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AEC RESEARCH AND DEVELOPMENT REPORT

# PROPERTIES OF THULIUM METAL AND OXIDE

P. K. SMITH  
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C. L. ANGERMAN

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*Savannah River Laboratory*

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## PROPERTIES OF THULIUM METAL AND OXIDE

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## ABSTRACT

The properties of thulium metal and thulium oxide were surveyed to establish specifications for reactor target materials for experimental production of  $^{170}\text{Tm}$  for isotopic power source applications. Radiation characteristics and chemical, thermophysical, and mechanical properties are presented that are pertinent to the use of the activated targets without reprocessing after irradiation.

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## INTRODUCTION

Thulium-170 and thulium-171 are promising heat sources for isotopic power generators. Thulium-170, a  $\beta$ -emitter with a half-life of 128 days, can be made by irradiating natural  $^{169}\text{Tm}$ . No separations, fuel compound synthesis, or fuel form fabrication are required after irradiation; the irradiated  $^{169}\text{Tm}$  target can be used directly as a heat source fuel. Thulium-171, a  $\beta$ -emitter with a half-life of 1.9 years, can be made by irradiating  $^{169}\text{Tm}$  at high flux or by irradiating erbium enriched in  $^{170}\text{Er}$ ; in the former case the  $^{170}\text{Tm}$  may be allowed to decay to increase the 171/170 ratio, and in the latter case chemical separation is required following irradiation.

The Savannah River Laboratory is developing technology for production of  $^{170}\text{Tm}$ . In an initial test, thulium oxide was irradiated to 2.48 w/g in the Savannah River high flux demonstration. In subsequent work, both thulium oxide and thulium metal are being irradiated to evaluate cost and production parameters and to provide material for testing and evaluation.

In the course of work to establish specifications suitable for  $^{169}\text{Tm}$  target materials for the irradiation studies, a detailed literature survey was made of the properties of thulium oxide and thulium metal applicable to the direct utilization of the irradiated target materials as heat source fuels. The information obtained is presented in the following data compilation.

For the most part, the thermal and mechanical properties reported here are for unirradiated natural thulium. Many of the properties have not been determined, but some could be calculated or estimated reliably from information on related and similar rare earths. The source of each datum is referenced; if calculated or estimated by the authors, the method is indicated. An attempt is made to evaluate the uncertainty in certain critical properties.

## SUMMARY

Thulium sesquioxide, with an estimated melting point of  $2375^{\circ}\text{C}$ , is well suited as a target material for production of  $^{170}\text{Tm}$  to be used subsequently in high-temperature isotopic heat sources. The oxide is readily available in adequate purity and can be fabricated to high-density solid forms before irradiation. It is highly refractory; inert in oxidizing, vacuum, or reducing environments; and is potentially nonreactive with refractory metal containers up to  $2000^{\circ}\text{C}$ .

Thulium metal, with a melting point of  $1545^{\circ}\text{C}$ , is a convenient target material, but may be limited to lower temperature heat-source applications.

## PROPERTIES

Thulium-170 Half-Life:  $128 \pm 1\text{d}$

Thulium-171 Half-Life:  $700 \pm 5\text{d}$

Ref.

2,3

3

### A. THULIUM METAL

#### 1. Composition

- a. Radionuclide Abundance (calculated for an arbitrarily selected flux of  $4 \times 10^{14} \text{ n}/(\text{cm}^2)(\text{sec})$  at reactor discharge for  $^{169}\text{Tm}$  irradiation).

4

Isotope	Specific Activity, w/g $\rightarrow$	Concentration, wt %		
		0.62	2.24	2.94
$^{169}\text{Tm}$		95.3	77.9	60.6
$^{170}\text{Tm}$		4.7	16.3	21.5
$^{171}\text{Tm}$		-	2.9	8.4
$^{170}\text{Yb}$		-	2.9	9.0
$^{171}\text{Yb}$		-	-	0.5



b. Chemical Impurities (commercial samples before irradiation)

Elements not listed were <0.001 wt % or were not detected by the spark-source emission spectrograph. Variation in product is within 10X.

<u>Element</u>	<u>Wt %</u>
Ta	0.107
Yb	.0046
Er	.030
Ho	.0030
Dy	.0010
Tb	.0028
Gd	.063
Nd	.021
La	.0025
Y	.0053
Ni	.0155
Fe	.033
Mn	.0033
Cr	.010
Ti	.0012
Ca	.071
Si	.0055
Al	.0016
Mg	.014
F	0.0034

Ref.

4

2. Specific Power

- 2 to 3 w/g of metal at reactor discharge is feasible
- 900 to 1400 Ci/g of metal at reactor discharge is feasible
- 445 ±2 Ci/w of <sup>170</sup>Tm measured on typical irradiated wafers

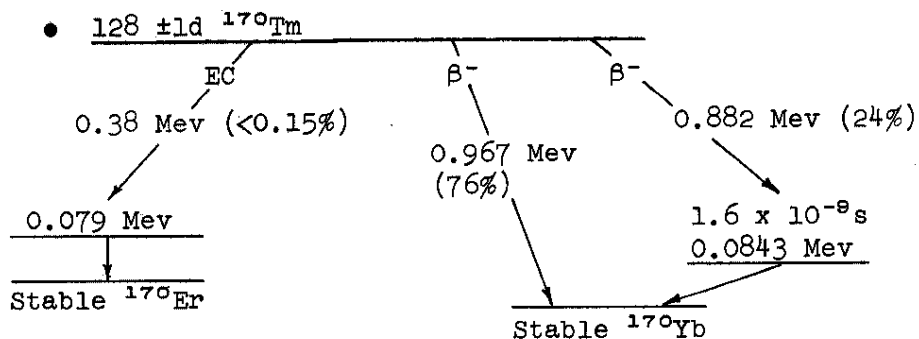
1,4

1,4

4

### 3. Radiation

#### a. $^{170}\text{Tm}$ and $^{171}\text{Tm}$ Decay Processes



#### 1) Internal Conversion of $^{170}\text{Tm}$ Gamma

87% of the 0.0843 Mev gamma is internally converted.  
Conversion coefficients:

$$\alpha_K = 1.38 \pm 0.04 \text{ (59.7 and 52.0 kev);}$$

$$1.47 \pm 0.07; 1.32 \pm 0.05$$

$$\alpha_L = 4.1 \pm 0.5 \text{ (8 kev); } 4.11 \pm 0.21$$

$$\alpha_M = 1.2 \pm 0.2$$

$$\alpha_M + N + \dots = 1.38 \pm 0.08$$

$$I_K = 4.9 \pm 0.5\%/\beta\text{-disintegration;}$$

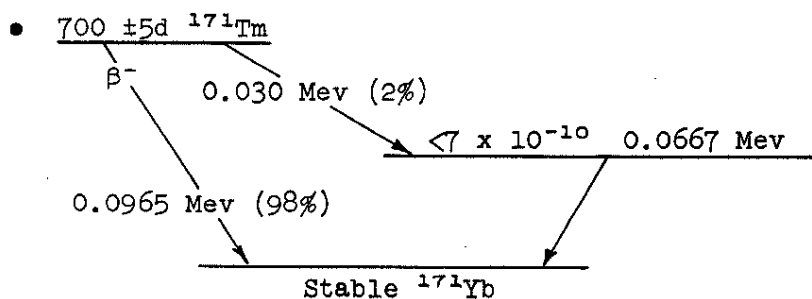
$$I_{(L+M)} = 16 \pm 2\%/\beta\text{-disintegration;}$$

$$I_Y = 3.1 \pm 0.3\%/\beta\text{-disintegration.}$$

Ref.

5,6  
7,8

9,10  
11



Ref.  
5,6  
7,8

2) Internal Conversion of  $^{171}\text{Tm}$  Gamma

Over 87% of the 0.0667 Mev gamma is internally converted.

$$\alpha_K = 6.5 \pm 0.9$$

Ref.  
8

b. Radiation by Particle and Type

1) Alpha particles

None

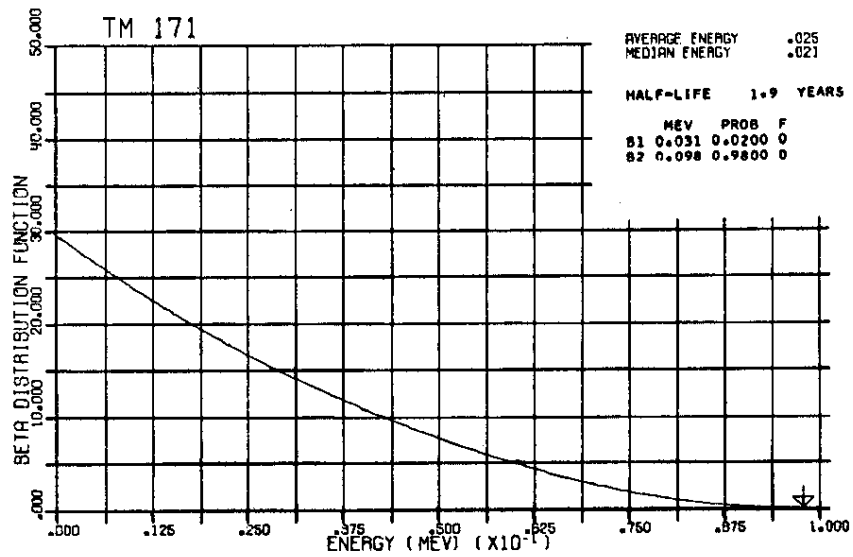
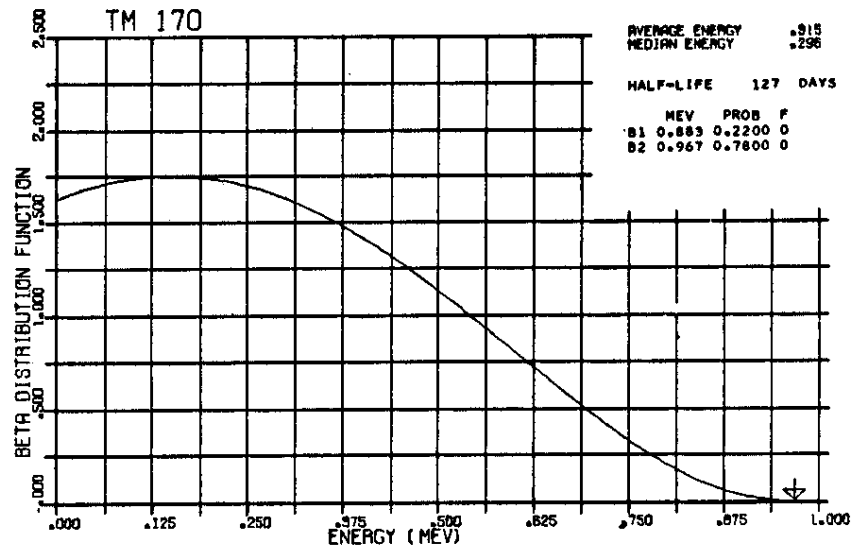
2) Beta particles

