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AEC RESEARCH AND DEVELOPMENT REPORT

TAFI-II, A COMPUTER CODE FOR MANAGEMENT OF RADIOACTIVE WASTE

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Waste Disposal and Processing
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**TAFI - II, A COMPUTER CODE FOR
MANAGEMENT OF RADIOACTIVE WASTE**

by

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ABSTRACT

A computer program, TAFI-II, was written in FORTRAN II to assist in the regulation and inventory control of radioactive fission products that are stored in waste tanks at the Savannah River Plant. The inventories and heat generation rates are computed for thirteen isotopes in each of twenty-four waste tanks. The program prepares a report that summarizes the data and provides an up-to-date status of the conditions in the waste tanks.

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TAFI-II, A COMPUTER CODE FOR MANAGEMENT OF RADIOACTIVE WASTE

INTRODUCTION

The chemical separations processes at the Savannah River Plant generate large volumes of aqueous waste that, because of their high fission product content and resultant gamma heat, are stored in cooled underground steel tanks until the short-lived isotopes have decayed to low levels. During this storage time the wastes separate into two layers: the sludge layer at the bottom containing about 85% of the total activity, and the liquid fraction or supernate containing the remainder of the isotopes. After the waste has decayed and separated for some time, the supernate is removed and concentrated by evaporation. The residue from the evaporation is then stored in uncooled tanks⁽¹⁾ to decay and separate further. To schedule and regulate movement of the waste, it is necessary to know the inventory of fission products and the heat generation rates in each tank. To assist in this, a computer code, TAFI-II, was written to facilitate these calculations and prepare reports at regular intervals.

DESCRIPTION OF THE WASTE TANK FARM

The waste tank farm consists of twelve tanks and one evaporator in each of the two chemical separations areas, F and H. The tanks are numbered in the order in which they were built. Tanks numbered 1-8 and 17-20 are in F Area, and 9-16 and 21-24 are in H Area. The tanks in each area are connected to the chemical separations buildings and to each other by shielded pipes through which the separations process waste is added, transferred from tank to tank, or transferred from one tank to another through the evaporator. At the present time there is no physical connection between the areas. Tanks 1-16 are cooled and receive fresh waste from the separations processes; tanks 17-24 are uncooled⁽¹⁾ and receive the evaporator bottoms.

EQUATIONS USED IN COMPUTER PROGRAM

The equations used to compute the concentrations of the 13 isotopes are described below. The 13 isotopes are: ^{89}Sr , ^{90}Sr , ^{90}Y , ^{91}Y , ^{95}Zr , ^{95}Nb , ^{106}Ru , ^{106}Rh , ^{137}Cs , ^{137}Ba , ^{144}Ce , ^{144}Pr , and ^{147}Pm . These particular isotopes are of interest in management of the waste because they (a) represent a long-term health hazard, (b) account for about 95% of the heat generation which is within the accuracy of measurements

that can be made in waste tanks, or (c) may be of interest for future recovery. In the equations below the index J is used to define the isotope as it appears in this list; e.g., $J = 4 \equiv {}^{91}\text{Y}$.

In addition to the above 13 isotopes, the waste tanks contain small quantities of alpha emitters: ${}^{238}\text{U}$, ${}^{235}\text{U}$, ${}^{239}\text{Pu}$, and ${}^{238}\text{Pu}$. Because of their long half-lives, they are treated as if they were stable, and in the intertank transfers it is assumed that they follow the sludge.

Isotopic Concentration at Reactor Discharge

Equations 1-5 are used to compute the isotopic concentrations of an addition to the tank farm system at the end of the reactor irradiation.

The concentrations of ${}^{89}\text{Sr}$, ${}^{90}\text{Sr}$, ${}^{91}\text{Y}$, ${}^{95}\text{Zr}$, ${}^{106}\text{Ru}$, ${}^{137}\text{Cs}$, ${}^{144}\text{Ce}$, and ${}^{147}\text{Pm}$ are given by

$$A_J^0 = K P Y_J (1 - e^{-a_J T}) \quad J = 1, 2, 4, 5, 7, 9, 11, 13 \quad (1)$$

The concentrations of ${}^{90}\text{Y}$, ${}^{95}\text{Nb}$, ${}^{106}\text{Rh}$, and ${}^{144}\text{Pr}$, which are daughters of ${}^{90}\text{Sr}$, ${}^{95}\text{Zr}$, ${}^{106}\text{Ru}$, and ${}^{144}\text{Ce}$, respectively, are given by

$$A_J^0 = K P Y_J \left\{ \left[\left(\frac{a_J}{a_J - a_{J-1}} \right) (1 - e^{-a_{J-1} T}) \right] - \left[\left(\frac{a_{J-1}}{a_J - a_{J-1}} \right) (1 - e^{-a_J T}) \right] \right\} \quad (2)$$

$J = 3, 6, 8, 12$

The ${}^{137}\text{Ba}$ ($J = 10$) concentration is assumed to be 92% of the ${}^{137}\text{Cs}$ concentration since 8% of the ${}^{137}\text{Cs}$ decays directly to the stable ${}^{137}\text{Ba}$ isomer. Thus

$$A_J^0 = 0.92 A_{J-1}^0 \quad J = 10 \quad (3)$$

where

A_J^0 = initial concentration for isotope J, curies/addition

$$K = \left(\frac{(3.16 \times 10^{18} \text{ fissions/sec/MW})}{(3.7 \times 10^{10} \text{ disintegrations/sec/curie})} \right) = 0.85 \times 10^8 \text{ curies/MW}$$

Y_J = fractional yield, atoms/fission

$$a_J = 0.693/\text{half-life, days}^{-1}$$

T = irradiation, days

For processing of highly enriched fuel the value of P in Equations 1 and 2 is expressed in terms of the ^{235}U burnup per tube as follows:

$$P = \left[\frac{^{235}\text{U burnup, grams/tube}}{1.245 \text{ grams } ^{235}\text{U/MWD}} \right] \left[\frac{\text{No. tubes/addition}}{T, \text{ days}} \right], \text{ MW/addition} \quad (4)$$

whereas for processing of natural uranium fuel, P is expressed by

$$P = (\text{Megawatts/Ton of U})(\text{Tons of U/addition}) \quad (5)$$

Effect of Radioactive Decay

These equations are used to compute the effect of radioactive decay of the isotopes while they are in the reactor, from time-of-discharge until they are added to the waste tanks, and after they are in the waste system until the concentration reaches 10^{-5} curie at which time the concentration is set to zero.

Mother

$$B_J = A_J^0 e^{-a_J T} \quad J = 1, 2, 4, 5, 7, 9, 11, 13 \quad (6)$$

Daughter

$$B_J = \left[A_{J-1}^0 \left(\frac{a_J}{a_J - a_{J-1}} \right) \left(e^{-a_{J-1} T} - e^{-a_J T} \right) \right] + A_J^0 e^{-a_J T} \quad J = 3, 6, 8, 12 \quad (7)$$

$$B_J = 0.92 A_{J-1}^0 \quad J = 10 \quad (8)$$

where

B_J = concentration of isotope J, curies

T = decay time, days

$a_J = 0.693/\text{half-life, days}^{-1}$

Heat Generation

The decay heat, Q_J , is computed from the concentration of each isotope, B_J , and a parameter H_J , the energy release per disintegration.

$$Q_J = B_J H_J \quad J = 1, 13 \quad (9)$$

Distribution of Isotopes between Supernate and Sludge

In the process of cooling for 2 to 3 years the waste separates into two layers, the supernate and sludge. The heavier sludge layer contains about 85% of the total activity in a tank. Each of the 13 isotopes has a partition factor, PF_J , which is defined as the fraction of the isotope in the supernate of a tank. These partition factors range from 0.02 for ^{89}Sr to 0.95 for ^{137}Cs .

Intertank Transfers

Four types of intertank transfers can be made in the operation of the tank farm. The types are defined by the material transferred, supernate or sludge, and whether or not the material being moved has its partition factors changed while in transit. The curies to be transferred in a supernate transfer are computed by

$$CT_J = TB_J PF_J PC \quad J = 1,13 \quad (10)$$

and in a sludge transfer by

$$CT_J = TB_J PC(1.0 - PF_J) \quad J = 1,13 \quad (11)$$

where

CT_J = curies transferred, isotope J

TB_J = total curies of isotope J in tank from which material is removed

PF_J = partition factor for isotope J

PC = fraction of supernate or sludge to be moved

Thus, total curies in the tanks after a transfer are

$$NTB_J = TB_J - CT_J \quad J = 1,13 \quad (12)$$

for the sending tank, and

$$NTB_J = TB_J + CT_J \quad J = 1,13 \quad (13)$$

for the receiving tank for all types of transfers.

Supernate Transfers

In supernate transfers the new partition factors (NPF_J) for the tank from which material is removed are calculated by

$$NPF_J = \frac{(PF_J TB_J) - CT_J}{(TB_J - CT_J)} \quad J = 1,13 \quad (14)$$

and the new partition factors for the receiving tank are calculated by

$$NPF_J = \frac{(PF_J TB_J) + CT_J}{(TB_J + CT_J)} \quad J = 1,13 \quad (15)$$

However, if some of the material is precipitated by passing it through an evaporator, the new partition factors for the receiving tank are calculated by

$$NPF_J = \frac{(PF_J TB_J) + (CT_J PFA_J)}{(TB_J + CT_J)} \quad J = 1,13 \quad (16)$$

where

PFA_J = fraction of the J^{th} isotope that remains in supernate after precipitation

Sludge Transfers

In sludge transfers the new partition factors for the sending tank are recomputed by

$$NPF_J = \frac{(PF_J TB_J)}{(TB_J - CT_J)} \quad J = 1,13 \quad (17)$$

The new partition factors for the receiving tank are computed from

$$NPF_J = \frac{(PF_J TB_J)}{(TB_J + CT_J)} \quad J = 1,13 \quad (18)$$

and, as in the case of a supernate transfer in which some of the material is precipitated, the new partition factors for the receiving tank are given by

$$NPF_J = \frac{(PF_J TB_J)}{TB_J + (CT_J PFA_J)} \quad J = 1,13 \quad (19)$$

Transfer of Alpha Emitters

The alpha emitters are assumed to be contained completely in the sludge. The concentrations of the N isotopes are given by the following expressions in which N = 1,4 and corresponds to ^{238}U , ^{235}U , ^{239}Pu , and the combined total of the ^{238}Pu and ^{239}Pu .

$$UP_N = STUP_N \text{ PC} \quad N = 1,4 \quad (20)$$

$$NTUP_N = STUP_N - UP_N \quad N = 1,4 \quad (21)$$

$$RNTUP_N = RTUP_N + UP_N \quad N = 1,4 \quad (22)$$

where

UP_N = fraction of alpha emitter N that is transferred

$STUP_N$ = total of alpha emitter N in the sending tank

$NTUP_N$ = new total in sending tank

$RNTUP_N$ = new total in receiving tank

DESCRIPTION OF THE COMPUTER PROGRAM

TAFI-II was written in FORTRAN II for an IBM 704 with 10 tapes and a core memory of 32,000 words. The over-all flow is shown in Figure 1 and the FORTRAN listing is given in Appendix A. The code consists of the main program and four subroutines. COMMON is used to transfer data between the different parts of the code.

To allow for future expansion of the tank farm, as many as 34 tanks can be used with no changes to the code. Future tanks 25-28 have been assigned to H Area and 29-32 to F Area. The possibility of storing waste in deep-mined caverns⁽²⁾ has been considered by assigning tank number 33 to F Area and tank number 34 to H Area as deep-mined caverns. A transfer of waste into any one of these tanks is all that is necessary to put that tank into the TAFI-II system.

The summary of contents and conditions in each tank, permanent library data, is kept as a consecutively numbered series of binary records on a library tape. The library tape is updated at the end of each job by Subroutine PART 4. Each record, called file on the control card, includes the file (record) number, the year, month, day for the job, the final gamma and alpha emitter concentrations, and the final

