CORR-860398

FINAL REPORT
ON THE SAMPLING AND ANALYSIS OF SEDIMENT CORES
FROM THE L-AREA OIL AND CHEMICAL BASIN

Research Planning Institute, Inc.

Prepared For:

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Prepared By:

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RPI/R/85/8/5-7

August 1985



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INTRODUCTION

Nine vibracores were collected in the L-Area oil and chemical basin (904-83G) during late March and early April 1985. These cores were collected for analysis of the sludge on the basin floor and the underlying sediment. Several different field and laboratory analyses were performed on each three inch segment of all the cores. These included: 1) Sediment characterization; 2) Percent moisture; 3) Dry weight; 4) Spectral gamma analysis; 5) Gross alpha and beta analysis. Detailed chemical analysis were measured on selected intervals of 2 cores (LBC-5 and 6) for complete chemical characterization of the sediments. This sampling program was conducted to provide information so that a closure plan for the basin could be developed.

This report describes the methods employed during the project and provide a hard copy of the analytical results from the sample analyses. Included in the appendices are copies of all field and laboratory notes taken during the project and copies of the gas chromatograms for the petroleum hydrocarbon analysis. All chemical results were also submitted on a 5-inch floppy disk.

VIBRACORING AND CORE SAMPLING

Nine vibracores were taken in the L-Area oil and chemical basin (904-83G) in March and April 1985. Figure 1 shows both the location of the cores and the total depth of a given boring. This figure also shows the location of several fathometer traces run across the basin.

Prior to coring activities at the study site the perimeter of the basin was surveyed (Fig. 1). The elevation difference between the berm top and the water surface in the basin was also surveyed. The elevation difference between the concrete pad at test well 904-83G and the water level in the basin was 2.48 meters on 20 March 1985. The depth of water in the basin is shown on the fathometer traces. The fathometer transducer was positioned one foot beneath the boat and from the traces (Appendix VIII) it was determined that the basin had a maximum of 4 feet of water.

After the initial surveys were completed, the vibracoring of the basin floor was initiated. The vibracorer is a small, portable, gasoline-operated coring device. A strong vibration is developed by a cam-loaded shaft driven by a gas engine and is then transmitted to the core barrel. A three inch-diameter aluminum core barrel was used. To collect the samples, the vibracoring was conducted from a modified john boat (Fig. 2). When penetration of sediments was difficult for the standard vibracore, such as in dewatered silt and clay, a combination vibracorer/piston corer technique was employed.

A 2 inch-diameter thin gauged steel core barrel was employed when the vibracorer/piston core technique was used. This vibracorer/piston core technique was only used for borings LBC-2 and LBC-6 (Fig. 1). Using this technique, the initial boring made with the 3 inch-diameter core barrel was removed and the hole was re-entered with the 2 inch-diameter core barrel and sampling was continued. The core samples were pulled from the basin floor utilizing a large tri-pod and com-a-long.

Immediately after extraction of the core the core barrel was cut into 3-inch sections (0-3", 3-6"), etc. Each 3-inch sub-section of core barrel was split and the sample was removed intact and placed either in plastic containers (for sludge samples) or plastic bags (for clayey sediments). The samples were scanned on-site by personnel from Health Protection for radio-activity levels, labeled, and transported to a field laboratory. Cross-contamination of samples in the field was prevented by using new

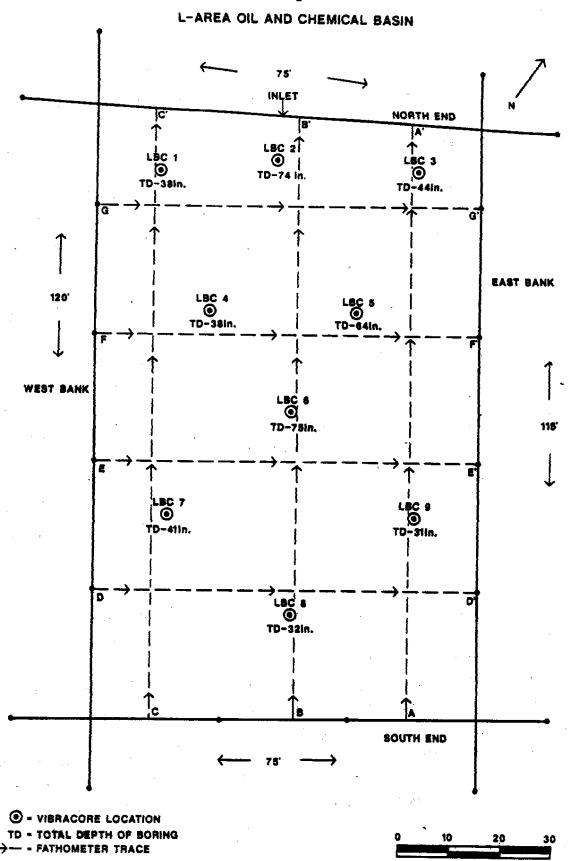


FIGURE 1. Location map of vibracores and fathometer traces.

BOAT SPECIFICATIONS

MAKE: SEA NYMPH-TRAVELER

MODEL #: JV-1544

CAPACITY: 450 POUNDS

MATERIALS: 72 GAUGE ALUMINUM

LENGTH: 15 FT. WIDTH: 62 IN.

FREEBOARD HEIGHT: 20 IN.

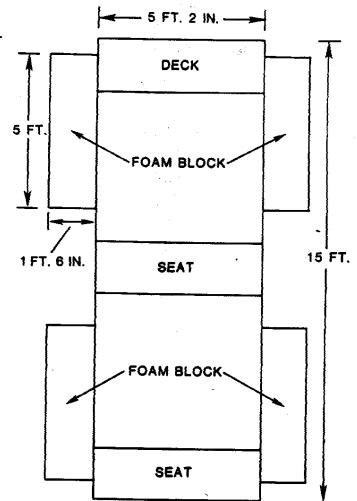


Figure 2. Drawing of the boat used while coring the L-Area oil and chemical basin. Foam blocks were cut and attached to the sides of the boat to increase the stability while coring.

cores barrels for each core. There was no means of contamination in this manner. A technician was on-site during sampling and was responsible for sample handling and labeling after they were taken. A field log was maintained during sample splitting (Appendix II), in which the date and time of core extraction and the field measurements for gross radioactivity were recorded.

The depth of each core was as follows:

Core	Depth (inches)
LBC-1	38
LBC-2	77
LBC-3	44
LBC-4	38
LCB-5	64
LBC-6	75
LBC-7	42
LBC-8	·· 32
LBC-9	31

SAMPLE PREPARATION AND LABORATORY PROCEDURES

ON-SITE PROCEDURES

At the field laboratory in the 700 area, the samples were logged in by sample ID and date in the lab notebook (Appendix I). A total of 133 subsamples were prepared in the field laboratory for analysis of percent moisture and more detailed on-site radioactivity measurements. All intervals of cores 2-9 were prepared and analyzed on-site; only interval 9-15 and 33-38 inches of LBC-1 were prepared and analyzed on-site.

The sludge samples were homogenized within the sample container by stirring and subsamples for on-site measurements were removed from the mixture. Samples of the underlying clayey sediments (usually beginning at or around the 9-12" interval) were scraped on all sides to remove any possible contamination from the coring process. Representative subsamples of each interval were collected in vertical slices through the core. During the sample preparation, a detailed visual sedimentological description was made of grain-size distribution, grain shape, sediment color, bedding and general physical characteristics. The subsamples were split into two unequal fractions: 1) a fraction of 50-100 grams (g) wet weight for spectral gamma activity measurement, and 2) a fraction of 1-10 g wet weight for determination of percent moisture and measurement of gross alpha and beta activity.

Vials for counting of the field spectral gamma activity were prelabeled and tared, with the weight recorded in the lab notebook. The sample was placed inside the vials and a pestal was used to pack the samples into a constant geometry and height of 4 centimeters (cm). The vials were reweighed, the weight recorded, and the total wet weight of the sample calculated (Appendix V).

The second split was weighed in a tared aluminum dish, dried overnight at 50°C and reweighed to determine percent moisture (Appendices IV and VII). The entire dried sample was then pulverized and an approximately 1 g sample was weighed out and placed in a counting planchet. These samples were transported to the on-site counting laboratory set up by E. Lang of the Geology Department of the University of South Carolina.

All remaining sample fractions were stored wet, in their original containers in the laboratory refrigerator until those to be analyzed further were selected.

Core LBC-6 was selected for detailed chemical characterization by an off-site laboratory (Envirodyne Engineers). Samples selected for detailed analysis included every interval from 0-43 inches, then every other interval from 48-75 inches. The original analytical plan called for triplicate analyses of all samples. However, for some intervals, there was inadequate sample quantity to perform triplicate analysis. For the sludge samples, there was not enough sample quantity to measure the entire suite of parameters to the specified detection levels. Therefore, selected intervals of core LBC-5 were used to supplement sample needed for certain parameters. Intervals 0-3 and 3-6 inches from LBC-5 were used for petroleum hydrocarbon and oil and grease measurements. Intervals 6-9 and 9-14 inches from LBC-5 were used for all inorganic, TOC, and COD measurements. Single analyses of all parameters were performed on LBC-6 intervals 48-51, 54-57, 60-63, 66-69, and 72-75 inches. Duplicate analyses were performed on LBC-6 intervals 12-15 and 15-18 inches. Therefore, various parameters were determined on a total of 23 samples.

PREPARATION OF SAMPLES FOR OFF-SITE ANALYSIS

Prior to shipment to the off-site laboratory selected sediment samples were processed in a portable laboratory provided by Du Pont. Sample intervals from the upper 15" of core holes LBC-5 and LBC-6 consisted of a dark oily sludge and were limited in solid material. Due to their extremely wet nature, it was decided to proceed these sample intervals in the controlled conditions of the off-site laboratory to minimize sample loss during processing. Those sample intervals forwarded for processing included LBC-5 (0"-3", 3"-6", 6"-9", 9"-14") and LBC #6 (0"-3", 3"-6" 6"-9" 9"-12", 12"-15", 15"-18"). Sample intervals processed onsite in the portable laboratory included LBC-6 (18"-21", 21"-24", 24"-27", 27"-30", 30"-33", 33"-36", 36"-39", 39"-43", 48"-51", 54"-57", 60"-63", 66"-69", 72"-75").

Sediments sealed in the plastic vials (from the field spectral gamma analysis) were dedicated for the petroleum derivative and EP Toxicity analyses. Samples contained in the plastic dishes were placed in labeled polyethylene trays and set out for air drying. The air drying of sediment samples was necessary to facilitate analytical procedures in the off-site laboratory. Drying time varied according to interstitial sample moisture and environmental conditions within the laboratory but averaged approximately 4-5

days. When full dired to the touch, samples were ground into a fine powder by use of a mortar and pestle. This pulverization process was accomplished under a hood to prevent the contamination of lab facilities or personnel. The resultant powder was then sieved through a number twenty mesh stainless steel screen. Residual soil clumps retained in the sieve were reground and resieved to ensure maximum sample retrieval. The ground and sieved sediments were sealed in appropriately labeled 250 ml amber glass jars and stored in a freezer until shipment off-site. The glass sample jars and plastic vials were prepared for shipment by first wrapping them in bubble-pack and then sealing them in zip-lock plastic bags. Preservation of samples during shipping off-site was accomplished by using Coleman coolers and blue ice. All transfers of sample custody to Du Pont prior to shipment off-site were documented by chain of custody records.

Quality assurance program for field laboratory off-site shipping included:

- A) Use of sample tracking log to track samples from date of processing to date of transfer of custody.
- B) Thorough cleaning of processing equipment with alconox, acetone and distilled water rinses between samples to prevent cross contamination.
- C) Use of fresh gloves between samples to prevent cross contamination.
- D) Use of proper labeling of sample containers (project number, sampling site, etc.) to ensure proper sample identification.
- E) Preservation of wet and processed samples at or below four degrees Centigrade prior to shipment off-site.
- F) Sample containers securely wrapped in bubble pack and zip-lock plastic bags to prevent breakage or spillage during shipment.
- G) Use of chain of custody sheets to document all transfers of custody.

The following tests and methods were performed:

Test	Method
As	Hydride, EPA 206.3
Se.	Hydride, EPA 270.3
Hg	Manual Cold Vapor, EPA 245.1
Sb	Flameless AA, EPA 204.2
U, Pb, Cr, Zn	,
Be, Ni, Ba, Cd	Plasma, EPA 200.7
Ag	Flameless AA, EPA 272.2
TOC	EPA 415.2
COD	EPA 410,1
CN	EPA 335.2
SiO ₂	NaOH Fusion*
Al ₂ O ₃	NaOH Fusion*
Fe ₂ O ₃	NaOH Fusion*
MgO	Plasma, EPA 200.7
CaO	Plasma, EPA 200.7
Na ₂ O	Plasma, EPA 200.7
κ ₂ 0	Flame AA, EPA 258.1
. TiO ₂	Plasma, EPA 200.7
P ₂ 0 ₅	EPA 365.1
MnO	Flame AA, EPA 243.1

In addition to the basin samples, NBS standard soils or NBS traceable check standards were analyses. Aqueous NBS standards were used for EP Toxicity. The results are shown in Table 1. There were several parameters which showed large differences between the reported "true" values and the measured values, with antimony (Sb) and uranium of greatest concern. The digestion method used for Sb was selected because of the limited sample size and was not the optimum procedure, which required a larger sample. The standard was analyzed in the same size and manner as the samples. The recovery rates are poor, ranging from 5-17 percent, but it was not possible to use these results to make corrections to the analytical results because of matrix differences. Therefore, the absolute values for Sb are questionable but the trend clearly shows decreases to relatively low levels.

TABLE 1. Results of analyses for NBS standards or NBS traceable check standard.

Measurement 1 2 3 4	Standard True Value (µg/g)		Measurement 1 2 3	Check Standard Value	Measurement 1 2 3	Standard Value (mg/l)		
			4.54 5.17 5.24	5.0 ppb	4.0	8.0	As	
7.23 8.46 2.69 2.60	51.0	Sb	0.239 0.233 0.238 0.270	ъ 0.25 ppm	0.53 0.545	0.5	Ba	
57.0 52.1	66.0	As	0.252 0.263 0.246	m 0.25 ppm	± ω • • • • • • • • • • • • • • • • • • •	3.0	Cd	EP
			0.221 0.214	0.25	23.0 32.0	30.0	Cr	Toxicity M
0.021 0.021 0.22 0.021	0.025	Be*	0.221 0.244 0.250	ppm 0.25	32.0 28.0	30.0	Pb	EP Toxicity Metals Standards
5.03 34.84 14.81	10.2	С		ppm	1.83 1.83 65	7. 5	Нд	ards
03 84 81	2	Q.	3.15 2.94	3.0 ppb	4.0 4.0	8.0	Se	
27,335 27,185 27,217	29,600	Cr	1.93 2.02) 2.0 ppb	9.3	10.0	Ag	

TABLE 1. Continued.

Measurement 1 2 3 4	Standard True Value (µg/g)		Measurement 1 2 3	Standard True Value (µg/g)		Measurement 1 2 3	Standard True Value (µg/g)	
3,529 3,560 5,705 6,358	22,600	<u>A</u>	19.6 18.4	1.11	C	647.5 642.0 599.8	714.0	Pb
77,238 78,223 80,975 80,662	113,000	Fr. e	1,741 1,753 1,421	1,720	Zn	0.75 0.95 0.82 0.86	1.1	Нg
6811,9 005,9 1400,9 850,9	7,400	Mg	2,008 2,016 2,016	2,000	тос	37.36 37.88 37.31	45.8	Z.
26,445 26,860 26,845 26,948	29,000	Ca	112 112 98	100	COD	4.036 2.773 2.936 4.266	3.0	Se*
978.0 989.5	5,400	Na	. 48 35 48	50	Cn	1.59 1.65 1.87	34- 34-	Ag

TABLE 1. Continued.

Measurement 1 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6.	Standard True Value (µg/g)	
627.9 630.2 629.6 633.9	1,260	×
0.214 0.212 0.226 0.230	0.250	Ţļ*
0.601 0.606 0.601 0.601	0.6	P*
638.7 634.9 640.6 636.6	785.0	Mn
		si*

 $[\]star$ - NBS standard not available; NBS traceable check standards where possible. $\star\star$ - True value not known.

The performance for U with NBS standard was also particularly poor and of concern. These results are for a large sample (5g) concentrated to 5 ml which was a second run to improve the detection levels with the plasma method. With these large sample volumes, aluminum and iron positively interferes with no way to make background corrections. The initial runs, which had a detection limit of 20 ppm, did not have this problem of background corrections.

DETERMINATION OF RADIOACTIVE NUCLIDES BY GAMMA-RAY SPECTROSCOPY IN THE FIELD LABORATORY

This method was used to measure gamma ray emitting nuclides present in all intervals of each core. The expected precision for a single determination varied with the nuclide composition of the sample. The range of sensitivity for this technique varied from 0.001 to 50 microcuries (μ Ci) per sample.

An aliquot of the sample was transferred to a polyethylene 40 dram round vial and the radionuclides present were determined using a lithium-drifted, germanium detector and a computer-based, multi-channel analyzer. The radionuclides present in the sample were determined by gamma-ray spectroscopic techniques.

The apparatus used included:

- 1) Counting Viais Polyethylene 40 dram round with lids.
- 2) Gamma Ray Detector Ge(Li) semiconductor detector with assolated electronics.
- 3) <u>Multichannel Analyzer</u> Computer-based Nuclear Data 76 system with associated peripherals. This system has built-in peak extraction and peak identification programs.

The following calibration procedure was used:

- 1) A clean 40 dram round filled with water to the 4 cm mark was placed directly on the Ge(Li) detector, which is protected by a piece of mylar film. The background spectrum was recorded.
- 2) The Ge(Li) detector was calibrated using NBS and secondary standards in the sample configuration. The standard sample was used to generate a calibration curve for the source position of the detector system.
- 3) The calibration was checked to assure that the results were within the control limits for the system.

Each sample was counted for 20 minutes. All calculations were performed by the computer using an extraction and peak identification procedure. The background was determined to be unimportant in all regions of interest. The results of the peak identification analyses (μ Ci/sample) were divided by the dry weight (Appendix VI) of the sample.

The following equation was used to calculate the activity for each nuclide detected:

Α

Activity = $\frac{}{\text{ExRx2.22x10}^{6}\text{xTxW}}$

where Activity = gamma activity of the sample for each particular nuclide in $\mu Ci/gram$.

A = Area under the gamma-ray peak known to belong to the nuclide in total counts corrected for background.

E = Efficiency of the detector at that energy in counts/disintegration (c/d).

R = Fraction of decays leading to that particular gamma-ray for that nuclide in gammas/disintergration.

T = Counting time in minutes.

 2.2×10^6 = Factor to convert disintergration per minute to μ Ci.

W = Weight of sample in grams.

Normal propagation-of-error techniques were used to determine the 2 sigma error associated with each measurement.

APPENDIX I SAMPLE LOG



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APPENDIX II
SUBSAMPLE FIELD NOTES



Sub-Sample Field Notes

· · · · · · · · · · · · · · · · · · ·	Field notes . pulled 3-26-85 2:30pm	
LBC 3	0-3" Sludge 300c/m Bo 2100	4.
* .	3-6" Sludge tooc/m.	
	6-9 SIndge 1000 c/m.	
	9-11. Sludge 2300c/m	
- 3 · ·	11-15 Sludge ends at 13".	
	15-18. Redictay Little studge.	51
	18-24" Red Clay 400 c/m	
HOUSE	21-24. Red clay 400 c/m	
	24-27 Red clay 250 c/m	
	27-301. Red clay 2000/m.	
to 🛣 i som 🙀 i i i i i i	30-33 Red clay 200 c/m.	
	33-36 Red clay 200 c/m	
De general	36-39 Red clay 300 c/m	
	39-44" Red/yellow Clay 200 c/m	
LBCZ	0-3" sludge 600 c/m	
3-27-85 9:30am	3-4" sludge 800 c/m	
, , , , , , , , , , , , , , , , , , ,	6-9" studge 1000 c/m	
	9-15" Hot spot . sludge to 12" 16,000 c/m	
	15-18" clay 1500c/m	
	18-21" red clay 350 c/m	
	21-24 red clay 500 c/m	
	.24-27 red clay 300c/m	
the grade of the	27-30 red clay 200c/m	
A STATE OF THE STA	30-33 red clay 200 c/m	
	33-38" red clay 200 c/m	

	Jield_	notes	pulled	4-1-2	35	2 pm
LBC 2	The second secon			· ·		•
0+3"	Sludge	200 c/m L10	οοβ 🗞		A	
		200 c/m			,	**************************************
4-9"	Sludge.	1,000c/m			•	ár.
7	. sludge_	-			-	
11-13	sludge . Ho	: ot spot3500c/m	, , ,		•	
17-20 03	Red clay	300·c/m	· ************************************		e de la compansión de l	
20-19	Redclay	zooch		rali a paller de bançon.	n ne skumer	
28-26	Red + grey	clay Zooclm	-			
26-24	Red + grey c	lay 200 c/m	· deader			
2932:	Red clay	200 c/m				
82-35	Red clay	200 c/m	•			
35-38	Red + grey	clay 200 c/m				
38 -: 41	Red+ grey	clay looclm				
41-44	grey clay	200 c/m				
14 -47·5	Red, y+g.	clay 200 c/m	\			,
t7-50	Red+grey	100c/m			er.	
50- 53	grey clay	100C/m		•	: •	
5 3 - 5%	red clay	100 c/m	. · ·			
57e - 59	Red+y, clay	100cm				
59-62	Red, yri grey	1 Clay 100 c/m		•		
02-65	Red + grey	clay zooch				
65-68	Red clay	200 c/m			*	•
8-71 1	Red Clay	200 c/m				
71-74"	Red clay	200 c/m				

```
Field
                         notes
                                     pulled 3-20-85.
                                                        noon
                        Sludge :
                 0-3.
                                      500 c/m
                                                ... 5 - L100 BY
                3-0 sludge
                                     1500 c/m
                6-9"
                        Sludge
                                    4000 c/m
                9-15
                        Studge . only 10" studge - rest clay
                    D Clay
                9-15
                                     700 4m 100
        52 not 15-18 . ...
                        clay-red+ grey 400Um
               18-21
                         red s.c.
                                     200 c/m
                       . red signer
                                     300 c/ms 7 2
               24-27 red s.c.
                                    200 c/m=
               27 - 30"
                        At 29" turns to grey s.c. 2000/m
1
               30-33"
                        grey + white s.c. 150c/m
               <u>33-38"</u>
                                        1504/m
 LBC 5
             · _0-3",,
                                                47-50" , red Sic ..
                       5 ludge : 250 c/m 4189
                                                                     :400c/m
 pulled
3-ab-85
            3-6
                     . sludge
                                  700 c/m
                                                50 - 53"
                                                          red 5. c., 300 c/m
               6-9
                      sludge
                                 2000 cm
                                                53-56
                                                          dense red chy 250 c/m
                      sludge
               9-14
                                2000c/m
                                                56-59"
                                                          red
                                                                       200 c/m
              14-17
                      sludge
                                1400 c/m
                                                59- 64"
                                                         red
                                                                      200 c/m
              17-20
                      Sludge
                                1200 c/m
                      sludge
              20-23
                               500 c/m
      t
sludge
              23-26
                      sludge
                                400 c/m
                                 800c/m
                       sludge
                       At 28" turns from, sludge to clay
              26-29
              24-32 · Sludge / clay
                                       1500 c/m
                      At 35" hit sludge again
              32 - 35°
                                                 1200 c/m
              35-38
                     sludge pocket 1000 c/m
              38-41
                     s. clay
                                   400 c/m
              41-44
                       grey S.C.
                                    300 6/m
                       red
```

42-45: red day 100 c/m

45-48 : red day 100 c/m

48-51 : red clay 100 c/m

: red day 100 c/m.

