.014637	7.6017
Error	298	0.5737791	0.001925	Prob>F
C Lotal	367	1.5837030		<.0001



Response: Manganese (wt%) Summary of Fit

RSquare	0.652567
Root Mean Square Error	0.035598
Mean of Response	0.835079
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

Batch 0.004183 Residual 0.003091

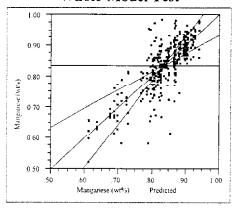
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

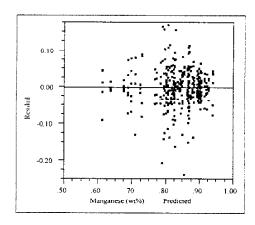
 Batch
 1.73018
 0.02508
 69
 8.1119
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	1.7301830	0.025075	8.1119
Error	298	0.9211677	0.003091	Prob>F
C Total	367	2.6513507		<.0001



Response: Sodium (wt%) Summary of Fit

RSquare	0.639623
Root Mean Square Error	0.249212
Mean of Response	8.846212
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

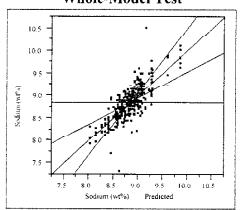
Component	var Comp Est
Batch	0.07877
Residual	0.062107

These estimates based on equating Mean Squares to Expected Value.

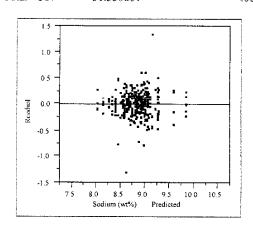
Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	32.849	0.47607	69	7.6654	<.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	32.848986	0.476072	7.6654
Error	298	18.507816	0.062107	Prob>F
C Total	367	51.356801		<.0001



Response: Nickel (wt%) Summary of Fit

RSquare	0.669147
Root Mean Square Error	0.017329
Mean of Response	0.107818
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

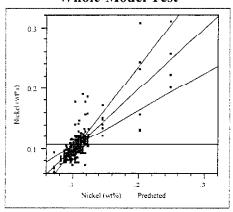
Batch 0.000442 Residual 0.0003

These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

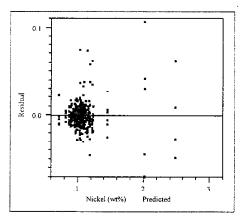
Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	0.18099	0.00262	69	8.7348	<.0001

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	0.18099273	0.002623	8.7348
Error	298	0.08949007	0.000300	Prob>F
C Total	367	0.27048280		<.0001



Response: Silicon (wt%) Summary of Fit

RSquare	0.633636
Root Mean Square Error	0.661416
Mean of Response	23.12764
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

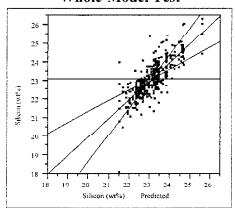
Component	var Comp Esi
Batch	0.538543
Residual	0.437472

These estimates based on equating Mean Squares to Expected Value.

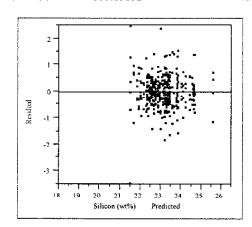
Tests wrt Random Effects

Source	SS	MS Num	DF Num	F Ratio	Prob>F
Batch	225.472	3.26771	69	7.4695	<.0001

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	225.47180	3.26771	7.4695
Error	298	130.36652	0.43747	Prob>F
C Total	367	355 83832		< 0001



Response: Titanium (wt%) Summary of Fit

RSquare	0.602765
Root Mean Square Error	0.007026
Mean of Response	0.02297
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

Batch 0.000052 Residual 0.000049

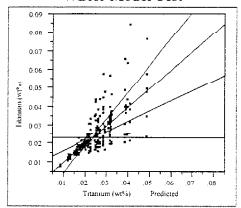
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