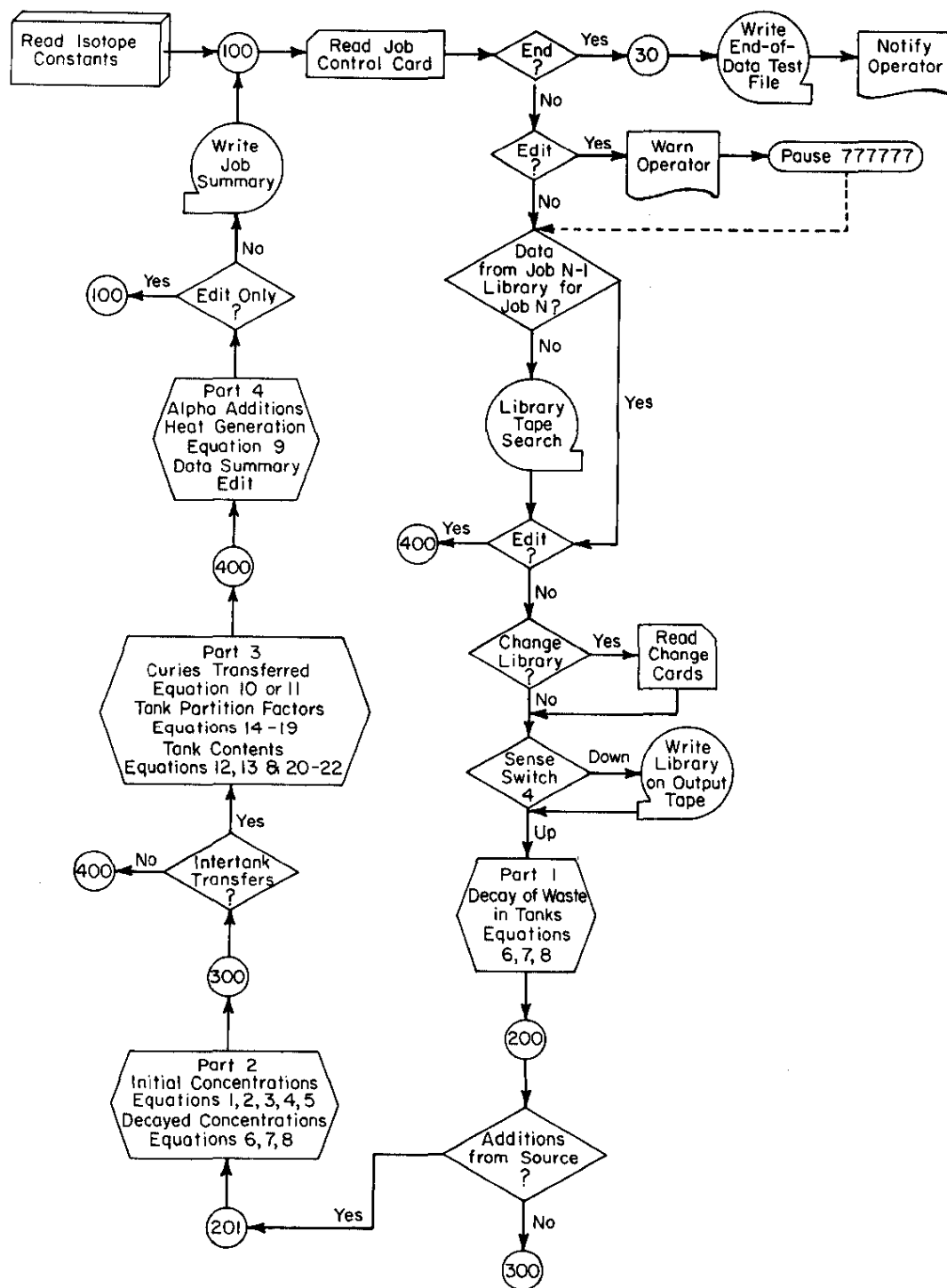


FIG. 1 OVER-ALL FLOW

tank partition factors. The file number for the current job is obtained by adding 1 to the starting file number (from the control card); this file number and the current data summary are written on the library tape as the starting file for the next job.

In the use of TAFI-II, care must be exercised in the sequencing of jobs. The job sequence and the transfers in a job must be in actual time sequence. At the end of a job or a set of jobs, if more than one is run at a time, the main program writes a dummy file to signal end-of-data. Because of this, care must be exercised in the use of the Edit option so that a good file will not be destroyed. At the end of each job, the main program writes a summary sheet that contains the file number and date that are required in the preparation of the control card for the next job.

Main Program

The main program reads the constants of the isotopes (half-life, yield, heat conversion factor, and name) from 13 cards (Appendix B, Figure 1) that immediately follow the transfer card. These constants are used for all jobs in a set, and if a constant for any isotope is to be changed the change must be made in the correct card in this deck.

The control card is read that identifies the job, the program options, and the library file for the job. The format and contents of the control card are given in Appendix B, Figure 2.

The binary library tape is then searched for the designated starting file. If changes are to be made in this file, the cards that contain the new information must follow the control card. The format of the change cards is shown in Appendix B, Figure 6. If Sense Switch 4 is DOWN the contents of the library file are written on the BCD output tape. The main program then calls Subroutine PART 1.

Subroutine PART 1

After the main program has set up the options and initial data, Subroutine PART 1 calculates the radioactive decay of the material in the tanks (from the library tape) for the specified number of days. Equations 6, 7, and 8 are used in this subroutine. If the concentration of an isotope becomes $\leq 10^{-5}$ curie, it is set to zero. The report written by PART 1 gives the concentration of each isotope in a tank at the beginning and the end of the decay time.

Subroutine PART 2

The additions to the system are handled by Equations 1-8 in PART 2. Each addition requires one input card that includes 1) the tank number

to which the addition is to be added; 2) tons of uranium for Purex calculations or ^{235}U burnup for the enriched uranium calculations; 3) irradiation time, days; 4) blank for Purex calculations or power conversion factor for the enriched uranium calculations; 5) days since discharge to the end of the reporting period for this job; 6) charge identification; and 7) an option that allows the partition factors for this charge to be changed. If this option is used, the two change cards must immediately follow the addition card. These two cards should contain, in order, the partition factors for this charge. The format of the cards for additions to the system is given in Appendix B, Figure 3. The report for PART 2 consists of the concentration in curies and the partition factor for each isotope in each addition as it is added to the tank. The total curies for each addition and the total of all additions in a job are also reported.

Subroutine PART 3

In this subroutine the four types of intertank transfer are made with Equations 10-22. The input for this subroutine requires one card per transfer that includes (a) tank transferred from, (b) tank added to, (c) percent of supernate or sludge transferred, and (d) option number. The options are: 1 = supernate transfer using the latest computed values for partition factors; 2 = supernate transfer and concentration of material during transit; 3 = sludge transfer using 1.0 - latest computed partition factors; and 4 = sludge transfer and changed partition factors. The detailed flow chart is Figure 2. Appendix B, Figure 4, illustrates the input cards.

Subroutine PART 4

PART 4 calculates the heat generated in the tanks by each isotope by Equation 9. It also makes additions to the alpha emitters; the input for these additions requires one card per addition with (a) tank number to which the addition is made; (b) ^{238}U , 10^3 lb; (c) ^{235}U , kg; (d) ^{239}Pu , kg; and (e) $^{238}\text{-}^{239}\text{Pu}$, curies, punched in this order (Appendix B, Figure 5).

The reports generated by PART 4 summarize the tank conditions (partition factors and concentration in curies) at the end of the job and gives a complete data summary of tank contents by area. The data summary is prepared for direct inclusion in a monthly report. PART 4 also updates the binary library tape at the end of each job.

The Subroutine is Under a DO Loop From 1, NX. NX is Read on the Control Card

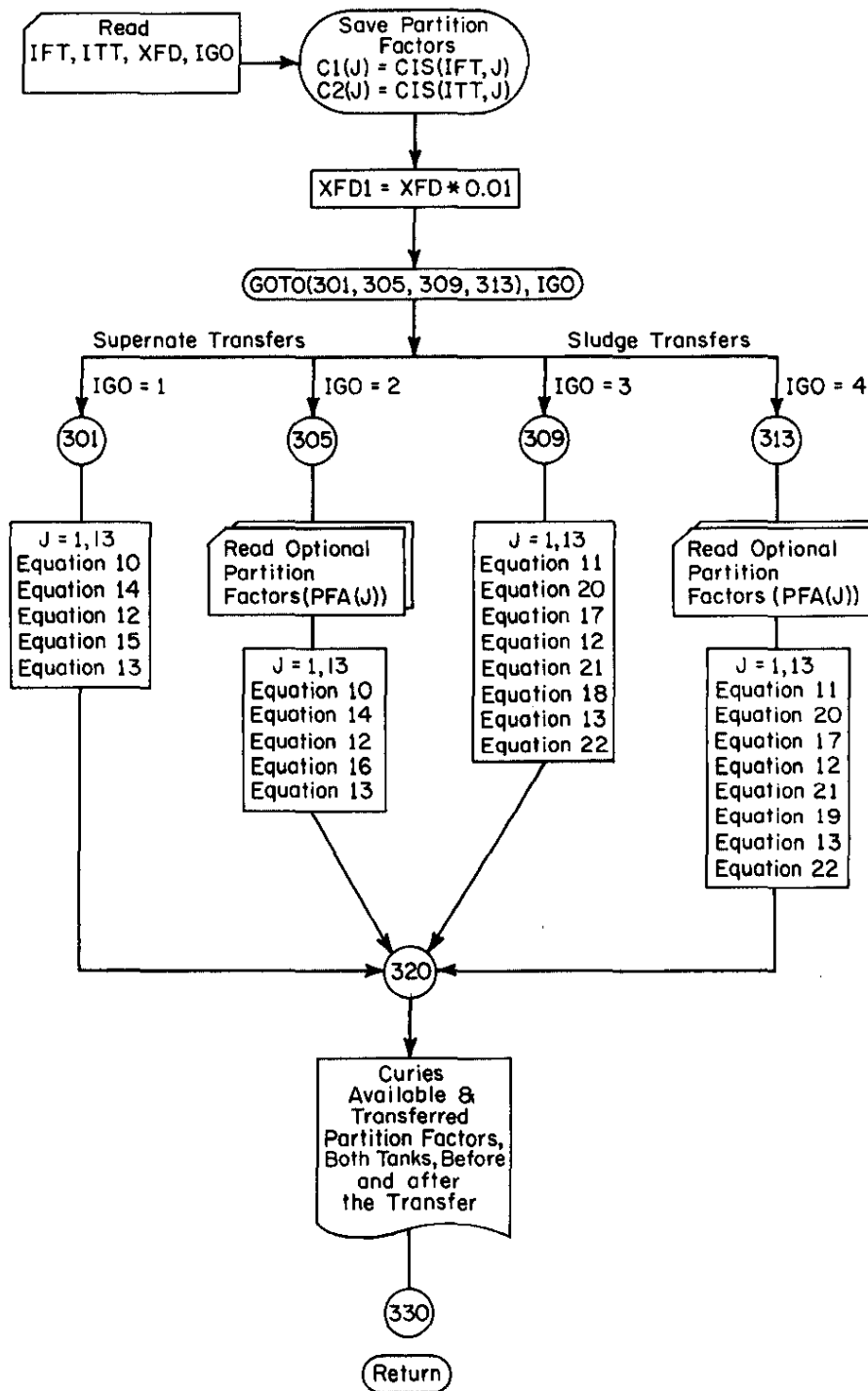


FIG. 2 SUBROUTINE PART 3 FLOW

ACKNOWLEDGMENT

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REFERENCES

1. A. N. Daniel. Underground Storage of Low-Level Radioactive Wastes at the Savannah River Plant. USAEC Report DP-478, E. I. du Pont de Nemours and Co., Wilmington, Del. (1960).
2. R. J. Christl. Storage of Radioactive Wastes in Basement Rock Beneath the Savannah River Plant. USAEC Report DP-844, E. I. du Pont de Nemours and Co., Savannah River Laboratory, Aiken, S. C. (1964).

APPENDIX A - FORTRAN Listing

TAFI-II

TAFI IS A PROGRAM TO KEEP AN INVENTORY OF CERTAIN ISOTOPES THAT ARE FISSION PRODUCT BY-PRODUCTS OF THE SEPARATIONS PROCESSES IN THE 200 AREAS. THESE WASTE PRODUCTS ARE ACCUMULATED IN THE WASTE TANKS IN EACH AREA.

TAFI-II IS DIVIDED INTO THE MAIN PROGRAM AND FOUR SUBROUTINES. THE MAIN PROGRAM READS THE IDENT. AND OPTIONS AND SETS UP THE TANK LIBRARY DATA AND THE CONSTANTS FOR EACH ISOTOPE TO BE USED BY THE OTHER PARTS OF THE CODE.

PART 1 DECAYS THE MATERIAL IN THE TANKS FOR DDT DAYS AND WRITES THE REPORT FOR CURIES IN THE TANKS BEFORE AND AFTER DECAY.

PART 2 CALCULATES THE ISOTOPIC CONTENTS OF AND ADJUSTS THE PARTITION FACTORS FOR ANY MATERIAL ADDED TO THE SYSTEM DURING THIS PERIOD OF TIME.

PART 3 HANDLES THE INTERTANK TRANSFERS BY CALCULATING THE FRACTION TRANSFERED AND RECALCULATING THE PARTITION FACTORS FOR THE TANKS INVOLVED IN THE TRANSFERS.

PART 4 MAKES THE ADDITIONS TO THE ALPHA EMITTERS, CALCULATES THE HEAT GENERATED IN EACH TANK AND WRITES THE FINAL DATA SUMMARY FOR BOTH AREAS.

```

DIMENSION TLIB(34,13),CIS(34,13),CURE(34,13),AHL(13),YLD(13),
1AHC(13),AQSS(34,4),PFN(13),PFA(13),CURA(13),PM(13),DUM2(13),
2DUM1(13),TAFI(3),ANAM(13),TOTB(34),TOTC(34),DENT(1),CURSV(13),THT(
334),SUHT(34),FTOT(13),HTOT(13),TNKS(34),AGN(4),BGN(4),UGN( 4),TGNTAFI
4(4),ASO(13)

```

```

COMMON CURE,TLIB,CIS,PFN,IPG,AHL,YLD,AHC,TAFI,ANAM,DDT,NC,NL,NX,
1AQSS,LIB,ILS,DUM1,DUM2,NTOUT,NF1,NF2,NTLIB,DA2,YR2,TMT2

```

```

CALL EFM
DO 6 I=1,34
DO 5 J=1,13
TLIB(I,J)=0.0
CIS(I,J)=0.0
CURE(I,J)=0.0
AQSS(I,J)=0.0
5 CONTINUE
6 CONTINUE
NTLIB=4
NTOUT=10
IPG=0
NF2=0
REWIND NTLIB

```

CONSTANTS FOR EACH ISOTOPE AND ISOTOPE NAME
AHL = HALF-LIFE, DAYS
YLD = YIELD, FRACTIONAL PERCENT
AHC = HEAT CONVERSION FACTOR
PFN = NORMAL PARTITION FACTOR, FRACTION IN SUPERNATE
ANAM = ISOTOPE NAME

```

1 DO 2 J=1,13
2 READ 600,I,(AHL(I)),(YLD(I)),(AHC(I)),(PFN(I)),(ANAM(I))