100c/m

= 60 red day 100c/m

100 c/m

Mocim

100 c/m

100 c/m

loocim

L100 B8

```
pulled.
           field note 3-25-85 10m
 LBC 4 0-3 200 c/m B.K. studge
                      800 cpm .... Studge.
           6-9-
                     25000 com ... shage
           9-12
                    3000 cpm____sudge__.
         12=15" 200 0 cpm 6.66 red
                     1800, com little bit of reast, /sheare
         15-18
           16-21 sandy : 500 comment
           21-24"
                  300cpm redu sa
           24:27 At 27" athin sludge layer.
                     400 com it red wow
           27 - 300"... natural fractures....in sample we siepages - brown stud
July 24000 1 1 30 Ft 33"
                     300 cpm br+grey color.
          33-136 __
                    200cpm. Red .. S. E.
        _ 34-39"
                    200cpm. Redy S.C., upward
3-45-85-134-39-43"
                   150 cpm Red, yellow, grey color, sic
                 250 40m
                           5/4dge_ .... 410.0 8.
        . 3-6".
                 1200 cpm . sludge .....
          6-1011
                 3500 cpm studge....
          10"-12"
                  800 cpm Brown sludge.
          12-15
                 600 cpm. contact zone
         15-18
                  400 cpm "
                            brown
          18-21 350 cpm
                             brown
           21-24
                  300c/m grey Ared
                  250c/m grey, yellow + red color
           24-27
                   200 c/m ted
          27 - 30
          30 - 33
          33-34
          3 u - 3 q
                            red
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5000 4 min Black swife 1/2 700 et /min, contact zone -200 cpm 3-20-85 inso la w 4 1.15 pma' -

LBC9 pulled 3-21-55 0-3 16 1 de L. 2100 por 1000 c/m = 9 section. (Office List - A Ho: Spot 15 - - dance story & 185 Br. 300 c/m. 15/18 derieday _ + 2100 Br . 300 dm 38-21 dere day 2100 pr: 300 c/m Lindense day . Los - 300 elm I Sor Boochman 2100 BT 410c/m.

APPENDIX III SEDIMENT CHARACTERIZATION



SEDIMENT CHARACTERIZATION

GRAIN SIZE SCALE (sediment sizes in millimeters, after Folk 1974)

Clay - Less than 0.004 mm

Silt - Between 0.004 mm and 0.06 mm

Sand - Very Fine - Between 0.06 mm and 0.1 mm Fine - Between 0.1 mm and 0.25 mm Medium - Between 0.25 mm and 0.5 mm

Coarse - Between 0.5 mm and 1.0 mm

SEDIMENT CHARACTERIZATION

LBC 1

9-15" Hot spot - sludge to 12" then clayey sand.
Sludge - liquid, dark colored, round grains.
Grain Size Distribution

clay		(35%)
silt		(20%)
sand	very fine	(30%)
	fine	(10%)
	medium	(5%)

33-38" Dense, compact, gray and red in color, sandy clay, does not crumble easily.

Grain Size	Distribution		
clay sand	very fine fine medium coarse	(50%) (10%) (10%) (20%) (10%)	Subangular sand grains, quartz rich

LBC 2

0-3" Siudge. Very little clay, mostly liquid, dark-colored round grains.

Grain Size	Distribu	tion	
clay silt sand	very fine fine	(10%) (40%) (30%) (20%)	Sand-silt, clay-mixture

3-6" Sludge. Liquid, dark-colored round sand grains.

Grain Size	Distribu	tion
clay silt sand	very fine	(30%) (25%) (30%)
	fine	(10%)
	medium	(58)

9-11"

6-9" Sludge. Liquid, dark-colored round sand grains.

Grain !	Size	Distri	bution	
clay	r			(30%)
silt				(25%)
sand		very fine		(30%)
		fine		(10%)
		medium		(5%)
Sludge.	Liquid,	dark-colored	round	grains.
Grain S	Size	Distri	hution	

Grain Size	Distribu	tion
clay		(35%)
silt		(20%)
sand	very fine	(30%)
	fine	(10%)
	medium	(5%)

11-17" Sludge to 14". Clayey sand to 17". Hot spot, clear-sub-rounded sand grains.

Grain Size	Distribu	ition
clay silt		(35%) (15%)
sand	very fine	(25%)
	fine	(15%)
	medium	(10%)

17-20" Clayey sand 1 red, 1 gray . Clear-sub-rounded sand grains.

Grain Size	Distribution		
clay sand	very fine fine	(45%) (10%) (15%)	Crumbles easily, abundant quartz.
	medium	(30%)	

20-23" Clayey sand ½ red, ½ gray. Clear, sub-angular sand grains.

Grain Size	Distribution		
clay		(45%)	Crumbles easily
sand	very fine	(5%)	•
	fine	(15%)	
	medium	(30%)	
	coarse	(5%)	

23-26" Predominately gray (w/red) clayey sand (in middle of core, a section of 85 percent clay).

Grain Size	Distri	ibution	
clay sand	very fine fine medium coarse	(45%) (5%) (15%) (10%) (10%)	Clear, sub-angular sand grains

26-29" Predominately gray (w/red) clayey sand in middle, small section of dense compact clay.

Grain Size	Distr	ibution	
clay sand	very fine fine medium coarse	(45%) (5%) (15%) (25%) (10%)	Clear, sub-angular sand, does not crumble easily

29-32" Clayey sand ½ red, ½ gray, very well-sorted, clear sub-angular sand grains.

Grain Size	Distribution		
clay sand	very fine fine medium coarse	(45%) (5%) (15%) (25%) (10%)	Red sediments are a little bit clay-lier than gray sediments.

32-35" Gray and red clayey sand. Gray sediment are noticeably more sandy in parts than red sediments.

Grain Size	Distribut	tion	
clay sand	very fine fine medium coarse	(40%) (5%) (15%) (30%) (10%)	Clear, sub-angular sand grains.

LBC 2

35-38" Predominately red clayey sand with a little bit of gray color (which swirls).

	•			
	Grain Size	Distribution		
	clay	very fine fine medium coarse	(45%) (5%) (5%) (15%) (20%) (15%)	Clear, sub-angular sand.
38-41"	Gray and red i Does not crumb	n colored clayey sand. le easily.	Compa	ct, dense sample.
	clay sand	very fine fine medium coarse	(45%) (5%) (15%) (20%) (15%)	Clear, sub-angular sand grains.
41-444	Gray and red o	layey sand compact, d	ense.	
	clay sand	very fine fine medium coarse	(45%) (5%) (15%) (20%) (15%)	Clear, sub-angular sand. No bedding visible in the sandy clay.
44-47"	Gray and red c	layey sand, some yello	w. Comp	pact, dense sample.
	Grain Size	Distribution		

Grain Size	Distribution	<u>1</u>	
clay sand	very fine fine medium coarse	(45%) (5%) (15%) (20%) (15%)	Clear, sub-angular grains. Cross bedded sandy clay. clayey sand

Dark to light gray and red colored sandy clay. Dark gray with vertical bedding (rooting?) located in the middle of core. 47-50#

Grain Size	Distribution		
clay		(50%)	(Beginning of 2" diameter core bar-
sand	very fine	(5%)	rel.) Clear,
	fine	(15%)	sub-angular sand
	medium	(20%)	grains, compact
	coarse	(10%)	dense. Does not

50-53" Gray, red and some mustard-yellow colored sandy clay.

sand very fine (5%) sample clear,	Grain Size	Distribut	ion	
medium (20%) grains coarse (10%)	•	fine medium	(5%) (15%) (20%)	sub-angular sand

53-56" Red sandy clay. Dense, compact. Clear sub-angular sand grains.

Grain Size	Distribut	tion	
clay sand	very fine fine medium coarse	(50%) (5%) (15%) (20%) (10%)	Does not crumble easily.

Red sandy clay with some gray. Dense, compact. Clear, sub-angular sand grains.

Grain Size	<u>Distribu</u>	tion '	
clay sand	very fine fine medium coarse	(50%) (5%) (15%) (25%) (10%)	Crumbles a little easier than 53-56".

59-62" Gray and mustard yellow sandy clay. Dense, clear, sub-angular sand grains.

Grain Size	Distribution		
clay sand	very fine fine medium coarse	(50%) (5%) (15%) (25%) (5%)	Some vertical bedding (rooting?).

62-65" Horizontally bedded which sweeps up on one side of the core. Red and gray sandy clay, clear, sub-angular sand grains.

Grain Size	Distribu	tion
clay		(50%)
sand	very fine	(5%)
	fine	(15%)
•	medium	(25%)
	coarse	(5%)

LBC 2

65-68" Gray sandy clay with dark gray swirls in middle of core.

Grain Size	Distribu	tion
clay		(55%)
sand	very fine	(5%)
	fine	(15%)
	medium	(25%)
	coarse	(5%)

68-71" Red, dark gray to light gray sandy clay. Vertically bedded (root ing?). Clear, sub-angular sand grains.

rain Size	Distribution	
clay		(55%)
sand	very fine	(5%)
	fine	(15%)
	medium	(20%)
	coarse	(5%)

71-74" Red and gray clayey sand. Dense and compact. Clear, sub-angular sand grains.

Distribu	tion
	(40%)
very fine	(15%)
fine	(25%)
medium	(15%)
coarse	(5%)
	fine medium

LBC 3

0-3" Sludge. Dark green/gray color. Dark colored (stained) round sand grains, liquid, very few lumps

Grain Size	Distribution	
clay silt		(30%) (35%)
sand	very fine	(25%)
	fine	(10%)

3-6" Sludge. Dark gray color. Liquid, a few lumps. Dark colored (stained) round sand grains.

Grain Size	Distribution	
clay silt sand	very fine fine medium	(30%) (30%) (25%) (10%) (5%)

6-9" Sludge. Dark gray color. Liquid, thicker than core interval 3-6".

Grain Size	<u>Distribu</u>	<u>tion</u>	
clay silt sand	very fine fine medium	(30%) (20%) (25%) (15%)	Dark-colored, round sand grains.

9-11" Dark gray sludge, many lumps, moist, pliable.

Grain Size	Distribution		
clay silt sand	very fine fine medlum coarse	(40%) (5%) (25%) (15%) (10%) (5%)	Dark-colored, round sand grains. Hot spot

11-15" Dark gray sludge, dark colored round sand grains. Moist, pliable, a few lumps.

Grain Size	Distribution	
clay		(40%)
sand	very fine	(15%)
	fine	(20%)
	medium	(15%)
•	coarse	(10%)

15-18" Gray and red sandy clay, ½ sludge, ½ clay. Pliable, moist clear, round sand grains.

Grain Size	in Size Distribution	
clay		(50%)
sand	very fine	(10%)
	fine	(15%)
	medium	(25%)

Gray, with some red and yellow, sandy clay. Clear, sub-rounded sand grains, compact, dense sample.

Grain Size	Distribution	
clay		(50%)
sand	very fine	(10%)
	fine	(15%)
	medium	(25%)

Red, with some blue and yellow sandy clay. Clear, sub-round sand grains, compact, dense clay.

Grain Size	Distribution	
clay	•	(50%)
sand	very fine	(10%)
	fine	(15%)
	medium	(25%)

24-27" Red, gray and yellow colored clayey sand. Crumbles easily. Clear, sub-angular sand grains.

Grain Size	Distribution	
clay		(35%)
sand	very fine	(5%)
	fine	(15%)
	medium	{25%}
	coarse	(5%)

27-30" Red with gray streaks (1 cm wide) in middle of core clayey sand. Crumbles easily. Clear, sub-angular sand grains.

Grain Size	Distribution	
clay		(35%)
sand	very fine	(5%)
	fine	(20%)
	medium	(35%)
	coarse	(58)

30-33" Red and blue with some yellow. Clayey sand. Clear, sub-angular sand grains. Crumbles easily.

Grain Size	Distribution	
clay sand	very fine fine medium coarse	(35%) (5%) (20%) (35%) (5%)

Red with gray swirls in middle of core. Clayey sand. Crumbles easily. Clear, sub-angular sand grains.

Grain Size	Distribution	
clay sand	very fine	(35%) (5%)
	fine	(20%)
	medium coarse	(35%) (5%)

Red, gray and yellow clayey sand. Crumbles easily. Clear, sub-angular sand grains.

Grain Size	<u>Distribution</u>	
clay		(35%)
sand	very fine	(5%)
1	fine	(20%)
	medium	(30%)
	coarse	(10%)

39-44" Gray, yellow and red clayey sand. Crumbles easily. Clear, sub-angular sand grains, crumbles easily.

Grain Size	Distribution	
ciay		(35%)
sand	very fine	(5%)
+	fine	(20%)
	medium	(30%)
•	coarse	(10%)

LBC 4

0-3" Sludge - green/gray color, liquid. Sand-silt-clay mixture. Dark colored round sand grains.

Grain Size	Distribu	Distribution	
clay silt		(30%) (40%)	
sand	very fine	(15%)	
	fine	(10%)	
	medium	(5%)	

3-6" Sludge - dark gray color, liquid. Sand-silt-clay mixture. Dark colored, round sand grains.

Distribution
(35%) (35%) fine (15%) (10%) um (5%)

6-9" Sludge - dark gray color. Sand-silt-clay mixture. Dark colored, round sand grains. Thicker sample than 3-6".

Grain Size	Distribution	
clay		(40%)
silt		(30%)
sand	very fine	(15%)
	fine	(10%)
	medium	(5%)

9-15" Brown sludge and gray sandy clay. Separated into 2 splits. Hot spot. Clear, sub-round sand grains, sludge to 10". Moist pliable.

Grain Size	Distribution	
clay		(50%) (10%) (15%)
sand	very fine fine medium	(10%) (10%) (15%)

Red and gray sandy clay, no bedding visible.
Clear, sub-angular sand grains; sticky.
Grain Size Distribution

rain Size	DISCIDUCION		
clay		(55%)	
sand	very fine	(10%)	
	finé	(15%)	
	medium	(20%)	

18-21" Gray and red mottled sandy clay. No bedding visible. Clear, sub-angular sand grains; sticky dense sample.

Grain S	<u>Distribu</u>	Distribution	
clay		(55%)	
sand	very fine	(10%)	
	fine	(15%)	
	medium	(20%)	

LBC 4

21-24" Predominantly red, with some gray in middle of core, sandy clay. Clear, sub-angular sand grains; dense sample.

Grain Size	Distribution	
clay		(55%)
sand	very fine	(10%)
	fine	(15%)
	medium	(20%)

Red; gray streak at bottom of core, sandy clay. Clear, sub-angular sand grains; dense sample.

Grain Size	Distribution	
clay -		(55%)
sand	very fine	(5%)
	fine	(15%)
	medium	(25%)

27-30" Gray sandy clay; small circle of red sandy clay at bottom of core, some of the gray sandy clay is tinged yellow. Clear, sub-angular grains, dense sample. Clay does not crumble easily.

Grain Size	Distribution	
clay sand	···	(608)
Sariu	very fine	(5%)
	fine	(15%)
	medium	(20%)

Red at top, gray at bottom, sandy clay. Slightly bedded in middle of core. Clear, sub-angular sand grains. Does not crumble easily. Dense sample.

Distribution	
very fine fine	(70%) (5%) (10%) (15%)
	very fine

Red sand clay, thin gray streaks on top ½ of core. Clear, sub-angular sand grains. Very dense and compact sample.

Grain Size	Distribution	
clay		(60%)
sand	very fine	(5%)
	fine	(10%)
	medium	{25%}

3-6" Sludge - dark gray color, liquid. Sand-silt-clay mixture. Dark colored, round sand grains.

Grain Size	Distribution	
clay		(35%)
silt		(35%)
sand	very fine	(15%)
	fine	(10%)
	medium	(5%)

6-9" Sludge - dark gray color. Sand-silt-clay mixture. Dark colored, round sand grains. Thicker sample than 3-6".

Grain Size	<u>Distribution</u>		
clay		(40%) (30%)	
silt sand	very fine	(308) (15 8)	
	fine	(10%)	
	medium	(5%)	

9-15" Brown sludge and gray sandy clay. Separated into 2 splits. Hot spot. Clear, sub-round sand grains, sludge to 10". Moist pliable.

Grain Size	rain Size <u>Distributio</u>	
clay silt	_	(50%) (10%)
sand	very fine fine medium	(15%) (10%) (15%)

Red and gray sandy clay, no bedding visible.
Clear, sub-angular sand grains; sticky.

Grain Size	Distribution	
clay sand	very fine	(55%) (10%) (15%) (20%)
	medium	(409)

18-21" Gray and red mottled sandy clay. No bedding visible. Clear, sub-angular sand grains; sticky dense sample.

Grain Size	Distribu	tion
clay		(55%)
sand	very fine	(10%)
	fine	(15%)
•	medium	(20%)

0-3" Sludge - dark gray/green color. Liquid-no lumps, dark-colored round sand grains.

Grain Size	Distribution	
clay silt		(30%) (40%)
sand	very fine	(15%)
	fine	(10%)
	medium	{5%}

3-6" Sludge - dark gray color. Dark colored, round sand grains. Liquid with a few lumps.

Grain Size	Distribution	
clay silt sand	very fine fine medium	(30%) (40%) (15%) (10%) (5%)

6-9" Sludge - dark gray color. Lumpy and much thicker than 3-6". Moist, dark-colored round sand grains.

Grain Size	<u>Distribution</u>		
clay silt sand	very fine	(40%) (30%) (15%) (10%)	
	medium	(5%)	

9-14" Dark gray color, two pints of sludge. Dark-colored, liquid - very few lumps. Hot spot.

Grain Size	<u>Distribution</u>		
clay silt		(30 8) (40 8)	
sint	very fine	(408) (15%)	
	fine	(10%)	
•	medium	(5%)	

Gray sludge. Very few lumps. Liquid, dark colored, round sand grains.

Grain Size	<u>D</u>	istribution	*.*	0.50
clay			(30%):	
silt			(45%)	1. 3
sand	very fine	•	(15%)	
	fine		(10%)	

17-20" Gray sludge. Thick consistency. Dark colored round sand grains.

Grain Size	Distribution	
clay silt		(35%) (20%)
sand	very fine	(25%)
	fine	(20%)

20-23" Sludge/clayey sand contact, 50/50 mixture. Brown and gray color. Clear, sub-round sand grains. Moist and pliable.

Grain Size	Distribution	
clay		(40%)
silt		(10%)
sand	very fine	(20%)
	fine	(20%)
	medium	(10%)

23-26" Sample is ½ sludge, ½ clay. Sludge is brown. Clayey sand is red, blue and yellow. Clear, sub-round sand grains. Moist and pliable.

Grain Size	ain Size Distribution	
clay silt		(45%) (5%)
sand	very fine	(15%)
	fine	(15%)
	medium	{20%}

26-29" Clayey sand with a little sludge. Red and blue in color. Crumbles easily. Clear, sub-angular sand grains.

Grain Size	ain Size Distribution	
clay		(35%)
sand	very fine	(15%)
	fine	(20%)
	medium	(30%)

29-32" Sludge and clayey sand. Pliable, crumbles easily. Clear sub-angular sand grains.

Grain Size	Distribution	
clay		(35%)
sand	very fine	(15%)
	fine	(20%)
	medium	(30%)

32-35" At 35" brown sludge. Clayey sand 1 red and blue. Very pliable. Clear, sub-round sand grains.

Grain Size	Distribution	
clay silt sand	very fine fine	(35%) (5%) (15%) (20%)
	medium	(25%)

35-38" Sludge pocket. Brown. Moist, pliable. Clear, sub-round sand grains. Lumpy-small amounts of red sandy clay.

Grain Size Distribution		ition
clay		(50%)
silt		(10%)
sand	very fine	(15%)
	fine	(20%)
	medium	(5%)

Red and blue sandy clay. Some sludge. Dense, compact sample; clear, sub-angular sand grains. Does not crumble easily.

Grain Size	<u>Distribution</u>	
clay		(55%)
sand	very fine	(10%)
	fine	(15%)
	medium	(20%)

41-44" Gray and red sandy clay; dense, compact sample. Clear, sub-angular sand grains.

Grain Size	<u>Distribution</u>	
clay		(55%)
sand	very fine	(10%)
	fine	(15%)
*	medium	(20%)

Gray and red sandy clay, pliable, moist, some sludge. Clear, sub-angular sand grains.

Grain Size	<u>Distribution</u>	
clay		(55%)
sand	very fine	(10%)
	fine	(15%)
	medium	(20%)

47-50" Red sandy clay, very pliable. Clear, sub-angular sand grains. Moist.

Grain Size	Distribution	
clay sand	very fine fine	(55%) (10%)
	medium	(15%) (20%)

Red and gray sandy clay, compact, dense sample. Subangular sand grains. Quartz rich.

Grain Size	Distribution	
clay		(55%)
sand	very fine	(10%)
	fine	(15%)
	medium	(15%)
	coarse	(5%)

Clayey sand . Some gray color. Crumbles easily. Sub-angular, clear sand grains, quartz rich.

Grain Size	Distribution	
clay		(45%)
sand	very fine	(10%)
	fine	(10%)
	medium	(20%)
	coarse	(15%)

56-59" Red and gray clayey sand. Crumbles easily.

Grain Size	Distribution	
clay	•	(45%)
sand	very fine	(10%)
	fine	(10%)
	medium	(20%)
•	coarse	(15%)

LBC 5

Gray with a red streak at top and bottom of sample, clayey sand. Crumbles easily. Clear, sub-angular sand grains.

Grain Size	Distribution	
clay		(45%)
sand	very fine	(10%)
	fine	(15%)
	medium	(25%)
	coarse	(5)

LBC 6

0-3" Sludge. Gray color, mostly a liquid. Silt-sand-clay mixture. Dark-colored round, smooth grains.

<u>Grain Size</u> <u>Distribution</u>		tion
clay		(40%)
silt		(30%)
sand	very fine	(20%)
	fine	(10%)

3-6" Sludge. Dark gray, thick liquid. Sand-silt-clay mixture. Predominantly very fine grained, dark-colored (stained) sand.

Grain Size	Distribution	
clay silt		(40%)
• • • •		(25%)
sand	very fine	(30%)
	fine	(5%)

6-9" Sludge. Dark gray color. Paste-like consistency. Liquid sand-silt-clay mixture.

Grain Size	rain Size Distribution	
clay siit	•	(30%) (25%)
sand	very fine	(20%)
	fine	(15%)
	medium	(10%)

9-12" Sludge. Thicker than 6-9" section. Liquid, dark-colored sand grains. Sand-silt-clay mixture.

Grain Size	Distribution	
clay		(30%)
silt		(10%)
sand	very fine	(25%)
	fine	(20%)
	medium	(159)

12-15" Brown colored sludge. Thick liquid. Smooth, round grains. Sand-silt-clay mixture.

Grain Size	Distribution	
clay		(40%)
siit		(10%)
sand	very fine	(15%)
	fine	(15%)
	medium	(20%)

Brown sludge, liquid. Sand-silt-clay mixture, sorted, smooth, round sand grains. Some red sandy clay.

Grain Size	Distribution	
clay		(40%)
silt		(5%)
sand	very fine	(10%)
	fine	(10%)
	medium	(35%)

18-21" Contact zone - sludge to red and gray sandy clay/predominantly sandy clay.

Grain Size Distribution		ition
clay siit		(55%) (5%)
sand	very fine	(5%)
	fine	(10%)
	medium	(25%)

21-24" Gray and red sandy clay. No bedding, Moist sample. Clear, sub-angular sand grains.

Grain Size	Distribution	
ciay		(55%)
sand	very fine	(5%)
	fine	(10%)
	medium	(30%)

LBC 6

24-27" Yellow and gray sandy clay. At 27" a thin layer of brown sludge. Clear, sub-angular sand grains. No bedding.

Grain Size	Distribution	
clay		(55%)
sand	very fine	(5%)
	fine	(10%)
	medium	(30%)

27-30" Orange/red and gray colored sandy clay. Sludge at 27". Moist sample, clear, sub-angular sand grains. No bedding.

Grain Size	Distribu	ition
clay		(60%)
sand	very fine	(5%)
	fine	(10%)
	medium	(20%)

30-33" Red, yellow and gray color, sandy clay. Crumbly, clear, sub-angular sand grains. No bedding visible.

Grain Size	Size <u>Distribution</u>	
clay		(50%)
sand	very fine	(5%)
	fine	(15%)
	medium	(30%)

33-36" Red and gray colored wavy bedded, sandy clay. Crumbly. Clear, sub-angular sand grains.

Grain Size	Distribution	
clay		(50%)
sand	very fine	(5%)
	fine	(15%)
	medium	(30%)

36-39" Red and yellow sandy clay, banded. Crumbly; clear, sub-angular sand grains.

Grain Size	<u>Distribution</u>	
clay sand	very fine fine medium	(50%) (5%) (15%) (25%) (5%)

39-42" Gray, yellow and red colored sandy clay. Red and yellow thin bands for an inch. Crumbly. Very clear sand grains.

	bands for an i	nch. Crumbly. Ver	y clear sand grains.
	Grain Size	Distributio	<u>n</u>
	clay sand	very fine fine medium coarse	(50%) (5%) (10%) (25%) (10%)
42-45"	Gray and red o	colored clayed sand.	Crumbles easily. Clear,
	Grain Size	Distribution	<u>n</u>
	clay sand	very fine fine medium coarse	(45%) (10%) (15%) (25%) (5%)
45-48"	Red clayey sand	d. Crumbles easily.	Clear, sub-angular grains.
	Grain Size	Distribution	<u>1</u>
	clay sand	very fine fine medium coarse	(40%) (10%) (15%) (25%) (10%)
48-51"	Red and gray c	olored, clayey sand. Ilar sand grains. N	Crumbles fairly easily.

4

Grain Size	Distribution	
clay		(40%)
sand	very fine	(10%)
	fine	(15%)
	medium	(20%)
	coarse	(158)

51-54" Red colored, clayey sand, crumbles easily. Clear, sub-angular sand grains.

Grain Size	Distribution	
clay		(40%)
sand	very fine	(10%)
,	fine	(15%)
	medium	(20%)
	coarse	(159)

54-57: Red colored, clayey sand. Crumbles easily; clear, sub-angular sand grains.

Grain Size	Distribu	Distribution	
clay		(30%)	
sand	very fine	(10%)	
	fine	(15%)	
	medium	(20%)	
	coarse	(25%)	

57-60" Red colored clayey sand, crumbles easily. Clear, sub-angular sand grains.

Grain Size	Distribution	
clay		(25%)
sand	very fine	(10%)
	fine	(15%)
	medium	(20%)
	coarse	(30%)

60-63" Red colored clayey sand. Crumbles easily. Compact sample, clear, sub-angular sand grains.

Grain Size	<u>Distribution</u>	
clay		(25%)
sand	very fine	(10%)
	fine	(15%)
	medium	(20%)
	coarse	(30%)

63-66: Clayey sand, red; crumbles easily. Clear, sub-angular sand grains.

Grain Size	Distribution	
clay		(25%)
sand	very fine	(10%)
	fine	(15%)
	medium	(20%)
	coarse	(30%)

66-69" Yellow, clayey sand. Thin red beds run horizontally. Clear sub-angular sand grains. Compact.

Grain Size	Distribution	
clay sand	very fine fine medium coarse	(20%) (10%) (15%) (20%) (35%)

Red and yellow horizontal banding, clayey sand. Compact, crumbles easily. Clear, sub-angular sand grains.

Grain Size	Distribution	
ciay		(20%)
sand	very fine	(10%)
	fine	(15%)
	medium	(20%)
	coarse	(35%)

72-75" Red colored clayey sand. Crumbles easily; compact. Clear, sub-angular sand grains.

Grain Size	Distribution	
clay		(15%)
sand	very fine	(10%)
	fine	(15%)
	medium	(20%)
	coarse	(40%)

LBC 7

0-3" Sludge - dark green color. Sand-silt-clay mixture. Sample mostly liquid. Very fine, round dark sand fraction.

Grain Size	ize <u>Distribution</u>	
clay		(30%)
silt		(40%)
sand	very fine	(25%)
	fine	(42)

3-6" Sludge - dark green color. Sand-silt-clay mixture. Liquid, dark-colored round sand grains.

Grain Size	Distribution	
clay		(30%)
silt		(40%)
sand	very fine	(20%)
	fine	(5%)
	medium	(5%)

6-10" Dark green sludge. Sand-silt-clay mixture.

Grain Size	Distribution	
clay silt sand	very fine fine medium	(40%) (35%) (15%) (5%) (5%)

LBC 7

Brb₩n liquid sludge. Dark colored, round, sand grains.

Grain Size	Distribution	
clay silt sand	very fine fine medium	(30%) (40%) (15%) (10%) (5%)

12-15" Chocolate brown sludge. Sand-silt-clay mixture. Clear, sub-rounded sand fraction, moist.

Grain Size	Distribution	
clay		(40%)
silt		(25%)
sand	very fine	(10%)
	fine	(15%)
	medium	(10%)

15-18" Sludge/clayey sand contact, gray and red. Clear, sub-rounded sand grains.

Grain Size	Distribution	
clay silt sand	very fine	(45%) (10%) (10%)
3 22	fine medium	(20%) (15%)

18-21" Brown and gray sludge mixed in with clayey sand. Clear, sub-rounded sand grains. Very moist, pliable, sticky.

Grain Size Distril		tion
clay silt		(45%) (10%)
sand	very fine	(108)
	fine	(20%)
	medium	(15%)

21-24" Red and gray sandy clay. No sludge. Clear, sub-angular sand grains. Crumbly. No bedding visible.

Grain Size	<u>Distribution</u>	
clay		(55%)
sand	very fine	(5%)
	fine	(15%)
•	medium	(25%)

24-27" Gray with red streaks sandy clay, No bedding present. Clear, sub-angular sand grains, crumbly.

Grain Size	<u>Distribution</u>	
clay		(50%)
sand	very fine	(5%)
	fine	(15%)
	medium	(25%)
	coarse	(5%)

27-30" Gray sandy clay - red streak on one side, and top and bottom of sample. Dense. Crumbly, clear, sub-angular sand fraction.

Grain Size	Distribution	
clay		(55%)
sand	very fine	(5%)
	fine	(20%)
	medium	(20%)

Red sandy clay with gray swirls. Crumbly, dense sample; clear, sub-angular sand fraction.

Grain Size	Distribution	
clay		(55%)
sand	very fine	(5%)
	fine	(25%)
	medium	(15%)

33-36" Sandy clay ½ red, ½ gray-interbedded vertically in middle of core. Crumbly, clear, sub-angular sand grains. Dense sample.

Grain Size	rain Size <u>Distribution</u>	
clay sand	very fine	(55%) (5%)
	fine	(15%)
	medium	(25%)

Red sandy clay with gray swirls in top half of core. Crumbly, clear, sub-angular sand grains. Dense sample.

Grain Size	Distribution	
clay		(50%)
sand	very fine	(5%)
	fine	(15%)
	medium	(30%)

Red sandy clay. Several thin gray streaks (2" long) on the side of the sample. Dense sample. Clear, sub-angular sand grains. Crumbly.

Grain Size	Distribution	
clay		(50%)
sand	very fine	(10%)
	fine	(15%)
	medium	(25%)

LBC 8

0-3" Olive green sludge; liquid. Silt-clay-sand mixture.

Grain Size Distribution		tion
clay		(30%)
silt		(40%)
sand	very fine	(20%)
	fine	(10%)

3-8" Hot spot. Liquid sludge. Thicker consistency than 0-3" section. Sand-silt-clay mixture. Clear, round sand grains.

Grain Size	ize <u>Distribution</u>	
clay		(20%)
silt		(35%)
sand	very fine	(20%)
	fine	{158}

LBC 8

8-11" Chocolate brown sludge; liquid. Feels gritty. Clear, sub-angular grains. Sand-silt-clay mixture.

Grain Size	Distribution	
clay silt		(30%) (5%)
sand	very fine fine	(25%) (20%)
	medium coarse	(15%) (15%) (5%)

Brown and gray sludge, thick liquid. Sand-silt-clay mixture. Clear, sub-angular sand grains. Smooth and sticky.

Grain Size	in Size Distribution	
clay		(35%)
silt		(5%)
sand	very fine	(15%)
	fine	(20%)
	medium	{15%}
	coarse	(10%)

14-17" Predominantly white/gray clayey sand. Horizontal bands between yellow, white/gray bands. Crumbly dry sample. Clear, sub-angular grains.

Grain Size	Distribu	ition
clay		(40%)
sand	very fine	(10%)
	fine	(15%)
	medium	(20%)
	coarse	(15%)

17-20" Red to gray/yellow colored clayey sand. Clear, sub-angular grains. Moist, crumbly.

Grain Size	rain Size Distribution	
clay		(40%)
sand	very fine	(5%)
	fine	(10%)
	medium	(30%)
	coarse	(15%)

20-23" Gray and yellow (and red - not predominate color) clayey sand with some horizontal bedding. Clear, sub-angular grains. Moist, crumbly.

Grain Size	Distribution	
clay		(40%)
sand	very fine	(5%)
	fine	(10%)
	medium	(30%)
	coarse	(15%)

23-26" Gray and yellow colored clayey sand with bands of red, yellow and gray, sand clay. Clear, sub-angular sand grains. Moist.

Grain Size	Distribution	
clay		(40%)
sand	very fine	(5%)
	fine	(10%)
	medium	(30%)
÷	coarse	(15%)

Alternating bands of gray and yellow (some white color) clayey sand. Dense, compact sample. Clear sand grains, sub-angular, quartz rich.

Grain Size	<u>Distribution</u>	
clay		(45%)
silt		(5%)
sand	fine	(5%)
	medium	(15%)
	coarse	(30%)

29-32" Sand clay with bands of gray and white/light yellow with swirls of dark red, (3 cm high by 5 cm long). Dense, compact sample. Sand grains are clear and sub-angular.

Grain Size	Distrib	ution
clay silt		(50%) (5%)
sand	fine	(5%)
	medium	(15%)
	coarse	(25%)

0-3" Dark gray sludge. Liquid, smooth, not gritty. Sand-silt-clay mixture.

Grain Size	Distribution	
clay		(30%)
silt		(35%)
sand	very fine	(20%)
	fine	(10%)
	medium	(5%)

3-6" Medium dark gray color sludge. Liquid, smooth, lumpy. Dark colored sand grains.

Grain Size	Distribu	tion
clay		(45%)
silt		(40%)
sand	very fine	(10%)
	fine	(5%)

6-12" Hot spot. Contact zone of sludge to clay. Sludge medium gray color. Smooth and sticky, gray color with little bit of red and yellow clay.

Grain Size	Distribution
clay	(95%)
silt	(5%)

12-15" Light gray sandy clay. Horizontal sections colored red, yellow. Clear sand grains; sub-angular.

Grain Size	Distribution		
clay		(55%)	
silt		(5%)	
sand	very fine	(5%)	
	fine	(5%)	
	medium	(10%)	
	coarse	(20%)	

Gray and yellow colored sandy clay. Smooth, clear, sub-angular sand grains. Dense, compact sample.

Grain Size	Distrib	ution
clay		(55%)
silt		(5%)
sand	fine	(5%)
	medium	(15%)
	coarse	(20%)

18-21" Gray and yellow colored sandy clay. Horizontal streak (2"wide) of red. Dense, compact sample. Clear, sub-angular sand grains.

Grain Size	Distrib	oution
clay		(55%)
silt		(5%)
sand	fine	(5%)
	medium	(15%)
*	coarse	(20%)

21-24" Gray and yellow sandy clay. 2" wide vertical red streak. Clear, sub-round sand grains. Dense, compact sample. Crumbles easily.

Grain Size	Distrib	ution
clay		(50%)
silt		(5%)
sand	fine	(5%)
	medium	(10%)
	coarse	(30%)

24-27" Clayey sand with swirls of red or gray between yellow/white swirls. Predominate color - yellow. Compact, dense sample.

Grain Size	Distribution		
clay		(40%)	
silt	•	(5%)	
sand	very fine	(5%)	
	fine	(5%)	
	medium	(15%)	
	coarse	(30%)	

27-31" Clayey sand with bands colored red, brown, yellow and orange. A 3" wide 1" high red section on one side of core. Very clear sand grains, sub-round. Dense, compact sample, crumbles.

Grain Size	Distribution	
clay		(40%)
silt		(5%)
sand	very fine	(5%)
•	fine	(5%)
Y	medium	(15%)
tw.	coarse	(30%)

APPENDIX IV

COPIES OF FIELD LABORATORY NOTES
FOR CALCULATION OF PERCENT MOISTURE
DETERMINATION OF ALL SUBSAMPLES



% moistre

•		4					
	Sample	oish wt.	WET LDISHT .sample)	Dry (Disht sample)	Dry sample:	0/a mois.	
1_6C 3	. 0-3"	1.009	11.01 (10.01)	2.78	1.78	62°/0	
	3-6	0.999	11.06 (10.07)	2.85	1.89	810/0	•
	6-9	1.009	11-109 (10:10)	4.32	3-32	670/0	
- -	9-11	1.009	11-189(10-18)	5.15	4.15	59%	
)	11-15	0.999	11.529	6.87		: 44%	
, •	.15-18	0.999	16.0(49	4.75		26%	
	118-21	0.999	6.279(5.28)	5.35	4/36		
)	21-24	11009	6.099(5.09)	5.169	4110 00		<u>.</u>
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	27-30	0.999	6.229(5.23)	5.32		制于%	
	30-33	1.009	(العلق والدما	5.30		\$ 160/0	
	.33-36	0.999	6.129 (5.13)	5.30		\$ 16%	
t b	36-39	0.89	(5.02)	5.20		Call 16 9/0	
* * * * * * * * * * * * * * * * * * * *	39-44	0.999	(م: 25 والناف	5:31 NE	4:32	16.10	
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	3-6	1.039	11-12	2.62	1.59	84010
	6-9	1:019	11.03	7.83	1.82	820/0.
t .	9-11	1.00	11-18 (10-14)	3.08	3.08	80% ·
i	11-17	1.009	· 6.559 (5.65)	3.33	2.33	580/0
	17-20	0.999	(5.494	5.14	445	17% -1
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	23-26	0.999	(5·n) (5·10)	5.12	4113	19%
	26-29	= 0.99	5.999	5.08	4109	18% 3
	29-32	1.00	(5.08)	:5.20	4120	17%
	32-35	1.00	(5.07)	5.23	4.23	17%
	35-38	1.00	(5:04) (6:04)	5-16	4.10	17%
	38-41	0.49	(5.09)	5.25	4.26	16%
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	59-64"			5.45		14%	
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	:		r entinge i en		inan mengerakan di kecamatan di Kecamatan di kecamatan d	n e som umatem men i de La comita de la comita del comita de la comita del la comita del la comita del la comita de la comita del la comita de la comita de la comita del la comita	
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						A LINE	
		7.4					
La Contraction						1	ere s
		المراجع والمستور والمستور			A 200 A		

1867	39-42"	واه،١	6.40)	5.539	4.52	14.010
	-/- ·		do moi			
	Sample #	Dish wt.	Wet (Dish+ Sample)	Dry (Dish+ sample)	Dry Sample	0/0 mois 11
C LBC	0-3"	0 . 48 9	11.010 (10.08)		٠ و ١٠٤٩م	87%
	, 3-4."	و اه ا	11.059 (10.04)		7. 1. 42	86%
	6-9"	0.999	6.02g(5.03)	:2·25g	- Jac 1	75*/0
	9-12	0.479	6.249 (5.27)	_52 = 3 + 9	1.40	74%
	12-15	0.999	6.019 (5.02)	£3.53g	2.54	490/0
4	15-18	0.999	5.999 (5.0)	و ٦٠٠٠	- 2.71	46%
	18-21	0.989	. 5.989 (5.0)	:4.969	3198	20%
	21-24	0.969	6.36)	:5.459	1.14.49	160/0 -
6	24-27	1.00 9	(5:31) (5:31)	£ 5489	ik:4·18g = ₩	\$ 220/0
•	27-30	1.019	6·05g	54.989	.d: 31974 : : : : : : : : : : :	210/05
	30 - 33	1.019	(5.05) وها٥٠ط	5-29g :	4 4.289 W	15%
	33-3le	1.019	(٥٠١٥ و١٥٠٥ س	_	_	\$. 15%
	36-39	1.019	(5،04) و ١٥٠٥ ما	. 5.40g	4.39	14.6
	39-43"	0.999	5.999 (5.0)	5·35g	1. 49.36 Ele	3130/0,
- LBC7	0-35	- Fliola	11.039	2.3793	the state of the	1 86 % To 34.
	3-6	mail olg	11.180 (10.13) 4.12.94.94	-1.95.200	80%
	1			_	2.15	7.3
	10-12	1.019	11.119 (10.10)	14.31g £	1330 SAL	67%
					5:78	
					3.61 . 115	
	18-21				4-24-04 <u>4</u>	
	21-24	و١٠٥٥	6.089 5.08) _ 5٠١3 _{- ١٤٤}	4.13	198%
39-42	24-27	1.009	45.00 G	5·22g	E 4.22	1306
E O	27-30	drolg	6.059 15.0	4) 5·0₹9 . <u>_</u>	4.00	19% ES
	30-33	د ودورا د ودورا	6.019	5.21g 2.1	4.19	110%
	33-34	1.029	6.109 (5.08)	_ 5-27g & W	3 4.25	16.06

samplet	Dish wt.	wet (Disht sample)	Loish- San	*	Day	ie ol	•
42-45"	0.999	(b.15	5.20		4.2)	w in	8%
45-48"	- D. 99	6.01	5.24	, •	4.25		50/0 1
48-51"	.0.99	6.0(5.07)	5.36				
51-54"	0.91	6:08	5.40		4. OT		
54-57"	1.01	6.14(5.13)	5.47		4.41		
57-60"	1.00	(5.0)	5.40	3	2.00		
60-63"	1.00	6.08(5.08)	5.48				
63-66"	1.00	6.02 5	·32		4.32		Mr.
66-69"	1.00	w.08 5	.41	Ţ	441	14	
69-72"	0.99	6:00 5	.42	ا مورود در د کور د د د	4.43	13' ************************************	10
72-75"	0.91	6-12 (5-13) 5	54		4.55		

nt'd)

			•	
olo	m	0	ŧ	sture

N.	,	<u>. </u>		ol- m	oisture	. (5-3) we	t-di,
				- <u> </u>		(5-3) 5 wet	,
			D 1	Wot	Dry	.	
		Sample #	Dish Wt	(Disht sample)	(Disht sample)	sample	mois
	LBC 8		1-01	3. 319 5	39) 1.879	0.869	8406)
		3 - 8"	1.05	_		1.189	780h
		811-11"	1.019		4.989	٠ <u>٠٠</u> ٤٠ عند.	25°70
G		W-14"	1.02	6.3-10 (5.	24) 5.08g	_4.0 leg	23%
10	Red	11"-14"	1.02	6 64 (50	sal 5.439	4.419	20%
	-	14"-17"	0.98	13:83 (bit		.;;. 5.429	2000
H	Red	17"- 20"	1.05	1.44 (s		2.459-	17°6
P	yllow	[7"-20"]	1:05	4.33 1	21) 5:47	4.429.4	
F	Phe	. 17 -ze."_	1.05	نا 38 وا	37 5.359	4139	1906
	Ž.	20"-23"	1101	6.56.65.21	51.489 : ±	4.429	14060
Ľ		234-26	11.09	10·56 (5·5	5.749	4.749	15%
H	•	20 - 29"	0.98	الع و 4 الم	5.389	4149	15°6
		29-32"	_0.97	10.019	5:303		14060
C	***************************************		·	·····	- A X 5	##:	
Þ	LBC9	0-34-1	30.995	109151	1 WATE	6.01680	43-40
	.	3 - 6	-4.019	(0.01g(5.0)) 1 2 105g	4049	710
F	· · · · - · · · · · · · · · · · · · · ·	6-12"	1.009	نه او <u>خون</u> ما	» <u>طعه</u> و	249	43600
P	<u> </u>	12-15"	واهداست	العا فالاط	5:93	4.089	25074
E	<u> </u>	- 18"		9 - 6.359 (6.3	5.45	4. +0	13.00
H		18-21	0.999	6·22 9 (5·3	5.40	4.41	16 orb
		21-24"	0.99		E 1 M 1	4.119	Jis of
F		. 24 - 27"	0.98	6.09915	(ग) के खेस	4.365	1500
1	· · · · · · · · · · · · · · · · · · ·	27-31"	0.98	45 45	44) 5-45	4.43.	F 1876
C		·		14. 04.			1.12.13
F	·	· .•		-	<u></u>	Total Control	
2) 						
4.4	į.	· · · · · · · · · · · · · · · · · · ·					

APPENDIX V

FIELD LABORATORY NOTES FOR DETERMINATION OF WET
WEIGHT OF SUBSAMPLES USED IN THE ON-SITE
SPECTRAL GAMMA ACTIVITY DETERMINATION



Spectral GAMMA Analysis

		vial+		. 1
sample+	t viatut	sample wt.	sample wti	
LBC3 0-3"	20.779	911799 -	71.02	
n _3-6	20.609	92.829	72.22	3 . 1
<u></u>	20.729	97.119	76.39	
9-11	20.619	101-249	80.63	
11-15	20:429	114.559	93.93	
. 15-18	20 619	130.689	HOOT	
18-21	20.585	121.939	: 101.35	. 1
21-24	20.659	· 121.779	1001112 益 統立	
24-27	11 22 40.79	117.679	96.88	7
27-30	20.71	.121.439	100.72	-1
30 - 33	20.64	119.109	98.46	-
33-36	20.62	118-64	18.02	
36-39	وْعَا 7.00	122.489	101.67	
39-44	20:039		98:22	_
LOCA		<u> </u>		
0-3		5010	M. A.	
1 13-le-31	7372162 - 14		78.70	-
6-9				às.
9-15	20.729		86.35	-
15-18		e e e e e e e e e e e e e e e e e e e	Same Line Land Control	
18-21	A Section Section	and the second	A-11 may and Color	•
21-24		 		*.
24-27	6 M. 78 A.L.	e de la companya de l	The second of the second of	
Z7 - 30	in the second of	La Carte Car	N YOU	-44-4
30-33		23 27 2	August 1	-
33-38	_21.019	127.969	. 106.97	

				•
	sample #	vial wt.	vial + s.	· sample wto sul
LBC:	2 0-3	20.629	87.749	67.12g
	3 - 4	20.67	86.87	66.20
	6-9	20.59	90.29	
•	9-11	20.62	91.04	70.42
K	11-17	20.58	106.41	85.83
Fø .	17-20"	20.72	128.38	107.46
Ľ	20 -23	20.70	123.79	103.09
F	. 23-26	20.70	124-18	241- 2103-48
•	26-29	20.72	121-38	2100.06
	29-32	20.71	113.35	92.64
H-	32 - 35	20.85	110-34	95.49
	35-38	20.70	119.00	298.36
	38-41	20.74	114.78	
•	I .	20.64	117.00	90:30
	44-47	20.63	107.79	U187:1U
				4 17 Su 94.81 day
•	50 - 63 <u>- 63</u>	20.61	11 6.43	<u>19±9</u> 5⋅82
	53-50	20.60	21108	100.48
-				<u> </u>
	59-42	20.01	119.51	98.98
F				2 3.09 1
•	65-68	20.63	<u> </u>	3.26
			•	3.73
F •			10.5° (c. 10.5°)	
13	•			

	sample#	vialuti	vial+ S. ut.	sample wto
LBC 4	0-3	20.969	91.409	70.649
	3-6	21.609	92.319	71:31
6	6-9	21.039	96.049	75.01
S	9-15	21.039	108.519	87.48
c	9-15	و949ء ٥٥	131.669	110.72
	15-18	21.049	134.339	113-29
	18-21	20.989	133.029	112.04
	21-24	21.029	136.949	115.92
	24-27	ن و٥٥١٩ ي	125.429	104.42
	27-30	وعا9 ٠٥٠ د	123-245	102-28
	30-33	20.969	120-159 100, 6 24	99-19
•	33-38	21.02	130.649	109.629
LBC 5	0-3 20.61	9 89.55 48.94	vial.	v+s 3.wt
2. No. 4			141-50: 20-71	
		- -	50:53: 20:71	
	•	•	63-56: 20-61	` - <u>.</u> `
* 2		200.00	56-59: 20.63	
!				115.70 95.12
			,	Mrs. Heren and Char
		128-13 107-5		
	26-29 20.74		8	
1		131.25 110.0	*	Hatev
	•	123.64 102.4	•	No. V. m. Company
	*85-38 20.73			and market
				ters talk
•			Samuel Continue Line 194	
•		128.08 107.4		