2,4,7  
12,13

Isotope	Max Energy, Mev	Abundance, %	Average Energy, Mev		Milliwatts/Curie	
			Calc	Meas	Calc	Meas
$^{170}\text{Tm}$	0.969	76	0.33	0.315	1.91	$2.25 \pm 0.10$
	0.885	24	0.30			
$^{171}\text{Tm}$	0.097	98	0.029	0.025	0.17	
	0.03	2	0.01			

• Calculated Beta Spectrum

Ref.  
14



3) Gamma

Isotope	Max Energy, Mev	Abundance, %	Milliwatts/Curie, calculated	Photons watts sec
$^{170}\text{Tm}$	0.0843	3.4	0.02	$3.2 \times 10^{12}$
$^{171}\text{Tm}$	0.0667	1	0.008	$1.86 \times 10^{11}$

4) Bremsstrahlung

Bremsstrahlung is the principal contributor to radiation doses. Energy distributions calculated for  $^{170}\text{Tm}$  and  $^{171}\text{Tm}$  oxide are shown in Section B,3,a. The metal would show a similar distribution.

5) Neutrons

None

## 4. Interaction with Materials of Containment

15

No direct measurements are available for interaction with materials of construction for containers. Estimates of the extent of interaction cannot be made easily because of the lack of pertinent phase diagrams and diffusion data.

Material	Interaction
Ta	Probably nonreactive; no intermetallic compounds; occurrence of low-melting eutectics not investigated.
Re,Ru,Os	Reactivity dependent on rate of growth of known intermetallic compounds; occurrence of low-melting eutectics not investigated.
W,Mo,Cr	Occurrence of intermetallic compounds or low-melting eutectics have not been investigated.
"Super-alloys"	Reactivity dependent on rate of growth of known intermetallic compounds, such as $\text{TmFe}$ , $\text{TmCo}_2$ and $\text{TmNi}_2$ ; occurrence of low-melting eutectics not investigated.

## 5. Thermophysical Properties

a. Density

9.318 g/cc, X-ray

16

9.135 g/cc, measured on commercial samples

4

(Section A,1,b.)

b. Coefficient of Thermal Expansion

$$\bar{\alpha} = 12.4 \times 10^{-6}/^{\circ}\text{C} \text{ (20 to } 853^{\circ}\text{C)}$$

The lattice constants increase as follows:

$$a = 3.5372 + 3.19 \times 10^{-5}t - 1.41 \times 10^{-8}t^2 + 1.19 \times 10^{-11}t^3$$

$$c = 5.5619 + 12.51 \times 10^{-5}t - 3.89 \times 10^{-8}t^2 + 3.27 \times 10^{-11}t^3$$

The lattice constants are in Angstroms and the temperature is in  $^{\circ}\text{C}$  ( $20^{\circ}$  to  $853^{\circ}\text{C}$ )

c. Specific Heat and Enthalpy

See Table 1.

$$\begin{aligned} H_T^{\circ} - H_{298.15}^{\circ} &= -1712 + 5.408T + 11.52T^2 - 0.65T^3 \\ &\quad (298 \text{ to } 1818^{\circ}\text{K}) \\ &= -2418 + 9.890T \quad (1818 \text{ to } 1863^{\circ}\text{K}) \end{aligned}$$

Debye temperature:  $167^{\circ}\text{K}$

Gruneisen constant: 0.94

TABLE 1

Thermodynamic Properties of Thulium					
$^{\circ}\text{K}$	$H_T^{\circ} - H_{298.15}^{\circ}$ (cal/mole)	$C_P$ (cal/mole-deg)	$S_T^{\circ}$ (cal/mole-deg)	$(H_T^{\circ} - H_{298.15}^{\circ})/T$ (cal/mole-deg)	$(G_T^{\circ} - H_{298.15}^{\circ})/T$ (cal/mole-deg)
Thulium					
298.15	0	6.07	17.371	0	17.37
300	12	6.08	17.41	0.04	17.37
400	631	6.30	19.19	1.58	17.61
500	1,272	6.51	20.62	2.54	18.07
600	1,933	6.72	21.83	3.22	18.60
700	2,616	6.93	22.88	3.74	19.14
800	3,318	7.13	23.82	4.15	19.67
900	4,041	7.33	24.66	4.49	20.17
1000	4,783	7.52	25.44	4.78	20.66
1100	5,544	7.71	26.17	5.04	21.13
1200	6,324	7.89	26.85	5.27	21.58
1300	7,123	8.08	27.49	5.48	22.01
1400	7,939	8.25	28.10	5.67	22.43
1500	8,773	8.43	28.67	5.85	22.82
1600	9,624	8.60	29.22	6.02	23.21
1700	10,492	8.77	29.74	6.17	23.57
1800	11,377	8.93	30.25	6.32	23.93
1818	11,537	8.96	30.34	6.35	23.99
1818	15,562	9.89	32.55	8.56	23.99
1900	16,373	9.89	32.99	8.62	24.37

d.	<u>Temperatures of Phase Transformations</u>	Ref.
	Melting point: $1545 \pm 5^{\circ}\text{C}$	20
	Investigations of Tm-Mg alloys indicate a possible transformation from hcp to bcc ( $a_0 = 3.92 \text{ \AA}$ ) near $1300^{\circ}\text{C}$ .	21
e.	<u>Latent Heats of Phase Transformations</u>	
	$\Delta H_{\text{fusion}}: 4.025 \text{ kcal/mole}$	18
	$\Delta S_{\text{fusion}}: 2.21 \text{ eu}$	18
	$\Delta H_{\text{subl}}: 57.44 \pm 0.20 \text{ kcal/mole}$ ( $809^{\circ}$ to $1219^{\circ}\text{K}$ )	22
	$\Delta H_{\text{vap}(298)}: 59.1 \text{ kcal/mole}$	22, 23
	$\Delta S_{\text{vap}(298)}: 28 \pm 2 \text{ eu}$	
f.	<u>Vapor Pressure</u>	
	$\text{Log } P_{\text{mm}} = (12552 \pm 45)/T + (9.1761 \pm 0.0457)$ (T in $^{\circ}\text{K}$ )	22
g.	<u>Thermal Conductivity</u>	
	$0.023 \pm 0.005 \text{ (cal-cm)/(sec)(cm}^2\text{)(}^{\circ}\text{C)}$ at 26 to $30^{\circ}\text{C}$ , estimated from data on other rare earth metals.	15
h.	<u>Thermal Diffusivity</u>	15
	$0.069 \pm 0.015 \text{ cm}^2\text{/sec}$ at 26 to $30^{\circ}\text{C}$ , calculated from the estimate of thermal conductivity.	
i.	<u>Viscosity</u>	
	Unknown	
j.	<u>Surface Tension</u>	
	Unknown	
k.	<u>Total Hemispherical Emittance</u>	
	Unknown	
l.	<u>Spectral Emissivity</u>	
	Unknown	

m.	<u>Crystallography</u>	Ref. 16
	Hexagonal: $a_o = 3.5375 \pm 0.0001 \text{ \AA}$	
	$c_o = 5.5546 \pm 0.0004 \text{ \AA}$	
	A3 structure, magnesium type	
n.	<u>Solubilities</u>	24
	Insoluble in water.	
o.	<u>Diffusion Rates</u>	
	Unknown.	
p.	<u>Electrical Characteristics</u>	
	Electrical Resistivity: $90 \times 10^{-8} \text{ (ohm)(cm)}$ at $25^\circ\text{C}$	15
	Hall Coefficient: $-1.8 \times 10^{-12} \frac{\text{(volt)(cm)}}{\text{(amp)(Oer)}}$ at $25^\circ\text{C}$	25
	Work function: 3.12 ev	15
	Electronegativity: 1.22	15
<b>6. Mechanical Properties</b>		
a.	<u>Hardness</u>	
	48 kg/mm <sup>2</sup> (Vickers DPH)	15
	69 Rockwell H	15
	53 kg/mm <sup>2</sup> (Brinell, arc melted)	26
b.	<u>Strength</u>	
	The following values of tensile properties are estimated by comparison with data for other rare earths, as given in Reference 15.	15
	• Proportional limit (0.2% offset):	
	30,000 to 44,000 psi	



- Ultimate tensile strength:  
29,000 to 44,000 psi (in tension)  
~51,800 psi (in compression)
- Elongation: 1 to 5% in tension  
20% in compression
- Young's Modulus: 11,500,000 psi
- Shear Modulus: 4,400,000 psi
- Poisson's ratio: 0.24

Compression values are as follows.