```

READ IDENTIFICATION AND OPTIONS

TAFI - IDENTIFICATION

DDT - DAYS TO DECAY THE TANKS

NF1,YR1,TMT1, DA1 - FILE NUMBER, YEAR, MONTH, DAY TO BE USED AS THE START FOR THIS JOB

YR2, TMT2, DA2 - YEAR, MONTH, DAY OF THIS JOB

ILB - NUMBER OF CHANGES TO CURIES IN TANKS (TLIB)

ICS - NUMBER OF CHANGES TO TANK PARTITION FACTORS (CIS)

ILS - NUMBER OF CHANGES TO ALPHA EMITTERS (AQSS)

NC - NUMBER OF CHARGES ADDED TO SYSTEM FROM SOURCE

NX - NUMBER OF INTERTANK TRANSFERS

NL - NUMBER OF ALPHA EMITTER LOSSES TO BE ADDED TO THE SYSTEM

LIB - 0= END, 1 = READ DESIGNATED FILE FOR COMPUTING, -1 = PRINT DESIGNATED FILE, NO COMPUTING

```

C          NOTE - EACH SET OF CHANGE CARDS (2 CARDS/SET) DESIGNATES
C                THE SPECIFIC TANK TO BE CHANGED AND THE ORDER
C                DETERMINES WHAT IS TO BE CHANGED.
C
C          THIS IS THE ENTRY POINT FOR RUNNING SUCESSIVE JOBS
C
C          100 READ 601, (TAFI(J), J=1,3),DDT,NF1,YR1,TMT1,DA1,YR2,TMT2,DA2,ILB,
C              1ICS,ILS,NC,NX,NL,LIB
C
C          TAPE READ COUNTER
C          IRD = 0
C
C          TEST FOR EDIT ONLY
C          IF(LIB)82,30,84
C          82 PRINT 632,NF1
C
C          PAUSE 777777
C
C          TEST - IS THE DATA JUST GENERATED TO BE USED AS THE STARTING POINT
C          FOR THE NEXT PROBLEM
C          84 IF(NF1-NF2)99,85,99
C
C          SWAP MATRICES
C
C          85 DO 86 I=1,34
C              DO 86 J=1,13
C                  TLIB(I,J)=CURE(I,J)
C          86 CONTINUE
C
C          GO TO 107
C
C          LIBRARY TAPE SEARCH
C
C          99 BACKSPACE NTLIB
C          101 READ TAPE NTLIB,IF,YR,TMT,DAY,TLIB,AOSS,CIS
C
C          TEST - RIGHT FILE
C          IF(IF-1000) 104,105,702
C          702 PRINT 628
C          PAUSE 707070
C
C          104 IF(NF1-IF)105,106,101
C
C          105 REWIND NTLIB
C              IRD = IRD + 1
C          IF AT FIRST YOU DON-T SUCEED TRY, TRY, THEN QUIT.
C          IF(IRD-3) 1061,702,702
C          1061 GO TO 101
C
C          106 IF((YR1+TMT1)-(YR+TMT))701,107,701
C
C          701 PRINT 604
C          PAUSE 777777
C
C          IF LIB = -1 PRINT THE REQUESTED FILE FROM TAPE
C          107 IF (LIB)400,102,102
C
C          TEST IS ANY OF THE INFORMATION IN THIS FILE TO BE UPDATED
C
C          102 IF(ILB+ICS + ILS)108,117,108
C
C          TEST - CHANGE CURIES FROM LIBRARY TAPE
C
C          108 IF(ILB)109,111,109
C          109 DO 110 I=1,ILB
C          110 READ 605, K, ((TLIB(K,J), J=1,13))
C
C          TEST TANK PARTITION FACTORS
C          111 IF (ICS)112,114,112
C          112 DO 113 I=1,ICS
C          113 READ 605, K, ((CIS(K,J),J=1,13))
C
C          TEST - CHANGE ALPHA EMITTERS
C          114 IF(ILS)115,117,115
C          115 DO 116 I=1,ILS
C          116 READ 600,K,((AOSS(K,J), J=1,4))
C
C          117 CONTINUE
C
C          TEST - DUMP LIBRARY