```
Sample#
                                                     Vial wt.
                                                                                 Vial+5
                                                                                                               Sample
                                                                                    92.889
                   ينين " 3 - 0 ...
                                                                                                                    71.839
1-BC 6
                                                    21.05
                                   و 20،99 ... ١٠٠٠
                                                                                    92.95
                                                                                                                  71.969
                    6-9"
                                                       20.949
                                                                                   101.289
                                                                                                                   80.349
                                                  20.989
                      9-12"
                                                                                   98.849
                                                                                                           77.869
                  . 12-15"
                                                      20.989
                                                                                    112-949 ... 91.949
                                             20.999
                  15-16"
                                                                                    116.219
                                                                                                         95.229
                  18-21"
                                             وها 8 يا ٥ د ال
                                                                                   134.63
                                                                                                             Wi-113.779
                  21-24" >= 20.939
                                                                                   114.22
                                                                                                             13.29g 13.29g
                                                20.269
                                                                                   135.459 4.14.79
                   27-30 1 h.
                                                                                   137.969 110.999
                                                     20.979
               ...30-33"
                                                 20-779
                                                                                 118.359 77.589
                  , 33-36" 20-1619 .
                                                                                   117.19 1 16.589
                                                                                  118.659 ___ 97.94
                  30 -34"
                                                      20.719
                                                                                  109.579
                                                                                                                88.47
                  39 - 42"
                                                      20.90 g
                 وما - الله و المديد الم
16-10 29 $ 95 Hag 3439 1 1
            10-12 - error 20189 5 35 93:845 4 173:09 1 444 TELEVILLE
                  . 12-15
                                  20.989 113.349 192.369 74
                  15-18 _ 20.57 _ 130.03g / 109.46 . &
                  . 18-21
                                                 20.589 139.949 119.36
              -1-21-24 20.73g 120.93g 100.2g
                  24-27 20.959 122.989 4 102.039 1 104 10 10
                 27-30 21.03, 21/13.834 92.89 1 A'AA
            √° 12,30 -33
                                       -20.969 1167199 n. 13 96.04 141 - Hitz
```

BC 6 (cont'd)	vial	vial+ 5,	sample
42-45	20.729	114.559	93.83
45-48	20.72	122.40	80.101
- 48-51	20.64	121.34	100.709
51-54	20.64	121.49	100.85
54-57	20.78	115.38	94.60
57-40	20.76	112.58	91.82
60-63	20.77	114.15	93.38
13-66	20:70	:117a1	90.41
16-69	20.60	111.68	91.08
129-72	20.71	114.88	94.17
72-75	20.61	93.799	73.18
•			

Petri Dish

LBCL	Dish	Dish+s	Sample
12-45 15-48	3.15	4.15	1.00
48-51	342	4.12	1.00
1-54	3.18	4.18	1.00
: 4-57	3.18	4.18	1.00
57-40	3.08	4.08	1.50
60-63	3:14	4.14	1.00
13-60	3.15	4.15	1.00
66-69	3.07	4.07	iloo
69-72	3.25	4 - 25	£. 50-1
- 1- - 15	3.26	4.26	1.00

يق ا		<u></u>		· · · · · · · · · · · · · · · · · · ·		
7	9 1	•				
				•		
						ř
		A sequence of the control of the con	vial	vial+3	Sample	B) No. 11. See and 11. See and
		LBC 8 0"-	5" 20.94	101.25	80.299	······································
4	9am 3-21-85	3''- 8	21.00	1100.08	79.06	•
		6"-1	21.03	115134	94.31	
		Blue 11"-11	4" 21:07	141.20	1.20-13	· Managements
			4" 20.00		115.64 g	
	e description for the second		20.93		-	·
40	n name destrois de la constante de la constant		20:05			
			20.95			
		B 17"	40.12 02.	12.6.47	105.43	The state of the s
		7.0"	231 2104	179:45	introductor :	ta i
70)	73"-	20 20.93)34.54	÷ 112.11	and the second second
1999	:	20 -	29" 20.93	121.42	11.4.019	
			32"20,94			•
	stanted		<u> </u>	3+	_	
		18 6-93		774		. **
	3-21-85	3-6	, –	· · · · · · · · · · · · · · · · · · ·	-35	40 t
	*		واه. احسب			
	t L		21,029		, <u>-4</u> ,	2.00
	90		811.01	_		At The contract of the contrac
1			11.009			
		71"-2	4421:029	_131.629	وها ١١٥٠ سي	
7-9) · · · · · · · · · · · · · · · · · · ·	74 - 2	7 20.979	122.889	بروله اهد	
1		22-31	21:04'9	122, 349	101.329	
			namenanie i i i i i i i i i i i i i i i i i i			10
45		- consider the community and a second second				
Po) ************************************			**		

APPENDIX VI

FIELD LABORATORY NOTES FOR CALCULATION OF DRY
WEIGHTS OF SUBSAMPLES USED IN THE ON-SITE
SPECTRAL GAMMA ACTIVITY DETERMINATIONS



	DRY WEIGHT		Isamoie .	
Sample #	b mois	1-0/0 mois	wetsample only) Vial wt	Dry weight
.0-3	92%	0.08	U7·12 -	- 5.369
-6	84%	0.16	66.20 -	-10.51g
1,-9	82%	0.18	69.70 -	_ 12.54
4-11	80%	0.20	70.42	_ 14.08
	6 8°b	0.42	86.5 ³ —	- 35.92
17-20	170%	0.83	107.06	89.35
2-23	17%	0.83	103.09 -	85.50
3-26	19010	0.81	103.48	- 33.81
	18%	0.82	100.00	82.54
: 1-32	17%	0.83	92.04 -	- 76.89
32-35	170/2	0.83	95.49 -	- 74.25
	170%	0.83	98.36 -	- 81.63
.55-38	10 0/2	0.84	94.04	78.99
8.41	10010	0.84		- 80.94
41-44	130/0	5.87	87.10	- 76 82
3.50	16.010	6.84	94.81	- 3-9.04
50-53	15'10	0.85	95.13.75	-81:44 7
53-56	140/0	0.81	100.98	51. 7 9.3
6.59	-16%	0.84	95.82	- 60.418
59.42	150%	0.85	98.98	8410
42-65	15%	0.85	93.09	3072
25-68	16.16	6.84	93.26	- 39.33
68-71	13%	D.87	93.33	- 8134
71- 74 -	990	0.91	83.40	- 75.UY X
		and the second		

71 700 400	9-15"	60%	0.40	86·35	34.545	- A -
	33-38"		0.83	106-97	88.789	
)	. <i>95-</i> 58			wet.	. •	
	<i>:</i>	÷		sample wt		
	Sample #	% mois	1-0/0 mois	(invial)	Dry	. *
1864	0-3"	84°/0	orlu	70.649		A
	3-6	80°/0	0.20	71:31	14.26	is N Symp
	6-9	₹6 %	0.24	75.01	18.00g	•,
	ิ _{9 -} เร	60%	0.40	87.48	34.99	-
•	9-15	240%.	9174	110.43	81.93	
	15-18	20%	0.80	113.29	90.63	-
	18-21	19%	0.81	112.04	90.75	
	21-24	18%	0.82	115.92	95.05	
	24-27	7.10	0.83	104.42	80.00	
	27-30	14%	0.81	102.28	81-84	
	30-33	16%	mj. 0184	99.19	83.3	
	33.38	17%	0.83	109.62	90.98	File
18c3	4:3°	\$29/0	15-18	71.02	142.150	1774
	3-4-6-2	1 8 %/o	19	42.2.2		
73.		1.7-/				
				T Value		
	7=4.		3 D 4	# 480.45		
	1133	44.10	5.56	33.93	7 12	
	15-18	44./o 44./o 26%	0:74	10.07		
4	18-31	18%. 18%. 18%.	0.83	101.36		
	21-24	18%	0.82	1 10 12	11111	
	24-27	18%	D.82	94.88		
	27-30	170/2	p.83	2 00.72	3.51	
E TOTAL	30 -23	1 10 10 10 10 10 10 10 10 10 10 10 10 10	141			
A" W.	AT CONTRACT		第 小师	1		
	27.36		Political Property of the Political Property	3:02		
	34.59	1 6 7	0.84			7
	39-44	10%	· 84 .		100	
THE STREET OF THE STREET STREET	ere oracis zenember - B	CONTROL TO THE PROPERTY OF THE PARTY OF THE	中國新門區 有數學學可以			

	ند. آ	• •				. •
3	7. 3			Wet		•
	Sapple	% mois	1-% mais	sample (in bial)	Dry	
LBC 5	(-0-3	86%	•	68:94	9.059	****
Carlos ago	3-6	80%		31.58	14.3)	
	16-9	71%	0.29	_	21.67	7
,	9-14	79./0			: 15.15	11
	14-17	67010		\$ 82.62 ·		
	17-20	50%		90.51	and the second of	
r _e	20-23	30°/•		110.81	73.50	
	1	22:/-	3.0	117.48		
	29-32	200/0		110.64		
	32-35	280/0		102:94	13.4	
f .	ましゅう ここ 子は高いで、	11470/0	0.53	*** Z ***	53.67	
	38-41	.34.	0.30	ارة الإلا القارة الإلا	33.63	
	41534	a la Ve	-83	995	4.5	
	94.41		0.82	10	110	
	1 - 2°		0.77		ATT LOT	The Later
			0.82		125.18	
		. 24% - 4	0.86	95.5		
		40	0.86	144		
	77				1 4 4 4	3
						Č
					ar.	
The state of the	A THE REST OF	7.5		4 4		- L

¥ .**

دوس	Sample#	% nois	1- % mais	wet Sample	Dry
	42-45	18%	0.82	<u>w+(9)</u> 93:83 9	7 6.94g
•	45-48	15%	0.85	101168	86.429
	48-51	140/0	0.86	100.70	86.60
11 ·	51-54	13%	0.87	100.85	87.73
the state of	54- 67	13%	0.87	94.60	82.30
	67-60	12%	0.88	91.83	80.80
	60-63	12%	0.88	93,38	8 2.14
	63-66	140%	0.86	96.41	82.9
	46-69	13%	0.87	91.08	79.23
, ,	69-72	120%	0.88	94.17	82.86
	72 - 75	11%	0.89	73.189	ا ا و3:30 و
	•	4			- 1 i

LBL7	39- 42"	160%	0.84	96.199	80.799	;
		•				• •
					*	
*	Sample#	olo mois	1- % m.	vial wet wt.	Dry wt	
LBCL	0-3"	87%	043	5. 15. 71.83	9.339	
	3-6	860/0	0.14	71.96	e F Q :01	
**************************************	6-9	75%	0+25	80.34	20.08	
	9-12	74%	10,26	£7.80 j	20:24	
	12-15	49%	0.51	j 91.96	46.89	
1	15-18	46%	8.0.54	95.22	51.41	
	18-21	20%	. 0.80	113.77	19101	
	21-24	10 %	0.84	03.29	3	
	24-27	22%		114.74	89.53	沙堡
	17 - 30	210/0	0.74	10199	12.42	
	30-33	15.%	0.85	47.58	1 82.94	
	33-34	15%	0.85	96.58	1209	
	36-34	14%	20.86	97.94	452	TANK.
PC T	39-43	13%	.p. 10.87	\$8.67		
74	9-3 /6	86%	-10.14	9.74	100	
		20%	10.70	70.83	Phila	
	4 6 - 90 A	340/	1 0.21	4.31	in the first	
	10-12 T	1,7%	0.83	127310	100	
	12-15	45%	20.55	1 7 7 2	10 79	
	NS-18	31.0/2	20.69	L lo lus to		
3-28-847	18-21	23%	J. 77.	41.9.34	1220	
	21-24	19%	4.00	100.20	13/6 (1)	
	24-21	17%		0.000	The Course	
	27-30	190%			1 21.00	
	30-33	16%	0.84	1000	1 1 27	
	33-36	P. P.	35.84	11.03	12.5	
	31	TO TO		· 在 10 mm	******	

		DRY	WEIGHT		
	S.C. C.	A	0/	vial"	12.84 9 12.84 9 12.84 9 12.50 12.50 12.50 12.51 85.27 85.27 85.34 91.23 91.23
4 K 3		The same of	- /o mois if	24	WT.
84.9	G 3/5/	84%	فا ٥	80.299	12.84 9
4373		78%	0.22	79.08	17.39
	711	25%	0.75	94.31	70.73
	1.4	22%	D. 11	120.12	
					12.50
		70 /o	0.80	115.0f	92.51
	T. ITA	20%	0.80 T	106:59	85 274
	420	17%	0.83	104.54	\$8.421
	300	160/0	0.84	9703	
		1906			
	20'-23'	16%	0.84	108:00	91-23
	23 -26	15%	0.85	والمجانا	96.14
	29'-32	15%	0.85	11 4.81	97.58
	29:-3 à	140/0			95.02
A Low	A 7				
		87%		ในวันผู้เกรีย สะตัด	
LBCT	D = 3."	87%	0.13	U 6.819	8.68
	3 - 4	79%	0.2K	72.829	15.29
	ø 12:	34%	0.64	48:87	63.27
	- 12 - 1 5	20%	0.80	109,52	87.41
		17%			4
	TION OF STREET	e de la companya de l	0'85.	104:50	4 86.43
	8-284	160/0	0:84	107.10	\$9.96
	21-24	18%	0.82	110:00	90.69
	24-27	15%	0.85	101.41	86.62
	24-31"	18%	0.82	101-32	·
		÷ .	1	70 1 JA	
	Asset Market Market Market Market	- And		,	

APPENDIX VII

FIELD LABORATORY NOTES FOR THE PREPARATION OF DRIED SUBSAMPLES FOR THE ON-SITE GROSS ALPHA AND BETA ACTIVITY DETERMINATION



FROSS Alph	* ** * *	Beta	Anay :
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16.	it is			6
	GROSS Alph	a and Beta	Anay 200	•
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0-3" 3:19.1	4:19	1.009	* Volponificação d'all rein-	*
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6-9 3.10	4.16	1.009	man and the control of the control o	
9-11-, 3:14	4:10	1.009	e*	**************************************
11-15c . 4c 3116.	4:10-	[1009]	4 - Grand Grand	4
15-18 1 2 303	4:072000	1:004	e e magazinana jiyaya <u>.</u>	\$
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24-23-3-07	4.07	1.00	ing of the same and the same in the same in the same of the same o	9
27-30 4 3:14	, 4:14	1:00	e anna com	
30-33	4.10		#S.	7
35 34. 3.09.	4.09	1.00	consist to) 7
.36:39., .3.12.	4.12	1.00		•
39-44, 316-4	4-16	l·oa	r man grange.	77.
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24-27	en e			
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11 LBC 2 Pem Dish	Sample Sample	The second secon	
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3:09.	4.09 1.009		0) 2
9-11 65 3.15	4:15		
3.15	4:15 1:00		•
12-20 3107	4.07 1.00	,	•
20,23 3.09	4:09 1:00		9~
23-26 3.16	4:14 1:00		-
26:29 3:13	5 4.13		→
29-32 3-19	4/19		•
32-35 3-18	4.181.00	•	•
3538 3.18	4.18		0 7
38-41 3-19	4.19		•
41-44: 3:09	4.09		•
44-47 319	4.14 1:00		6
47-50 3:15		C.	•
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53-56 3.07	4.07	• • •	
54-59 3.12.	4.12 1.00		•
59-62 3.19	4.18	·•	99999
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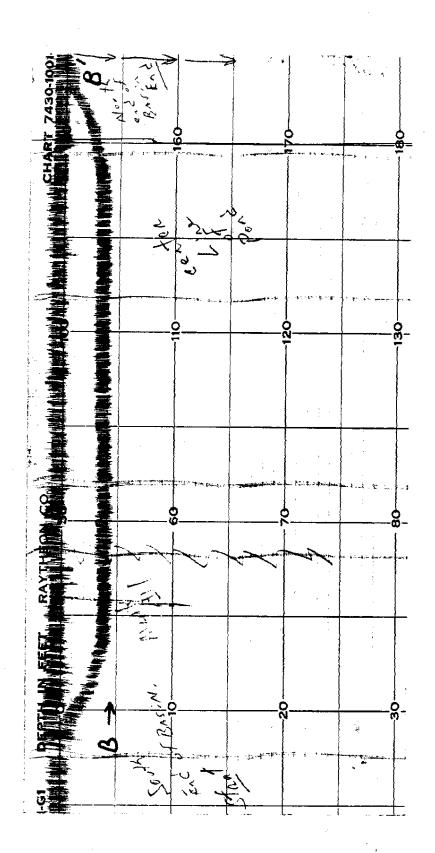
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	. 3.159 Som 4.159		
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	.3.10g 1 : 4.10g		· · · · · · · · · · · · · · · · · · ·
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_Z7-30	3.099 4.099	1.009	(1)
30 - 33	,	1.00g	▼ <i>D</i>
		1.00g	. •
4.36-39	3-189 4-189 a	1.00)	

	làm	into Pet	ri Dish				7
:L8C8	Perri Diske		Sample	· ·	3-22-85 9130am-1	1:30 am	7
* Q!4.3!	3.124		Q:770	· · · · · · · · · · · · · · · · · · ·	in the second se		*
311-1811	3.08	4.039		and the second s	1.1		
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14" F	3.19	1.179	409	4-	and the second district of the second second	<u>Lade</u>	•
PE13	3:149	4:109	- <u> </u>	., <u></u>			-
H = 20	3.144	4.149	1909	· ·		نمغ	•
	1. 3.154	1.0	\$ 1,000			_willy-	•
latz. B	3.064		1.00 g.			- Luc	-
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	3:159		2/1:009		· · · · · · · · · · · · · · · · · · ·		
· 212-29 "	* , *		1.009				*
6 1 32"	3:089	4.089	وهميا	<u> - , 1 </u>		- -	-
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₹. ~ ⊌. "	3:129	4.01.9	-0.899	***		e e y an	6
le - /2"	-3.189	4.189	1.009				-
12-15"	3499	4199	1:009		و مصادرة الأوام		-
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18-21"	3.209	4.209	1.809 -	· · · · · · · · · · · · · · · · · · ·	5 -80 ser .	V	•
21-, 24"	3.199:	4.195	1.009	* · •	4 - 4 .		-
24 - 27"	3.149	.4.149	1.009		, e e		-
27-31	3.099	4.099	1.009		•	3	-
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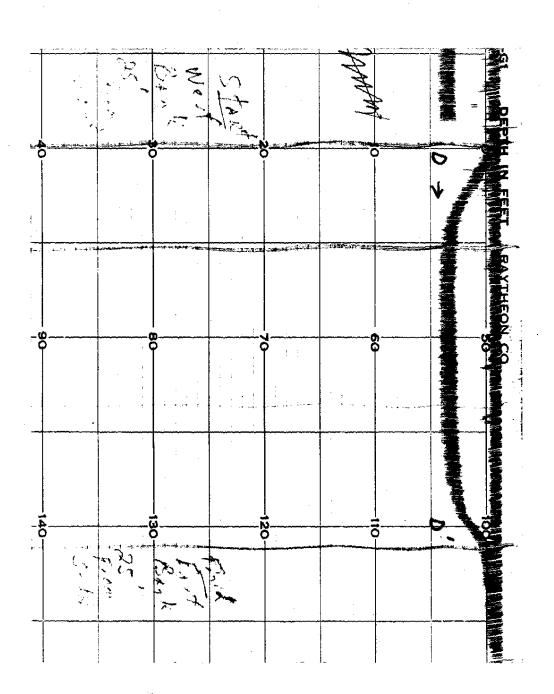
APPENDIX VIII
FATHOMETER TRACES



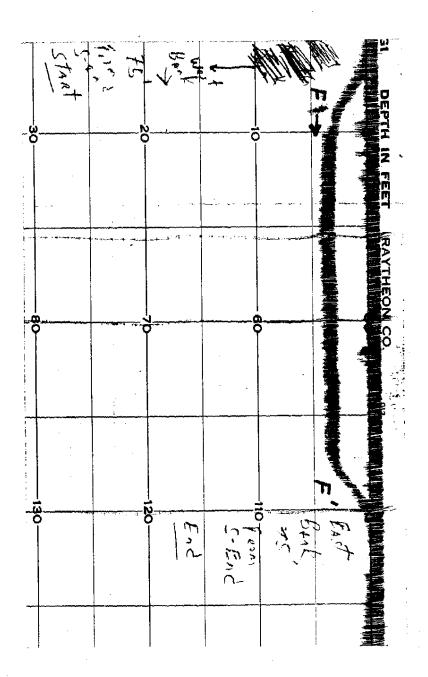
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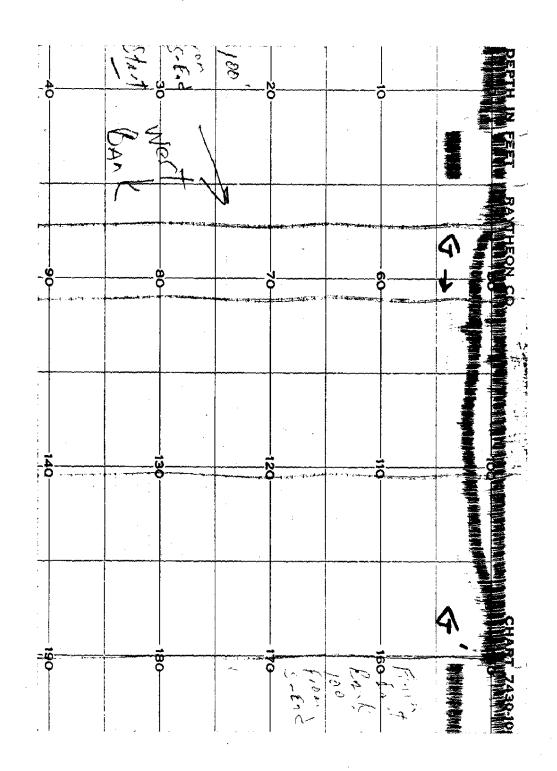
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APPENDIX IX LAB NOTES/COPIES OF GC CHROMATOGRAMS FOR ALL RE-RUNS AND FOR PHC ANALYSIS



8-19-85 2086-00110 Dupont Petroleum Hydrocarbons/soil Reruns (see pg 134-136)

6042	Col # 324
Operator Dok	_ Date _ 8/14/85
Celumn	Detector_F/A
Length 30 M	Range
DIA DITSO MM	Atten. 214
Liquid Phase SP8 - 5	
W. % Lum film Thick	Flow Rates, ml/min. Hydrogen 30 Air 300
Support	Scavenge
Mesh	Split
Carrier Gas HC	_ Temperature, *C
Rotsmeter	- Det. 250 In 225
Inlet Press 3/5 psi	g Column Initial _35-40
Rate	n . Final 300
CHART SPEED _0.50 cm/	MIN Rate 8
SAMPLE _30/	Solvent CH2C
Size 4M	- Conen.

Extraction Procedure: 10g of sample was extracted (Soxhlet) with 250 ml Methylene chloride. The extract was concentrated to 10 ml in methylene chloride. The extract concentrated were analyzed by GC/FIB of the above conditions. Injection volume was 4 ml in order to achieve maximum sonsitivity.

JD Blank CHZCIZ

PKS at 3.16, 4.48, 5.40 will not be included in Flandard response calculation.

A) Naphtha 264 jug/ml # 1661-1

R.T. Total Response #2 #14 #26 #35

5.71-13.68 305895 361781 286504 299069

133312 # of peak

SAW 8-2005 1 8-19-85

8-19-85 2086-110 Dupont Pot Hydroundons /soil Reruns contid

(42)(500) x 264 ma/ml x 10 ml/x x 24 4.42 mg/g)

- 3) M. Blank E.S. # 3913 Ext'd 6/3/85
- A) 76110/18-21
- 15) 76111/21-24
- 16/12/24-27
- 1) 761/3/27-30
- 18) 74114/30-33
- 9) 76/15/33-34
- 10) 76/16/36-39
- VII) 76/17/39-43
- 12) 76/18/48-51

} all empds = DL

all empds = DL

- * 13) Blank CH2Cl2
 - M) Naphtha 264 µs/ml # 1661-1
 - 15) 74119/34-57
 - 16) 76120/60-63
 - A) 74121/66-69

18) 76/22/72-75

all empds < DL

19) M. Blank E.S. # 3918 Estracted 6-5-85 all capples LDL

SAN 8-20-85 8-A-85

8-19-85 2086-110 Duport Pet, Hydrocarbons/soil Reruns contd. (20) 76110 A/18-21 120 76110B/ 162) 76111 A/21-24 - all empds < DL 133 76111B/ 761124/24-27 \$5) Blank CHZUZ (36) Naphtha 264 us/ml # 1661-1 -51) 76112B124-27 128) 76/13 A /27-30 SA) 76/138/·11 SU) 76/14 A/30-33 all empds = DL 131) 7611481 11 132) 76 115 A/ 33-36 /33) 76/15 8/ 134) Blank CHZCIZ /35) Naphtha 264 pg/al # 1661-1 DOK 8/19/85

8/19/85

18-20-85 2084-10 Dupont Pet. Hydrocarbons /soils veruns contd
(S) 76115/33-36"
16) 74116/36-39"
17) 76/17/ 39-43"
18) 76/19/54-57" all cupeds < DL
19) 76/19/39-57 all cmpds < DL
120) 76121/46-69"
(21) M. Blank E.S. # 3933 Extracted 6-20-85
12) 76949/76959
123) 76950/76960 Pet, Hydrocarbons < DL
1 25) Blank 4242 that are not petroleum hydrocarbons.
· · · · · · · · · · · · · · · · · · ·
(26) Naphtha 264pg/ml #1661-1
127) 76956/76966
My Collin On BAC
130) 76957/76967 DUP. I that are not pet, hydrocarbons,
132) Blank CH2Cl2
lost air (tank depleted) flame out.
1 53) Naphtha 244 pg/ml # 1661-1 do not use.
1 10Kning 8/20/85
5×20 8-20-8

