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Addendum  
DP-1488ELECTRICAL RESISTIVITIES OF GLASS MELTS  
CONTAINING SIMULATED SRP WASTE SLUDGES

This addendum corrects the resistivities given in DP-1488 (issued 8/78) for Frit 21 glass melts. The experimental data in DP-1488 are corrected in this addendum for the resistance that is developed at high temperatures by the platinum wires in the resistivity probe (Table 1). Earlier treatments of the resistivity data erroneously assumed that this correction was unimportant. However, for the more conductive melts, the reported resistivities were reduced by about 50% at 1150°C and about 10% at 800°C. Corrected curves for Frit 18 melts are not included in this addendum because this frit is no longer being considered for solidifying Savannah River Plant waste. Probe resistivities in Table 1 can be used to correct the Frit 18 curves in DP-1488. A resistivity curve for Frit 411\*, the newest candidate frit for solidifying waste sludge, is included in this addendum. Frit 411 was not discussed in DP-1488.

TABLE 1

## Resistivity of Probe Used in SRL Measurements

Temperature, °C	Resistivity, ohm-cm
1200	3.6
1150	3.5
1100	3.4
1050	3.3
1000	3.3
923	3.2
884	3.2
844	3.1
804	3.0
763	2.8

\* The composition of Frit 411 is SiO<sub>2</sub>, 58.3; Na<sub>2</sub>O, 12.5; B<sub>2</sub>O<sub>3</sub>, 11.1; CaO, 5.6, Li<sub>2</sub>O, 12.5 wt %.

The description of the effects of waste components on resistivity that is given in DP-1488 is unchanged because subtracting the probe resistance from the original data does not affect the ordering of the corrected curves (Figures 1-4). Correlations between resistivity and viscosity are also essentially unchanged. Ordinates (resistivities) in Figures 12 and 13 (in DP-1488) would change with the corrected values, and slopes of the lines in the figures would change slightly.

To facilitate comparing the corrected resistivities with previously published melt viscosities, the experimental data shown in Figure 1-4 were fit to the same function used to fit the viscosity data.<sup>1</sup>

$$\ln \rho = A + \frac{B}{T-T_0} \quad (1)$$

Expanding the last term leads to the polynomial form used in DP-1488. Coefficients to Fit Equation 1 to data in Figures 1-4 are listed in Table 2.

**TABLE 2**

**Constants for Fitting Resistivity Curves of Frit 21 Glasses**

$$\ln \rho = A + B/(T-T_0) \quad (\rho \text{ in ohm-cm, } T \text{ in } ^\circ\text{K})$$

<u>Sludge</u>	<u>Amount, wt %</u>	<u>A</u>	<u>B</u>	<u>T<sub>0</sub></u>
Composite	25	-5.84	8545	202
	30	-5.93	9610	96.9
	35	-6.06	10559	14.3
Average	25	-3.02	4054	431
	35	-2.92	3470	538
High Fe	25	-2.97	3644	545
	35	-3.09	3539	539
High Al	25	-2.97	4078	480
	35	-3.63	4678	480
Pure Frit 21	-	-1.60	2132	577

1. M. J. Plodinec. **Viscosity of Glasses Containing Simulated Savannah River Plant Waste.** USDOE Report DP-1507, Savannah River Laboratory, E. I. du Pont de Nemours and Company, Aiken, S. C. (1978).

Figure 5 shows resistivity curves of Frit 411 glass measured by four investigators. Battelle Pacific Northwest Labs (PNL) and SRL curves were measured by the technique described in DP-1488. The method used by Owens-Corning Fiberglas (OCF) was not given. The SRL-TNX curve was measured with an operating, small-scale, electric melter. While the SRL-TNX curve is fairly close to the other curves, current density at an electrode can greatly affect resistivity. Therefore resistivities experienced in a large melter operating at high current densities may be appreciably different from those measured in laboratory apparatus.