```

```

C
1113 IF(SENSE SWITCH 4)1113,130
      IPG=IPG+1
      LINE=0
      DO 118 I=1,34
      IF(LINE)119,120,119
120 WRITE OUTPUT TAPE NTOUT,630,(TAFI(J),J=1,3),IPG
119 T1=0.0
      DO 121 J=1,13
      T1=T1+TLIB(I,J) +CIS(I,J)
121 CONTINUE
      IF(T1)122,118,122
122 WRITE OUTPUT TAPE NTOUT,631,I,((TLIB(I,J),CIS(I,J)),J=1,13)
      LINE=LINE+1
      IF(I-34)123,124,123
123 IF(LINE-5)118,124,118
124 WRITE OUTPUT TAPE NTOUT,609
      LINE=0
      IPG=IPG+1
118 CONTINUE
C
130 CONTINUE
C
C CALL PART1
C
C TEST - TRANSFERS (ADDITIONS) FROM SOURCE
C
C 200 IF(NC)201,300,201
C 201 CALL PART2
C
C TEST - INTERTANK TRANSFERS
C
C 300 IF (NX)303,400,303
C 303 CALL PART3
C
C 400 CALL PART4
C
C IF(LIB)100,500,500
C 500 IPG=IPG+1
C
C WRITE OUTPUT TAPE NTOUT,606,(TAFI(J),J=1,3),IPG
C WRITE OUTPUT TAPE NTOUT,627,DCT,NF1,YR1,TMT1,DA1,NF2,YR2,TMT2,DA2,
11LB,ICS,ILS,NC,NX,NL
C
C WRITE OUTPUT TAPE NTOUT,609
C
C GO TO 100
C
C 30 NEND=1000
C WRITE TAPE NTLIB,NEND,YR2,TMT2,DA2,CURE,AOSS,CIS
C REWIND NTLIB
C PRINT 602
C
C 600 FORMAT (I2,4E9.4,1A6)
C
C 601 FORMAT(3A6,E9.4,I3,6F2.0,7I2)
C
C 602 FORMAT(60HOPROBLEM COMPLETED - HAVE TAPE 10 PRINTED AT 6 LINES PERTAFI
11NCH/25H STORE TAPE 4 IN THE SAFE,20X1H=/////////)
C
C 604 FORMAT(96HOKKOR - FILE DATE ON CARD DOES NOT APPEAR ON LIBRARY TATAFI
1PE. END RUN. NOTIFY SUBMITTOR AT ONCE./////////)
C
C 605 FORMAT(7X,I2,6E9.4/(7E9.4))
C
C 606 FORMAT(1H1,50X,17HSECRET WORK SHEET/ 50X,3A6,37X,5HPAGE ,I2)
C
C 609 FORMAT(1H0,49X,17HSECRET WORK SHEET)
C
C 627 FORMAT(1H0,25X,27HSUMMARY SHEET FOR THIS JOB.///10X,18HTANKS DECAYTAFI
1ED FOR ,F6.0,1X,4HDAYS/10X,12HFILE NUMBER ,I3,1X,15HWITH THIS DATETAFI
1 ,F3.0,1H/,F3.0,1H/,F3.0,31H WAS USED AS THE STARTING POINT/10X,12TAFI
2HFILE NUMBER ,I3,16H WITH THIS DATE ,F3.0,1H/,F3.0,1H/,F3.0, 55H STAFI
3SHOULD BE USED AS THE STARTING POINT FOR THE NEXT JOB./10X,43HTHE CTAFI

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      TOTB(I)=TOTB(I)+TLIB(I,J)
      TOTC(I)=TOTC(I)+CURE(I,J)
141 CONTINUE
140 CONTINUE
C      MATERIAL IN THE TANKS HAS BEEN DECAYED FOR THE SPECIFIED NUMBER
C      OF DAYS.  WRITE REPORT FOR PART 1
C
      IPG=IPG+1
      LINE=0
      DO 180 I=1,34
        IF(TOTB(I)+TOTC(I))150,180,150
150 IF(LINE)152,151,152
151 WRITE OUTPUT TAPE NTOUT,606,      (TAFI(J),J=1,3),IPG
      WRITE OUTPUT TAPE NTOUT,607
      IPG = IPG + 1
C
152 T1=0.0
      DO 153 J=1,13
153 T1=T1+TLIB(I,J)+CURE(I,J)
        IF(T1)156,159,156
156 LINE=LINE+1
        WRITE OUTPUT TAPE NTOUT,608,I,((ANAM(K)),K=1,4), ((TLIB(I,J),CURE(I,
1I,J)),J=1,4),((ANAM(K)),K=5,8),((TLIB(I,J),CURE(I,J)),J=5,8), ( (
2ANAM (K)),K=9,12),((TLIB(I,J),CURE(I,J)),J=9,12), ANAM(13),
3TLIB(I,13),CURE(I,13),TOTB(I),TOTC(I)
C
159 IF(I-34)157,158,157
157 IF(LINE-5)180,158,180
158 WRITE OUTPUT TAPE NTOUT, 609
      LINE = 0
180 CONTINUE
C
190 RETURN
C
606 FORMAT(1H1,50X,17HSECRET WORK SHEET/ 50X,3A6,37X,5HPAGE ,I2)
C
607 FORMAT(71H CURIES IN TANKS BEFORE AND AFTER DECAY, IF LESS THAN 10
1 E-5 SET = 0.0.//1X4HTANK,3X,6HBEFORE,7X,5HAFTER,6X,6HBEFORE,7X,
25HAFTER,6X,6HBEFORE,7X5HAFTER,6X,6HBEFORE,7X,5HAFTER//)
C
608 FORMAT(13,11X,1A6,18X,1A6,18X,1A6,18X,1A6/4X,8E12.4/14X,1A6,18X,1ATAFI
16,18X,1A6,18X,1A6/4X,8E12.4/14X,1A6,18X,1A6,18X,1A6,18X,1A6/4X,8E1TAFI
22.4/14X,1A6,18X,6HTOTALS/4X,4E12.4//)
C
609 FORMAT(1H0,49X,17HSECRET WORK SHEET)
C
      END(2,0,1,0,0)

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C      PART 2
C      THIS SUBROUTINE HANDLES THE CHARGES THAT ARE ADDED TO THE SYSTEM
C      IN THIS PERIOD OF TIME.  THE INITIAL ISOTOPIC CONCENTRATIONS
C      ARE CALCULATED AND THEN DECAYED AND ADDED TO THE TANKS.
C      THE TANK PARTITION FACTORS ARE RECALCULATED FOR EACH ADDITION
C      ACCORDING TO THE OPTION ON THE ADDITION CARD
C
      SUBROUTINE PART2
C
      DIMENSION TLIB(34,13),CIS(34,13),CURE(34,13),AHL(13),YLD(13),
1AHC(13),AOSS(34,4),PFN(13),PFA(13),CURA(13),PM(13),DUM2(13),
2DUM1(13),TAFI(3),ANAM(13),TOTB(34),TOTC(34),DENT(1),CURSV(13),THT(TAFI
334),SUHT(34),FTOT(13),HTOT(13),TNKS(34),AGN(4),BGN(4),OGN( 4),TGNTAFI
4(4),ASO(13)
C
      COMMON CURE,TLIB,CIS,PFN,IPG,AHL,YLD,AHC,TAFI,ANAM,DDT,NC,NL,NX,
1AOSS,LIB,ILS,DUM1,DUM2,NTOUT,NF1,NF2,NTLIB,DA2,YR2,TMT2
C
205 CONK=0.85E+6
      SUM2=0.0
      LINE=0
C
      ADD ALL TRANSFERS FROM SOURCE TO THE SYSTEM

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DO 250 NT=1,NC
DENT = 0.0
P4=0.0
SUM1=0.0
READ 610,JT,P1,P2,P3,P4,DSD,DENT,NML
P4=0.0 CALCULATE P BY PUREX METHOD
C 210 IF(P4)212,211,212
C 211 P=P1*P2
GO TO 214
C 212 P=((P1/P4)*(1./P3))*P2
C 214 DO 230 J=1,13
ASO(J)=0.0
CURSV(J)=0.0
C SAME SCHEME TO DECAY THE ISOTOPES AS THE TANK DECAY
C GO TO(1 2 3 4 5 6 7 8 9 10 11 12 13
C 215,215,216,215,215,216,215,216,215,216,215,216,215),J
C MOTHER
C CONCENTRATION AT REACTOR DISCHARGE - ASO
C 215 SA=0.693/AHL(J)
ASO(J)=(CONK*P*YLD(J))*(1.-(EXP(-SA*P3)))
C CONCENTRATION AS ADDED TO TANKS - CURSV
C CURSV(J)=ASO(J)*EXP(-SA*DSD)
IF(CURSV(J))229,230,230
C DAUGHTER
C CONCENTRATION AT REACTOR DISCHARGE
C 216 SA=0.693/AHL(J-1)
SB=0.693/AHL(J)
Z1=SB/(SB-SA)
Z2=SA/(SB-SA)
ASO(J)=(CONK*P*YLD(J)) * (Z1*(1.-EXP(-SA*P3)))-Z2*(1.-EXP(-SB
1*P3))
C CONCENTRATION AS ADDED TO TANKS
CURSV(J) = Z1 * (ASO(J-1) * (EXP(-SA*DSD)-EXP(-SB*DSD))) + ASO(J)*
1EXP(-SB*DSD)
IF(CURSV(J))229,230,230
C 217 CURSV(J)=0.92*CURSV(J-1)
IF(CURSV(J))229,230,230
C 229 CURSV(J)=0.0
230 CONTINUE
C CALCULATE NEW PARTITION FACTORS FOR EACH ISOTOPE
AND ADD THE ISOTOPES TO THE DESIGNATED TANK
IF NML=0 NORMAL PARTITION FACTORS WILL BE USED TO RECALCULATE
THE PARTITION FACTORS FOR THE TANK
TANK PARTITION FACTORS ARE CALLED CIS
NORMAL PARTITION FACTORS FOR EACH CHARGE ARE CALLED PFN
ABNORMAL PARTITION FACTORS ARE CALLED PFA
C IF(NML)240,231,240
C 231 DO 235 J=1,13
CIS(JT,J)=((CIS(JT,J)*CURE(JT,J))+CURSV(J)*PFN(J))/(CURE(JT,J)+CUR
1SV(J))
SUM1=SUM1+CURSV(J)
235 CURE(JT,J)=CURE(JT,J)+CURSV(J)
GO TO 245
C 240 READ 605,NG,(PFA(J),J=1,13)
NG=0
DO 241 J=1,13
CIS(JT,J)=(CIS(JT,J)*CURE(JT,J)+CURSV(J)*PFA(J))/(CURE(JT,J)+CUR
1SV(J))
SUM1=SUM1+CURSV(J)
241 CURE(JT,J)=CURE(JT,J)+CURSV(J)
GO TO 245
C 245 SUM2=SUM2+SUM1
C WRITE THE REPORT FOR THE TRANSFERS FROM SOURCE
C PRINT HEADING

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C      XFD1=XFD*0.01
PRESERVE PARTITION FACTORS FOR COMPARISONS
DO 3301 J=1,13
C1(J) = 0.0
C2(J) = 0.0
3301 C1(J) = CIS(IFT,J)
C2(J) = CIS(ITT,J)
C      GO TO (301,305,309,313),IGO
C      SUPERNATE TRANSFER
TRANSFER COMPUTED ON THE BASIS OF THE LATEST COMPUTED VALUES OF
THE TANK PARTITION FACTORS
301 DO 302 J=1,13
DUM1(J) = 0.0
DUM2(J) = 0.0
PM(J) = 0.0
PM(J)=XFD1*CURE(IFT,J)*CIS(IFT,J)
IF(PM(J)) 302,302,303
303 DUM1(J) = CURE(IFT,J)
SUM1=SUM1+DUM1(J)
SUM2=SUM2+PM(J)
CIS(IFT,J) = (CIS(IFT,J) * CURE(IFT,J) - PM(J))/(CURE(IFT,J)-PM(J)
1))
C      SUBTRACT FROM TANK IFT
CURE(IFT,J)=CURE(IFT,J)-PM(J)
C      ADD TO TANK ITT
DUM2(J)=CURE(ITT,J)
CIS(ITT,J) = (CIS(ITT,J)*CURE(ITT,J)+PM(J))/(CURE(ITT,J)+PM(J))
CURE(ITT,J) = CURE(ITT,J) + PM(J)
302 CONTINUE
GO TO 320
C      SUPERNATE TRANSFER WITH OPTIONAL PARTITION FACTORS
305 READ 605,NG,(PFA(J),J=1,13)
DO 306 J=1,13
PM(J) = 0.0
DUM1(J) = 0.0
DUM2(J) = 0.0
PM(J)=XFD1*CURE(IFT,J)*CIS(IFT,J)
IF(PM(J)) 306,306,307
307 DUM1(J) = CURE(IFT,J)
SUM1 = SUM1 + DUM1(J)
SUM2=SUM2+PM(J)
CIS(IFT,J) = (CIS(IFT,J) * CURE(IFT,J) - PM(J))/(CURE(IFT,J)-PM(J)
1))
CURE(IFT,J)=CURE(IFT,J)-PM(J)
C      CIS(ITT,J) = (CIS(ITT,J)*CURE(ITT,J)+PM(J)*PFA(J))/(CURE(ITT,J)
1+PM(J))
DUM2(J)=CURE(ITT,J)
CURE(ITT,J) = CURE(ITT,J) + PM(J)
306 CONTINUE
GO TO 320
C      SLUDGE TRANSFER WITH COMPUTED PARTITION FACTORS
ALPHA EMITTERS (PL+U ISOTOPES) ARE TRANSFERED WITH THE SLUDGE
309 DO 310 J=1,13
PM(J) = 0.0
DUM1(J) = 0.0
DUM2(J) = 0.0
A=(1.-CIS(IFT,J))
PM(J)=CURE(IFT,J)*A*XFD1
IF(PM(J)) 310,310,311
311 DUM1(J) = CURE(IFT,J)
SUM1 = SUM1 + DUM1(J)
SUM2=SUM2+PM(J)
CIS(IFT,J) = (CIS(IFT,J)*CURE(IFT,J))/(CURE(IFT,J) - PM(J))
CURE(IFT,J)=CURE(IFT,J)-PM(J)
C      CIS(ITT,J)=(CIS(ITT,J)*CURE(ITT,J))/(CURE(ITT,J)+PM(J))
DUM2(J) = CURE(ITT,J)
CURE(ITT,J) = CURE(ITT,J) + PM(J)

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```

310 CONTINUE
C
C   ALPHA EMITTER TRANSFER
DO 312 N = 1,4
  ATR(N) = 0.
  ATR(N) = AOSS(IFT,N) * XFD1
  AOSS(IFT,N) = AOSS(IFT,N) - ATR(N)
  AOSS(ITT,J) = AOSS(ITT,N) + ATR(N)
312 CONTINUE
GO TO 320

C
C   SLUDGE TRANSFER WITH OPTIONAL PARTITION FACTORS
313 READ 605,NG,(PFA(J),J=1,13)
DO 314 J=1,13
  DUM1(J) = 0.0
  DUM2(J) = 0.0
  PM(J) = 0.0
  PM(J) = XFD1 * CURE(IFT,J) * (1.0 - CIS(IFT,J))
  IF(PM(J)) 314,314,315
315 DUM1(J) = CURE(IFT,J)
  SUM1 = SUM1 + DUM1(J)
  SUM2 = SUM2 + PM(J)
  CIS(IFT,J) = (CIS(IFT,J) * CURE(IFT,J)) / (CURE(IFT,J) - PM(J))
  CURE(IFT,J) = CURE(IFT,J) - PM(J)
C
C   CIS(ITT,J) = (CIS(ITT,J) * CURE(ITT,J)) / (CURE(ITT,J) + PM(J) * PFA(J))
DUM2(J) = CURE(ITT,J)
CURE(ITT,J) = CURE(ITT,J) + PM(J)
314 CONTINUE

C
C   ALPHA EMITTER TRANSFER
DO 316 N = 1,4
  ATR(N) = 0.
  ATR(N) = AOSS(IFT,N) * XFD1
  AOSS(IFT,N) = AOSS(IFT,N) - ATR(N)
  AOSS(ITT,N) = AOSS(ITT,N) + ATR(N)
316 CONTINUE

C
C   WRITE REPORT ON THE TRANSFERS BETWEEN TANKS
320 IF(LINE)322,321,322
321 IPG=IPG+1
  HEADING FOR TRANSFERS BETWEEN TANKS
  WRITE OUTPUT TAPE NTOUT,606,((TAFI(I),I=1,3),IPG)
  WRITE OUTPUT TAPE NTOUT,614
322 WRITE OUTPUT TAPE NTOUT,615,IFT,ITT,XFD,IGO
  WRITE OUTPUT TAPE NTOUT,608,NT,((ANAM(J)),J=1,4),((DUM1(I),PM(I)),TAFI
  1I=1,4),((ANAM(J)),J=5,8),((DUM1(I),PM(I)),I=5,8),((ANAM(J)),J
  2=9,12),((DUM1(I),PM(I)),I=9,12),ANAM(13),DUM1(13),PM(13),SUM1,
  3SUM2
C
C   IF (IGO - 3) 3221,3222 ,3222
3222 WRITE OUTPUT TAPENTOUT,620, ((AOSS(IFT,N),ATR(N)),N=1,4)
C
3221 WRITE OUTPUT TAPE NTOUT,617,IFT,((C1(      J),CIS(IFT,J)),J=1,5),
  1((C1(      J),CIS(IFT,J)),J=6,10),((C1(      J),CIS(IFT,J))),
  2J=11,13)
  WRITE OUTPUT TAPE NTOUT, 617,ITT,((C2(      J),CIS(ITT,J)),J=
  11,5),((C2(      J),CIS(ITT,J)),J=6,10),((C2(      J),CIS(ITT,J))),
  2J=11,13)
  LINE=LINE+1
  IF(NT-NX)323,329,323
323 IF(LINE-2)330,329,330
329 WRITE OUTPUT TAPE NTOUT,609
  LINE=0
C
330 CONTINUE
C
  RETURN
C
605 FORMAT(7X,I2,6E9.4/(7E9.4))
C
606 FORMAT(1H1,50X,17HSECRET WORK SHEET/ 50X,3A6,37X,5HPAGE ,I2//)
C
608 FORMAT(I3,11X,1A6,18X,1A6,18X,1A6,18X,1A6,18X,1A6/4X,8E12.4/14X,1A6,18X,1ATAFI
  16,18X,1A6,18X,1A6/4X,8E12.4/14X,1A6,18X,1A6,18X,1A6,18X,1A6/4X,8E1TAFI
  22.4/14X,1A6,18X,6HTOTALS/4X,4E12.4)

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C 609 FORMAT(1H0,49X,17HSECRET WORK SHEET) TAFI
C 612 FORMAT(2I2,E9.4,I1)
C 614 FORMAT(40X,19HINTERTANK TRANSFERS/6X,9HAVAILABLE,3X,10HTRANSFERED,TAFI
13X,9HAVAILABLE,2X,10HTRANSFERED,3X,9HAVAILABLE,2X,10HTRANSFERED,3XTAFI
2,9HAVAILABLE,2X,10HTRANSFERED//) TAFI
C 615 FORMAT(17H0INPUT DATA, FROM,I3,1X,3HTO ,I2,1X14HPERCENT MOVED ,F6.TAFI
12,1X,11HOPTION NO. ,I1//)
C 617 FORMAT(35H0PARTITION FACTOR CHANGES FOR TANK I2,1X,42HEACH ISOTOPE
1 BEFORE AND AFTER THE TRANSFER/ 4X,8E12.4/4X,8E12.4/4X,8E12.4
2/4X,2E12.4)
C 620 FORMAT(16H ALPHA TRANSFER ,8E12.4//)
C END(2,0,0,0,0)

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C PART 4 TAFI
C
C SUBROUTINE PART4
C DIMENSION TLIB(34,13),CIS(34,13),CURE(34,13),AHL(13),YLD(13), TAFI
1AHC(13),AOSS(34,4),PFN(13),PFA(13),CURA(13),PM(13),DUM2(13), TAFI
2DUM1(13),TAFI(13),ANAM(13),TOT8(34),TOTC(34),DENT(1),CURSV(13),THT(TAFI
334),SUHT(34),FTOT(13),HTOT(13),TNKS(34),AGN(4),BGN(4),OGN( 4),TGNTAFI
4(4),ASO(13)
C DIMENSION T8(34,13),T9(34,13)
C COMMON CURE,TLIB,CIS,PFN,IPG,AHL,YLD,AHC,TAFI,ANAM,DDT,NC,NL,NX,
1AOSS,LIB,ILS,DUM1,DUM2,NTOUT,NF1,NF2,NTLIB,DA2,YR2,TMT2
C
C THIS PART OF THE PROGRAM CALCULATES THE HEAT GENERATED IN EACH TANK AND SPLITS THE HEAT INTO SLUDGE AND SUPERNATE ACCORDING TO THE COMPUTED PARTITION FACTORS. IT ALSO WRITES THE FINAL REPORT FOR THE MONTH AND UPDATES THE LIBRARY TAPE. IF IT IS NECESSARY TO ADD TO THE ALPHA EMITTERS IT IS DONE IN THIS PART OF THE CODE
C
C LINE = 0
C TEST - ADDITIONS TO ALPHA EMITTERS
IF(NL)4501,4505,4501
4501 DO 4502 I=1,NL
DO 4503 J=1,4
4503 OGN( J)=0.0 TAFI
C
C I - TANK NUMBER
OGN(1) - U-238, THOUS. LB.
OGN(2) - U-235, KG.
OGN(3) - PU-239, KG.
OGN(4) - PU-238-239, CURIES
C
C READ 618,I,(OGN( J),J=1,4)
DO 4502 J=1,4 TAFI
AOSS(I,J)=AOSS(I,J)+OGN( J) TAFI
4502 CONTINUE
C
C PLACE LIBRARY DATA IN CURE MATRIX FOR PRINTING
4505 IF(LIB)4100,4500,4500 TAFI
4100 DO 4110 I=1,34 TAFI
DO 4110 J=1,13 TAFI
4110 CURE (I,J) = TLIB(I,J) TAFI
C
C CALCULATE HEAT IN EACH TANK
DO 410 I=1,34 TAFI
THT(I) = 0.0 TAFI
SUHT(I) = 0.0 TAFI
DO 401 J=1,13 TAFI
C
C CALCULATION OF ISCTOPIC CONTRIBUTIONS TO HEATS
T8(I,J)=0.0
T9(I,J)=0.0

