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Thermal-Fluids Analyses of Model 9977 and 9975 Shipping Packages Under Normal and Hazard Analysis Conditions

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ABSTRACT

The Model 9975 and Model 9977 Shipping Packages have been designed as replacements for the Department of Transportation (DOT) Fission Specification 6M package. Each shipping package consists of a 6-inch diameter Containment Vessel (6CV), a drum overpack filled with foam insulation, and a lid that also has several layers of insulation. While originally designed to ship Heat Source and RTG contents, the 9975 and 9977 shipping packages have been reanalyzed to significantly expand their Contents in support of additional Department of Energy (DOE) missions. The design and analysis details of the 9975 and 9977 packages are given in the Safety Analysis Report for Package (SARP).

The Model 9977 Shipping Package is evaluated to determine the decay heat wattage that can be placed inside of two 2-quart SAVY containers held inside the package containment vessel while remaining under the thermal limits set in the 9977 SARP. These analyses determine the temperatures of components of interest during normal conditions of transport (NCT) and hypothetical accident conditions (HAC). Additionally, the Model 9975 Shipping Package is evaluated to determine the maximum O-ring temperatures under HAC using 20-year and 30-year degraded fiberboard insulation material properties.

INTRODUCTION

The Model 9977 package has been designed as a replacement for the Department of Transportation (DOT) Fissile Specification 6M package. The 9977 package consists of a 6-inch diameter Containment Vessel (6CV), a drum overpack filled with foam, and a lid that has several layers of insulation [1]. Previous analyses of the 9977 shipping package have been conducted for wattage variations and storage array conditions [2,3]. The purpose of this study was to determine the maximum allowable content wattage in each of two 2-quart sized SAVY containers inside the 6CV. The analysis will evaluate both Normal Conditions of Transport (NCT) and a Hypothetical Accident Condition (HAC) of a 30-minute fully engulfing fire.

The 9975 shipping package is used to store plutonium bearing materials packaged in a DOE-STD-3013 container. The 9975 shipping package consists of a 35 gallon drum, a primary containment vessel (PCV), a secondary containment vessel (SCV), lead shielding, and fiberboard thermal insulation and has been previously analyzed for sensitivity to material variations [4]. For the K-Area Complex (KAC) at the Savannah River Site, the 9975 package is used as a storage container and has therefore been analyzed for facility accident conditions [5,6]. Recent structural and thermal accident analyses have shown that a 9975 with a 3013 container maintains containment for up to 20 years for both the 3013 container and at least one of the two 9975 containment vessels [7]. This study further evaluates the used of the 9975 package beyond 20 years.

Figure 1 is a schematic of the 9977 (left) and 9975 (right) packages. The 9977 package is shown to contain two SAVY containers. The contents will be placed within the 6CV, which is closed with a cone seal plug having a set of double O-rings and a cone seal nut. The CV is loaded into a cylindrical drum liner and held in place by upper and lower load distributor fixtures (LDF) and surrounded by a Heat Dissipation Sleeve. The packages are closed by bolting the lid in place. The design and analysis details of the 9977 package are given in the Safety Analysis Report for Packaging (SARP) [1].

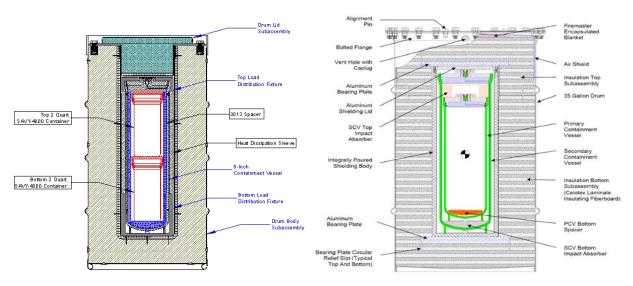


Figure 1. Left) 9977 Package with two SAVY containers, Right) 9975 Package with Primary and Secondary Containment Vessels.

DESCRIPTION OF THE WORK

9977 Model Analyses

The 9977 package with SAVY containers internal to the CV is analyzed for the 10CFR71 [8] normal conditions of transport (NCT) and hypothetical accident conditions (HAC). The internal heat source was varied from 12.5 W to 19 W per SAVY (for a total of 25-38 watts in the CV) to determine the maximum content heat load that can be placed in the 9977 package and still meet thermal requirements for shipping described in the SARP [1].

Evaluations for the suitability of shipping include analyzing the package under solar heat flux and fire conditions. In all cases, predicted component temperatures are compared to thermal limits to

ensure that the package CV does not leak. For NCT solar conditions, 10CFR71 prescribes a total heat of 800 cal/cm² for flat surfaces facing upwards and 400 cal/cm² for curved surfaces over a 12 hour period. For fire analysis, the package starts at the NCT conditions, is exposed to a 30 minute 800°C fire, and allowed to cool down post fire without artificial cooling.

The 9977 package has foam insulation between the inner drum liner and the exterior drum surface. This foam decomposes when exposed to high (fire) temperatures. The decomposition rate and heat of reaction is not well documented. Therefore, based on past engulfing fire tests of the 9977 package, it was determined that the 9977 internal contents reach a maximum of 87°F over their NCT temperatures during a fire/post fire event. For this thermal analysis, the NCT and the post-fire cooldown were modeled. The initial conditions of the post fire transient are 87°F above the NCT temperature predictions for contents located within the drum liner. The foam is assumed to char and have thermal properties of air and a temperature equal to the fire temperature, 800°C.

9975 Model Analyses

The 9975 package has been used for extended storage of nuclear materials. Periodic surveillance of the 9975 packages has show degradation of the fiberboard insulation between the drum liner and the outer drum surface. Simulations have been conducted to determine the effects of the degraded fiberboard on the thermal performance of the package.