```
DIL FACTOR: 1.0000 E+ 0
                                        8/14/85
2086-110
Jupont
 ATTN 2+
 TEMP1
           400
                  35
                       35
 TIME1
             4.00
 RATE
             8.00
 TEMP2
           488
                 300
                                  pet. Hydrocarbons/soil
 TIME2
            28.88
 INJ TEMP
           499
                 225
                      225
                                          Reruns
 FID TEMP
                 258
           488
                      250
 AUX TEMP
           488
                      225
                                         61#324
 CHT SPD
             9.59
                                         DOK
4 pl inj
 ZERO
            15.0
                                                     attn = ar
 ATTN 2+
             4
 FID SGNL
             +B
 SLP SENS
             0.10
 AREA REJ
                 1888
 FLOW
                    28.0
 FL0₩
       8
             8.8
                    43.7
  0.50 YLY/EXT-
 20.00 STOP
DELETE MIN? 2 8 8
STOP MIN? 3 8 2
CHANGE RUN Ø @
START
                                                  1)
       ٧L
                           Blank CH2C12
                                                                   3.16
                                                4.43
                                                                   5.40
                           7.19
```

13.64

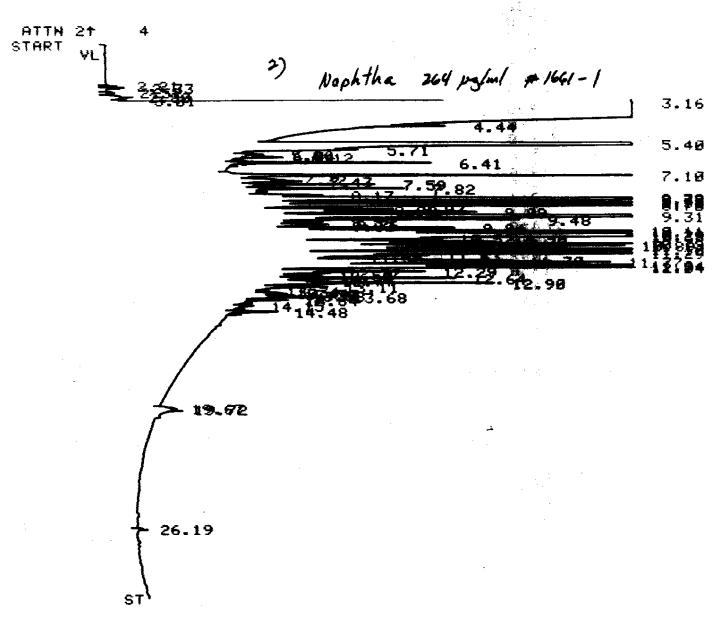
1602