```

C	TOTAL HEAT	TAFI
	T8(I,J)=T8(I,J)+(CURE(I,J)*AHC(J))	
	THT(I)=THT(I)+T8(I,J)	
C	HEAT IN SUPERNATE	TAFI
	T9(I,J)=T9(I,J)+(CURE(I,J)*AHC(J)*CIS(I,J))	
401	SUHT(I)=SUHT(I)+T9(I,J)	
C		TAFI
C	WRITE SUMMARY REPORT FOR THE TANK PARTITION FACTORS	TAFI
C		TAFI
	IF(THT(I) + SUHT(I)) 4002,405,4002	
4002	IF(LINE) 403,402,403	
C	PAGE HEADING	TAFI
402	IPG=IPG+1	TAFI
C		TAFI
	WRITE OUTPUT TAPE NTOUT,606,(TAFI(J),J=1,3),IPG	TAFI
	WRITE OUTPUT TAPE NTOUT,616	TAFI
C		TAFI
403	WRITE OUTPUT TAPE NTOUT,617,(ANAM(K),K=1,7),I,(CIS(I,J),J=1,7)	
	1(ANAM(K),K=8,13),(CIS(I,J),J=8,13)	
	WRITE OUTPUT TAPE NTOUT,617,(ANAM(K),K=1,7),I,(T8(I,J),J=1,7),	TAFI
	1(ANAM(K),K=8,13),(T8(I,J),J=8,13)	
C		
404	LINE=LINE+2	
405	IF(I-34)406,409,406	TAFI
406	IF(LINE-8)410,409,410	TAFI
409	WRITE OUTPUT TAPE NTOUT,609	TAFI
	LINE=0	TAFI
410	CONTINUE	TAFI
C		TAFI
C		TAFI
C	SUM THE ISOTOPES IN EACH AREA	TAFI
C		TAFI
	DO 426 N=1,4	TAFI
C		TAFI
	DO 425 J=1,13	TAFI
	BGN(N)=0.0	TAFI
	AGN(N)=0.0	TAFI
	FTOT(J)=0.0	TAFI
	HTOT(J)=0.0	TAFI
	DUM1(J)=0.0	TAFI
C		
C	TOTALS FOR F AREA	TAFI
C	F-AREA TANKS 1-8	TAFI
	DO 411 I=1,8	TAFI
C	ALPHA EMITTER SUM	
	AGN(N)=AGN(N)+AOSS(I,N)	TAFI
C	TOTAL CURIES IN EACH TANK	
	TNKS(I)=0.0	TAFI
	DO 4111 K=1,13	TAFI
	TNKS(I)=TNKS(I)+CLRE(I,K)	TAFI
4111	CONTINUE	TAFI
C		
C	TOTAL ISOTOPES IN AREA	
411	FTOT(J)=FTOT(J)+CLRE(I,J)	TAFI
C		
C	F-AREA TANKS 17-20	TAFI
	DO 412 I=17,20	TAFI
	AGN(N)=AGN(N)+AOSS(I,N)	TAFI
	TNKS(I)=0.0	TAFI
	DO 4121 K=1,13	TAFI
	TNKS(I)=TNKS(I)+CLRE(I,K)	TAFI
4121	CONTINUE	TAFI
C		
412	FTOT(J)=FTOT(J)+CLRE(I,J)	TAFI
C		TAFI
C	H-AREA TANKS 9-16	TAFI
	DO 413 I=9,16	TAFI
C	ALPHA EMITTER SUM	
	BGN(N)=BGN(N)+AOSS(I,N)	TAFI
C	TOTAL CURIES IN EACH TANK	
	TNKS(I)=0.0	TAFI
	DO 4131 K=1,13	TAFI
	TNKS(I)=TNKS(I)+CLRE(I,K)	TAFI
4131	CONTINUE	TAFI
C		
C	TOTAL ISOTOPES IN AREA	
413	HTOT(J)=HTOT(J)+CLRE(I,J)	TAFI
C		TAFI
C	H-AREA TANKS 21-24	TAFI
	DO 414 I=21,24	TAFI
	BGN(N)=BGN(N)+AOSS(I,N)	TAFI

	TNKS(I)=0.0	TAFI
	DO 4141 K=1,13	TAFI
	TNKS(I)=TNKS(I)+CLRE(I,K)	TAFI
4141	CONTINUE	TAFI
414	HTOT(J)=HTOT(J)+CLRE(I,J)	TAFI
C		
C	FIRST ADDITIONAL TANK NUMBERS ARE ASSIGNED TO H-AREA	TAFI
C		
416	DO 417 I=25,28	TAFI
	BGN(N)=BGN(N)+ADSS(I,N)	TAFI
	TNKS(I)=0.0	TAFI
	DO 4171 K=1,13	TAFI
	TNKS(I)=TNKS(I)+CLRE(I,K)	TAFI
4171	CONTINUE	TAFI
417	HTOT(J)=HTOT(J)+CLRE(I,J)	TAFI
C		TAFI
C	SECOND SET OF TANKS ASSIGNED TO F-AREA	TAFI
419	DO 420 I=29,32	TAFI
	AGN(N)=AGN(N)+ADSS(I,N)	TAFI
	TNKS(I)=0.0	TAFI
	DO 4201 K=1,13	TAFI
	TNKS(I)=TNKS(I)+CLRE(I,K)	TAFI
4201	CONTINUE	TAFI
420	FTOT(J)=FTOT(J)+CLRE(I,J)	TAFI
C	ALPHA EMITTER SUM	
	TGN(N)=TGN(N)+AGN(N)+BGN(N)	TAFI
C		TAFI
C	SUM FOR GRAND TOTAL F +H INTO DUM1	TAFI
	DUM1(J)=DUM1(J)+FTOT(J)+HTOT(J)	TAFI
C		TAFI
425	CONTINUE	TAFI
426	CONTINUE	TAFI
C		TAFI
	GFT=0.0	TAFI
	GHT=0.0	TAFI
	GTD=0.0	TAFI
	FT1=0.0	TAFI
	FT2=0.0	TAFI
	HT1=0.0	TAFI
	HT2=0.0	TAFI
	GTHT=0.0	TAFI
	GTSU=0.0	TAFI
	DO 4601 I=1,8	TAFI
C		
	M=I+8	
C	TOTAL HEATS	
	FT1=FT1+THT(I)	
	HT1=HT1+THT(M)	
C		
C	SUPERNATE HEATS	
	FT2=FT2+SUHT(I)	
	HT2=HT2+SUHT(M)	
4601	CONTINUE	
C		
	DO 4602 I=17,20	
	M=I+4	
	FT1=FT1+THT(I)	
	HT1=HT1+THT(M)	
	FT2=FT2+SUHT(I)	
	HT2=HT2+SUHT(M)	
4602	CONTINUE	
C	FUTURE FIRST TANK NUMBERS ASSIGNED TO H-AREA SO INDEX IS CHANGED	
	DO 4603 I=25,28	
	M=I+4	
	HT1=HT1+THT(I)	
	FT1=FT1+THT(M)	
	HT2=HT2+SUHT(I)	
	FT2=FT2+SUHT(M)	
4603	CONTINUE	
	DO 427 J=1,13	
	GFT = GFT + FTOT(J)	
	GHT = GHT + HTOT(J)	
427	CONTINUE	
	GTHT=FT1+HT1	TAFI
	GTSU=FT2+HT2	TAFI
	GTO=GHT+GFT	TAFI
C		
	DO 428 N =1,4	
	TGN(N)=0.0	
428	TGN(N) = TGN(N) + AGN(N) + BGN(N)	TAFI
C		

C	WRITE THE FINAL REPORT FOR THIS JOB	TAFI
C		TAFI
C	FIRST PAGE	TAFI
	IPG=IPG+1	TAFI
	WRITE OUTPUT TAPE NTOUT,619,IPG,(TAFI(J),J=1,3)	TAFI
	WRITE OUTPUT TAPE NTOUT,620,(ANAM(J),J=1,8)	TAFI
C	F-AREA TANKS	TAFI
	DO 430 I=1,8	TAFI
430	WRITE OUTPUT TAPE NTOUT,621,I,(CURE(I,J),J=1,8)	TAFI
	DO 431 I=17,20	TAFI
431	WRITE OUTPUT TAPE NTOUT,621,I,(CURE(I,J),J=1,8)	TAFI
C	MORE TANKS IN F-AREA	TAFI
432	DO 433 I=29,32	TAFI
C	TEST FOR PRINTING OF ADDITIONAL TANKS	TAFI
	T1=0.0	TAFI
	DO 4333 J=1,13	TAFI
4333	T1=T1+CURE(I,J)	TAFI
	IF(T1)4334,433,4334	TAFI
4334	WRITE OUTPUT TAPE NTOUT,621,I,(CURE(I,J),J=1,8)	TAFI
433	CONTINUE	TAFI
C	TOTALS OF EACH ISCTOPE IN F-AREA	TAFI
C		TAFI
434	WRITE OUTPUT TAPE NTOUT,622,(FTOT(J),J=1,8)	TAFI
C	IS THE DEEP MINE CAVERN IN USE	TAFI
	FDM=0.0	TAFI
	DO 435 I=1,13	TAFI
435	FDM=FDM+CURE(33,I)	TAFI
	IF(FDM)436,440,436	TAFI
436	WRITE OUTPUT TAPE NTOUT,625,(CURE(33,J),J=1,8)	TAFI
C		TAFI
C	H-AREA TANKS	TAFI
440	DO 441 I=9,16	TAFI
441	WRITE OUTPUT TAPE NTOUT,621,I,(CURE(I,J),J=1,8)	TAFI
	DO 442 I=21,24	TAFI
442	WRITE OUTPUT TAPE NTOUT,621,I,(CURE(I,J),J=1,8)	TAFI
C	MORE TANKS IN H-AREA	TAFI
C		TAFI
443	DO 444 I=25,28	TAFI
C	TEST FOR PRINTING OF ADDITIONAL TANKS	TAFI
	T1=0.0	TAFI
	DO 4443 J=1,13	TAFI
4443	T1=T1+CURE(I,J)	TAFI
	IF(T1)4444,444,4444	TAFI
4444	WRITE OUTPUT TAPE NTOUT,621,I,(CURE(I,J),J=1,8)	TAFI
444	CONTINUE	TAFI
C	TOTALS FOR H-AREA TANKS	TAFI
C		TAFI
445	WRITE OUTPUT TAPE NTOUT,622,(HTOT(J),J=1,8)	TAFI
C	WRITE OUTPUT TAPE NTOUT,622,(DUM1(J),J=1,8)	TAFI
	HDM=0.0	TAFI
	DO 446 J=1,13	TAFI
446	HDM=HDM+CURE(34,J)	TAFI
	IF(HDM)447,450,447	TAFI
447	WRITE OUTPUT TAPE NTOUT,625,(CURE(34,J),J=1,8)	TAFI
450	WRITE OUTPUT TAPE NTOUT,626	TAFI
C		TAFI
C	PAGE 2 OF THE FINAL REPORT	TAFI
C		TAFI
	IPG=IPG+1	TAFI
	WRITE OUTPUT TAPE NTOUT,619,IPG,(TAFI(J),J=1,3)	TAFI
	WRITE OUTPUT TAPE NTOUT,623,(ANAM(J),J=9,13)	TAFI
C		TAFI
	DO 451 I=1,8	TAFI
451	WRITE OUTPUT TAPE NTOUT,621,I,(CURE(I,J),J=9,13),TNKS(I),THT(I),	TAFI
	1SUHT(I)	TAFI
	DO 452 I=17,20	TAFI
452	WRITE OUTPUT TAPE NTOUT,621,I,(CURE(I,J),J=9,13),TNKS(I),THT(I),	TAFI
	1SUHT(I)	TAFI
C		TAFI
453	DO 455 I=29,32	TAFI
	T1=0.0	TAFI
	DO 4541 J=1,13	TAFI

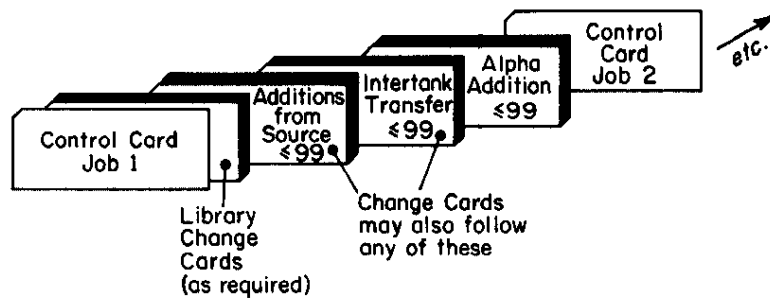
4541	T1=T1+CURE(I,J)	TAFI
	IF(T1)454,455,454	TAFI
454	WRITE OUTPUT TAPE NTOUT,621,I,(CURE(I,J),J=9,13),TNKS(I),THT(I),	TAFI
	ISUHT(I)	TAFI
455	CONTINUE	TAFI
C		
	TOTALS FOR F-AREA	TAFI
	WRITE OUTPUT TAPE NTOUT,622,(FTOT(J),J=9,13),GFT,FT1,FT2	TAFI
	IF(FDM)456,460,456	TAFI
456	WRITE OUTPUT TAPE NTOUT,625,(CURE(33,J),J=9,13),FDM,THT(33),	TAFI
	ISUHT(33)	TAFI
460	CONTINUE	TAFI
C		
	H-AREA TANKS	TAFI
	DO 461 I=9,16	TAFI
461	WRITE OUTPUT TAPE NTOUT,621,I,(CURE(I,J),J=9,13),TNKS(I), THT(I),	TAFI
	ISUHT(I)	TAFI
	DO 462 I=21,24	TAFI
462	WRITE OUTPUT TAPE NTOUT,621,I,(CURE(I,J),J=9,13),TNKS(I),THT(I),	TAFI
	ISUHT(I)	TAFI
C		
	DO 465 I=25,28	TAFI
	T1=0.0	TAFI
	DO 463 J=1,13	TAFI
463	T1=T1+CURE(I,J)	TAFI
	IF(T1)464,465,464	TAFI
464	WRITE OUTPUT TAPE NTOUT ,621,I,(CURE(I,J),J=9,13),TNKS(I),THT(I),	TAFI
	ISUHT(I)	TAFI
465	CONTINUE	TAFI
C		
	WRITE OUTPUT TAPE NTOUT,622,(HTOT(J),J=9,13),GHT,HT1,HT2	TAFI
	WRITE OUTPUT TAPE NTOUT,622,(DUM1(J),J=9,13),GTO,GTHT,GTSU	TAFI
	IF(HDM)467,469,467	TAFI
467	WRITE OUTPUT TAPE NTOUT,625,(CURE(34,J),J=9,13),HDM,THT(34),	TAFI
	ISUHT(34)	TAFI
C		
469	CONTINUE	TAFI
	WRITE OUTPUT TAPE NTOUT,626	TAFI
C		
	PAGE 3	TAFI
C		
470	IPG=IPG+1	TAFI
C		
	WRITE OUTPUT TAPE NTOUT,619,IPG,(TAFI(J),J=1,3)	TAFI
	WRITE OUTPUT TAPE NTOUT,624	TAFI
C		
	DO 471 I=1,8	TAFI
471	WRITE OUTPUT TAPE NTOUT,621,I,(AOSS(I,J),J=1,4)	TAFI
	DO 472 I=17,20	TAFI
472	WRITE OUTPUT TAPE NTOUT,621,I,(AOSS(I,J),J=1,4)	TAFI
C		
	DO 475 I=29,32	TAFI
	T1=0.0	TAFI
	DO 473 J=1,4	TAFI
473	T1=T1 + AOSS(I,J)	TAFI
	IF(T1)474,475,474	TAFI
474	WRITE OUTPUT TAPE NTOUT,621,I,(AOSS(I,J),J=1,4)	TAFI
475	CONTINUE	TAFI
	WRITE OUTPUT TAPE NTOUT,627,(AGN(J),J=1,4)	TAFI
C		
	T1=0.0	TAFI
	DO 476 J=1,4	TAFI
476	T1=T1+AOSS(33,J)	TAFI
	IF(T1)477,478,477	TAFI
477	WRITE OUTPUT TAPE NTOUT,625,(AOSS(33,J),J=1,4)	TAFI
C		
	DO 479 I=9,16	TAFI
479	WRITE OUTPUT TAPE NTOUT,621,I,(AOSS(I,J),J=1,4)	TAFI
	DO 480 I=21,24	TAFI
480	WRITE OUTPUT TAPE NTOUT,621,I,(AOSS(I,J),J=1,4)	TAFI
C		
	DO 484 I=25,28	TAFI
	T1=0.0	TAFI
	DO 481 J=1,4	TAFI
481	T1=T1+AOSS(I,J)	TAFI
	IF(T1)483,484,483	TAFI
483	WRITE OUTPUT TAPE NTOUT,621,I,(AOSS(I,J),J=1,4)	TAFI
484	CONTINUE	TAFI
C		
	WRITE OUTPUT TAPE NTOUT,622,(BGN(J),J=1,4)	TAFI
	WRITE OUTPUT TAPE NTOUT,622,(TGN(J),J=1,4)	TAFI