- Ultimate strength: 110,000 psi
- Yield strength (0.2%): 20,300 psi
- Modules of compression: 5,500,000 psi

c. Compressibility

$$\frac{\Delta V}{V_0} = 2.579 \times 10^{-6}(P-P_0) + 2.160 \times 10^{-11}(P-P_0)^2 - 1.527 \times 10^{-18}(P-P_0)^3. \quad (P \text{ is in kg/cm}^2)$$

$$P_0 = 0$$

$$P_{\max} = 40,000 \text{ kg/cm}^2$$

$$\text{Std Deviation} = 2.6 \times 10^{-4}$$

Ref.

26

15

## 7. Chemical Properties

Ref.

### a. Heat and Free Energy of Formation, Entropy

Heat of formation: 0

Free energy of formation: 0

Entropy:  $S_{298.15} = 17.371$  cal/mole-deg

18

### b. Chemical Reactions and Reaction Rates

These data are for unirradiated thulium and may be different for irradiated material.

<u>Media</u>	<u>Temp, °C</u>	<u>Corrosion Rate, mils per year</u>
Distilled H <sub>2</sub> O	30	<1
	boiling	<1
1N H <sub>3</sub> PO <sub>4</sub>	30	10-100
	boiling	<1
5N H <sub>3</sub> PO <sub>4</sub>	30	$1-9 \times 10^3$
1N CrO <sub>3</sub>	30	$1-9 \times 10^3$
	boiling	$1-9 \times 10^2$
1N H <sub>2</sub> C <sub>2</sub> O <sub>4</sub>	30	1-10
	boiling	1-10
1:1 (48%) HF - (65%) HNO <sub>3</sub>	25	<1
1N NaOH	30	<1
1N NH <sub>4</sub> OH	30	<1
1N NaNO <sub>2</sub>	30	1-10
	boiling	<1

Oxidation proceeds with a linear rate from 100 to 800°C; moisture accelerates the reaction. Rate constants for oxidation in dry air are:

28

<u>Temp, °C</u>	<u>Const., mg/(cm<sup>2</sup>)(min)</u>
200	$6.4 \times 10^{-5}$
300	$3.4 \times 10^{-4}$
400	$5.0 \times 10^{-4}$
500	$6.8 \times 10^{-4}$
700	$2.2 \times 10^{-3}$

Activation energy is 3.1 kcal from 300 to 700°C.

## 8. Biological Tolerances

Maximum Permissible Concentrations of Tm  
for Continuous Occupational Exposure

Isotope	Form	Organ of Reference	Max Permissible Body Burden (Total Body), $\mu\text{Ci}$	Max Permissible Conc. $\mu\text{Ci}/\text{cm}^3$			
				For 40-hr week		For 168-hr wk	
				Water	Air	Water	Air
$^{170}\text{Tm}$	Soluble	GI <sup>(a)</sup>		$10^{-3}$	$3 \times 10^{-7}$	$5 \times 10^{-4}$	$10^{-7}$
		Bone	9	0.8	$4 \times 10^{-8}$	0.3	$10^{-8}$
		Kidney	30	4	$2 \times 10^{-7}$	1	$6 \times 10^{-8}$
		Total body	60	5	$2 \times 10^{-7}$	2	$7 \times 10^{-8}$
	Insoluble	Lung		-	$3 \times 10^{-8}$	-	$10^{-8}$
$^{171}\text{Tm}$	Soluble	GI <sup>(a)</sup>		$10^{-3}$	$2 \times 10^{-7}$	$5 \times 10^{-4}$	$8 \times 10^{-8}$
		Bone	90	0.01	$3 \times 10^{-8}$	$5 \times 10^{-3}$	$10^{-8}$
		Kidney	700	3	$10^{-7}$	0.9	$4 \times 10^{-8}$
		Total body	700	20	$8 \times 10^{-7}$	6	$3 \times 10^{-7}$
	Insoluble	Lung		-	$2 \times 10^{-7}$	-	$8 \times 10^{-8}$
		GI <sup>(a)</sup>		0.01	$3 \times 10^{-8}$	$5 \times 10^{-3}$	$9 \times 10^{-7}$

(a) Gastrointestinal.

Maximum Permissible Inhalation of Tm  
for Short-Term Exposure

(Pertinent to accident situations)

Isotope	Critical Organ	Effective Half-life, days	$\mu\text{Ci}$ Inhaled That Will Present a Dose of:		
			0.3 rem in 1 wk	15.7 rem in 1 yr	150 rem in 70 yr
$^{170}\text{Tm} + ^{170}\text{Yb}$	Bone	113	22	54	$4.61 \times 10^2$
$^{171}\text{Tm}$	Bone	410	$2.45 \times 10^2$	$3.28 \times 10^2$	$1.44 \times 10^3$

## 9. Shielding Data

The contributions, of bremsstrahlung from  $^{171}\text{Tm}$  and gamma radiation from  $^{171}\text{Yb}$ , to dose rates from a  $^{170}\text{Tm}$  heat source are small compared to the bremsstrahlung from  $^{170}\text{Tm}$  decay because of the low energy for  $^{171}\text{Tm}$  decay and its low concentration in irradiated  $^{169}\text{Tm}$ . Further, the gamma radiation from  $^{170}\text{Yb}$  is negligible because of its low energy and internal conversion. To a first approximation, shielding requirements for  $^{170}\text{Tm}$  fuel are determined only by bremsstrahlung from  $\beta$ -decay of  $^{170}\text{Tm}$ .

Calculated gamma plus bremsstrahlung dose rates for unshielded, iron-shielded, lead-shielded, and uranium-shielded sources are shown in Fig. 1-4 for  $^{170}\text{Tm}$  sources from 0.1 to 20 kw. Dose rates for unshielded and iron-shielded  $^{171}\text{Tm}$  sources are shown in Fig. 5 and 6.

Ref.

29

30

12

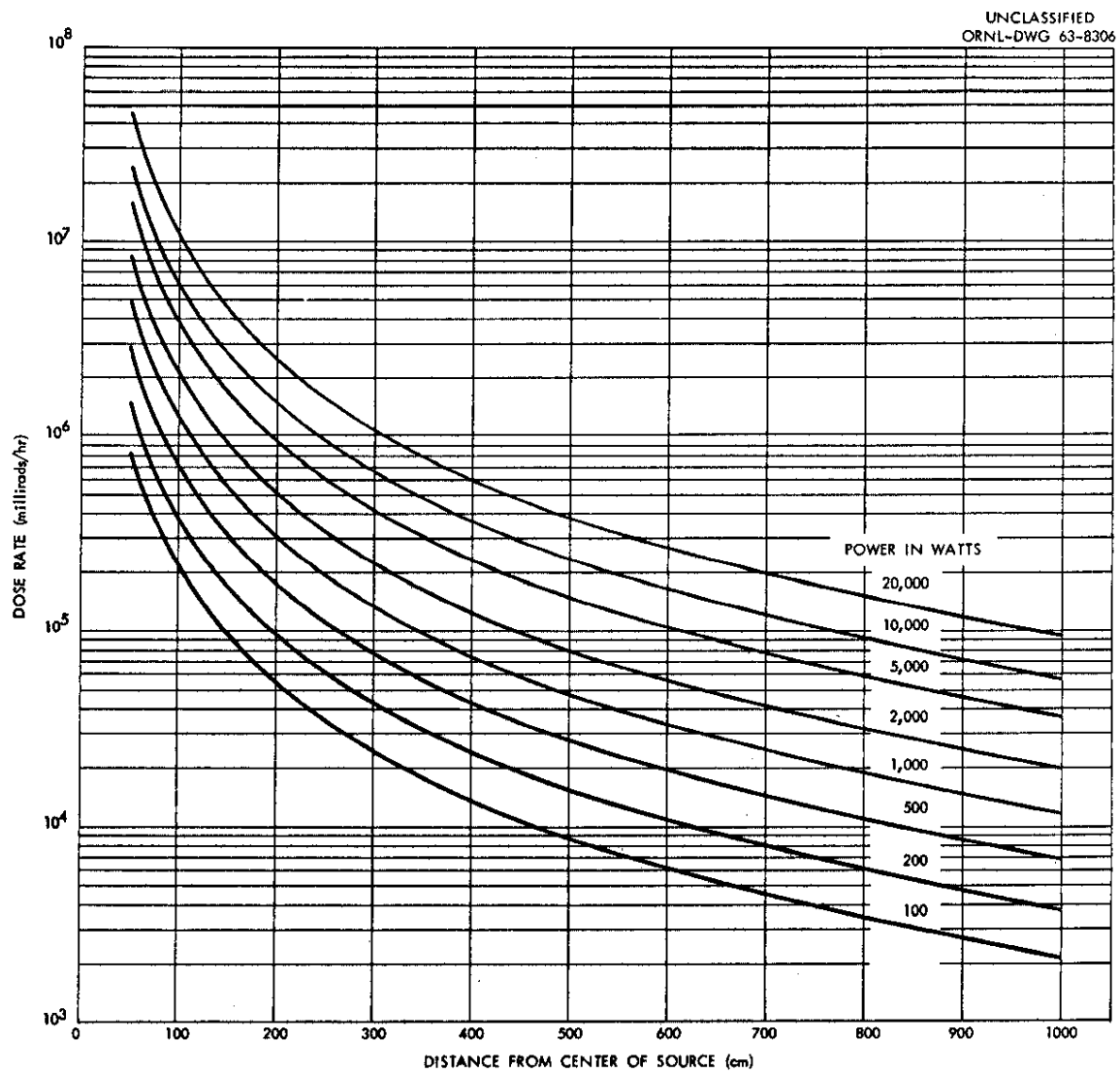


FIG. 1 GAMMA PLUS BREMSSTRAHLUNG DOSE RATES FROM UNSHIELDED ISOTOPIC POWER SOURCES OF THULIUM-170 AS A FUNCTION OF DISTANCE FROM CENTER OF SOURCE <sup>(12)</sup>