```
HP RUN # 1
BOTTLE 1
AREA %
```

RT AREA AREA %

3.16 1546**00000 99.871** 5.40 199**600 0.**129

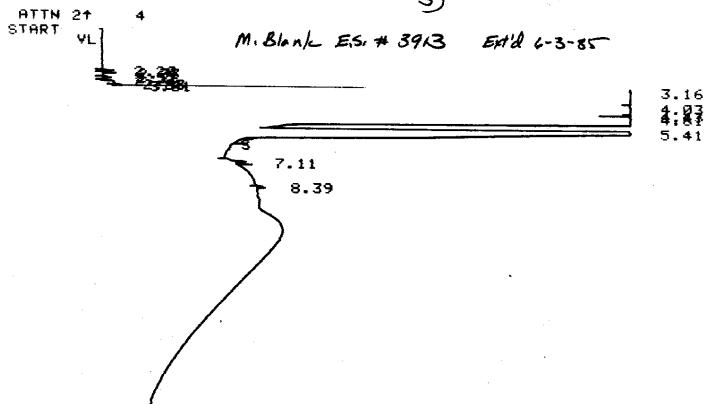
DIL FACTOR: 1.0000 E+ 0



HP RUN # 2 BOTTLE 2 BREA %

RT	AREA	AREA %
3.16	154400000	99.675
5.40	197300	Ø.127
5.71	2294	0.001
6.41'	2593	0.002
7.10	9 0 98	9.996
7.43	1329	0.001
7.59	1731	0.001
7.82	1994	0.001
	- -	

```
8.32
                  9146
                              0.006
   8.39
                  6750
                              0.004
   8.55
                  7284
                              0.005
   8.70.
                 14330
                             0.009
   8.93.
                  1899
                             0.001
   8.98.
                  1141
                             0.001
   9.89
                  3716
                             0.002
   9.31.
                 38520
                             0.025
   9.48
                  3804
                             0.002
   9.59.
                  1424
                             0.001
  9.76.
                  1181
                             0.001
  9.94
                  3002
                             0.002
 10.11.
                 11889
                             0.008
 10.29.
                19778
                             0.013
 10.38.
                15070
                             9.919
 10.52.
                 3008
                             0.002
 18.78.
                 5925
                             9.003
 18.79.
                 5664
                             9.884
 10.89
                 5177
                             0.803
 18.97
                 3305
                             0.002
 11.10.
                19518
                             8.913
 11.29.
                35240
                             0.023
 11.43.
                 3712
                             9.992
 11.55
                 1362
                             0.001
 11.70-
                 5166
                             9.993
 11.77
                 7214
                             9.995
 11.94
                 7914
                             9.995
 12.84.
                26418
                             0.017
 12.29.
                 3747
                             0.002
 12.37
                 1082
                             0.001
 12.50.
                 1350
                             0.001
 12.64
                 3431
                             0.002
 12.77
                 1244
                             0.001
 12.90
                 4416
                             0.003
 13.11.
                 1538
                             0.001
 13.68 -
                 1420
                             0.001
DIL FACTOR:
            1.0000 E+ 0
```



```
26.21
```

```
3
             3
BOTTLE
AREA %
```

RT	AREA	AREA %
3.16	148400000	95.391
4.83	52 0000	3.343
4.43	12768	9.998
4.61	1502000	Ø.965
5.41	455800	0.293

DIL FACTOR: 1.8888 E+ 8

ATTN 21

4) 76/10 18-21"

7.09 8.39 19.73 21.27 26.21

HP RUN BOTTLE

```
AREA, %
    RT
                   AREA
                             AREA %
   2.82
                  16050
                               0.007
   3.13
             131400000
                             57.673
   3.65
                292388
                               Ø.128
   3.76
                689000
                               8.392
   4.19
              87299999
                             38.273
   4.66
               7856999
                               3.448
   5.40
                382200
                               Ø.168
 DIL FACTOR: 1.0000 E+ 0
  ATTN
        21
                                           21-24
                           5) 76111
START
        YL
                                                                3.80
                                                                         4:49
5:42
                                           <del>5 . 18</del>
                            7.09
                             18.68
                            11.29
                         13.77
                  269167
                 21.26
HP RUN #
             5
BOTTLE
         5
AREA %
   RT
                  AREA
                            AREA %
  2.66
                  2089
                              8.000
```

2.81

3.07

3.43

3.52

3.80

4.40

4 70

74428

31828

124788

3769888

3188**00000**

73448888

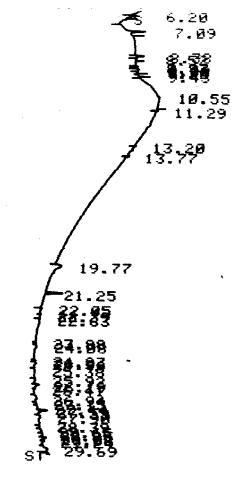
9.917

8.887

0.029

Ø.882

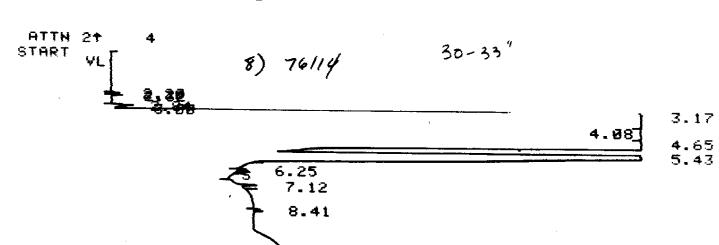
74.628

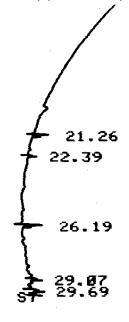


HP RUN # 7 BOTTLE 7 AREA %

2.66 1268 8.8 2.81 47159 8.8 3.18 18528888 29.8 3.88 2478888 8.2	×
3.18 18528888 29.8	99
	13
7 99 - 0470000 - 0 2	92
3.80 2479999 9.6	83
4.34 230700000 63.7	97
4.74 22629999 6.2	
5.42 573799 9.1	
10.55 1954 0.0	

DIL FACTOR: 1.8888 E+ 8





HP RUN # 8 BOTTLE 8 AREA %

RT	AREA	AREA %
3.17	1582 99999	88.662
4.98	16310000	9.141
4.65	3291 000	1.844
5.43	63 8888	0.353

24.93

DIL FACTOR: 1.0000 E+ 0

ATTN 2+ 4
START VL 9) 76/15 33-36"

9) 76//5
33-36

4.63

4.63

5.43

19.78

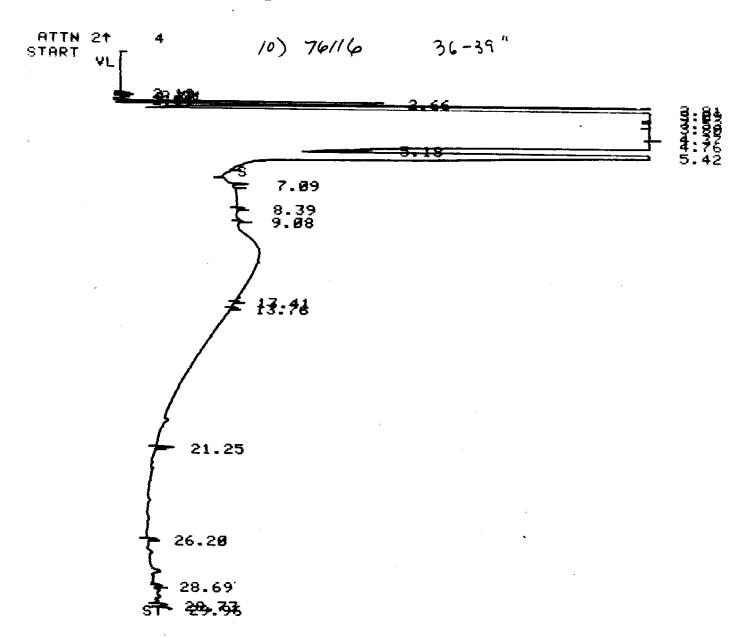
11.25
22:35



HP RUN # 9 BOTTLE 9 AREA %

RT	AREA	AREA %
3.19	1638 88888	94.578
4. 9 4	6972 888	4.825
4.63	19 8 3 88 8	1.899
5.43	5213 00	9.391
10.78	7464	9.994
11.29	1435	9.991

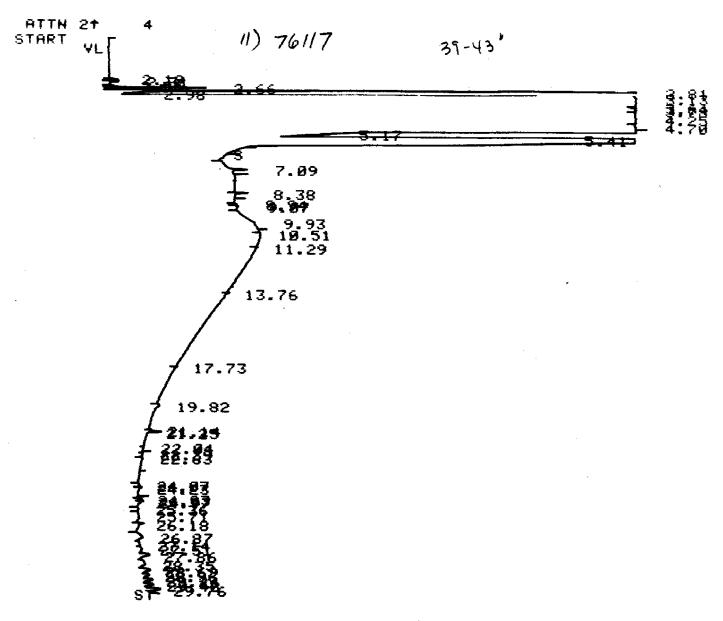
DIL FACTOR: 1.8888 E+ 8



HP RUN # 10 80TTLE 10 AREA %

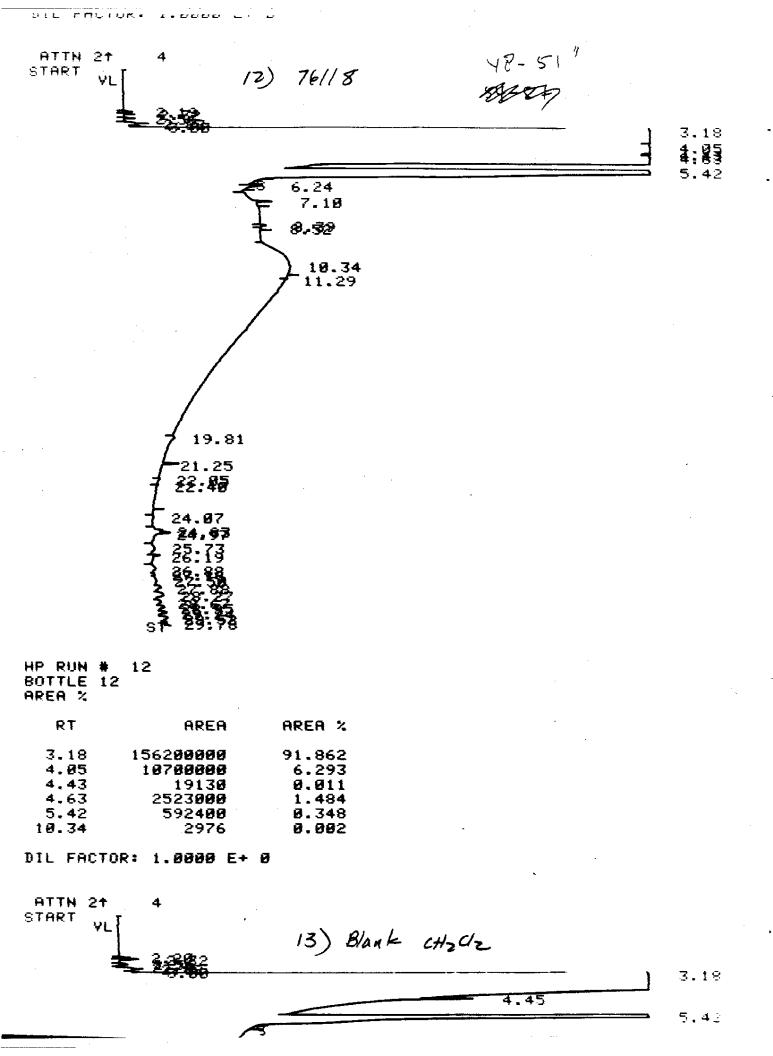
```
2.66
               1879
                            9.999
2.81
              65868
                           9.916
3.89
3.52
3.80
                          23.998
          95828888
              3818Ø
                           0.010
            3109000
                           Ø.785
4.37
         271200000
                          68.469
4.76
                           6.589
          26100000
5.42
             555700
                           0.140
```

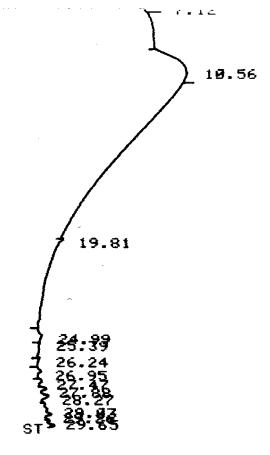
BIL FACTOR: 1.0000 E+ 0



HP RUN # 11 BOTTLE 11 BREA %

RT	AREA	AREA %
2.81 3.13 3.64 3.78 4.25 4.70 5.41	25238 125488888 172788 1198888 132888888 13538888	8.889 45.948 8.863 8.439 48.366 4.958 8.214
11.29	4001 2125	0.001 0.001

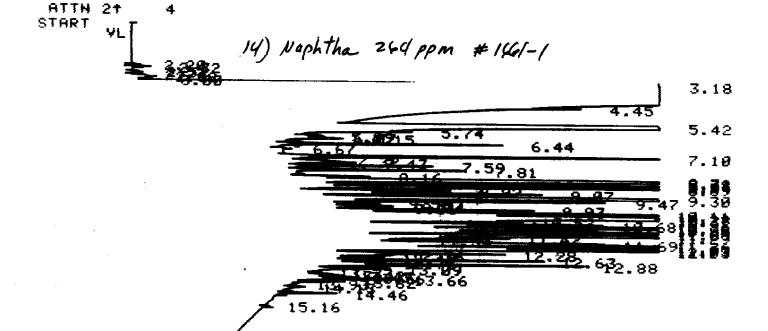




HP RUN # 13 BOTTLE 13 BREA %

RT AREA AREA %
3.18 158700000 99.871
5.42 200700 0.126
10.56 4065 0.003

DIL FACTOR: 1.0000 E+ 0

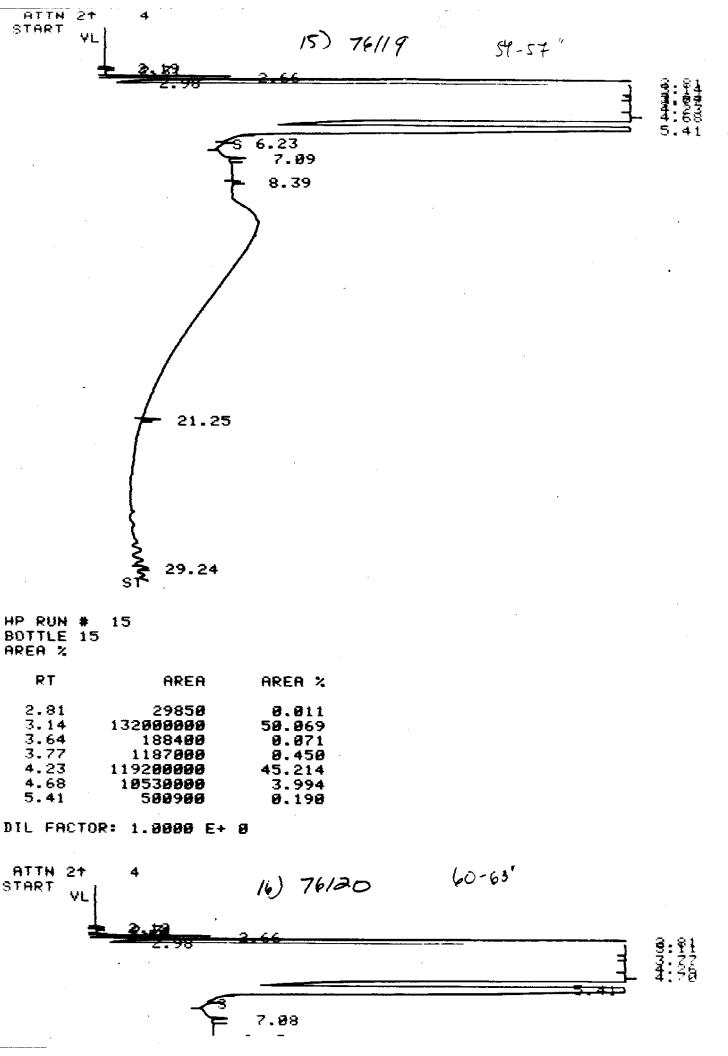


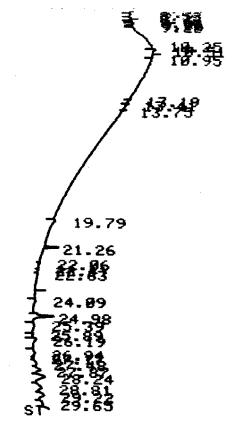
ST

HP RUN # 14 BOTTLE 14 BREA %

RT	AREA	AREA %
3.18	171400000	99.662
5.42	220000	9.128
5.74	1889	9.991
6.44	2982	9.992
7.10	10150	9.996
7.43	1458	8.881
7.59	1936	8.881
7.81	2394	9.991
8.16	1231	0.001
8.31	19399	8.006
8.38	7672	0.004
8.54	8892	0.005
8.69	16160	9.889
8.92	3357	0.882
9.07 9.30	4127	0.002
7.30 9.47	43988	8.826
9.58.	4406	0.003
9.74.	1954	9.991
9.81	1717	9.991
9.93	1292 3913	9.991
18.11	14368	8.88 2
10.28	23120	8.99 8 8.9 13
10.37	17710	0.013 0.010
10.52	37 80	9.982
18.68	6211	8.884
10.78	6882	9.004
19.88,	6269	9.994
10.95.	4814	0.002
11.09	23030	8.913
11.29.	40980	8.824
11.42	4661	9.993
11.54	1816	0.001
11.69	6384	8.884
11.76	8688	0.005
11.93	9496	0.006
12.93	38888	0.018
12.28.	4876	9.003
12.36. 12.49.	1495	0.001
12.63	1973	9.991
12.76	44 0 2 1775	8.883
12.88	5628	9.881
13.09	2503	0.003 0.001
13.66	2J 0 3 1916	
	1710	8.881

4ን DIL FACTOR: 1.8888 E+ 8

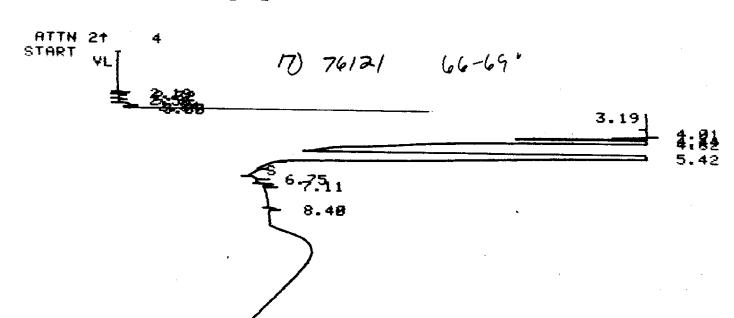


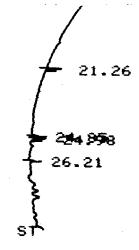


HP RUN # 16 BOTTLE 16 BREA %

RT	AREA	AREA %
2.81	29478	9.911
3.11	112900000	40.823
3.77	158 5000	8.573
4.26	147100000	53.189
4.78	14499999	5.207
5.41	546 000	8.197
10.95	1251	8.999

DIL FACTOR: 1.0000 E+ 0





HP RUN # 17 BOTTLE 17 AREA %

RT	AREA	AREA %
3.19	1639 00000	99.307
4.81	574400	Ø.348
4.44	1745	9.881
4.62	133200	0.081
5.42	434688	Ø.263

DIL FACTOR: 1.0000 E+ 0

ATTN 2+ START ... 18) 76122 72-75"

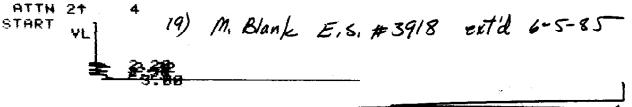
3.171 **6.43** 7.88 8.37

21:37 26.19