C	T1=0.0	TAFI
	DO 485 J=1,4	TAFI
485	T1=T1+AOSS(34,J)	TAFI
C	IF(T1)486,487,486	TAFI
486	WRITE OUTPUT TAPE NTOUT,625,(AOSS(34,J),J=1,4)	TAFI
C	487 WRITE OUTPUT TAPE NTOUT,626	TAFI
C		TAFI
C	IF(LIB)495,490,490	TAFI
C	UPDATE THE LIBRARY TAPE	TAFI
C	490 NF2=NF1+1	TAFI
C	WRITE TAPE NTLIB,NF2,YR2,TMT2,DA2,CURE,AOSS,CIS	TAFI
C	495 RETURN	TAFI
C	606 FORMAT(1H1,50X,17HSECRET WORK SHEET/ 50X,3A6,37X,5HPAGE ,12)	TAFI
C	608 FORMAT(I3,11X,1A6,18X,1A6,18X,1A6,18X,1A6/4X,8E12.4/14X,1A6,18X,1A6,18X,1A6,18X,1A6/4X,8E12.4/14X,1A6,18X,6HTOTALS/4X,4E12.4)	TAFI
C	609 FORMAT(1H0,49X,17HSECRET WORK SHEET)	TAFI
C	616 FORMAT(30X, 54H PARTITION FACTORS AND HEAT (BTU/HR.) FOR EACH ISOT 10PE//1X,4HTANK,41X,8HISOTOPES//)	TAFI
C	617 FORMAT(11X,1A6,7X,1A6,6X,5(1A6,7X)/1X,I3,2X,7E13.4/11X,1A6,7X,1A6, 16X,4(1A6,7X)/8X,6E13.4//)	TAFI
C	618 FORMAT(I2,4E9.4)	TAFI
C	619 FORMAT(1H1,80X,6HSECRET,20X,4HPAGE,I3//33X,45HCOMPUTED RADIOACTIVI ITY CONTENT OF WASTE TANKS/46X,3A6//)	TAFI
C	620 FORMAT(5X,4HTANK,6X,8(A6,7X)/6X,3HNO.,46X,6HCURIES)	TAFI
C	621 FORMAT(6X,I2,2X,8E13.4)	TAFI
C	622 FORMAT(10H0 TOTAL,8E13.4//)	TAFI
C	623 FORMAT(5X,4HTANK,6X,1A6,4(7X,1A6),8X,4HTANK,6X,21H HEAT OUTPUT, BT 1U/HR./6X,3HNO.,32X,6HCURIES,34X,5HTOTAL,8X,5HTOTAL,6X,9HSUPERNATE)	TAFI
C	624 FORMAT(27X,15HALPHA EMITTERS /5X,4HTANK,6X,6HU-238,7X,6HU-235,7X, 17HPU-239,4X,11HPU-238-239,7X,3HNO.,4X,10HTHOUS. LB.,7X,3HKG.,10X, 23HKG.,8X,6HCURIES)	TAFI
C	625 FORMAT(10H DEEP MINE/4X,6HCAVERN,8E13.4//)	TAFI
C	626 FORMAT(20X,6HSECRET)	TAFI
C	627 FORMAT(10H0 TOTAL,4E13.4//)	TAFI
C	END(2,0,0,0,0)	

APPENDIX B - Input Data Formats and Sample Problem

The formats and contents of the input data cards are presented in the order in which they would appear in an actual job. Each job(s) requires one set of 13 Isotope Constant cards, one/isotope; a Control card for each job; and the appropriate number of data cards and/or change cards. The required order of the data deck is illustrated below.

Data Deck



A blank Control card indicates end-of-job(s). Isotope constant cards are not considered part of the data deck.

FIGURE 1

Isotope Constants Card - 13 required per job or set of jobs

FORMAT(I2,4E9.4,1A6)

Isotope index (1-13)												
.	E	.	Half-life, days
.	E	.	Yield, fraction
.	E	.	Heat conversion factor
.	E	.	Normal partition factor, fraction in supernate
Isotope name												

FIGURE 2

Control Card - 1 required per job

FORMAT(3A6,E9.4,I3,6F2.0,7I2)

Job identification												
10	E	.	Days to decay tanks (used in PART 1)
File number to be used to start this job												
.	Starting file
.	
.	
.	Output file
.	
.	
.	*Number of changes to concentrations
.	*Number of changes to partition factors
.	*Number of changes to alpha emitters
.	Number of additions to the system
.	Number of intertank transfers
.	Number of additions to alpha emitters
Edit option. Normally +1. If -1, designated file will be edited. If blank or 00, job will be terminated at once.												

*If any of these are used, the cards to effect the changes must immediately follow this Control Card.

FIGURE 3

Addition(s) to the System Card - 1 required per addition in a job
 FORMAT(I2,5E9.4,1A6,I2)

Tank number										Highly enriched										Purex									
E										Burnup										Tons of uranium									
E										Number of tubes										Megawatts/ton									
E										Irradiation time, days																			
E										Power conversion factor										Blank									
E										Days since discharge																			
										Charge identification																			
										Normally 00: *Otherwise change partition																			
										factors for this charge.																			

*This card must then be followed by 2 cards that contain the desired partition factors for this charge.

FIGURE 4

Intertank Transfer Card(s) - 1 required per transfer in a job
 FORMAT(2I2,E9.4,I1)

From tank number																			
To tank number																			
E										Percent of supernate or sludge transferred									
Transfer type																			

1 = Supernate using latest computed partition factors
 2 = *Supernate using changed partition factors
 3 = Sludge using (1.0-latest computed partition factors)
 4 = *Sludge using changed partition factors

*This option requires 2 cards, immediately following this card, that contain the desired partition factors.

FIGURE 5

Addition(s) to Alpha Emitter Card - 1 required per addition in a job

FORMAT(I2,4E9.4)

	Tank number	
.	E	^{238}U , 10^3 lb
.	E	^{235}U , kg
.	E	^{239}Pu , kg
.	E	$^{238-239}\text{Pu}$, curies

FIGURE 6

Change Cards - These 2 cards must immediately follow any option that calls for a change in concentration or partition factors

FORMAT(7X,I2,6E9.4/(7E9.4))

Card 1	b, b, b, b, b, b, b, b	Tank number
	E	^{89}Sr
	E	^{90}Sr
	E	^{90}Y
	E	^{91}Y
	E	^{95}Zr
	E	^{95}Nb
Card 2	E	^{106}Ru
	E	^{106}Rh
	E	^{137}Cs
	E	^{137}Ba
	E	^{144}Ce
	E	^{144}Pr
	E	^{147}Pm

TABLE B-2 - Sample Output

CURIES IN TANKS BEFORE AND AFTER DECAY, IF LESS THAN 10 E-5 SET = 0.0.

TANK	BEFORE	AFTER	BEFORE	AFTER	BEFORE	AFTER	BEFORE	AFTER
1	SR-89		SR-90		Y-90		Y-91	
	0.1000E 04 0.6625E 03		0.1000E 04 0.9980E 03		0.1000E 04 0.9982E 03		0.1000E 04 0.6988E 03	
	ZR-95		NB-95		RU-106		RH-106	
	0.1000E 04 0.7263E 03		0.1000E 04 0.9294E 03		0.1000E 04 0.9452E 03		0.1000E 04 0.9452E 03	
	CS-137		BA-137		CE-144		PR-144	
	0.1000E 04 0.9981E 03		0.1000E 04 0.9183E 03		0.1000E 04 0.9284E 03		0.1000E 04 0.9285E 03	
PM-147		TOTALS						
0.1000E 04 0.9787E 03		0.1300E 05 0.1166E 05						
3	SR-89		SR-90		Y-90		Y-91	
	0.1000E 04 0.6625E 03		0.1000E 04 0.9980E 03		0.1000E 04 0.9982E 03		0.1000E 04 0.6988E 03	
	ZR-95		NB-95		RU-106		RH-106	
	0.1000E 04 0.7263E 03		0.1000E 04 0.9294E 03		0.1000E 04 0.9452E 03		0.1000E 04 0.9452E 03	
	CS-137		BA-137		CE-144		PR-144	
	0.1000E 04 0.9981E 03		0.1000E 04 0.9183E 03		0.1000E 04 0.9284E 03		0.1000E 04 0.9285E 03	
PM-147		TOTALS						
0.1000E 04 0.9787E 03		0.1300E 05 0.1166E 05						
10	SR-89		SR-90		Y-90		Y-91	
	0.1000E 04 0.6625E 03		0.1000E 04 0.9980E 03		0.1000E 04 0.9982E 03		0.1000E 04 0.6988E 03	
	ZR-95		NB-95		RU-106		RH-106	
	0.1000E 04 0.7263E 03		0.1000E 04 0.9294E 03		0.1000E 04 0.9452E 03		0.1000E 04 0.9452E 03	
	CS-137		BA-137		CE-144		PR-144	
	0.1000E 04 0.9981E 03		0.1000E 04 0.9183E 03		0.1000E 04 0.9284E 03		0.1000E 04 0.9285E 03	
PM-147		TOTALS						
0.1000E 04 0.9787E 03		0.1300E 05 0.1166E 05						
12	SR-89		SR-90		Y-90		Y-91	
	0.1000E 04 0.6625E 03		0.1000E 04 0.9980E 03		0.1000E 04 0.9982E 03		0.1000E 04 0.6988E 03	
	ZR-95		NB-95		RU-106		RH-106	
	0.1000E 04 0.7263E 03		0.1000E 04 0.9294E 03		0.1000E 04 0.9452E 03		0.1000E 04 0.9452E 03	
	CS-137		BA-137		CE-144		PR-144	
	0.1000E 04 0.9981E 03		0.1000E 04 0.9183E 03		0.1000E 04 0.9284E 03		0.1000E 04 0.9285E 03	
PM-147		TOTALS						
0.1000E 04 0.9787E 03		0.1300E 05 0.1166E 05						
17	SR-89		SR-90		Y-90		Y-91	
	0.1000E 04 0.6625E 03		0.1000E 04 0.9980E 03		0.1000E 04 0.9982E 03		0.1000E 04 0.6988E 03	
	ZR-95		NB-95		RU-106		RH-106	
	0.1000E 04 0.7263E 03		0.1000E 04 0.9294E 03		0.1000E 04 0.9452E 03		0.1000E 04 0.9452E 03	
	CS-137		BA-137		CE-144		PR-144	
	0.1000E 04 0.9981E 03		0.1000E 04 0.9183E 03		0.1000E 04 0.9284E 03		0.1000E 04 0.9285E 03	
PM-147		TOTALS						
0.1000E 04 0.9787E 03		0.1300E 05 0.1166E 05						
22	SR-89		SR-90		Y-90		Y-91	
	0.1000E 04 0.6625E 03		0.1000E 04 0.9980E 03		0.1000E 04 0.9982E 03		0.1000E 04 0.6988E 03	
	ZR-95		NB-95		RU-106		RH-106	
	0.1000E 04 0.7263E 03		0.1000E 04 0.9294E 03		0.1000E 04 0.9452E 03		0.1000E 04 0.9452E 03	
	CS-137		BA-137		CE-144		PR-144	
	0.1000E 04 0.9981E 03		0.1000E 04 0.9183E 03		0.1000E 04 0.9284E 03		0.1000E 04 0.9285E 03	
PM-147		TOTALS						
0.1000E 04 0.9787E 03		0.1300E 05 0.1166E 05						