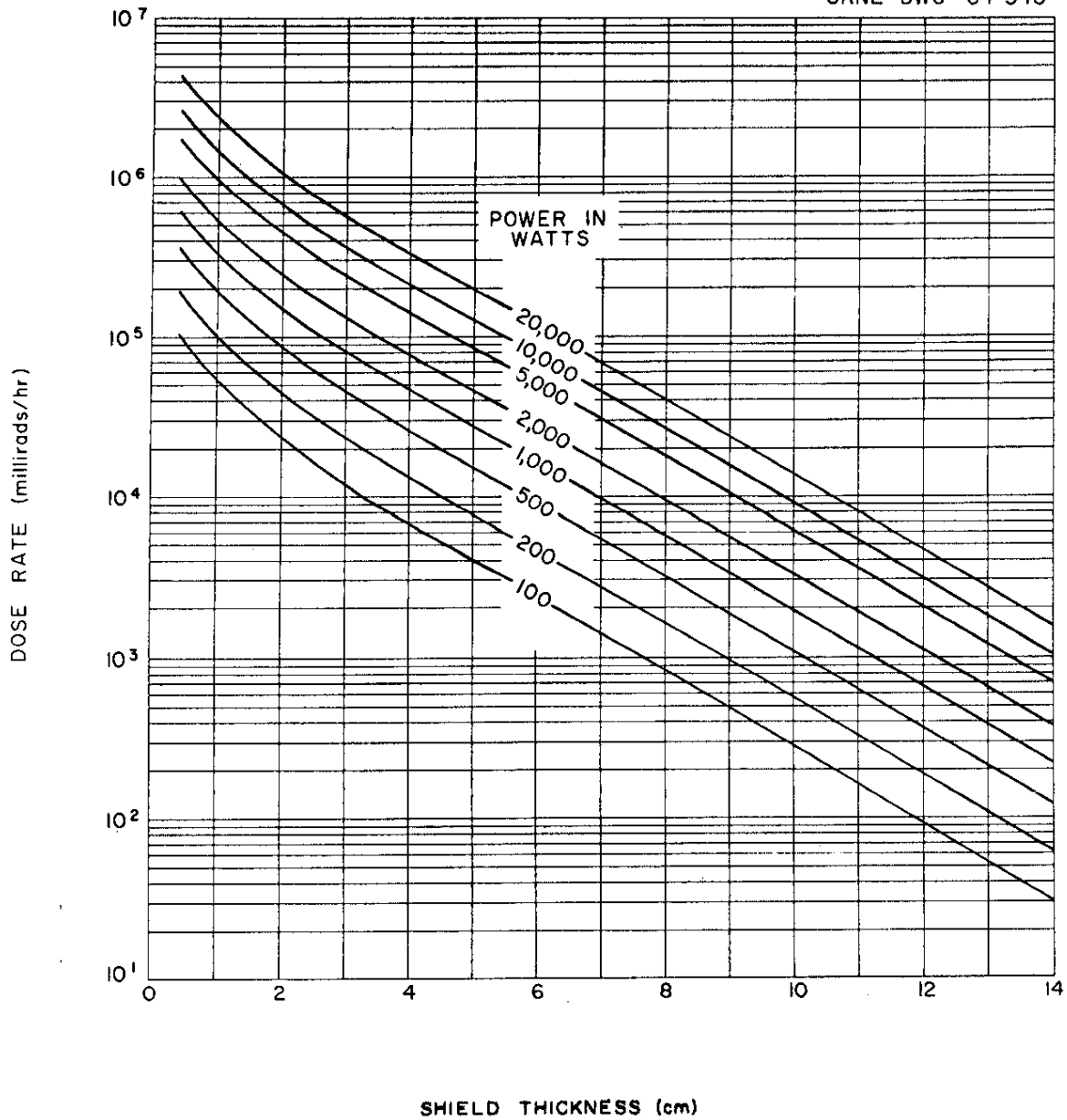


FIG. 2 GAMMA PLUS BREMSSTRAHLUNG DOSE RATES FROM IRON-SHIELDED ISOTOPIC POWER SOURCES OF THULIUM-170. CENTER OF SOURCE TO DOSE POINT SEPARATION DISTANCE = 100 cm <sup>(12)</sup>

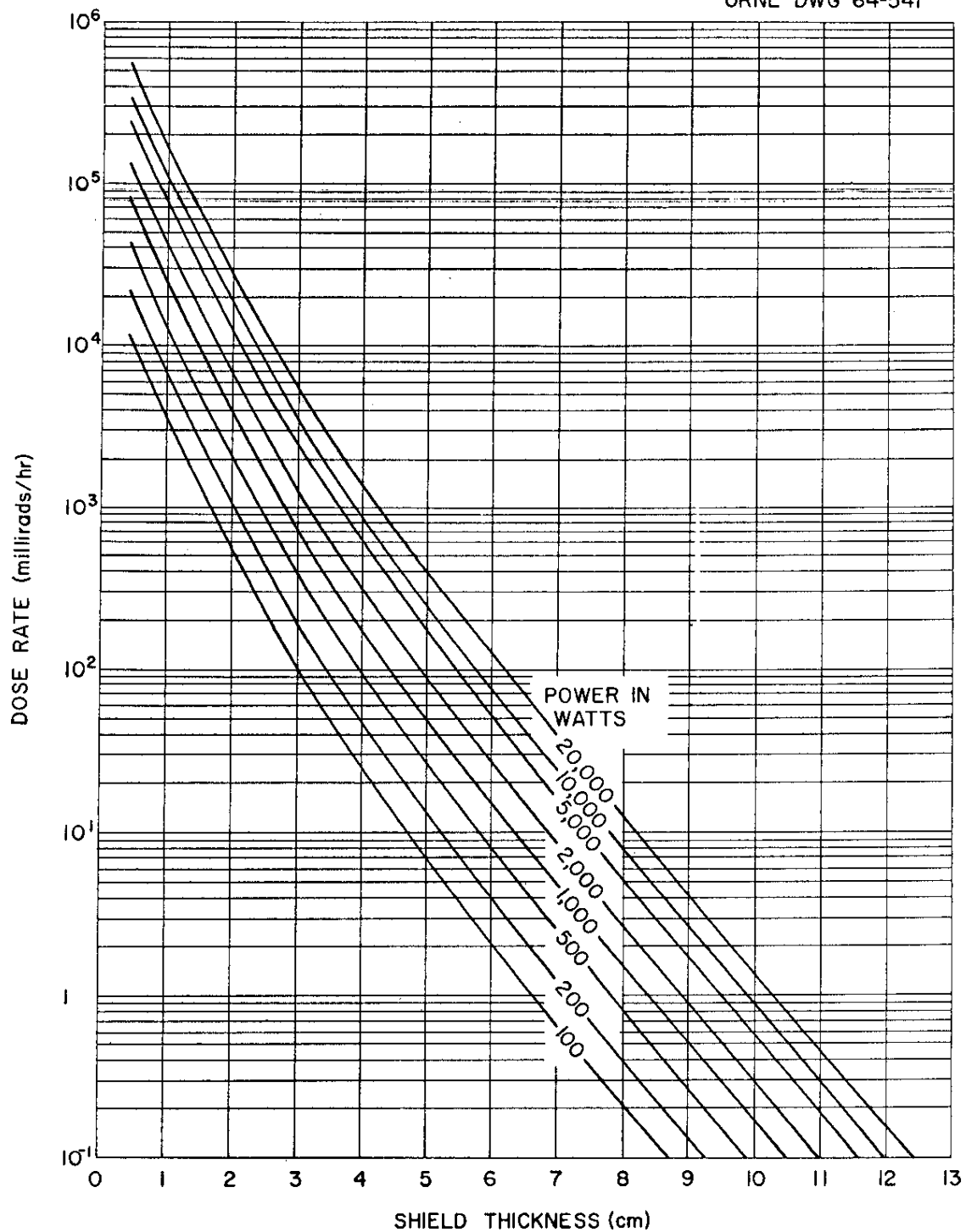


FIG. 3 GAMMA PLUS BREMSSTRAHLUNG DOSE RATES FROM LEAD-SHIELDED ISOTOPIC POWER SOURCES OF THULIUM-170. CENTER OF SOURCE TO DOSE POINT SEPARATION DISTANCE = 100 cm (12)