```
HP RUN # 18
BOTTLE 18
BREA %
```

RT	AREA	AREA %
3.17	151199999	89.142
4.06	1478 9999	8.729
4.63	3136888	1.859
5.42	4883 99	Ø.288

DIL FACTOR: 1.8988 E+ 8



3.19
4.45
5.42
11.67

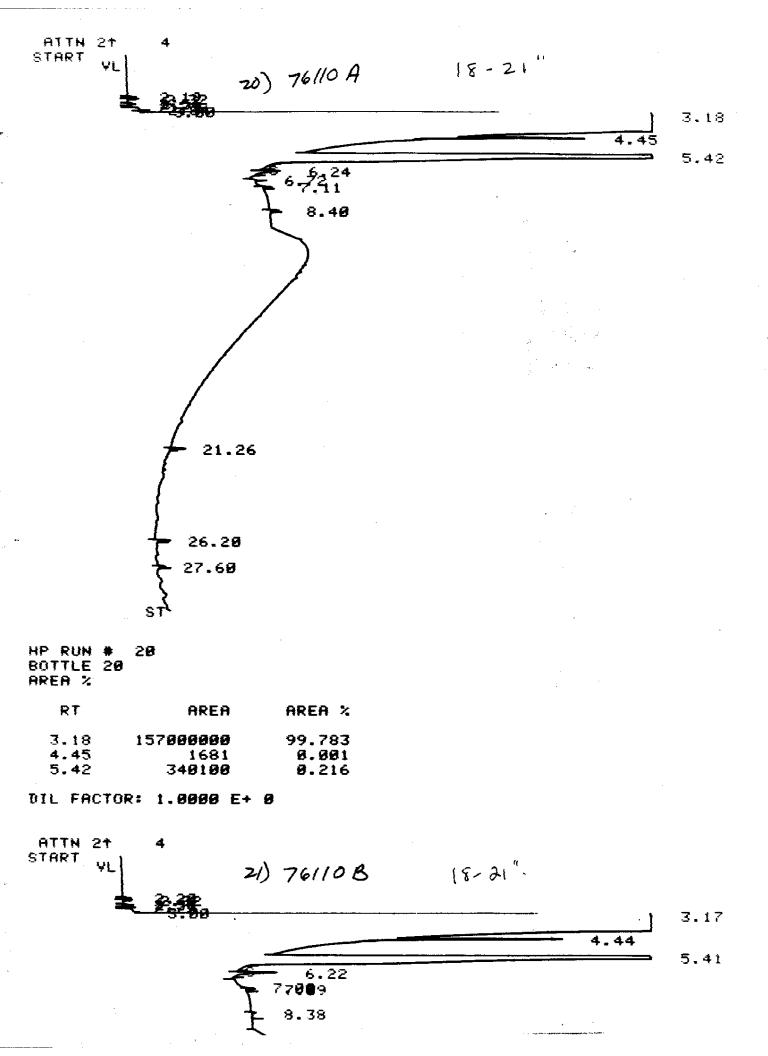
21.25

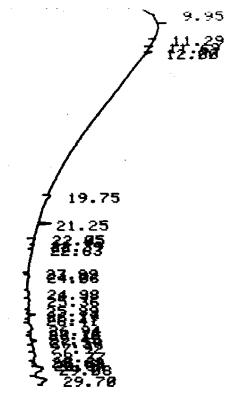
26.18

HP RUN # 19 BOTTLE 19 BREA %

RT	AREA	AREA %
3.19	16 0608000	99.747
4.45	2146	0.001
5.42	4 0 59 00	0.252

TO TOUTODA & BOOK TO A





HP RUN # 2 BOTTLE 21 AREA %

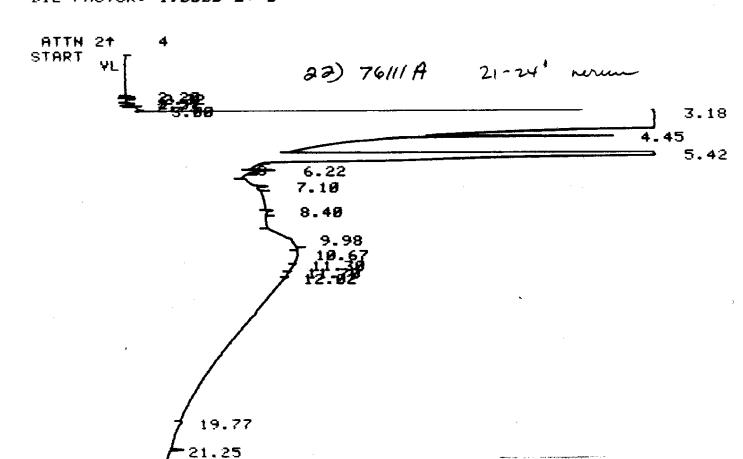
RT REA AREA %

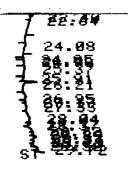
3.17 149500000 99.761

4.44 1781 0.001

5.41 356500 0.238

DIL FACTOR: 1.8888 E+ 8

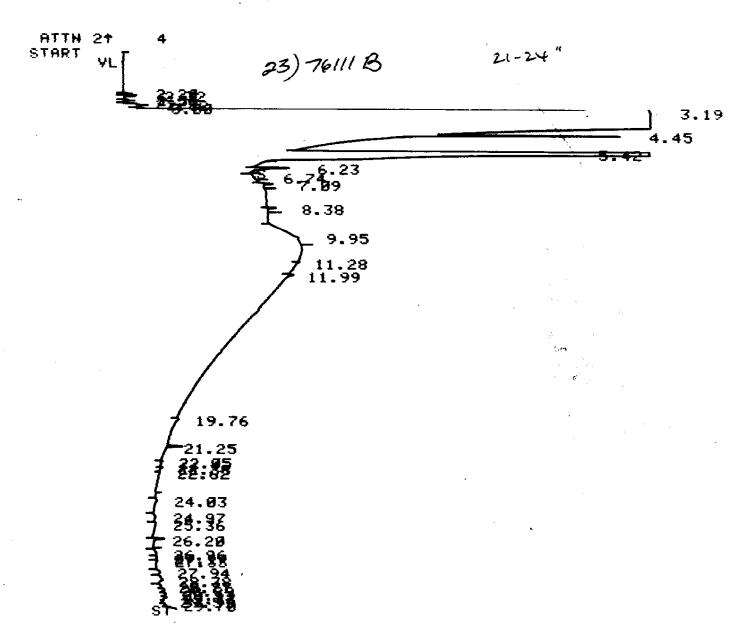




HP RUN # 22 BOTTLE 22 AREA %

RT	AREA	AREA %
3.18	162100000	99.753
4.45	2 9 35	9.991
5.42	3996 88	8.246

DIL FACTOR: 1.0000 E+ 0



HP RUN # 23 BOTTLE 23 BREA %

3.19 167499999 99.766 4,45 1992 0.001 389900 5.42 0.232 DIL FACTOR: 1.0000 E+ 0 ATTN 21 TEMP1 400 35 65 START 24) 761/2 A YL 3.17 5.41 6.22 7.09 8.38 9.95 11.29 12.88 19.76 21.25 HP RUN # 24 **BOTTLE 24** AREA % RT AREA % AREA 99.742 3.17 153300000 0.001 4.44 2046 5.41 394000 8.256

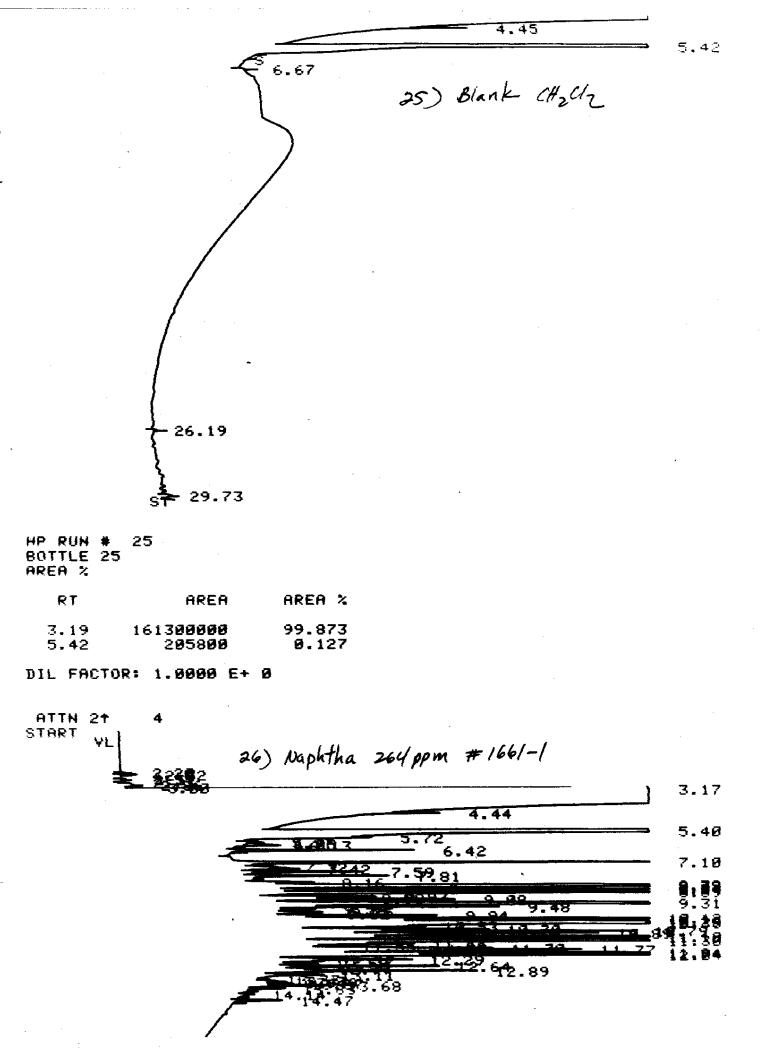
AREA

RT

AREA %

ATTN 2† 4
START VL

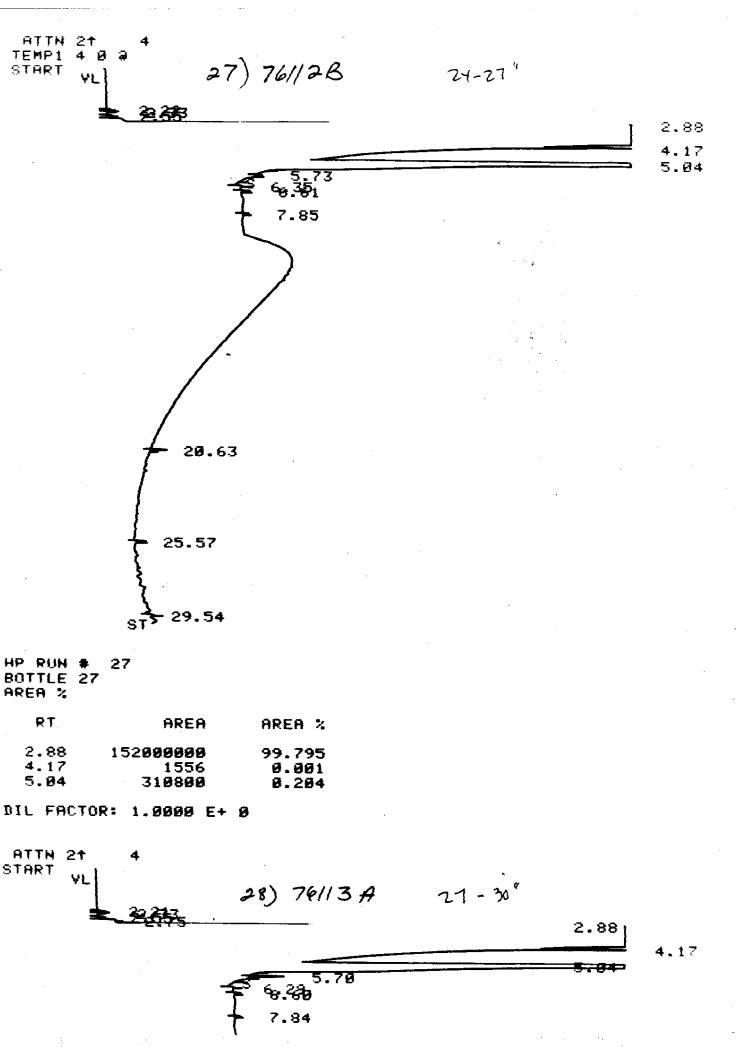
DIL FACTOR: 1.0000 E+ 0

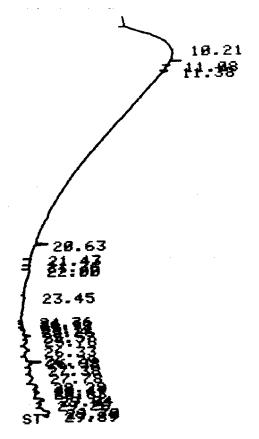




HP RUN # 26 BOTTLE 26 AREA %

RT	AREA	AREA %
3.17	148200000	99.682
5.40	185900	8.125
5.72	2395	0.002
6.42	2416	0.002
7.10	8624	0.99 6
7.42	1240	0.001
7.59	1625	9.991
7.81	1829	0.001
8.32	85 9 8	9.996
8.39 ·	6269	0.004
8.54	6686	9.994
8.69	13340	0.009
8.93	1754	9.991
8.98-	1819	0.001
9.28	3393	9.992
9.31	3 5 87 9	0.024
9.48	3513	0.002
9.58	1488	0.001
9.75.	1164	0.001
9.94	2877	9.992
10.12	11248	9.998
18.29.	18369	0.012 0.010
10.38 10.53	14398	9.992
10.70	2828 4699	9.983
10.79	537 8	8.884
10.89	4873	6.663
10.97	3 989	9.882
11.10	1835Ø	0.002
11.38	32998	0.022
11.44	3432	0.002
11.55	1309	0.001
11.70	4786	0.003
11.77	69 00	0.005
11.94	7444	0.005
12.84	24768	9.917
12.29	3624	0.092
12.37.	1861	0.001
12.50-	1341	0.001
12.64	3318	9.992
12.77.	1263	9.991
12.89	4274	0.003
13.11	1624	0.001
13.68	1356	9.991





HP RUN # 28 BOTTLE 28 AREA %

RT	AREA	AREA %
2.88	153900000	99.821
4.17	1169	0.001
5.84	2682 99	8.174
10.21	5196	g.983
27.78	1995	9. 99 1

DIL FACTOR: 1.0000 E+ 0

ATTN 2+ 4
START VL 29) 761/38 27-30"

7.85

18.28

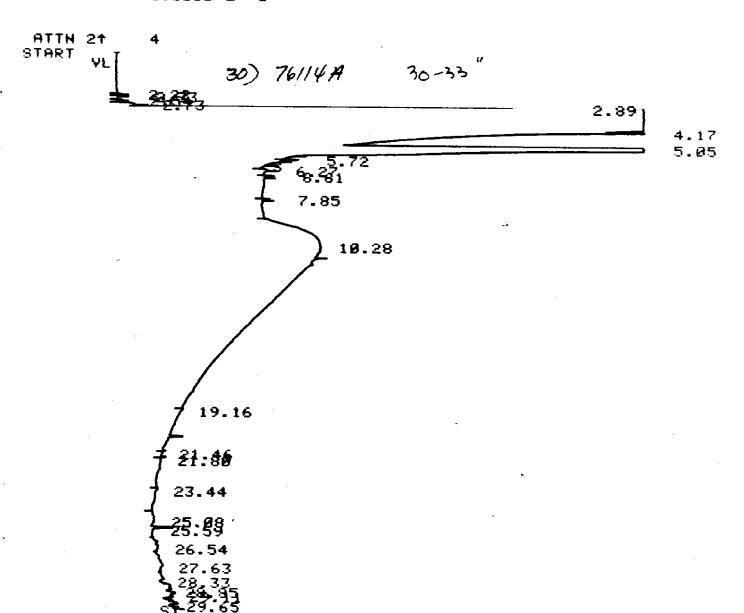
4.17 5.05

```
28.67
21.48
23.45
24.74
29.82
26.96
28.83
51.29.67
```

HP RUN # 29 BOTTLE 29 BREA %

RT	AREA	AREA %
2.89	156200000	99.718
4.17	2985	9.991
5.05	431800	8.276
10.28	7614	9.995

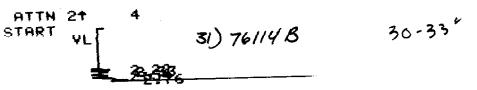
DIL FACTOR: 1.0000 E+ 0

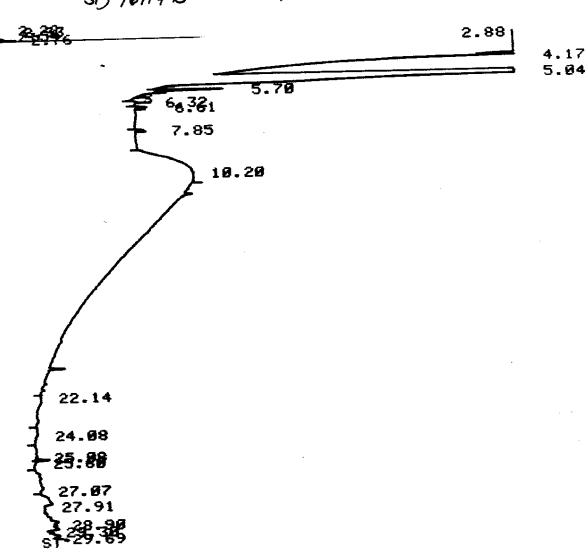


```
HP RUN # 30
BOTTLE 30
AREA %
```

RT	AREA	AREA %
2.89	1529 08000	99.778
4.17	162 0	0.001
5.05	341 000	0.223
10.28	8156	0.005
27.63	1513	0.001

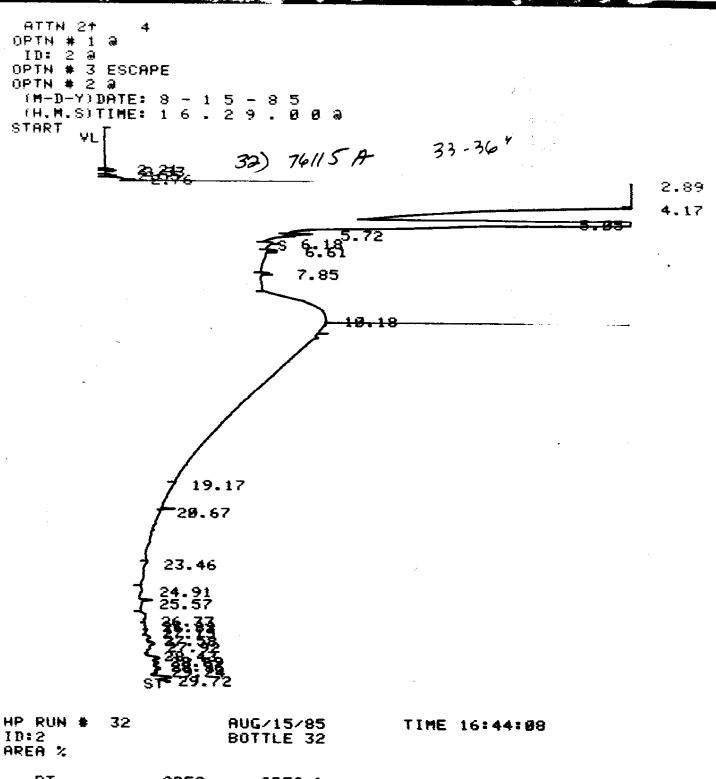
NIL FACTOR: 1.0000 E+ 0





HP RUN # 31 BOTTLE 31 AREA %

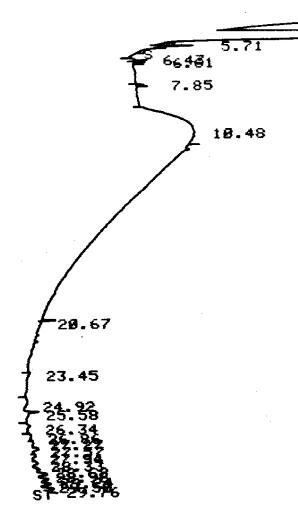
	•	
RT	AREA	AREA %
2.88	154900000	99.729
4.17	1922	9.991
5.84	411800	Ø.265
10.20	5797	8.994
27.91	1892	0.001
21.72		



ID:2 AREA % RT AREA AREA % 2.89 161100000 99.788 4.17 1762 0.001 5.05 373988 0.231 10.18 107800 0.067 27.92 1490 9.991

DIL FACTOR: 1.8888 E+ 8

START VL 33) 76/15 8 33-34"



TIME 17:31:24 AUG/15/85 HP RUN # 33 BOTTLE 33 ID:2 AREA % AREA AREA % RT 153699999 99.745 2.89 9.991 4.17 1843 8.249 383499 5.84 7788 9.995 19.48

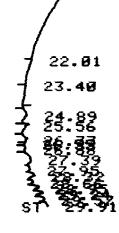
DIL FACTOR: 1.8888 E+ 8

START VL 22 34) Blank CH2C/2

2.89

5.84

19.19



HP RUN # ID:2 34 AUG/15/85 TIME 18:19:09 BOTTLE 34 AREA % RT AREA AREA % 2.89 169199999 99.868 9.126 9.006 9.001 5.84 201800 8889 18.18 1195

DIL FACTOR: 1.0000 E+ 0

START YL

35) Naphtha 264 ppm # 1661-1

4.17 5.84 4.17 5.84 5.95 6.61

	کم		. `
	STS		
HP RUN # ID:2 AREA %	35	AUG/15/85 BOTTLE 35	TIME 19:06:34
RT	AREA	AREA %	
2.89 5.84 5.31 5.95 6.67 7.28 7.28 7.28 7.28 8.37 8.37 8.37 8.37 8.37 9.35 9.35 9.35 9.79	148898999 175999 3597 2367 8119 1512 1792 8812 5950 6798 13318 2838 3439 36149 3698 1369 1992 2984 11369 19210 14510 3039	99.664 8.125 8.993 8.996 8.991 8.991 8.996 9.995 9.995 8.999 8.992 8.992 8.992 8.993 8.991 8.991 8.992 9.993 8.991 8.993	
10.10 10.20 10.29 10.37	5081 5577 5119 3405	0.004 0.004 0.002	
10.49 10.69	1911 0 3441 0	9.914 9.924	

Ø.003

9.991

8.994

0.985

9.996

8.918

8.883

0.001

8.881

0.003

0.991

0.003

12.28 0.002 2363 12.49 0.001 1735 13.05 9.991 1083 13.22

3866

1498

5320

7286

7812

4164

1276

1725

3800

1536

4923

26070

1.0000 E+ 0 DIL FACTOR:

ATTN 21 TEMP1 3 8 9

18.69

18.83

18.95

11.89

11.16

11.33

11.43

11.67

11.75

11.88

12.02

12.15

36 39 400 TEMP1 TEMP1 4 8 2

TEMP1 400 40 TIMEI 4.00 2086-00110 Dupont RHTE 8.00 TEMP2 400 300 TIME2 20.00 INJ TEMP 488 225 225 FID TEMP 400 250 250 AUX TEMP 400 225 225 CHT SPD 0.50 ZERO 15.0 ATTN 2+ 4 Pet. Aydrocarbons/soi FID SGNL +8 SLP SENS 8.18 AREA REJ Reruns 1000 FLOW A 8.8 28.0 FLOW В 8.8 43.8 DOK COI# 324 0.50 YLY/EXT-30.00 STOP Atta 24 CHANGE RUN 1 a Ypel inj val. **OPTN #1** ID: 2 ESCAPE OPTN #3 INJ/BTL,STROKE: 1,2 1) Blank CHZCZ START 2.89 4.17 8-840 6.27 18.28

HP RUN # 2 ID:2

BOTTLE 2

TIME 18:88:34

```
2.89
           157900000
                           99.865
  5.04
              203000
                            8.128
 18.28
                9958
                            8.886
DIL FACTOR: 1.0000 E+ 0
 ATTN 21
CHANGE RUN 3 @
                    2) Naphtha 264 ppm # 1661-1
START
             2.89
                                               4.16
                                                                   5.84
                                        5.38
5.95
                                                                   6.68
                                   7.8628
                                                                   海特
8.72
                                                  8.98
                                        1.63.822.27
HP RUN #
                                         TIME 19:55:39
                       AUG/16/85
ID:2
                       BOTTLE
AREA %
   PT
                AREA
                          AREA %
  2.89
                          99.678
           135600000
  5.84
              167500
                           0.123
                            0.003
  5.30 -
                3970
                            8.002
  5.95
                2196
                7656
                            0.006
  6.60
  7.86
                1429
                            9.991
                1674
  7.28
                            9.991
```

AREA %

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7.76

7.84

7.98

8220

5459

6354

0.006

0.004

0.005

AREA

AREA %

				· · · · · · · · · · · · · · · · · · ·
ర.ు/ 8. 5 1-	2552 3173	0.002 0.002	•	
		9.925		
8.72	3356 0 34 4 8	0.023 0.003		
8.9 0 9.01	1242	9.991		
	1927	0.001		
9.17	2633	9.001 9.002		•
9.34		9.992 9.998		
9.52	19268	g.g13		
9.78	17480	9.010		
9.78 · 9.92 ·	1346 8 2592	0.002		
	4438	9.883		
18.18	4973	9.663 9.664		
19.19 10.28	4545	0.003		
18.36	2 958	8.88 2	,	
18.48	17328	Ø. Ø13		
18.68	31318	ø.ø23		
19.82	327 8	9.892		
18.94	1248	9.991		
11.09	4644	0.003		
11.16	6484	9.995		
11.32	6948	9.995		
11.42 `	23640	0.017		
11.67-	3522	9.993		
11.75	1849	9.991		
11.88	1398	0.001		
12.82 -	3254	9.992		
12.14	1277	9.991		
12.27	4251	0.90 3		
12.48 -	1792	Ø.001	1	
17 45 -	1354	9.001		
40				
DIL FACTOR:	1.0000 E+	8		
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		_		
		_		
ATTN 2+	4			
START .		76116 A	36-35 ×	
	4		36-35 4	
START .	4		36-35	
START .	4		36-35 4	1 2.89
START .	4		36-35 *	1
START .	4		36-39 *	4.17
START .	4	76116 A		1
START .	4	76116 A		4.17
START .	4	76/16 A 66381		4.17
START .	4	76116 A		4.17
START .	4	76/16 A 66381		4.17
START .	4	76/16 A 66381 7.85		4.17
START .	4	76/16 A 66381		4.17
START .	4	76/16 A 66381 7.85		4.17
START .	4	76/16 A 66381 7.85		4.17
START .	4	76/16 A 66381 7.85		4.17
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START .	4	76/16 A 66381 7.85		4.17
START .	4	76/16 A 66381 7.85		4.17
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START .	4	76/16 A 66381 7.85		4.17
START .	4	76/16 A 66381 7.85		4.17
START .	4	76/16 A 66381 7.85		4.17
START .	4 3)	76/16 A 66381 7.85		4.17
START .	4 3)	76/16 A 66381 7.85		4.17
START .	4 3)	76/16 A 66381 7.85		4.17
START .	28.66 21.46	76/16 A 66381 7.85		4.17
START .	4 3)	76/16 A 66381 7.85		4.17
START .	29.66 21.46 23.44	76/16 A 66381 7.85		4.17
START .	29.66 21.46 23.44 24.79	76/16 A 66381 7.85		4.17
START .	29.66 21.46 23.44	76/16 A 66381 7.85		4.17

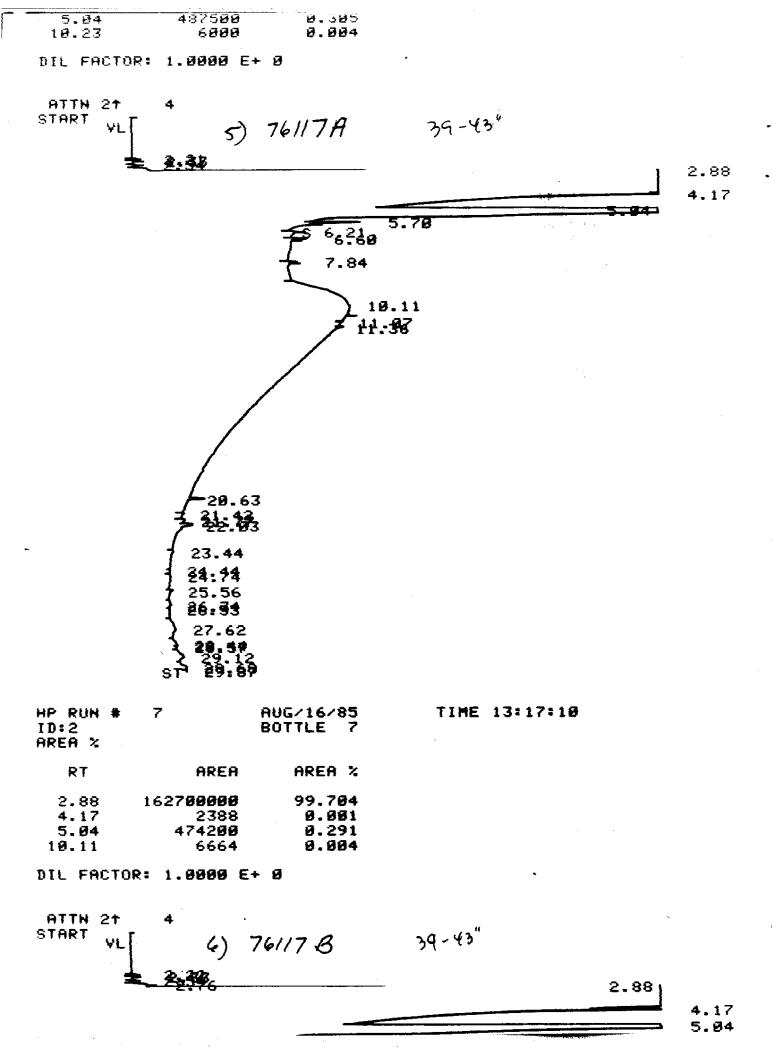
```
HP RUN #
            5
                                       TIME 11:42:39
                      AUG/16/85
ID:2
                      BOTTLE 5
AREA %
   RT
                AREA
                         AREA %
  2.89
           158900000
                         99.731
  4.17
                2085
                          0.001
  5.05
              417188
                          8.262
 10.29
                8736
                          0.005
DIL FACTOR: 1.0000 E+ 0
 ATTH 21
                                     36-39"
START
                   4) 76/16B
                                                                2.88
                                                                5.84
                            66381
                              7.85
                                 19.23
                 29.63
               23.46
               24.74
               26.38
               27.62
                29.13
HP RUN #
                      AUG/16/85
                                       TIME 12:29:46
ID:2
                      BOTTLE 6
```

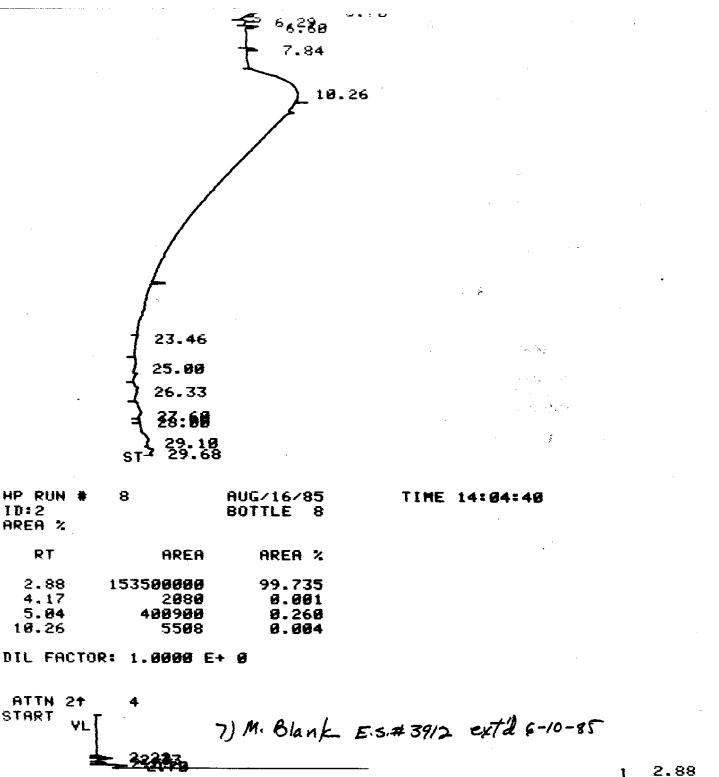
AREA %

RT AREA AREA %

2.88 159400000 99.687

3.73 5243 0.003





%.?5₽

4.17 5.04

ID:2

RT

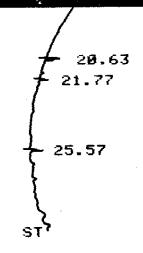
2.88

4.17

5.04

10.26

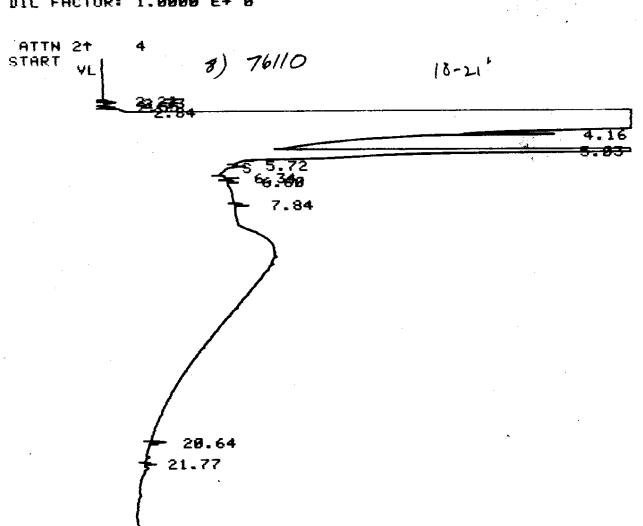
START