SAMPLE PROBLEM

TANK	CURIES		PART. FACT.		TRANSFERS FROM SOURCE				CURIES		PART. FACT.		CURIES		PART. FACT.	
INPUT 2	.1C00E 02	.2000E 02	.1600E 02	.	.2C00E 03	DP	JOB	OPTION	NO.	0	P=	.2000E 03				
	SR-89				SR-90		Y-90					Y-91				
	0.1032E 06	0.2000E-01	0.1048E 05	0.2000E-01	0.1049E 05	0.2000E-01	0.1464E 06	0.2000E-01	0.1464E 06	0.2000E-01						
	ZR-95				NB-95		RU-106					RH-106				
	0.1960E 06	0.2000E-00	0.4246E 06	0.2000E-00	0.1313E 05	0.2000E-00	0.1313E 05	0.2000E-00	0.1313E 05	0.2000E-00						
	CS-137				BA-137		CE-144					PR-144				
	0.1045E 05	0.9500E 00	0.9612E 04	0.9500E 00	0.2414E 06	0.5000E-01	0.2414E 06	0.5000E-01	0.2414E 06	0.5000E-01						
	PM-147				TOTALS											
	0.4006E 05	0.5000E-01	0.1460E 07	0.1460E 07												
INPUT 2	.1C00E 02	.2000E 02	.1600E 02	.	.2C00E 03	DP	JOB	OPTION	NO.	0	P=	.2000E 03				
	SR-89				SR-90		Y-90					Y-91				
	0.1032E 06	0.2000E-01	0.1048E 05	0.2000E-01	0.1049E 05	0.2000E-01	0.1464E 06	0.2000E-01	0.1464E 06	0.2000E-01						
	ZR-95				NB-95		RU-106					RH-106				
	0.1960E 06	0.2000E-00	0.4246E 06	0.2000E-00	0.1313E 05	0.2000E-00	0.1313E 05	0.2000E-00	0.1313E 05	0.2000E-00						
	CS-137				BA-137		CE-144					PR-144				
	0.1045E 05	0.9500E 00	0.9612E 04	0.9500E 00	0.2414E 06	0.5000E-01	0.2414E 06	0.5000E-01	0.2414E 06	0.5000E-01						
	PM-147				TOTALS											
	0.4006E 05	0.5000E-01	0.1460E 07	0.2921E 07												
INPUT 2	.1C00E 02	.2000E 02	.1600E 02	.	.2C00E 03	DP	JOB	OPTION	NO.	0	P=	.2000E 03				
	SR-89				SR-90		Y-90					Y-91				
	0.1032E 06	0.2000E-01	0.1048E 05	0.2000E-01	0.1049E 05	0.2000E-01	0.1464E 06	0.2000E-01	0.1464E 06	0.2000E-01						
	ZR-95				NB-95		RU-106					RH-106				
	0.1960E 06	0.2000E-00	0.4246E 06	0.2000E-00	0.1313E 05	0.2000E-00	0.1313E 05	0.2000E-00	0.1313E 05	0.2000E-00						
	CS-137				BA-137		CE-144					PR-144				
	0.1045E 05	0.9500E 00	0.9612E 04	0.9500E 00	0.2414E 06	0.5000E-01	0.2414E 06	0.5000E-01	0.2414E 06	0.5000E-01						
	PM-147				TOTALS											
	0.4006E 05	0.5000E-01	0.1460E 07	0.4381E 07												
INPUT 2	.1C00E 02	.2000E 02	.1600E 02	.	.2C00E 03	DP	JOB	OPTION	NO.	0	P=	.2000E 03				
	SR-89				SR-90		Y-90					Y-91				
	0.1032E 06	0.2000E-01	0.1048E 05	0.2000E-01	0.1049E 05	0.2000E-01	0.1464E 06	0.2000E-01	0.1464E 06	0.2000E-01						
	ZR-95				NB-95		RU-106					RH-106				
	0.1960E 06	0.2000E-00	0.4246E 06	0.2000E-00	0.1313E 05	0.2000E-00	0.1313E 05	0.2000E-00	0.1313E 05	0.2000E-00						
	CS-137				BA-137		CE-144					PR-144				
	0.1045E 05	0.9500E 00	0.9612E 04	0.9500E 00	0.2414E 06	0.5000E-01	0.2414E 06	0.5000E-01	0.2414E 06	0.5000E-01						
	PM-147				TOTALS											
	0.4006E 05	0.5000E-01	0.1460E 07	0.5842E 07												

SAMPLE PROBLEM

INTERTANK TRANSFERS

AVAILABLE TRANSFERED AVAILABLE TRANSFERED AVAILABLE TRANSFERED AVAILABLE TRANSFERED

INPUT DATA, FROM 1 TO 6 PERCENT MOVED 50.00 OPTION NO. 1

1	SR-89		SR-90		Y-90		Y-91
0.6625E 03	0.6625E 01	0.9980E 03	0.9980E 01	0.9982E 03	0.9982E 01	0.6988E 03	0.6988E 01
ZR-95		NB-95		RU-106		RH-106	
0.7263E 03	0.7263E 02	0.9294E 03	0.9294E 02	0.9452E 03	0.9452E 02	0.9452E 03	0.9452E 02
CS-137		BA-137		CE-144		PR-144	
0.9981E 03	0.4741E 03	0.9183E 03	0.4362E 03	0.9284E 03	0.2321E 02	0.9285E 03	0.2321E 02
PM-147		TOTALS					
0.9787E 03	0.2447E 02	0.1166E 05	0.1369E 04				

PARTITION FACTOR CHANGES FOR TANK 1 EACH ISOTOPE BEFORE AND AFTER THE TRANSFER

0.2000E-01	0.1010E-01	0.2000E-01	0.1010E-01	0.2000E-01	0.1010E-01	0.2000E-01	0.1010E-01
0.2000E-00	0.1111E-00	0.2000E-00	0.1111E-00	0.2000E-00	0.1111E-00	0.2000E-00	0.1111E-00
0.9500E 00	0.9048E 00	0.9500E 00	0.9048E 00	0.5000E-01	0.2564E-01	0.5000E-01	0.2564E-01
0.5000E-01	0.2564E-01						

PARTITION FACTOR CHANGES FOR TANK 6 EACH ISOTOPE BEFORE AND AFTER THE TRANSFER

0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01
0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01
0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01
0.	0.1000E 01						

INPUT DATA, FROM 6 TO 18 PERCENT MOVED 100.00 OPTION NO. 2

2	SR-89		SR-90		Y-90		Y-91
0.6625E 01	0.6625E 01	0.9980E 01	0.9980E 01	0.9982E 01	0.9982E 01	0.6988E 01	0.6988E 01
ZR-95		NB-95		RU-106		RH-106	
0.7263E 02	0.7263E 02	0.9294E 02	0.9294E 02	0.9452E 02	0.9452E 02	0.9452E 02	0.9452E 02
CS-137		BA-137		CE-144		PR-144	
0.4741E 03	0.4741E 03	0.4362E 03	0.4362E 03	0.2321E 02	0.2321E 02	0.2321E 02	0.2321E 02
PM-147		TOTALS					
0.2447E 02	0.2447E 02	0.1369E 04	0.1369E 04				

PARTITION FACTOR CHANGES FOR TANK 6 EACH ISOTOPE BEFORE AND AFTER THE TRANSFER

0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01
0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01
0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01	0.1000E 01
0.1000E 01	0.1000E 01						

PARTITION FACTOR CHANGES FOR TANK 18 EACH ISOTOPE BEFORE AND AFTER THE TRANSFER

0.	0.5000E 02	0.	0.5000E 02	0.	0.5000E 02	0.	0.5000E 02
0.	0.5000E 02	0.	0.5000E 02	0.	0.5000E 02	0.	0.5000E 02
0.	0.5000E 02	0.	0.5000E 02	0.	0.5000E 02	0.	0.5000E 02
0.	0.5000E 02						

SAMPLE PROBLEM

INTERTANK TRANSFERS

AVAILABLE TRANSFERED AVAILABLE TRANSFERED AVAILABLE TRANSFERED AVAILABLE TRANSFERED

INPUT DATA, FROM 10 TO 11 PERCENT MOVED 10.00 OPTION NO. 1

3	SR-89		SR-90		Y-90		Y-91
	0.6625E 03 0.1325E 01	0.9980E 03 0.1996E 01	0.9982E 03 0.1996E 01	0.6988E 03 0.1398E 01			
	ZR-95	NB-95	RU-106	RH-106			
	0.7263E 03 0.1453E 02	0.9294E 03 0.1859E 02	0.9452E 03 0.1890E 02	0.9452E 03 0.1890E 02			
	CS-137	BA-137	CE-144	PR-144			
	0.9981E 03 0.9482E 02	0.9183E 03 0.8723E 02	0.9284E 03 0.4642E 01	0.9285E 03 0.4642E 01			
	PM-147	TOTALS					
	0.9787E 03 0.4893E 01	0.1166E 05 0.2739E 03					

PARTITION FACTOR CHANGES FOR TANK 10 EACH ISOTOPE BEFORE AND AFTER THE TRANSFER

0.2000E-01	0.1804E-01	0.2000E-01	0.1804E-01	0.2000E-01	0.1804E-01	0.2000E-01	0.1804E-01
0.2000E-00	0.1837E-00	0.2000E-00	0.1837E-00	0.2000E-00	0.1837E-00	0.2000E-00	0.1837E-00
0.9500E 00	0.9448E 00	0.9500E 00	0.9448E 00	0.5000E-01	0.4523E-01	0.5000E-01	0.4523E-01
0.5000E-01	0.4523E-01						

PARTITION FACTOR CHANGES FOR TANK 11 EACH ISOTOPE BEFORE AND AFTER THE TRANSFER

0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01
0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01
0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01
0.	0.1000E 01						

INPUT DATA, FROM 12 TO 21 PERCENT MOVED 20.00 OPTION NO. 1

4	SR-89		SR-90		Y-90		Y-91
	0.6625E 03 0.2650E 01	0.9980E 03 0.3992E 01	0.9982E 03 0.3993E 01	0.6988E 03 0.2795E 01			
	ZR-95	NB-95	RU-106	RH-106			
	0.7263E 03 0.2905E 02	0.9294E 03 0.3718E 02	0.9452E 03 0.3781E 02	0.9452E 03 0.3781E 02			
	CS-137	BA-137	CE-144	PR-144			
	0.9981E 03 0.1896E 03	0.9183E 03 0.1745E 03	0.9284E 03 0.9284E 01	0.9285E 03 0.9285E 01			
	PM-147	TOTALS					
	0.9787E 03 0.9787E 01	0.1166E 05 0.5477E 03					

PARTITION FACTOR CHANGES FOR TANK 12 EACH ISOTOPE BEFORE AND AFTER THE TRANSFER

0.2000E-01	0.1606E-01	0.2000E-01	0.1606E-01	0.2000E-01	0.1606E-01	0.2000E-01	0.1606E-01
0.2000E-00	0.1667E-00	0.2000E-00	0.1667E-00	0.2000E-00	0.1667E-00	0.2000E-00	0.1667E-00
0.9500E 00	0.9383E 00	0.9500E 00	0.9383E 00	0.5000E-01	0.4040E-01	0.5000E-01	0.4040E-01
0.5000E-01	0.4040E-01						

PARTITION FACTOR CHANGES FOR TANK 21 EACH ISOTOPE BEFORE AND AFTER THE TRANSFER

0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01
0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01
0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01	0.	0.1000E 01
0.	0.1000E 01						

SAMPLE PROBLEM
PARTITION FACTORS AND HEAT (BTU/HR.) FOR EACH ISOTOPE

TANK	ISOTOPES						
	SR-89	SR-90	Y-90	Y-91	ZR-95	NB-95	RU-106
1	0.1C10E-01 RH-106 0.1111E-00	0.1010E-01 CS-137 0.9048E 00	0.1010E-01 BA-137 0.9048E 00	0.1010E-01 CE-144 0.2564E-01	0.1111E-00 PR-144 0.2564E-01	0.1111E-00 PM-147 0.2564E-01	0.1111E-00
1	0.6428E 01 RH-106 0.2875E 02	0.3359E 01 CS-137 0.1782E 01	0.1799E 02 BA-137 0.7038E 01	0.7056E 01 CE-144 0.1992E 01	0.1111E 02 PR-144 0.2281E 02	0.1338E 02 PM-147 0.1183E 01	0.1701E-00
2	0.2C00E-01 RH-106 0.2000E-00	0.2000E-01 CS-137 0.9500E 00	0.2000E-01 BA-137 0.9500E 00	0.2000E-01 CE-144 0.5000E-01	0.2000E-00 PR-144 0.5000E-01	0.2000E-00 PM-147 0.5000E-01	0.2000E-00
2	0.4C45E 04 RH-106 0.1776E 04	0.1426E 03 CS-137 0.1421E 03	0.7633E 03 BA-137 0.5614E 03	0.5974E 04 CE-144 0.2124E 04	0.1333E 05 PR-144 0.2433E 05	0.2718E 05 PM-147 0.1987E 03	0.1051E 02
3	0.2C00E-01 RH-106 0.2000E-00	0.2000E-01 CS-137 0.9500E 00	0.2000E-01 BA-137 0.9500E 00	0.2000E-01 CE-144 0.5000E-01	0.2000E-00 PR-144 0.5000E-01	0.2000E-00 PM-147 0.5000E-01	0.2000E-00
3	0.6493E 01 RH-106 0.3195E 02	0.3393E 01 CS-137 0.3394E 01	0.1817E 02 BA-137 0.1341E 02	0.7127E 01 CE-144 0.2043E 01	0.1235E 02 PR-144 0.2340E 02	0.1487E 02 PM-147 0.1214E 01	0.1890E-00
6	0.1C00E 01 RH-106 0.1000E 01	0.1000E 01 CS-137 0.1000E 01	0.1000E 01 BA-137 0.1000E 01	0.1000E 01 CE-144 0.1000E 01	0.1000E 01 PR-144 0.1000E 01	0.1000E 01 PM-147 0.1000E 01	0.1000E 01
6	0.1168E-08 RH-106 0.6447E-07	0.8106E-09 CS-137 0.2594E-07	0.4339E-08 BA-137 0.1114E-06	0.1216E-08 CE-144 0.1049E-08	0.3242E-07 PR-144 0.1202E-07	0.3052E-07 PM-147 0.5913E-09	0.3815E-09
10	0.1804E-01 RH-106 0.1837E-00	0.1804E-01 CS-137 0.9448E 00	0.1804E-01 BA-137 0.9448E 00	0.1804E-01 CE-144 0.4523E-01	0.1837E-00 PR-144 0.4523E-01	0.1837E-00 PM-147 0.4523E-01	0.1837E-00
10	0.6480E 01 RH-106 0.3131E 02	0.3386E 01 CS-137 0.3071E 01	0.1813E 02 BA-137 0.1213E 02	0.7113E 01 CE-144 0.2032E 01	0.1210E 02 PR-144 0.2328E 02	0.1457E 02 PM-147 0.1207E 01	0.1853E-00