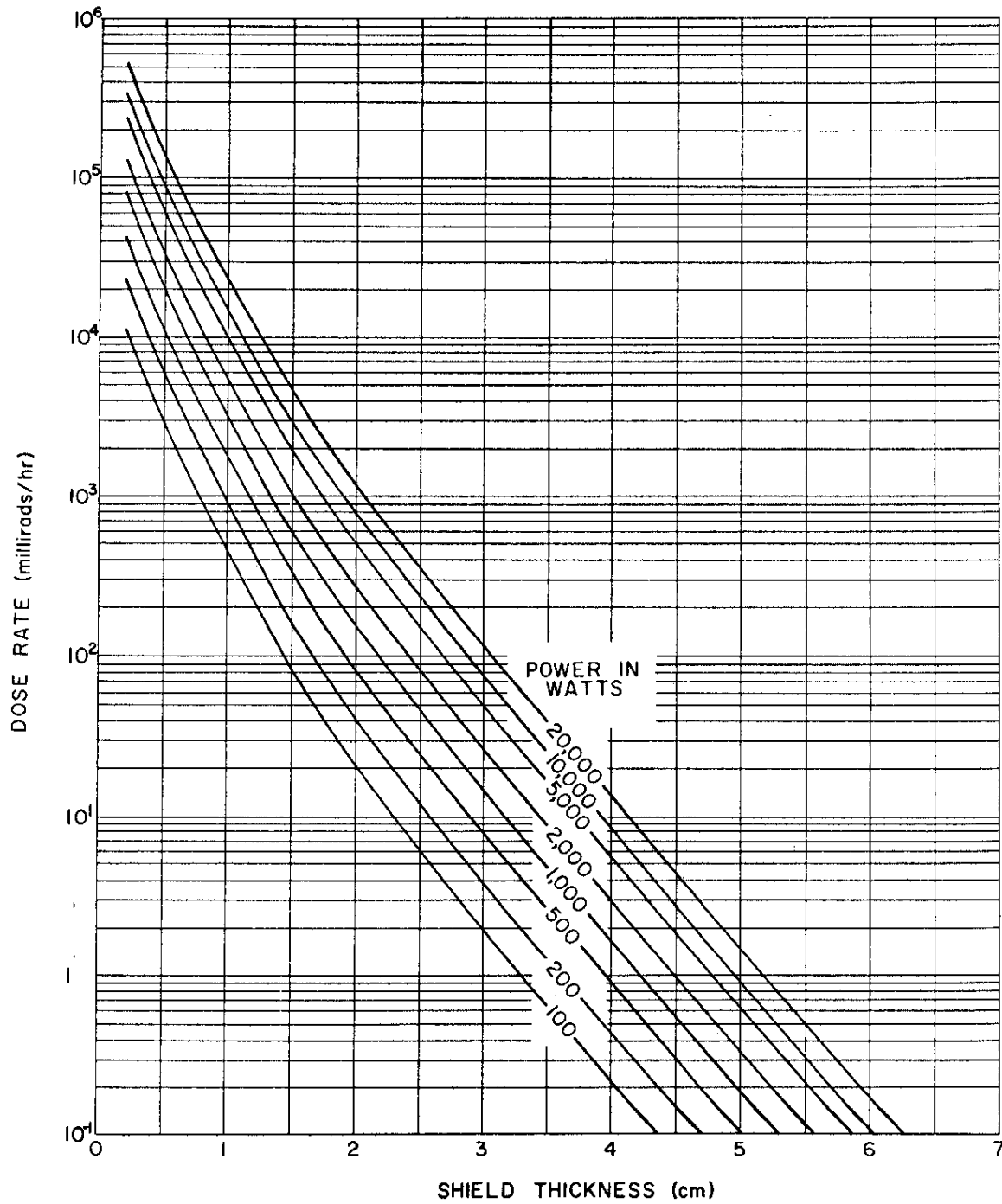


FIG. 4 GAMMA PLUS BREMSSTRAHLUNG DOSE RATES FROM URANIUM-SHIELDED ISOTOPIC POWER SOURCES OF THULIUM-170. CENTER OF SOURCE TO DOSE POINT SEPARATION DISTANCE = 100 cm <sup>(12)</sup>

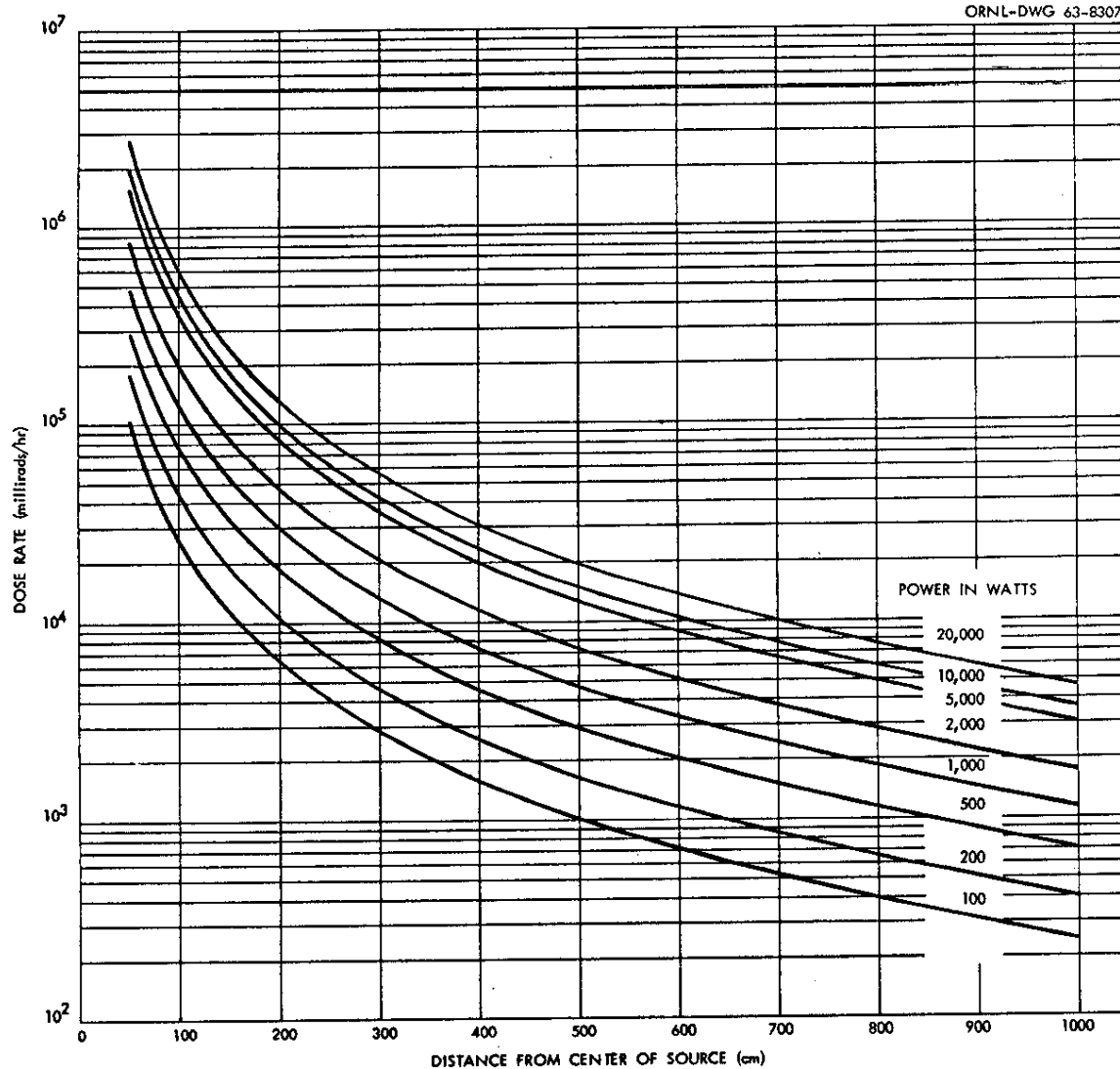


FIG. 5 GAMMA PLUS BREMSSTRAHLUNG DOSE RATES FROM UNSHIELDED ISOTOPIC POWER SOURCES OF THULIUM-171 AS A FUNCTION OF DISTANCE FROM CENTER OF SOURCE <sup>(12)</sup>