Evaluations of the 9975 package include boundary conditions equivalent to the previously mentioned 9977 conditions. Additional modifications in the simulation include the changes to the thermal properties of the fiberboard material. The density, thermal conductivity, and heat capacity of the material are taken to be 90% and 80% of the beginning of life (BOL) values for the 20 year and 30 year degraded scenarios, respectively.

Additional inputs for both models consist of package geometry and all material thermal properties. These inputs are used in creating finite element thermal models that are used to analyze the Normal Conditions of Transport (NCT) and the Hypothetical Accident Conditions (HAC).

Table 1. Beginning of Life Fiberboard Properties

Material	Density (kg/m³)	Thermal Conductivity (W/m/K)	Heat Capacity (J/kg/K)
Pre-Fire Softwood Fiberboard (Radial)	16.598	0.05824 @ 77°F 0.05824 @ 122°F 0.05761 @ 185°F	0.3057 @ 77°F 0.3511 @ 122°F
Pre-Fire Softwood Fiberboard (Axial)	16.598	0.03253@ 77°F 0.03357 @ 122°F 0.03386 @ 185°F	0.3057 @ 77°F 0.3511 @ 122°F
During-Fire Fiberboard	15.40 @ 80°F 15.40 @ 475°F 8.5 @ 810°F 3.5 @ 1500°F	0.035 @ 80°F 0.450 @ 170°F 0.550 @ 200°F 0.090 @ 210°F 0.070 @ 500°F	0.25 @ 80°F 0.50 @ 475°F 0.50 @ 810°F 0.50 @ 1500°F

Note: The material properties for the post fire cooldown mode are equivalent to the pre-fire values. This causes the package to retain heat longer yielding conservative temperature results.

RESULTS

9977

For the 9977 package, thermal analysis show that each SAVY container can have a maximum of 15 watts (30 watts for the total 9977 package) and still remain below the thermal limits set in the SARP.

Table 2. Maximum Temperatures (F) of components during NCT for various content wattages.

	623 600	(=) =	Component	Dual 12.5 watts	Dual 15 watts	Dual 17 watts	Dual 19 watts	Limit (F)
	550		CV	271	290	306	321	300
	500		CV O-rings	259	277	290	304	400
	450		Foam	247	263	276	288	300
	350	°F	Drum	188	189	189	190	N/A
•	300		Top Contents	552	621	676	729	N/A
	250 200		Bottom Contents	506	571	622	673	N/A
· ·	162		SAVY O- rings	293	315	333	351	392

Table 3. Maximum Component Temperatures during Post Fire Cooldown with Dual 15 watt SAVYs

	2.3-Inch Un-decomposed Foam			1.0-Inch Un-decomposed Foam			All Char		
Time (hr)	CV (°F)	CV O-rings (°F)	Contents (°F)	CV (°F)	CV O-rings (°F)	Contents (°F)	CV (°F)	CV O-rings (°F)	Contents (°F)
0.0	377	377	708	377	377	708	377	377	708
0.5	410	393	754	410	393	754	411	394	754
1.0	416	405	787	417	406	787	416	404	787
1.5	422	413	798	422	412	798	419	408	798
2.0	427	417	794	425	415	794	420	409	794
2.5	430	420	785	427	416	785	421	409	785
3.0	433	422	775	428	416	775	421	408	775
3.5	434	422	767	428	416	767	420	407	766
4.0	435	422	761	428	415	760	420	406	758

4.5	435	422	755	427	413	755	419	405	752
5.0	434	421	752	426	412	750	418	404	747
5.5	434	420	749	425	411	747	417	403	743
6.0	433	419	747	423	409	744	416	402	740
7.0	431	417	745	422	408	741	415	401	737
8.0	430	416	744	421	406	739	414	400	734
9.0	429	414	742	419	405	737	413	398	732
10.0	427	413	741	418	403	736	412	397	730

9975

Simulations of the 9975 package with degraded thermal properties has shown that thermal limits as defined in the SARP are not exceed. Maximum temperatures for components on interest in the 9975 package are shown in **Table 4** below for the HAC evaluations.

Table 4. Maximum 9975 Component Temperatures during Post Fire Cooldown with Degraded Fiberboard Properties.

Component	20yr Degraded Fiberboard HAC Temperature (F)	30yr Degraded Fiberboard HAC Temperature (F)	Temperature Limit (F)
Drum Surface	1471	1471	NA
Fiberboard	1471	1471	NA
PCV	342	337	NA
PCV O-rings	321	314	400
SCV	333	331	NA
SCV O-rings	317	310	400
Lead Shield	371	425	600
Contents	568	562	NA

CONCLUSIONS

Based on the thermal analysis of a 9977 shipping package containing dual 2-quart SAVY containers a maximum wattage of 15 watts of decay heat per SAVY container (30 watts per 9977 package) ensures that all maximum temperatures remain below their respective temperature limits. Based on the temperature limits set in the 9977 SARP, the limiting conditions/component is the 300°F temperature limit of the CV under NCT conditions. For the case of 38 watts total (19 watts per SAVY), the NCT temperature of the CV reaches a temperature of 321°F, exceeding the limit of 300°F. The temperature limit of 300°F for the CV was chosen to maximize the allowed design pressure but the calculated CV temperature of 321°F is well below the melting point for stainless steel.

Based on the thermal analysis of the 9975 package using 20yr and 30yr degraded thermal properties for the fiberboard insulation, it is calculated that the maximum PCV and SCV O-Ring temperatures remain below the 400°F temperature limit.

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