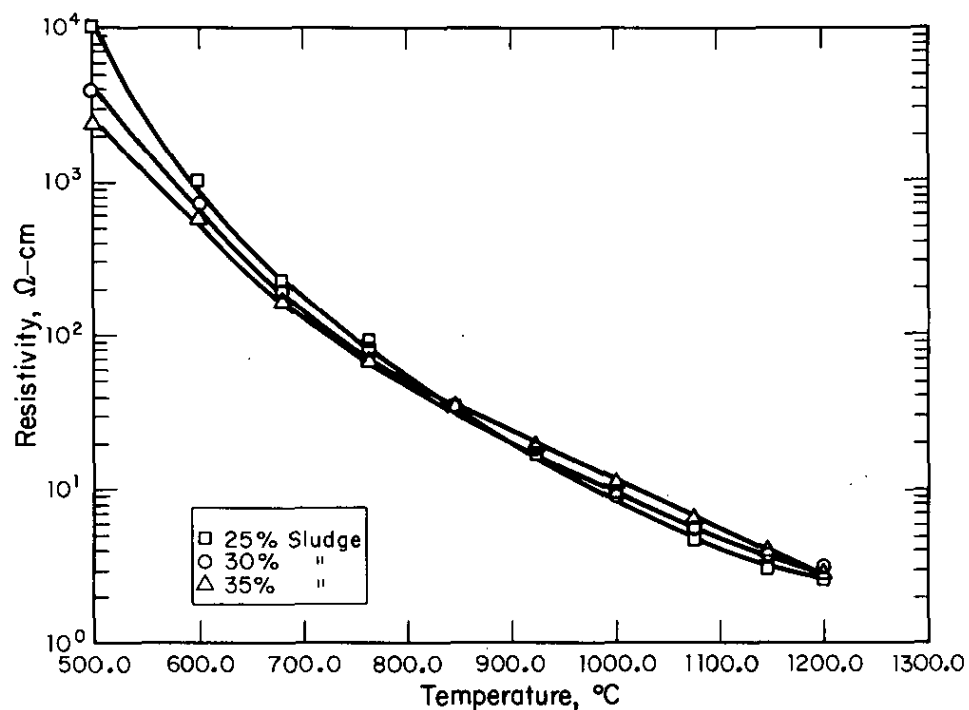


FIGURE 1. Resistivity of Frit 21 Melts Containing Composite Sludge

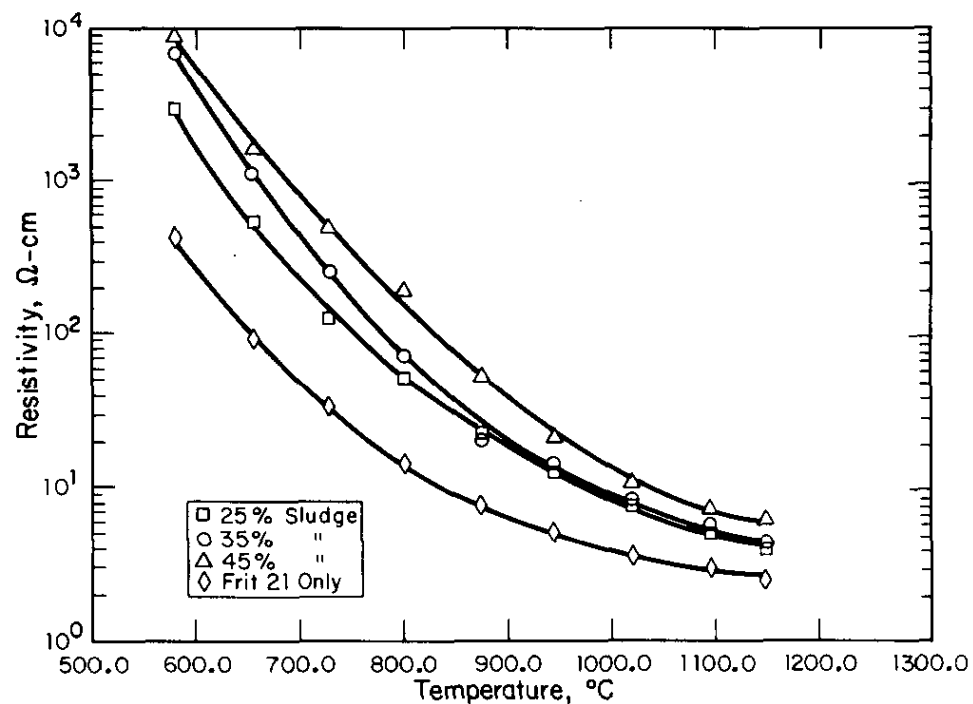


FIGURE 2. Resistivity of Frit 21 