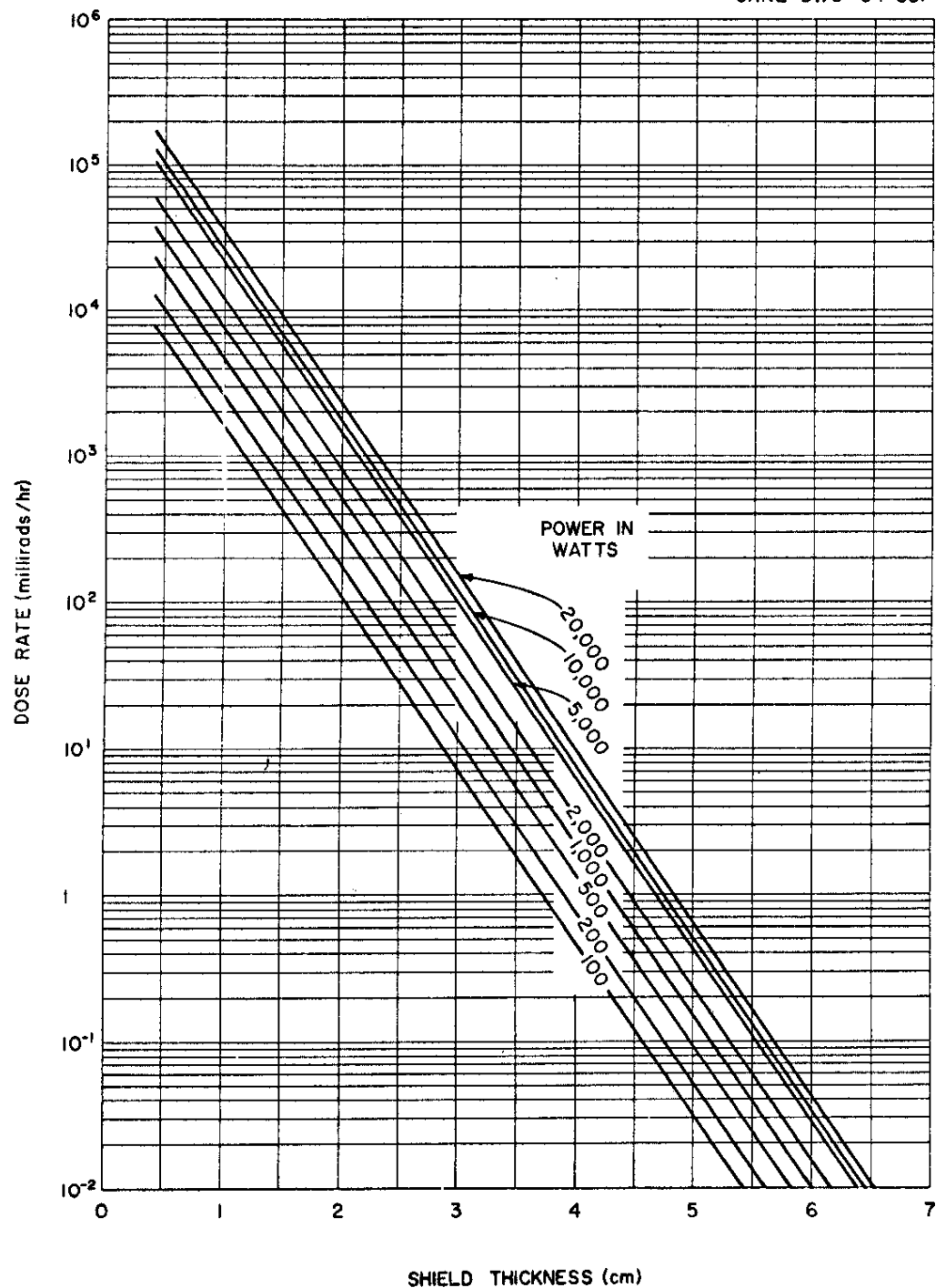


FIG. 6 GAMMA PLUS BREMSSTRAHLUNG DOSE RATES FROM IRON-SHIELDED ISOTOPIC POWER SOURCES OF THULIUM-171 <sup>(12)</sup>

Center of source to dose point separation distance = 100 cm.  
Estimate required thickness of lead or uranium shield by using the following relationship: 1 cm of iron = 0.039 cm lead and 0.137 cm of uranium for 0.1-Mev gamma rays

## B. THULIUM OXIDE - $Tm_2O_3$

### 1. Composition

The composition of unirradiated wafers is 99.9%  $Tm_{2.00}O_{3.00}$ . At temperatures over 1500°C in vacuum, inert gas, or hydrogen, the unirradiated thulium oxide will lose a small amount of oxygen to a composition of  $Tm_{2.00}O_{2.90}$ .

- a. Radionuclide Abundance (calculated) for an arbitrarily selected flux of  $4 \times 10^{14}$  n/(cm<sup>2</sup>)(sec) at reactor discharge for  $^{169}Tm$  irradiation).

<u>Isotope</u>	<u>Specific Activity, w/g →</u>	<u>Concentration, wt %</u>		
		<u>0.62</u>	<u>2.24</u>	<u>2.94</u>
$^{169}Tm$		83.5	68.2	53.1
$^{170}Tm$		4.0	14.3	18.8
$^{171}Tm$		-	2.5	7.3
$^{170}Yb$		-	2.5	7.9
$^{171}Yb$		-	-	0.4
$^{16},^{17},^{18}O$		12.4	12.4	12.4

- b. Chemical Impurities (commercial samples before irradiation)

<u>Impurity</u>	<u>Range of Conc, wt %</u>
Yb (natural)	0.003 to 0.056
Er	0.001 to 0.052
Si	0.014 to 0.029
Fe	0.003 to 0.019
Ca	0.006 to 0.013
Y	0.005 to 0.009
Al	<0.001 to 0.009
All other impurities	<0.001

## 2. Specific Power

- 2 to 3 w/g of oxide at reactor discharge is feasible
- 800 to 1200 Ci/g of oxide at reactor discharge is feasible
- $445 \pm 2$  Ci/w of  $^{170}\text{Tm}$  measured on typical irradiated wafers

## 3. Radiation

The gamma and beta radiation is given in Section A,3,b,2).

### a. Bremsstrahlung

Calculated bremsstrahlung distributions for the two betas of  $^{170}\text{Tm}_2\text{O}_3$  and for  $^{171}\text{Tm}_2\text{O}_3$  are shown in Tables 2-4.

The gamma emission rate from thulium oxide matrices, including bremsstrahlung from the 0.969- and 0.885-Mev  $^{170}\text{Tm}$  betas and the 0.1-Mev  $^{171}\text{Tm}$  beta, is given in the following table.

	<u>Photon Energy, Mev</u>	<u>Photons/w sec</u>
$^{170}\text{Tm}$	0.2 Bremsstrahlung	$7.465 \times 10^{11}$
	0.475 Bremsstrahlung	$5.01 \times 10^{10}$
	0.775 Bremsstrahlung	$1.158 \times 10^9$
	0.1 Actual gamma	$3.208 \times 10^{12}$
$^{171}\text{Tm}$	0.1 Bremsstrahlung	$2.325 \times 10^{11}$
	0.1 Actual gamma	$1.86 \times 10^{12}$

Ref.

1,4

1,4

4

12

12

TABLE 2

Production of Bremsstrahlung Photons from  
Thulium-170 Beta 1 in Thulium Oxide Matrix

Maximum beta-particle energy, Mev 0.968  
Average beta-particle energy, Mev 0.326

<u>Bremsstrahlung Energy Group (Mev)</u>	<u>Number of Photons per Beta Particle Within <math>\Delta E</math> Energy Group</u>
0.050 $\pm 0.025$	$5.736 \times 10^{-2}$
0.100 $\pm 0.025$	$2.085 \times 10^{-2}$
0.150 $\pm 0.025$	$1.026 \times 10^{-2}$
0.200 $\pm 0.025$	$5.686 \times 10^{-3}$
0.250 $\pm 0.025$	$3.340 \times 10^{-3}$
0.300 $\pm 0.025$	$2.020 \times 10^{-3}$
0.350 $\pm 0.025$	$1.236 \times 10^{-3}$
0.400 $\pm 0.025$	$7.551 \times 10^{-4}$
0.450 $\pm 0.025$	$4.562 \times 10^{-4}$
0.500 $\pm 0.025$	$2.696 \times 10^{-4}$
0.550 $\pm 0.025$	$1.542 \times 10^{-4}$
0.600 $\pm 0.025$	$8.410 \times 10^{-5}$
0.650 $\pm 0.025$	$4.296 \times 10^{-5}$
0.700 $\pm 0.025$	$2.000 \times 10^{-5}$
0.750 $\pm 0.025$	$8.138 \times 10^{-6}$
0.800 $\pm 0.025$	$2.680 \times 10^{-6}$
0.850 $\pm 0.025$	$6.111 \times 10^{-7}$
0.900 $\pm 0.025$	$6.278 \times 10^{-8}$
0.950 $\pm 0.025$	$2.196 \times 10^{-10}$
Total bremsstrahlung energy, Mev/beta particle	$1.033 \times 10^{-2}$

TABLE 3

Calculated Production of Bremsstrahlung Photons  
from Thulium-170 Beta 2 in Thulium Oxide Matrix

Maximum beta-particle energy, Mev 0.884

Average beta-particle energy, Mev 0.293

<u>Bremsstrahlung Energy Group (Mev)</u>	<u>Number of Photons per Beta Particle Within <math>\Delta E</math> Energy Group</u>
0.050 $\pm 0.025$	$4.999 \times 10^{-2}$
0.100 $\pm 0.025$	$1.765 \times 10^{-2}$
0.150 $\pm 0.025$	$8.429 \times 10^{-3}$
0.200 $\pm 0.025$	$4.522 \times 10^{-3}$
0.250 $\pm 0.025$	$2.562 \times 10^{-3}$
0.300 $\pm 0.025$	$1.487 \times 10^{-3}$
0.350 $\pm 0.025$	$8.674 \times 10^{-4}$
0.400 $\pm 0.025$	$5.011 \times 10^{-4}$
0.450 $\pm 0.025$	$2.828 \times 10^{-4}$
0.500 $\pm 0.025$	$1.538 \times 10^{-4}$
0.550 $\pm 0.025$	$7.907 \times 10^{-5}$
0.600 $\pm 0.025$	$3.753 \times 10^{-5}$
0.650 $\pm 0.025$	$1.584 \times 10^{-5}$
0.700 $\pm 0.025$	$5.592 \times 10^{-6}$
0.750 $\pm 0.025$	$1.459 \times 10^{-6}$
0.800 $\pm 0.025$	$2.091 \times 10^{-7}$
0.850 $\pm 0.025$	$4.896 \times 10^{-8}$
Total bremsstrahlung energy, Mev/beta particle	$8.310 \times 10^{-3}$

TABLE 4

Calculated Production of Bremsstrahlung Photons  
from Thulium-171 Beta in Thulium Oxide Matrix

12

Maximum beta-particle energy, Mev 0.097  
Average beta-particle energy, Mev 0.029

<u>Bremsstrahlung Energy Group (Mev)</u>	<u>Number of Photons per Beta Particle Within <math>\Delta E</math> Energy Group</u>
0.010 $\pm 0.005$	$1.632 \times 10^{-3}$
0.020 $\pm 0.005$	$4.124 \times 10^{-4}$
0.030 $\pm 0.005$	$1.367 \times 10^{-4}$
0.040 $\pm 0.005$	$4.785 \times 10^{-5}$
0.050 $\pm 0.005$	$1.599 \times 10^{-5}$
0.060 $\pm 0.005$	$4.632 \times 10^{-6}$
0.070 $\pm 0.005$	$9.973 \times 10^{-7}$
0.080 $\pm 0.005$	$1.068 \times 10^{-7}$
0.090 $\pm 0.005$	0.000
Total bremsstrahlung energy, Mev/beta particle	$3.126 \times 10^{-5}$

#### 4. Interaction with Materials of Containment

Ref.