SAMPLE PROBLEM
PARTITION FACTORS AND HEAT (BTU/HR.) FOR EACH ISOTOPE

TANK	ISOTOPIES						
	SR-89	SR-90	Y-90	Y-91	ZR-95	NB-95	RU-106
11	0.1000E 01 Rf-106 C.1000E 01	0.1000E 01 CS-137 0.1000E 01	0.1000E 01 BA-137 0.1000E 01	0.1000E 01 CE-144 0.1000E 01	0.1000E 01 PR-144 0.1000E 01	0.1000E 01 PM-147 0.1000E 01	0.1000E 01
11	0.1299E-01 Rf-106 0.6390E 00	0.6786E-02 CS-137 0.3224E-00	0.3634E-01 BA-137 0.1274E 01	0.1425E-01 CE-144 0.1021E-01	0.2469E-00 PR-144 0.1170E-00	0.2974E-00 PM-147 0.6068E-02	0.3781E-02
12	0.1606E-01 Rf-106 0.1667E-00	0.1606E-01 CS-137 0.9383E 00	0.1606E-01 BA-137 0.9383E 00	0.1606E-01 CE-144 0.4040E-01	0.1667E-00 PR-144 0.4040E-01	0.1667E-00 PM-147 0.4040E-01	0.1667E-00
12	0.6467E 01 Rf-106 0.3067E 02	0.3380E 01 CS-137 0.2749E 01	0.1810E 02 BA-137 0.1086E 02	0.7099E 01 CE-144 0.2022E 01	0.1185E 02 PR-144 0.2316E 02	0.1428E 02 PM-147 0.1201E 01	0.1815E-00
17	0.2000E-01 Rf-106 0.2000E-00	0.2000E-01 CS-137 0.9500E 00	0.2000E-01 BA-137 0.9500E 00	0.2000E-01 CE-144 0.5000E-01	0.2000E-00 PR-144 0.5000E-01	0.2000E-00 PM-147 0.5000E-01	0.2000E-00
17	0.6493E 01 Rf-106 0.3195E 02	0.3393E 01 CS-137 0.3394E 01	0.1817E 02 BA-137 0.1341E 02	0.7127E 01 CE-144 0.2043E 01	0.1235E 02 PR-144 0.2340E 02	0.1487E 02 PM-147 0.1214E 01	0.1890E-00
18	0.5000E 02 Rf-106 0.5000E 02	0.5000E 02 CS-137 0.5000E 02	0.5000E 02 BA-137 0.5000E 02	0.5000E 02 CE-144 0.5000E 02	0.5000E 02 PR-144 0.5000E 02	0.5000E 02 PM-147 0.5000E 02	0.5000E 02
18	0.6493E-01 Rf-106 0.3195E 01	0.3393E-01 CS-137 0.1612E 01	0.1817E-00 BA-137 0.6368E 01	0.7127E-01 CE-144 0.5106E-01	0.1235E 01 PR-144 0.5849E 00	0.1487E 01 PM-147 0.3034E-01	0.1890E-01
21	0.1000E 01 Rf-106 C.1000E 01	0.1000E 01 CS-137 C.1000E 01	0.1000E 01 BA-137 0.1000E 01	0.1000E 01 CE-144 0.1000E 01	0.1000E 01 PR-144 0.1000E 01	0.1000E 01 PM-147 0.1000E 01	0.1000E 01
21	0.2597E-01 Rf-106 0.1278E 01	0.1357E-01 CS-137 0.6448E 00	0.7267E-01 BA-137 0.2547E 01	0.2851E-01 CE-144 0.2043E-01	0.4939E-00 PR-144 0.2340E-00	0.5948E 00 PM-147 0.1214E-01	0.7562E-02
22	0.2000E-01 Rf-106 0.2000E-00	0.2000E-01 CS-137 0.9500E 00	0.2000E-01 BA-137 0.9500E 00	0.2000E-01 CE-144 0.5000E-01	0.2000E-00 PR-144 0.5000E-01	0.2000E-00 PM-147 0.5000E-01	0.2000E-00
22	0.6493E 01 Rf-106 0.3195E 02	0.3393E 01 CS-137 0.3394E 01	0.1817E 02 BA-137 0.1341E 02	0.7127E 01 CE-144 0.2043E 01	0.1235E 02 PR-144 0.2340E 02	0.1487E 02 PM-147 0.1214E 01	0.1890E-00

COMPUTED RADIOACTIVITY CONTENT OF WASTE TANKS
SAMPLE PROBLEM

TANK NO.	SR-89	SR-90	Y-90	Y-91 CURIES	ZR-95	NB-95	RU-106	RH-106
1	0.6559E 03	0.9880E 03	0.9882E 03	0.6918E 03	0.6536E 03	0.8365E 03	0.8507E 03	0.8507E 03
2	0.4127E 06	0.4193E 05	0.4194E 05	0.5857E 06	0.7839E 06	0.1699E 07	0.5254E 05	0.5254E 05
3	0.6625E 03	0.9980E 03	0.9982E 03	0.6988E 03	0.7263E 03	0.9294E 03	0.9452E 03	0.9452E 03
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.1192E-06	0.2384E-06	0.2384E-06	0.1192E-06	0.1907E-05	0.1907E-05	0.1907E-05	0.1907E-05
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
17	0.6625E 03	0.9980E 03	0.9982E 03	0.6988E 03	0.7263E 03	0.9294E 03	0.9452E 03	0.9452E 03
18	0.6625E 01	0.9980E 01	0.9982E 01	0.6988E 01	0.7263E 02	0.9294E 02	0.9452E 02	0.9452E 02
19	0.	0.	0.	0.	0.	0.	0.	0.
20	0.	0.	0.	0.	0.	0.	0.	0.
TOTAL	0.4147E 06	0.4493E 05	0.4494E 05	0.5878E 06	0.7861E 06	0.1701E 07	0.5538E 05	0.5538E 05
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.6612E 03	0.9960E 03	0.9962E 03	0.6974E 03	0.7117E 03	0.9108E 03	0.9263E 03	0.9263E 03
11	0.1325E 01	0.1996E 01	0.1996E 01	0.1398E 01	0.1453E 02	0.1859E 02	0.1890E 02	0.1890E 02
12	0.6599E 03	0.9940E 03	0.9942E 03	0.6960E 03	0.6972E 03	0.8923E 03	0.9074E 03	0.9074E 03
13	0.	0.	0.	0.	0.	0.	0.	0.
14	0.	0.	0.	0.	0.	0.	0.	0.
15	0.	0.	0.	0.	0.	0.	0.	0.
16	0.	0.	0.	0.	0.	0.	0.	0.
21	0.2650E 01	0.3992E 01	0.3993E 01	0.2795E 01	0.2905E 02	0.3718E 02	0.3781E 02	0.3781E 02
22	0.6625E 03	0.9980E 03	0.9982E 03	0.6988E 03	0.7263E 03	0.9294E 03	0.9452E 03	0.9452E 03
23	0.	0.	0.	0.	0.	0.	0.	0.
24	0.	0.	0.	0.	0.	0.	0.	0.
TOTAL	0.1988E 04	0.2994E 04	0.2995E 04	0.2096E 04	0.2179E 04	0.2788E 04	0.2836E 04	0.2836E 04
TOTAL	0.4167E 06	0.4792E 05	0.4793E 05	0.5899E 06	0.7883E 06	0.1704E 07	0.5821E 05	0.5821E 05

COMPUTED RADIOACTIVITY CONTENT OF WASTE TANKS
SAMPLE PROBLEM

TANK NO.	CS-137	BA-137	CE-144 CURIES	PR-144	PM-147	TANK TOTAL	HEAT OUTPUT, BTU/HR. TOTAL SUPERNATE
1	0.5240E 03	0.4821E 03	0.9052E 03	0.9053E 03	0.9542E 03	0.1029E 05	0.1231E 03
2	0.4179E 05	0.3845E 05	0.9656E 06	0.9657E 06	0.1603E 06	0.5842E 07	0.8058E 05
3	0.9981E 03	0.9183E 03	0.9284E 03	0.9285E 03	0.9787E 03	0.1166E 05	0.1380E 03
4	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.
6	0.7629E-05	0.7629E-05	0.4768E-06	0.4768E-06	0.4768E-06	0.2503E-04	0.2863E-06
7	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.
17	0.9981E 03	0.9183E 03	0.9284E 03	0.9285E 03	0.9787E 03	0.1166E 05	0.1380E 03
18	0.4741E 03	0.4362E 03	0.2321E 02	0.2321E 02	0.2447E 02	0.1369E 04	0.1493E 02
19	0.	0.	0.	0.	0.	0.	0.
20	0.	0.	0.	0.	0.	0.	0.
TOTAL	0.4479E 05	0.4120E 05	0.9684E 06	0.9685E 06	0.1632E 06	0.5877E 07	0.8099E 05
9	0.	0.	0.	0.	0.	0.	0.
10	0.9033E 03	0.8310E 03	0.9238E 03	0.9238E 03	0.9738E 03	0.1138E 05	0.1350E 03
11	0.9482E 02	0.8723E 02	0.4642E 01	0.4642E 01	0.4893E 01	0.2739E 03	0.2987E 01
12	0.8085E 03	0.7438E 03	0.9192E 03	0.9192E 03	0.9689E 03	0.1111E 05	0.1320E 03
13	0.	0.	0.	0.	0.	0.	0.
14	0.	0.	0.	0.	0.	0.	0.
15	0.	0.	0.	0.	0.	0.	0.
16	0.	0.	0.	0.	0.	0.	0.
21	0.1896E 03	0.1745E 03	0.9284E 01	0.9285E 01	0.9787E 01	0.5477E 03	0.5973E 01
22	0.9981E 03	0.9183E 03	0.9284E 03	0.9285E 03	0.9787E 03	0.1166E 05	0.1380E 03
23	0.	0.	0.	0.	0.	0.	0.
24	0.	0.	0.	0.	0.	0.	0.
TOTAL	0.2994E 04	0.2755E 04	0.2785E 04	0.2785E 04	0.2936E 04	0.3497E 05	0.4140E 03
TOTAL	0.4778E 05	0.4396E 05	0.9712E 06	0.9712E 06	0.1661E 06	0.5912E 07	0.8140E 05

COMPUTED RADIOACTIVITY CONTENT OF WASTE TANKS
SAMPLE PROBLEM

TANK NO.	ALPHA EMITTERS			
	U-238, THOUS. LB.	U-235, KG.	PU-239, KG.	PU-238-239, CURIES
1	0.5000E 01	0.1500E 01	0.1200E 01	0.1333E 04
2	0.	0.	0.	0.
3	0.	0.	0.	0.
4	0.	0.	0.	0.
5	0.	0.	0.	0.
6	0.	0.	0.	0.
7	0.	0.	0.	0.
8	0.	0.	0.	0.
17	0.	0.	0.	0.
18	0.	0.	0.	0.
19	0.	0.	0.	0.
20	0.	0.	0.	0.
TOTAL	0.5000E 01	0.1500E 01	0.1200E 01	0.1333E 04
9	0.	0.	0.	0.
10	0.	0.	0.	0.
11	0.	0.	0.	0.
12	0.5000E 01	0.1500E 01	0.1200E 01	0.1333E 04
13	0.	0.	0.	0.
14	0.	0.	0.	0.
15	0.	0.	0.	0.
16	0.	0.	0.	0.
21	0.	0.	0.	0.
22	0.	0.	0.	0.
23	0.	0.	0.	0.
24	0.	0.	0.	0.
TOTAL	0.5000E 01	0.1500E 01	0.1200E 01	0.1333E 04
TOTAL	0.1000E 02	0.3000E 01	0.2400E 01	0.2666E 04

SAMPLE PROBLEM

SUMMARY SHEET FOR THIS JOB.

TANKS DECAYED FOR 30. DAYS
 FILE NUMBER 0 WITH THIS DATE 0./ 0./ 0. WAS USED AS THE STARTING POINT
 FILE NUMBER 1 WITH THIS DATE 65./ 2./20. SHOULD BE USED AS THE STARTING POINT FOR THE NEXT JOB.
 THE CURIES IN THE LIBRARY FILE WERE CHANGED 6 TIMES
 THE PARTITION FACTORS WERE CHANGED 6 TIMES
 THE ALPHA EMITTERS WERE CHANGED 0 TIMES
 THERE WERE 4 CHARGES ADDED TO THE SYSTEM
 THERE WERE 4 INTERTANK TRANSFERS
 THERE WERE 2 ADDITIONS TO THE ALPHA EMITTERS