Melts Containing Average Sludge

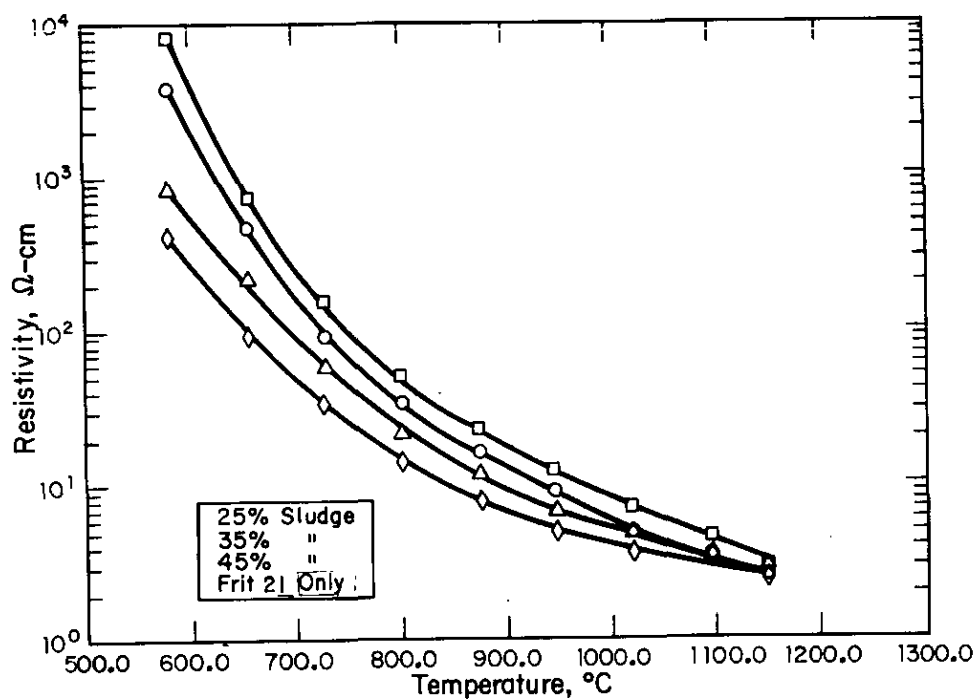


FIGURE 3. Resistivity of Frit 21 Melts Containing High-Iron Sludge

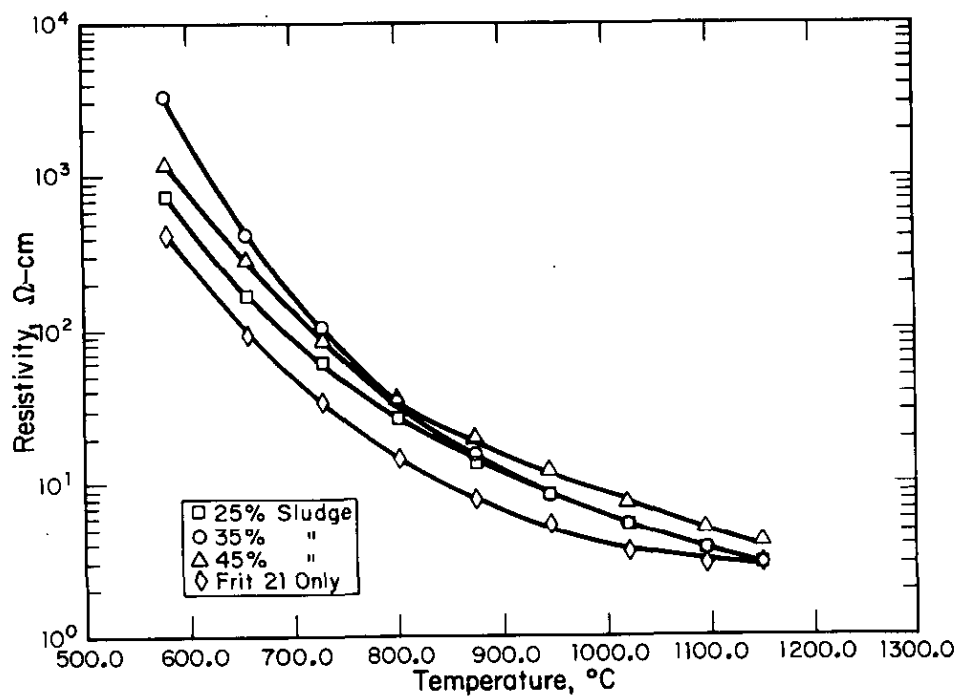