4

Preliminary evaluations of rare earth oxide interactions with tungsten, tantalum, molybdenum, and rhenium, and their alloys indicate that  $Tm_2O_3$  probably will not react with these metals up to 2000°C in sealed systems.

#### 5. Thermophysical Properties

##### a. Density

8.884 g/cc at 25°C, X-ray

31

##### b. Coefficient of Thermal Expansion

The following values were derived by Stecura and Campbell from the lattice parameter changes for  $Tm_2O_3$  from 0°C, as determined by high-temperature X-ray diffraction. The (10.6.2) and (12.4.2) hkl reflections were used to calculate the expansion. The maximum deviation between values calculated from each line was  $\pm 2\%$  above 500°C.

32

Temperature, °C	Linear Expansion, %	Linear Expansion Coefficient (multiply by $10^{-6}$ )
0	0.00	-
28	0.019	6.8
134	0.090	6.6
264	0.189	7.1
364	0.272	7.4
477	0.360	7.5
575	0.444	7.7
695	0.546	7.8
814	0.652	8.0
911	0.743	8.1
1031	0.849	8.2
1132	0.943	8.3
1196	1.005	8.4
1271	1.084	8.5
1295	1.104	8.5

The following values were derived by W. C. Mosley at the Savannah River Laboratory from lattice expansion of  $\text{Tm}_2\text{O}_3$  from 28°C using high temperature X-ray diffraction. Over thirty diffraction peaks were used to calculate the lattice constant at each temperature.

4

<u>Temperature, °C</u>	<u>Linear Expansion, %</u>
28	0.00
535	0.51
1135	0.92
1380	1.17
1745	1.48

A value of  $6.3 \times 10^{-6}/^\circ\text{C}$  has been reported for the linear expansion coefficient of a 97% dense ceramic, but the temperature range was not given.

33

c. Specific Heat and Enthalpy

• Heat capacity:

$$C_p = 31.00 + 0.78 \times 10^{-3}T - 3.42 \times 10^{-5}T^{-2} \quad \text{cal/(mole)(deg)} \quad (298 \text{ to } 1680^\circ\text{K})$$

34

$$C_p = 32.00 \text{ cal/mole} \quad (1680 \text{ to } 2000^\circ\text{K})$$

34

$$C_p = 30.58 + 2.32 \times 10^{-3}T - 4.07 \times 10^{-5}T^{-2} \quad \text{cal/(mole)(deg)} \quad (298.1 \text{ to } 1606.5^\circ\text{K})$$

35

• Heat content:

$$H_T - H_{298.15} = 31.00T + 0.39 \times 10^{-3}T^2 + 3.42 \times 10^{-5}T^{-1} - 10,424 \text{ cal/mole} \quad (\pm 0.1\%; 298 \text{ to } 1680^\circ\text{K})$$

34

$$H_T - H_{298.15} = 32.00T - 10,490 \text{ cal/mole} \quad (\pm 0.1\%; 1680 \text{ to } 2000^\circ\text{K})$$

34

$$H_T - H_{298} = 30.58T + 1.16 \times 10^{-3}T^2 + 4.07 \times 10^{-5}T^{-1} - 10,584 \text{ cal/mole} \quad (298.1 \text{ to } 1606.5^\circ\text{K})$$

35



d. Temperatures of Phase Transformations

Cubic to hexagonal: 2280°C

Melting point: 2375 ±25°C, estimated by analogy with other rare earth sesquioxides.

Boiling point: 4150 ±200°C

e. Latent Heats of Phase Transformations

Unknown.

f. Vapor Pressure

Approximately  $10^{-6}$  atm at 2300°K.

The vapor pressure has been estimated within a range of three decades to be

$$\log P_T(\text{atm}) = 7.36 - 31730T^{-1} (T \text{ in } ^\circ\text{K})$$

This relationship is for the predominant vaporization process, formation of the gaseous elements. Calculated pressures at three temperatures are listed in the following table.

<u>Temperature, °K</u>	<u>Pressure, atm</u>
2000	$3.2 \times 10^{-9}$
2500	$4.4 \times 10^{-6}$
3000	$6.0 \times 10^{-4}$

g. Thermal Conductivity

Eastly and Matson report a value for thermal conductivity of 0.125 (cal-cm)/(sec)(cm<sup>2</sup>)(°C) at 500°C. However, this value appears too high by a factor of 10 when compared to most other oxides. A value of 1.3 to 4.0 (Btu)(ft)/(ft<sup>2</sup>)(hr)(°F) [0.006 to 0.019 (cal)(cm)/(cm<sup>2</sup>)(sec)(°C) at 1000°C] was estimated based on values for yttria and other oxides as shown in Fig. 7.

Ref.

36

37

37

38

37

33,39

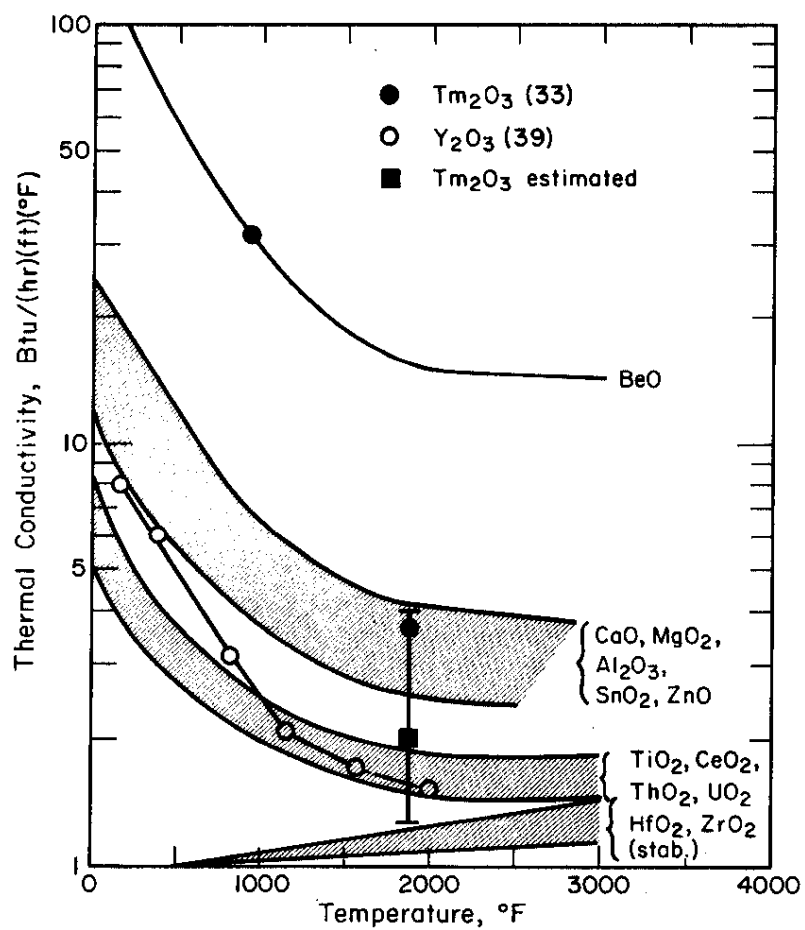


FIG. 7 THERMAL CONDUCTIVITY OF  $Tm_2O_3$  AND OTHER OXIDES  
(Figure and data for other oxides from Reference 39)

h.	<u>Thermal Diffusivity</u>	Ref.
	0.009 to 0.027 cm <sup>2</sup> /sec at 1000°C calculated from thermal conductivity estimate of Section B.6.g.	
i.	<u>Viscosity</u>	
	Unknown.	
j.	<u>Surface Tension</u>	
	Unknown.	
k.	<u>Total Hemispherical Emittance</u>	
	Unknown	
l.	<u>Spectral Emissivity</u>	
	Unknown.	
m.	<u>Crystallography</u>	
	<ul style="list-style-type: none"> <li>• Cubic: Thallium oxide type structure (rare earth oxide type C), space group Ia3 (No. 206), 16 molecules per unit cell.</li> </ul>	31
	<p><math>a = 10.488 \text{ \AA}</math> at 25°C for 99.9% pure, stoichiometric, Tm<sub>2</sub>O<sub>3</sub> annealed at 1100°C for 16 hours.</p>	
	<ul style="list-style-type: none"> <li>• Hexagonal (2280°C to melting):</li> </ul>	36
	<p><math>c = 6.04 \text{ \AA}</math> at 2280°C</p> <p>Assuming <math>c/a = 1.60</math> as for Y<sub>2</sub>O<sub>3</sub> at 2380°C and Er<sub>2</sub>O<sub>3</sub> at 2300°C, one would have for Tm<sub>2</sub>O<sub>3</sub></p> <p><math>a = 3.78 \text{ \AA}</math> at 2280°C</p>	
	<ul style="list-style-type: none"> <li>• Monoclinic: <math>a = 13.18 \text{ \AA}</math>, <math>b = 3.447 \text{ \AA}</math>,</li> </ul>	40
	<p><math>c = 8.505 \text{ \AA}</math>, <math>\beta = 100.2^\circ</math>.</p> <p>Stable above 1100°C at 20 kb pressure and above 400°C at 40 kb pressure.</p>	
n.	<u>Solubility</u>	
	Soluble in mineral acids	24
	Low solubility in water	

•. Diffusion Rates

Unknown.