```
TIME 14:52:23
HP RUN #
           9
                      AUG/16/85
                      BOTTLE 9
ID:S
AREA %
   RT
                AREA :
                         AREA %
                          99.838
  2.88
          158000000
  4.17
               1847
                          0.001
                           8.162
  5.84
              255988
```

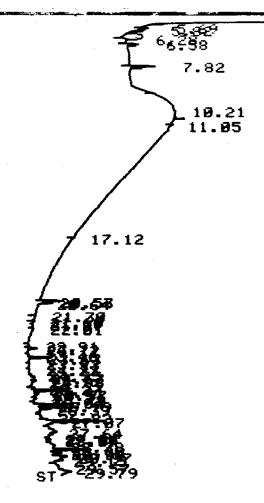
DIL FACTOR: 1.0000 E+ 0

25.57 26.98



2.88

157700000 99.849 2.86 5.02 238500 0.151 DIL FACTOR: 1.0000 E+ 0 21) Blank E.S. # 3933 Ext'd 6-20-85 ATTN 2+ START ٧L 2.21 2.86 4.15 5,82 6189 7.83 28.64 23.44 HP RUN # AUG/17/85 TIME 92:97:44 23 BOTTLE 23 ID:2 AREA % RT AREA AREA % 159200000 99.685 2.86 0.002 4.15 2521 0.313 588988 5.02 27.55 0.001 1033 DIL FACTOR: 1.0000 E+ 0 CBC-5(0-3") ATTN 21 22) 76949/76959 START



HP RUN # 24 AUG/17/85 ID: 2 BOTTLE 24 AREA % RT AREA AREA % 2.86 99.752 158100000 3.72 4479 0.003 0.001 4.15 1897 5.02 373899 **8.236** 18.21 8.881 2871 26.39 9.991 1114 9.992 27.87 2488 27.64 0.002 3979 28.38 1946 8.991

1595

DIL FACTOR: 1.0000 E+ 0

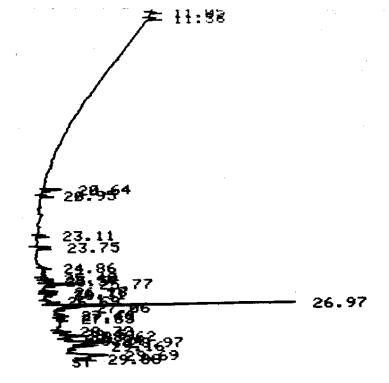
28.62

RTTN 2† 4 START VL 23) 76950/76960 (BCS (3-6") 2.86 4.15

8.991

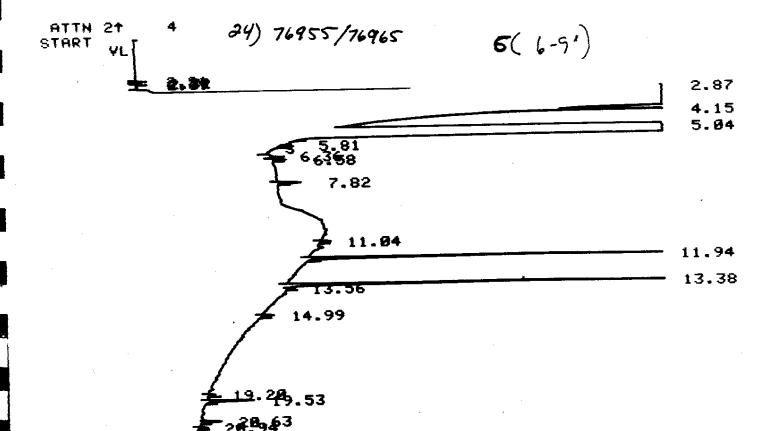
∠ 11.95

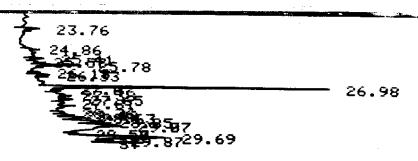
TIME 02:55:51