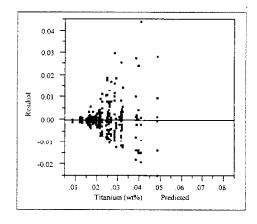
 Batch
 0.02232
 0.00032
 69
 6.5534
 < 0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	0.02232320	0.000324	6.5534
Error	298	0.01471147	0.000049	Prob>F
C Total	367	0.03703467		<.0001



Response: Uranium (wt%) Summary of Fit

RSquare	0.821613
Root Mean Square Error	0.081926
Mean of Response	1.123565
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

- · · · <u>I</u> · · · · · · · · · · · · · · · · · · ·	
Batch	0.024128
Residual	0.006712

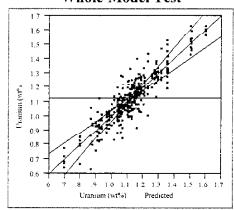
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

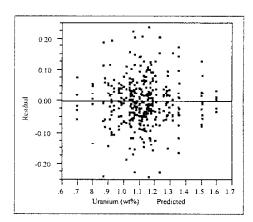
 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 9.21226
 0.13351
 69
 19.8917
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	9.212256	0.133511	19.8917
Error	298	2.000147	0.006712	Prob>F
C Total	367	11.212402		<.0001



Response: Zirconium (wt%) Summary of Fit

RSquare	0.60057
Root Mean Square Error	0.02164
Mean of Response	0.043859
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

Сошровен	vai Comp Es
Batch	0.00049
Residual	0.000468

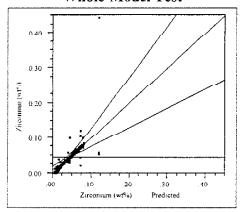
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

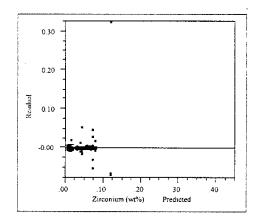
 Batch
 0.20983
 0.00304
 69
 6.4937
 <.0001</td>

Whole-Model Test



Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	0.20982765	0.003041	6.4937
Error	298	0.13955300	0.000468	Prob>F
C Total	367	0.34938065		<.0001



Response: Fe/Li Summary of Fit

0.686585
0.000000
0.307847
4.990823
368

Variance Component Estimates Component Var Comp Est

Component	vai Comp Est
Batch	0.152578
Residual	0.09477

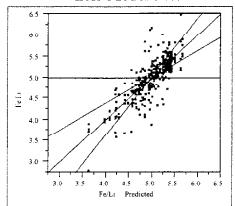
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 61.867
 0.89662
 69
 9.4611
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	61.867039	0.896624	9.4611
Егтог	298	28.241319	0.094770	Prob>F
C Total	367	90.108358		<.0001

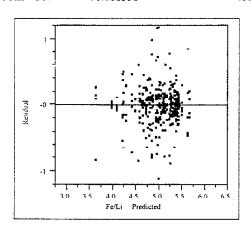


Exhibit 20: Random Effects Study for MFT by Cation from MA Dissolution Method

Response: Fe/Al Summary of Fit

RSquare	0.782142
Root Mean Square Error	0.086224
Mean of Response	3.416207
Observations (or Sum Wgts)	368

Variance Component Estimates Component Var Comp Est

Batch 0.02052 Residual 0.00/454

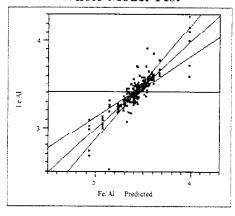
These estimates based on equating Mean Squares to Expected Value.

Tests wrt Random Effects

 Source
 SS
 MS Num
 DF Num
 F Ratio
 Prob>F

 Batch
 7.95388
 0.11527
 69
 15.5052
 <.0001</td>

Whole-Model Test



Source	DF	Sum of Squares	Mean Square	F Ratio
Model	69	7.953882	0.115274	15.5052
Error	298	2.215481	0.007434	Prob>F
C Total	367	10.169362		<.0001