6. Mechanical Properties

a. Hardness

Unknown.

b. Crush Strength

- o Modulus of rupture: 20,000 psi on 97% dense ceramic

33

7. Chemical Properties

a. Heat and Free Energy of Formation, Entropy

$$\Delta H_{f, 298}^{\circ} = -451.4 + 1.4 \text{ kcal/mole}$$

41

$$S_{298}^{\circ} = 36.3 \pm 0.3 \text{ eu (estimated from data on rare earth oxides)}$$

42

b. Heat and Free Energy of Vaporization to Gaseous Atoms, Entropy

37

$$\Delta H_{v, 298}^{\circ} = 748.3 \text{ kcal/mole}$$

$$\Delta S_{v, 298}^{\circ} = 169 \pm 5 \text{ eu}$$

c. Chemical Reactions and Reaction Rates

4

No measurable reaction with oxygen, nitrogen, water, steam, or hydrogen.

8. Biological Tolerances

Radiobiological tolerances are given in Section A,8.

9. Shielding Data

Dose rates for unshielded, iron-shielded, lead-shielded, and uranium-shielded sources are specified in Section A,9. Computer calculations of the fraction of bremsstrahlung absorbed internally in pure  $^{170}\text{Tm}_2\text{O}_3$  and pure  $^{171}\text{Tm}_2\text{O}_3$  are shown in Fig. 8 and 9.

13

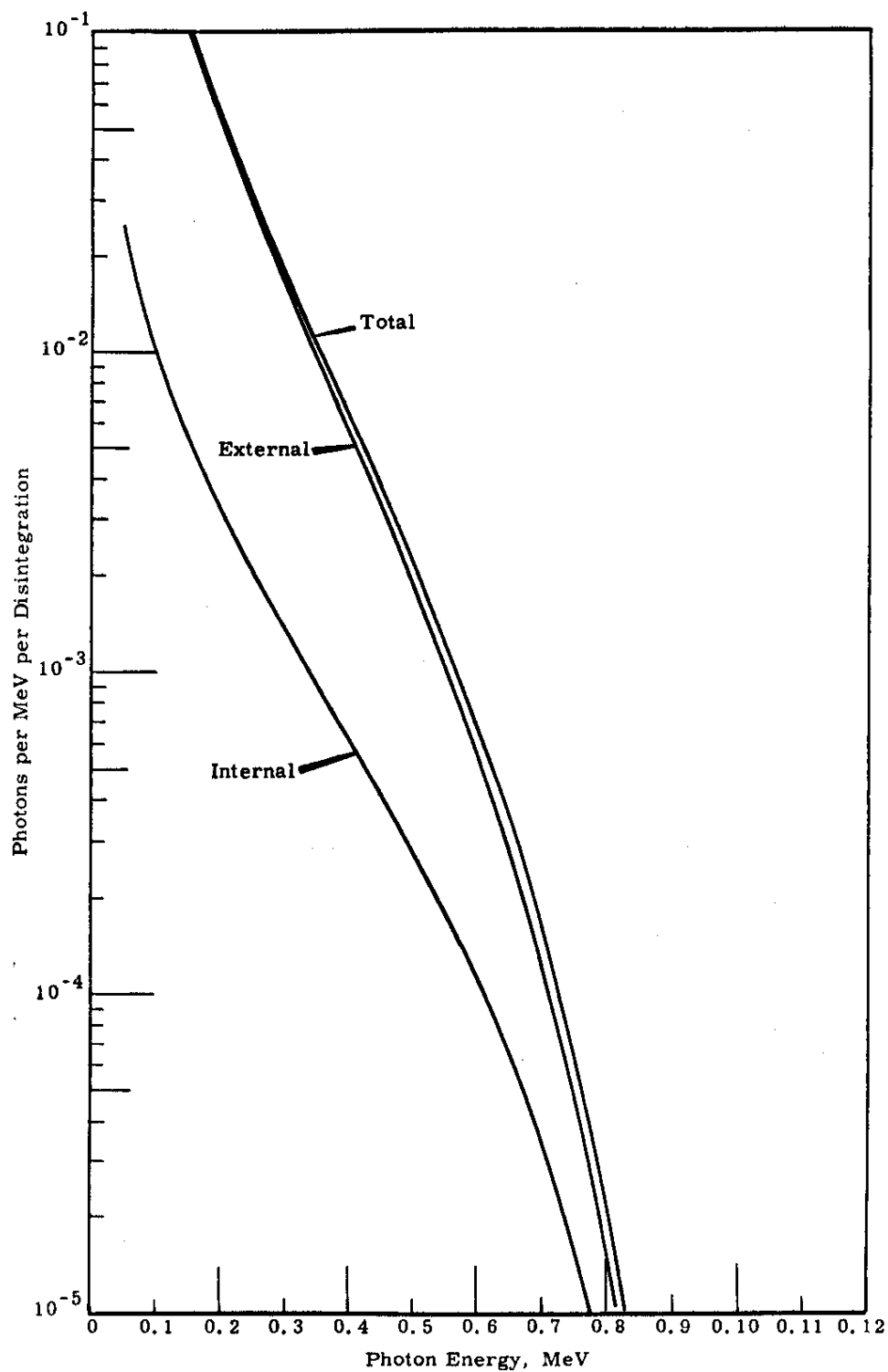


FIG. 8 BREMSSTRAHLUNG FROM  $^{170}\text{Tm}$  BETAS STOPPED IN THULIUM OXIDE (13)

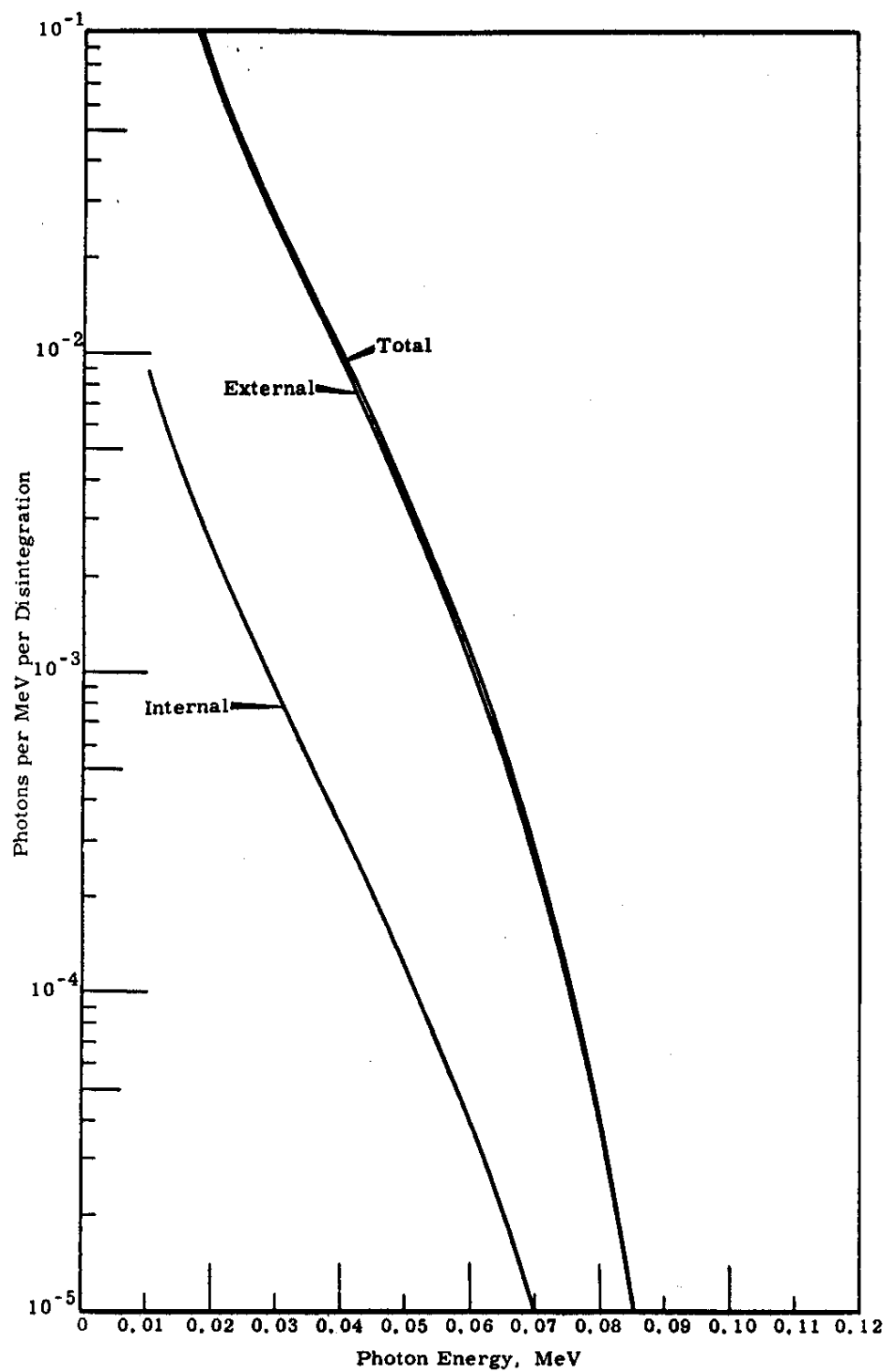


FIG. 9 BREMSSTRAHLUNG FROM  $^{171}\text{Tm}$  BETAS STOPPED IN THULIUM OXIDE (13)

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