FIGURE 4. Resistivity of Frit 21 Melts Containing High-Aluminum Sludge

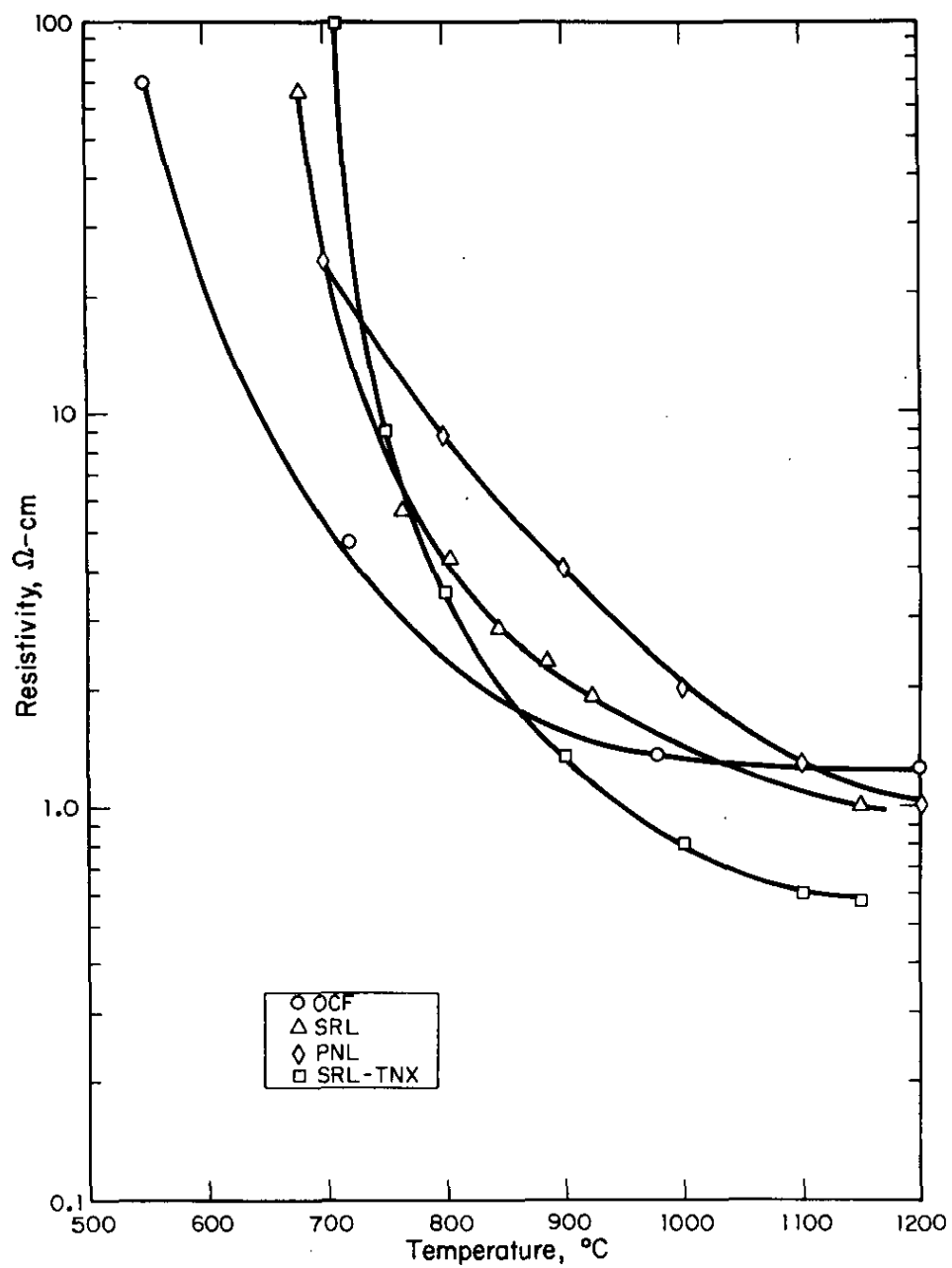


FIGURE 5. Resistivities of Pure Frit 411 Melts by Four Investigations