```
TIME #3:43:58
                       AUG/17/85
HP RUN #
           25
                       BOTTLE 25
[D:2
AREA %
                          AREA %
                AREA
   RT
                           99.746
           158488888
  2.86
                            0.001
  4.15
                1823
                            Ø.25Ø
              376899
  5.82
                            0.002
 26.97
                 3211
                            9.881
                 1155
 28.97
```

DIL FACTOR: 1.8999 E+ 8





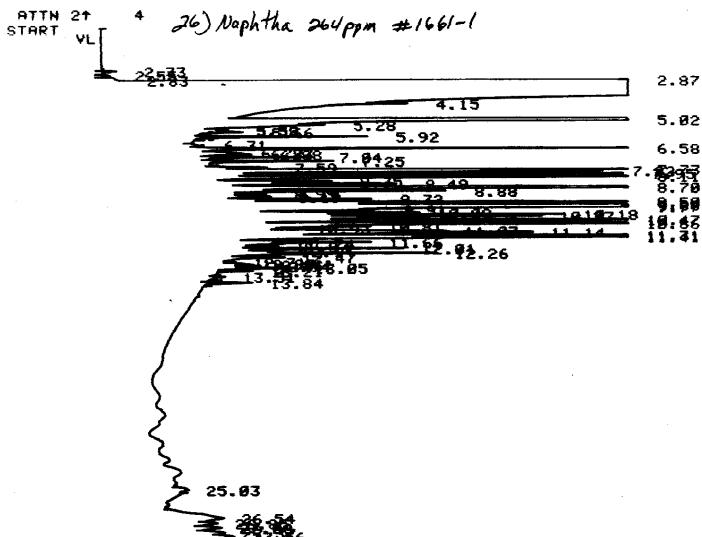
HP RUN # 26 AUG/17/85 TIME 04:32:17 ID:2 BOTTLE 26 AREA % RT AREA AREA % 2.87 154800000 99.337 4.15 2300 0.001 5.04 1012000 **0.649** 11.94 4876 0.003 13.38 6588 8.994 26.98 3648 8.882 29.87 9.992 2756 29.69 2875 8.881

DIL FACTOR: 1.8888 E+ 8

START VL 35) Blank CH2CIZ

25.56 26.38 25.56 26.38 25.56

AUG/17/85 TIME 05:20:32 HP RUN # 27 BOTTLE 27 10.2 AREA % AREA % RT AREA 2.87 99.864 147800000 5.02 186399 Ø.126 27.37 1629 0.001 0.001 27.59 1454 0.002 28.86 2693 0.003 29.08 4228 0.001 29.27 2844 0.002 29.66 2882 DIL FACTOR: 1.0000 E+ 0



HP RUN # ID:2 AREA %	28	AUG/17/85 BOTTLE 28	TIME 06:08:30
RT	AREA	AREA %	
2.87 5.02 5.28 5.92	13 9899999 1622 99 3 987 2169	99.631 9.124 9.992 9.992	man one of the control of the contro

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7. 0 4 '	1423	8.881
7.25	1781	9.991
7.73	826 9	8.99 6
7.82	5545	
		9.884
7.95.	6326	8.885
8.11	12488	9.889
8.35'	2664	9.002
8.49	322 8	9.992
8.70	3375 8	
		9.926
8.88 ·	3485	9.993
8.99	1223	9.991
~ *		
9.32	2672	0.002
9.58	19389	9.998
9.68		
	17730	8.814
9.77	13310	9.919
9.91	2634	0.002
10.08	4478	0.003
18.18	5884	8.884
10.27	464 Ø	8.084
10.36.	2961	0.002
18.47	17650	0.013
18.66	32010	0.024
18.81.	3414	0.003
18.93		
	1389	8.881
11.07	4893	0.004
11.14	6594	9.995
•		
11.31.	72 90	9.996
11.41	24198	9.918
11.66	3727	9.99 3
11.74.	1145	9.991
11.87	1539	0.001
12.81.	3473	
		9.993
12.14	1388	8.891
12.26.	4559	0.093
12.47.	2145	0.99 2
T3.05.34	155 0	0.001
26.54.	4886	9.994
26.8 5 °	2385	0.002
27 .0 8	23 85	0.002
27.37	2 456	0.002
27.56.	3216	9.99 2
27.94	6363	8.885
28.19	23 65	9.992
28.36	4336	9.993
28.69	3939	
		9.993
28 .92	4817	9.994
29.12	4739	8.884
29.33		
	3908	0.093
29 .58	1988	0.001
29.69	1385	9.991
27.07	1303	0.551

DIL FACTOR: 1.8888 E+ 8

ATTN 21 4
START VL 27) 76956/76966 6(9-12")

2.88
4.16
5.83
7.84

10.25

	•		,
HP RUN #	29	AUG/17/85 BOTTLE 29	TIME #6:56:45
AREA %			
. RT	AREA	AREA %	
		_	
2.88	164199999	99.763	
4.16	1211	Ø. ØØ1	
5.03	3 96999	9.186	
18.25	6344	Ø. ØØ4	
21.28	27 9 3	9.882	
22.53	1980	Ø. ØØ1	
23.46	3829	Ø.992	
24.42	2468	0. 9 62	
25.02	2586	0.00 2	
25.79	295 8	9.992	
26.44	4792	9.99 3	
26.98	8464		
27.68	5912	9.994	
27.98	9846		
28.21	4884		
28.44	5386	9.993	
28.69	5999		
28.96	5677		
29.28	8444	9.995	
29.73	2794	0.002	
	-		

DIL FACTOR: 1.8999 E+ 9

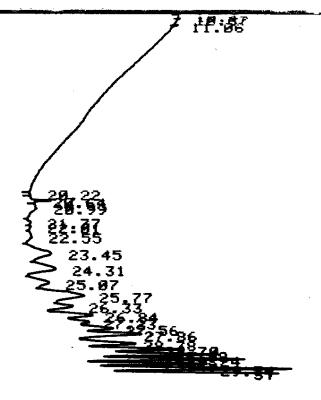
START VL 28) 76957/76967 6(12-15")

2.87 4.16 5.03

5.8

7.83

9 99



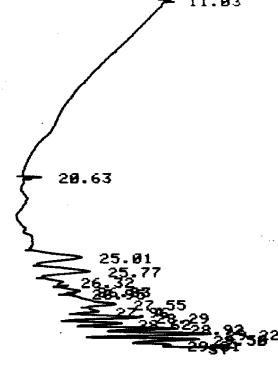
44:45

RT AREA AREA % 2.87 16740000 99.619 4.16 3009 0.002 5.03 562200 0.335 23.45 2924 0.002 24.31 3057 0.002 25.07 2130 0.001 25.77 7100 0.004 26.33 3725 0.002 26.84 4656 0.003 27.23 3790 0.002 27.56 6052 0.005 27.26 7726 0.005 28.38 7538 0.004 27.86 7726 0.005 28.38 7538 0.004 28.70 6598 0.004 28.98 6508 0.004 29.24 5339 0.003 29.49 3137 0.002	HP RUN # ID:2 AREA %	39	AUG/17/85 BOTTLE 30	TIME 07:
4.16 3009 0.002 5.03 562200 0.335 23.45 2924 0.002 24.31 3057 0.002 25.07 2130 0.001 25.77 7100 0.004 26.33 3725 0.002 26.84 4656 0.003 27.23 3790 0.002 27.56 6052 0.004 27.86 7726 0.005 28.38 7538 0.004 28.70 6598 0.004 28.90 6508 0.004 29.24 5339 0.002	RT	AREA	AREA %	
C 21, 4 0014 0.003	4.16 5.03 23.45 24.31 25.07 25.77 26.33 26.84 27.23 27.56 27.86 28.38 28.70 28.98 29.24	3009 562200 2924 3057 2130 7100 3725 4656 3790 6052 7726 7538 6598 6508 5339	8.082 8.082 8.082 8.084 8.083 8.083 8.084 8.084 8.084 8.084 8.084	

DIL FACTOR: 1.0000 E+ 0

ATTN 21 4
START VL 29) 76958/76968 ((15-18")
2.86
4.16

7.81



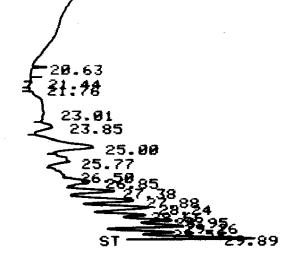
AUG/17/85 TIME #8:32:43 HP RUN 31 BOTTLE 31 ID:2 AREA % RT AREA % AREA 99.654 2.86 172200000 0.002 0.325 3025 4.16 5.02 561900 0.002 25.81 3814 3498 8.882 25.77 0.883 27.55 9.991 27.96 9.992 28.29 9.991 28.62 28.92 29.22 0.002 9.993 5212 0.982 2994 29.50

DIL FACTOR: 1.0000 E+ 0

6(12+5") ATTN 21 30) 76957/76967 Dup. START 2.88

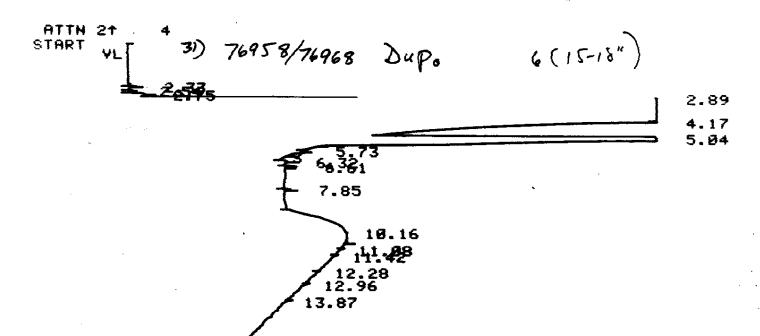
7.84

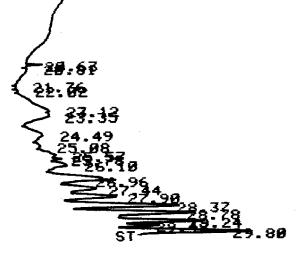
4.16 5.03



HP RUN # ID:2 AREA %	32	AUG/17/85 BOTTLE 32	09:20:4 9
RT	AREA	AREA %	
2.88 4.16 5.83 18.44 23.85 25.86 25.77 26.58 27.38 27.38 27.38 27.38 27.38 27.38 27.38 27.38 27.38 27.38	158 00000 1695 3585 00 5833 47 0 5 2675 8586 5362 393 0 6242 622 0 825 0 7984 4382 4998 5 0 89	99.721 9.991 9.226 9.204 9.993 9.993 9.994 9.995 9.995 9.993 9.993	
29.89	4894	0.003	

DIL FACTOR: 1.8888 E+ 8





HP RUN # ID:2 AREA %	33	AUG/17/85 BOTTLE 33	TIME 19:98:46
RT	AREA	AREA %	
2.89	159300000	99.683	
4.17	197 8	0.001	
5.94	426299	Ø.267	
18.16	652 6	9.994	
23.12	4985	0.003	
23.35	2892	0.002	
24.49	38 79	9.992	•
25.08	1779	8.881	•
25.57	4124	9.993	•
25.78	1271	9.991	
26.18	5751	8.884	
26.96	9516	9.996	
27.44	7740	9.995	
27.98	6239	9.994	
28.37	7104	0.004	
28.78	6518	8.804	
29.24	4568	9.993	
29.48	1354	9.991	
29.89	4826	9.993	

DIL FACTOR: 1.0000 E+ 9

ATTN 21 4

32) Blank C4242

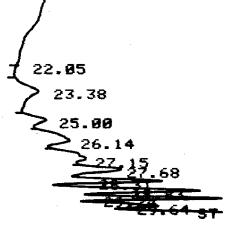
6.29

2.89

4.16

5.04

10.46



HP RUN # ID:2 AREA %	34	AUG/17/85 BOTTLE 34	TIME 10:56:02
RT	AREA	AREA %	
2.89 5.84 18.46 23.38 25.88 26.14 27.15 27.68 28.31 28.83 29.24 29.64	154899999 198799 26299 5217 4457 10119 11639 11449 6559 7450 5861 2992	99.813 9.128 9.917 9.993 9.993 9.997 9.997 9.994 9.995 9.994	

DIL FACTOR: 1.0000 E+ 0

START VL STOP air me out

HP RUN # 35 ESCAPE START ... (AUG/17/85

TIME 12:40:43

33) Naphtha 264 ppm # 1661-1

2.94)

4.14

5.82

5.82

6.58

8.68

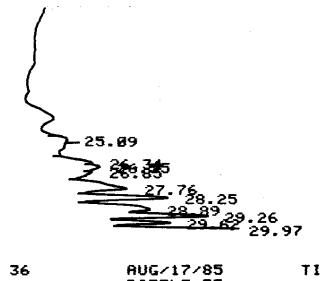
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10.05	1859	9.994		
10.15	1635	9.993		
18.24	1490	9.003		
18.32	1129	8.89 2		
18.44	4316	9.999		
18.64	6579	9.814		
10.78	1549	9.993		
11.05	1748	Ø. 9 9 4		
11.12	2002	9.994		
11.29	1837	9.994		
11.39	5134	0.011		
11.64	2734	0.006		
12.24	1012	9.882		
26.34	1579	9.993		
26.55	3171	0.007		
26.85	2453	9.005		
27.76	6893	9.913		
28.25	4939	9.010		
28.89	4748	0.010		*
29.26	5488	9.912		
29.62	238 4	9.995		

DIL FACTOR: 1.8999 E+ 9

APPENDIX X

STANDARD OPERATING PROCEDURE, LAB NOTES AND COMMENTS FOR GREASE AND OIL EXTRACTION;
AND GENERAL ANALYSIS COMMENTS





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August 20, 1985 2086-00110

Dr. Jacqueline Michel Research Planning Institute, Inc. 925 Gervais St. Columbia, SC 29201

Dear Dr. Michel:

Enclosed are the latest revisions/reanalyses results for several of the Dupont L-Area basin samples. The standard operating procedures for petroleum hydrocarbons and bulk chemistry are also enclosed. A brief discussion of the enclosed information follows.

- 1. The uranium reanalysis to achieve a lower detection limit of 2 ug/g was done on July 31, 1985. Triplicate analysis on the samples was not possible due to the short sample quantity (5 gms of sample was required for each analysis).
- 2. The nickel and zinc data were recalculated using the detection limits recommended by the instrument manufacturer. We can routinely measure these metals at these lower limits, but generally use the higher detection limits because we are in the process of developing our own in-house detection limits (the start point of which is to double the instrument detection limits and then carry out tests to see how much lower you can go).
- 3. A reanalysis for mercury at a detection limit of 0.01 ug/g was not done because the additional sample required to meet this limit would also increase the amount of interferences present.
- 4. Reanalysis for beryllium, cadmium, and selenium were not possible since two separate digestions would be required and there was not sufficient sample available.
- 5. Analysis for hexachrome was not possible since the "wet" unprocessed sample is required for that analysis. The "grease and oil" analyses exhausted that sample supply.
- 6. The grease and oil extractions (with freon) for the LBC 6 6-9, 9-12, LBC 5 0-3, and 3-6 suggest the presence of high levels of hydrocarbons. However the GC analyses for these samples (based upon a naptha standard) suggest the presence of high molecular weight hydrocarbons not low weight, petroleum hydrocarbons. The chromatographs enclosed are from a reanalysis of the sample extracts using a lower standard value. This reanalysis, along with the original analysis, support the absence of low molecular weight, petroleum hydrocarbons in the sample.

ENVIRODYNE ENGINEERS

Dr. Jacqueline Michel August 20, 1985 Page 2

7. The NBS standards data are provided. In the case of those metals where a suitable NBS standard is not available, an aqueous standard was run to verify the calibration curve. At this time there are still a few metals which fall into that category. The spiking of a blank soil for a central standard is not normally done because of the inability to match the matrix of the unknown soil. For those metals where the recovery was poor, a special situation exists. We use the data from these metals to match against the historical recovery data. There will be differences between our data and NBS certified values because of instrumentation differences. One cannot compare Mass Spectrometry, Neutron activation, and polarity to the Inductively Coupled Argon Plasma or Atomic Absorption. In all cases an external check standard is used to verify instrument operations.

If you have any questions, please feel free to call.

Sincerely

fohn J./Coniglio Program Manager

JJC/bsm Enclosure

SOP # EEI 17 Date: May 26, 1985 Prepared by: Charles Johnston.

STANDARD OPERATING PROCEDURE GREASE AND OIL EXTRACTION METHOD FOR SLUDGE SAMPLES

APPLICATION

Drying acidified sludge by heating leads to low results. Magnesium sulfate monohydrate is capable of combining with 75% of its own weight in water in forming MgSO₄.7H₂O and is used to dry sludge. After drying, the oil and grease can be extracted with trichlorotrifluoroethane.

Ref: Standard Methods.

PROCEDURE

Extraction apparatus, Soxhlet; vacuum pump or other source of vacuum; extraction thimble, paper; IPS filter paper.

In a 150 ml beaker, weigh a smple of wet sludge, 20+0.5 g, of which the dry solids content is known. Acidify to pH 2.0 (generally, 0.3 ml conc HCl is sufficient). Add 25 g MgSO₄.H₂O. Stir to a smooth paste and spread on sides of beaker to facilitate subsequent removal. Let stand until solidified (15 to 30 minutes). Remove solids and grind in a porcelain mortar. Add the powder to a paper extraction thimble. Wipe beaker and mortar withsmall pieces of filter paper moistened with solvent and add to thimble. Fill thimble with glass wool or small glass beads. Extract in a Soxhlet apparatus, using trichlorotrifluoroethane, at a rate of 20 cycles/hr for 4 hours. If any turbidity or suspended matter is present in the extraction flask, remove by filtering through IPS filter paper into another weighed flask. Rinse flask and filter with solvent. Distill solvent from extraction flask in water at 70°C for 15 seconds. Draw air through it using an applied vacuum. Cool in a desiccator for 60 minutes and weigh to constant weight.

INSTRUMENT OPERATION

Soxhlet apparatus should be thoroughly cleaned with detergent and hot water. Then rinsed with acetone and freon to remove any grease and oil.

Measure all digits of display on balance. Round off insigificant figures when reporting final results of grease and oil.

REAGENTS

- Hydrochloric acid, HCl, conc.
- 2. Magnesium sulfate monohydrate: Prepare MgSO $_4$.H $_2$ O by overnight drying of thin layer in an oven at 150°C. (Sodium sulfate anhydrous may be substituted for magnesium sulfate.)
- 3. Trichlorotrifluoroethane (1,1,2-trichloro-1,2,2-trifluoroethane)

 INTERFERENCE: Heavier residuals of petroleum mot contain
 a significant portion of materials insoluble in trichlorotrifluoroethere

 STANDARD PREPARATION

Measure an amount of oil (Crisco vegetable oil) for extraction. Record percent recovery.

SAMPLE PREPARATION

Preservation: Store at 4°C.

QA/QC

One blank, one standard (* recovery), and one duplicate for every ten samples. It is the responsibility of the chemist/technician to check the control charts after the analysis is performed, and notify the section manager for out of control situations.

CALCULATION

Oil and grease = gain in weight of flask, $g \times 100$ weight of wet solids, $g \times dry$ solids fraction

ug/g grease and oil = % grease and oil x 104

DETECTION LIMIT

5 ug/g

SAFETY

Beware of heating mantles and of hot solvent when Soxhlet is running. Follow all EEI safety regulations.

DATA SHEET

Sample copy of data sheet attached; modify as needed. An updated version is being prepared.

STANDARD OPERATING PROCEDURE FLAME ATOMIC ABSORPTION

APPLICATION

Metals in solution may be readily determined by atomic absorption spectroscopy. The method is simple, rapid and applicable to a large number of metals in drinking, surface and saline waters, and domestic and industrial wastes. While drinking waters free of particulate matter may be analyzed directly, domestic and industrial wastes require processing to solubilize suspended material. Sludges, sediments and other solid type samples may also be analyzed after proper pretreatment.

PROCEDURE

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Setting Instrument Conditions

- 1. Make sure the drain tube is filled with DI water.
- 2. Press power button ON.
- 3. Turn restart/std-by switch to OPERATE. The instrument automatically sets to the double beam mode. The AUTO button lights.
- 4. Place the proper burner head, air-acetylene or nitrous oxide-acetylene, in position. Wet the bottom of the burner head with DI water so that it will slide over the O-ring easier.
- 5. Turn the voltage knob down before inserting the hollow cathode lamp. Place the hollow cathode lamp in turret. Turn the voltage knob to proper operating current.
- 6. Turn the bandwidth switch to proper setting ..
- 7. Using the wavelength selector, set the wavelength to the value recommended for the element to be analyzed.
- 8. Adjust the voltage as necessary when peaking out the energy meter. The optimum indication on the energy meter is within the green zone on the meter. Using the adjustable zoom lens and the wavelength selector, make sure that all settings combine to give the lowest reading on the meter.

Igniting the Flame

A. Air/Acetylene

- 1. Align the burner head with the hollow cathode beam.
- Turn on the gas tanks that are needed. Make sure that the two-stage regulator is at the proper settings.

- a. Above 100 psi on the tank contents
- b. 14-15 psi is the working range for acetylene
- c. 50 psi is the working range for nitrous oxide
- 3. Set the oxidant and fuel flow rates at their proper settings.
 - a. Air (oxidant) is set at 14 SCFH
 - b. Air/fuel (fuel) is set at 6 SCFH
- 4. Press the pilot button to light the flame.
- 5. Aspirate with DI water.
- 6. Check the nebulizer flow.
 - a. 2.5 mls/30 seconds for air/acetylene flame
 - b. 3.0 mls/30 seconds for nitrous oxide/acetylene flame
- 7. Warm up the burner head for about 10 minutes with an oxidizing (fuel-lean) flame for air/acetylene and with a fuel-rich flame for nitrous oxide.

B. N₂O/Acetylene

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- 1. Light the air/acetylene flame as above using the N2O burner head. DO NOT ASPIRATE WATER.
- Increase your fuel while decreasing your oxidant. The flame should become very white.
- 3. Warm up the burner head for 5 to 7 minutes.
- 4. Turn knob from air/fuel to N2O/fuel.
- 5. Place aspirator tubing in DI after N2O takeover.
- 6. DO NOT RUN IN A LEAN CONDITION: A "red feather" is wanted in the flame. If a red feather does not appear:
 - a. Increase the fuel
 - b. Decrease the oxidant
 - c. If necessary, increase sample flow by turning the knob on the nebulizer clockwise.
- 7. Once a red feather has been established, let the burner head warm up for 2 to 3 minutes.

Zeroing the Instrument

- 1. Zero the instrument by pressing zero while aspirating matrix blank solution.
- After zeroing, aspirate the highest standard and press read. Obtain the greatest absorbance readings while adjusting the burner head (vertically and horizontally) and optimizing flame conditions. To stop, press read.

- 3. Re-zero the instrument.
- 4. Re-check the absorbance value again for the highest standard. (The rezeroing and absorbance checking might have to be repeated 2 to 4 times to get the best reading.)

Calibrating the Instrument

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- 1. SEt the integration time. It is normally 4.0 seconds. It changes sometimes with sample availability. The integration time for hydride analysis is 8.0 seconds.
- 2. Press the mean button twice for standard deviation and relative standard deviation.
- 3. Aspirate the desired standard.
 - a. Press standard number
 - -b. Press enter
 - c. Enter concentration value
 - d. Press enter
 - e. Press read. Take three readings.
 - f. Press enter. (The instrument will give you 4 readings since it is in auto mode.)
- 4. Enter the 4 to 5 standards to be used for the calibration curve by repeating step 3 for each. If the instrument gives a flex curve, check the standard make up.

Sample Analysis

- i. Four readings per sample is normal procedure.
- 2. Periodically check the zero with matrix blank and the calibration with calibration standards. Re-zero and re-calibrate as necessary. Only use the standard used as standard #1 in calibration for re-calibration.

Instrument Shutdown

- A. Air/Acetylene
 - 1. Remove aspirator tubing from DI water.
 - Turn the knob from air/fuel to air, let the flame go out, then from air to off.
 - 3. Turn off the acetylene gas tank depressurizing the line.
- B. N2O/Acetylene
 - 1. Remove aspirator tubing from DI water.

- 2. Turn from N_{20} /fuel to air/fuel. Decrease fuel and increase oxidant until slightly fuel-rich air/acetylene flame. Turn from air/fuel to air. After the flame goes out, turn off.
- 3. Turn off the acetylene and N2O gas tanks depressurizing the lines.

Hydride Analysis of As and Se with the Use of the ILAVA

- 1. Place the hydride cell assembly, with the Teflon spacer, into the burner/premix chamber.
- 2. Adjust the burner mount so that the hollow cathode beam is centered in the absorption cell.
- 3. Ignite the air/acetylene flame as described above. Heat the hydride cell for at least 20 minutes.
- 4. Purge nitrogen or argon gas through the cell.
- 5. Program the instrument with the following information.
 - a. Single beam mode
 - b. Integration time equals 8 seconds
 - c. Peak height mode
- 6. Take readings one at a time with the use of the Instrumentation Laboratories Atomic Vapor Accessory (ILAVA).
- 7. Establish a zero baseline with the minimum amount of drift by analyzing and autozeroing on a number of matrix blanks. (All samples and standards have a matrix of 5N HCl.)
- 8. Run the standards in duplicate at minimum. Average the values and manually plug the absorbance readings into the atomic absorption unit after all the standards have been run.
- 9. Analyze the samples.
- 10. Periodically check for drift. Re-zero and re-calibrate as necessary.

REAGENTS

- 1. Concentrated HCl; concentrated HNO3, HF
- 2. Hydride Analysis: As 1% NaBH4 (1% NaOH)
 Se 50% KI (1% Ascorbic Acid)
- 3. Deionized water
- 4. Stock standard metal solution

STANDARD PREPARATION

All glassware must be cleaned with 1:1 HNO3. Use 25, 50, 100, 250 and 500 ul micro-pipets in making the standard solutions. A small quantity of a 1000 mg/l stock solution is poured into a snap cap vial and micro-pipeted into a 100 ml volumetric flask. Routinely 4 to 5 standards are used for calibration curves.

As and Se standards are made up as follows:

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1 ml of a 1000 mg/l solution diluted to 100 ml = 10 mg/l
1 ml of a 10 mg/l solution diluted to 100 ml = 0.1 mg/l (or 100 ug/l)
250 ul of a 100 ug/l solution diluted to 25 ml (5N HCl matrix) = 1 ug/l
750 ul of a 100 ug/l solution diluted to 25 ml (5N HCl matrix) = 3 ug/l
1250 ul of a 100 ug/l solution diluted to 25 ml (5N HCl matrix) = 5 ug/l
2000 ul of a 100 ug/l solution diluted to 25 ml (5N HCl matrix) = 8 ug/l
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Standard concentrations and detection limits (in mg/l) for the designated elements are listed below. If a fifth standard is run, it is one-half the lowest concentration listed.

Concen	trations				Detection	Limits
Ag	0.5	1.0 5.0	1.5	2.0 10.0	0.02 0.300	-
Al Ba	0.5	1.0	2.0 1.5	5.0 2.0	0.10 0.01	
Be Ca	0+5 0+5	1.0	2.0	4.0	0.04 0.01	
Cđ Cr	0.5	1.0	1.5 2.0	4.0	0.04	
Cu Pe	0.5 0.5	1.0	2.0	4.0	0.04	
K Mg	0•5 0•5	1.0	2.0 1.5	5.0 2.0	0.01	
Mn Na	0.5 0.5	1.0 1.0	2.0 1.5	5.0 2.0	0.04	ł
Ni Ps	0.5 1.0	1.0 2.0	2.0 5.0	4. 0 10.0	0.04)
Zn	0.5	1.0	1.5	2.0	0.01	

INTERFERENCES

- Suspended and dissolved solids
- Viscosity of samples
- 3. Chemical and spectral interference

QUALITY ASSURANCE/QUALITY CONTROL

- 1. Four to five standards used in calibration curve
- 2. Matrix blank used to zero the instrument

- Daily control standards (used to calibrate instrument) routinely read between samples to check for drift
- 4. Digested sample blanks read twice for QA/Qc
- Digested standards and duplicates analyzed
- 6. EP Toxicity samples spiked

CALCULATION

Strip chart read outs in concentrations of mg/l or ug/l, depending on how the curve was entered. If a dilution was required, multiply by the dilution factor.

Solid: Wet Sample

mg metal/kg sample = $\frac{(Z/1000)V}{W \times P}$

where: Z = ug/l of metal in processed sample from calibration curve

V = final volume of processed sample in ml

W = weight of wet sample in grams

P = percent solids

SAFETY

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- 1. No smoking in laboratory or around gas tanks
- 2. Chains should be around gas tanks.
- 3. Make sure gas tanks at proper pressure settings when in use
- 4. Check drain tube; make sure filled with water
- 5. Gloves, protective glasses, laboratory coats must be worn
- 6. Keep aspirating tubing clear of clogs
- 7. Keep burner head slots clean
- 8. O-rings should be changed periodically to avoid wear and tear, and the possibility of flashback
- Burner heads should not be changed when hot unless asbestos gloves are worn
- 10. Use proper gases with proper burner heads
- 11. All gas cylinders must be closed and regulator depressurized at when not in use

- 12. When changing tanks, check new tank for leaks with SNOOP
- 13. When using a 5% HF solution to clean hydride cells, caution must be used to avoid possible severe burn

STANDARD OPERATING PROCEDURE MERCURY

APPLICATION

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This method is applicable to drinking, surface, and saline waters, domestic an industrial waste, and will measure total mercury (organic, inorganic) in soils sediments, bottom deposits and sludge type materials. Reference material EPA 245.1 and 245.5

PROCEDURE

Soils

- 1. Rinse approximately 0.200 g of dried sample (dried at 60° C) with 5 ml DI into BOD bottles. Soil wieight must be known to 0.000g.
- Add 5 ml aqua regia to sample.
- Heat 2 minutes in a 95°C H₂O bath.
- 4. Cool samples and add 50 ml DI.
- 5. Add 15 ml of 5% KMnO4 (W/V).
- 6. Heat 30 minutes in a 95°C H2O bath.
- 7. Cool samples.
- 8. Add 6 ml hydroxylamine hydrochloride 12% w/v x NaCl 12% w/v.
- 9. Add 55 ml DI.

Water

- 1. Pipette 100 ml of agitated sample into BOD bottles.
- 2. Add 5 ml concentrated H2SO4.
- 3. Add 2.5 ml concentrated HNO3.
- 4. Add 15 ml 15% W/v KMnO4.
- 5. Allow to stand 15 minutes. If brown MnO2 precipitate is prominent, add more KMnO4, up to 30 ml and note addition in data.
- 6. Add 8 ml 5% potassium persulfate.
- 7. Digest in 95°C H2O bath for 2 hours.
- 8. Add 6 ml hydroxylamine hydrochloride 12% w/v x NaCl 12% w/v.

INSTRUMENT OPERATION

The samples and standards are analyzed on an Atomic Absorption Unit (AAU) utilizing an Atomic Vapor Accessory (AVA). The AAU is turned on and put into the operator mode. A mercury hollow cathode lamp is inserted and set at 3 ma. The bandpass is set at 1, wavelength at 253.7 nm, and the strip chart is turned on. The absorbance is checked to insure that it reads 1.000 and the instrument is set into the pk ht mode with an 8 second integration time. The mercury cell is cleaned with 1:1 HNO3 (ultra pure) and dried. It is set in place and adjusted to maximize the light beam passing through it which is shown by a minimum energy reading (minimum interference).

The AVA is integrated to the AAU and a flow gas of nitrogen is introduced at 20 P.S.I. The flow rate on the AVA is set at 6-7 liters per minute. A 5% SnCl₂ in 3 M HCl solution is introduced and the AVA is thoroughly flushed with thei solution (A preliminary flushing with DI is suggested to prevent cross reactions with any reagents left in the tubing). The AVA is calibrated to deliver 2.5 ml + 0.25 ml SnCl2.

DI blanks (reagent blank) are run to insure a response of approximately 0.000 is being achieved and then samples, standards, and method blanks are analyzed.

A correlation ≥ 0.9960 between the calibration points is desired and the concentration of samples is read off the plot of these points.

REAGENTS

- 1. Aqua regia: 3 parts concentrated HCl to one part concentrated HNO3.
- 5% KMnO4 (w/v): 50 g KMnO4/1 liter.
- 3. 5% Potassium persulfate: 12.5 g/250 ml.
- 60.0 NaCl and 60.0 g hydroxylamine Hydroxylamine hydrochloride: hydrochloride/500 ml.
- 5. SnCl₂: 62.5 ml concentrated HCl and 12.5 g SnCl₂/250 ml.

ANALYSIS

See Procedure.

INTERFERENCE

Possible iterference from sulfide is eliminated by the addition of KMnO4. Interfering volatile materials are removed when the dead air space in BOD bottle is purged with the flow gas in AVA before addition of SnCl2.

STANDARD PREPARATION

Dilution flasks are acidified with 0.2 ml concentrated HNO3. A 5-point calibration standard is prepared from a stock standard of 1,000 ppm Hg:

1 ml of 1,000 ppm diluted to 100 ml yields a 10 ppm standard solution 1 ml of 10 ppm diluted to 100 ml yields a 0.1 ppm standard solution

Calibration standard concentrations:

Method blank(100 ml DI)
0.05 ug/100 ml (0.5 ml of 0.1 ppm)
0.10 ug/100 ml(1.0 ml of 0.1 ppm)
0.30 ug/100 ml (3.0 ml of 0.1 ppm)
0.50 ug/100 ml (5.0 ml of 0.1 ppm)

The preparation of standards is completed as per the type of sample being analyzed.

Soils

Standards are brought up to a volume of 10 ml, and then treated as soil samples except 50 ml instead of 55 ml DI is added in 9.

Water

Standards are brought up to a volume of 100 ml and then treated as $\rm H_{20}$ samples.

SAMPLE PREPARATION

See Procedure.

QA/QC

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Check standards and duplicates are prepared for every 10 samples in the run. Calibration standards includes a method bland and four standards.

Soil

NBS river sediment (1.1 \pm 0.5 ug/g) are prepared as samples, weight recorded to four decimal places.

Water

1.5 ug/l check standards are prepared from separate stock and dilutions that are used for preparing calibration plot. (1.5 ml of 0.1 ppm Hg treated as $_{\rm H_2O}$ sample).

CALCULATION

Soils

- 1. Peak height is corrected to ug/100 ml from calibration plot.
- 2. (#ug/100ml) + (g sample) = ug/g.

Water

- 1. Peak height is converted to ug/100 ml from calibration plot
- 2. (#ug/100 ml)(100ml/.1 liter) = ug/l.

DETECTION LIMIT

Report data \geq 0.20 ug/l or 0.20 ug/g; anything less is reported ad <0.20.

SAFETY

All sample and standard preparation is done under hood. Dispose of concentrated Hg standards and samples in Hg waste contaiers. Make sure all hose connections are tight to prevent Hg vapor from leaking out of closed system.

DATA SHEET

No data sheet made up, write results directly in laboratory book.

STANDARD OPERATING PROCEDURE HYDRIDE DIGESTION FOR WATERS

APPLICATION

This method is used to prepare all waters for determination of arsenic and selenium in waters, using the aa/ae spectrophotometer 457 and IL atomic vapor accessory 440.

PROCEDURE

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- 1. 50 ml of well-shaken, acid preserved sample is measured in a volumetric pipet and transferred to a 300 ml tall form beaker.
- 2. 5.0 ml of concentrated HCl and 5.0 ml 70% HNO3 are added to the sample.
- 3. The sample is covered with a watchglass and digested on the hotplate at about 90° C until near dryness $\{1-2\text{ ml}\}$.
- 4. After cooling, 25 ml DI water is added to the sample.
- 5. The sample is covered again and returned to the hotplate, where it is digested to near dryness.
- 6. After cooling, 42 ml HCl is added to the sample.
- 7. The sample is transferred quantitatively to a specimen cup and diluted to the 100 ml mark with DI water.

INTERFERENCE

- 1. Heavy metals in the sample cause problems.
- 2. HNO3 in digested sample interferes
- 3. Losses of selenium seem to be a surface effect of glass.
- 4. Losses of both arsenic and selenium occur if volume gets too low during digestion, but volume must get low enough to drive off HNO3.

STANDARD PREPARATION

The stock standards are made up into an intermediate standard from which the standards for each run are taken. This intermediate standard is made fresh daily.

QA/QC

Normally one blank and a pair of standards are run with each set (≤ 20) of samples. A duplicate is also done for every 10 samples.

Cleaning Glassware

Beakers and watchglasses are washed with soap and water, using a wooden-handled brush (wire handles scratch glass). They are then rinsed in tap water followed by alternate DI and 1:1 HNO3 rinses, a minimum of 2. This followed with four rinses with DI. Beakers are drained and stored upside down on paper towels.

SAFETY

Samples are handled with gloves at all times. Beakers are placed in the hood before any reagents are added, and the digestions are done in the hood as well. The beakers are not removed from the hood until the sample has cooled. Lab coats and safety glasses are worn in the lab at all times. Also, heavier gloves and plastic aprons are available for use when needed.

STANDARD OPERATING PROCEDURE PLASMA DIGESTION FOR WATERS

APPLICATION

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This method is used to prepare all waters for determination of metals on the Plasma 200 (ICAP).

PROCEDURE

- 1. 200 ml of well-shaken, acid-preserved sample (pH <2) is measured in a graduate cylinder and poured into a 300 ml tall-form beaker.
- 2. 1 ml of 70% HNO_3 and 4 ml of 30% H_2O_2 are added to the sample.
- 3. The beaker is covered with a watchglass and the sample is digested on the hotplate at about 90°C until the volume is less than 20 ml.
- 4. After cooling, the sample is transferred quantitatively to a 50 ml conical tube and diluted to 20ml with DI.

INTERFERENCE

- 1. Certain samples, particularly E.P. Toxicity extracts, are frequently basis. These must have the pH adjusted to ≤ 2 with 70% HNO3 before adding the reagents.
- 2. Samples high in organic compounds require additional HNO3 and $\rm H_{2}O_{2}$ in order to break these compounds down. Normally, enough $\rm H_{2}O_{2}$ is added before digesting to dissolve crystals and lighten sample color (these samples are often dark colored) if possible; but some samples require digestion with repeated small aliquots (1-5 ml) of $\rm HNO_{3}$ and $\rm H_{2}O_{2}$ added as volume decreases. The ideal final product will be clear to straw colored.

STANDARD PREPARATION

For convenience, most stock standards are made up into intermediate standards from which the standards from each run are taken. These are as follows.

Standard Ia: May be HNO_3 preserved for one week; add 1 ml HNO_3/ml . 1 ml, 1000 ppm stock, diluted to 1 liter for Be, Zn, Ca, Sr, Mg, Ti, Sn, Co.

Standard Ib: May be HNO3 preserved for one week; add 0.1 ml HNO3/100 ml. 1 ml, 1000 ppm stock, diluted to 100 ml for Na, Mn, Fe, Ba, K, Al, Mo.

Standard Ic: Not able to preserve. 1 ml, 1000 ppm stock, diluted to 1 liter for V.

Standard IIa: May be HNO3 preserved for one week; add 1 ml HNO3/liter. 0.1 ml, 1000 ppm stock, diluted to 1 liter for Cd; 1 ml, 1000 ppm stock, diluted to 1 liter for Cr, Cu, Pb, Ni.

Standard IIb: Not able to preserve. 1 ml, 1000 ppm stock, diluted to 1 liter for Ag.

Standards are made from intermediates as follows:

Standard I = 10 ml Ia + 10 ml Ib + 10 ml Ic in 300 ml tall-form beaker.

Standard II = 6 ml IIa + 2 ml IIb in 300 ml tall-form beaker.

Standards are then diluted to about 200 ml with DI. A blank of 200 ml of DI is also made. The standards and the blank are idgested in the same manner as the samples.

QA/QC

Normally, one blank and one set of standards are run with each batch of samples. (A bath is usually 20 samples or less). Also, one duplicate is run for every 10 samples or fraction of 10. Thus, a batch of 17 samples would include one blank, two standards and two duplicates.

Cleaning Glassware

Beakers and watchglasses are washed with soap and water, using a wooden-handled brush (wire handles scratch glass). They are then rinsed in tap water followed by alternate DI and 1:1 HNO3 rinses, a minimum of 2. The final rinses are four with DI. Beakers are drained and stored upside down on paper towels.

SAFETY

Samples are handled with gloves at all times. Beakers are placed in the hood before any reagents are added, and the digestions are done in the hood as well. The beakers are not removed from the hood until the sample has cooled. Lab coats and safety glasses are worn in the lab at all times. Heavier gloves and plastic aprons are available when needed.

STANDARD OPERATING PROCEDURE PLASMA METALS

APPLICATION

This method may be used for the determination of dissolved suspended or total elements in drinking and surface waters, domestic and industrial wastewaters, and soil and sludge extractions. Because of the differences between various makes and models of satisfactory instruments, no detailed instrumental operating instructions can be provided. Instead, the analyst is referred to the instructions provided by the manufacturer of the particular instrument.

SUMMARY OF METHOD

The method describes a technique for the sequential multi-element determination of trace elements in solution. The basis of the method is the measurement of atomic emission by an optical spectroscopic technique. Samples are nebulized and the aerosol that is produced is transported to the plasma torch where excitation occurs. Characteristic atomic-line emission spectra are produced by a radio-frequency inductively coupled plasma (ICP). The spectra are dispersed by a grating spectrometer and the intensities of the lines are monitored by photomultiplier tubes. The photocurrents from the photomultiplier tubes are processed and controlled by a computer system. A background correction technique is required to compensate for variable background contribution to the analyte concentrations.

INSTRUMENT OPERATION

To prepare the Plasma-200 instrument for operation:

- 1. Turn on the cooling water at the coolant circulator on the floor.
- 2. Then turn on the argon supply; the operating pressure should be 60 psi at the instrument and 65 to 70 psi at the tank.
- 3. Turn on the circuit breaker located on the upper right portion of the lower panel.
- 4. Next, verify that the external venting system is open and operating at between 150 and 190 cubic feet per minute with a vaneometer.
- 5. Verify that there is water in the drain line.
- 6. Verify that the anode breaker, located to the left of the main circuit breaker, is in the UP position.
- 7. Press the eject button opening the cassette drive door, and insert the IL Systems Tape Cassette (green label). All the user program tapes have the systems operation recorded.

- 8. After inserting the IL Systems Tape Cassette, type (ENABLE) (TAPE). The screen then displays the word TAPE for 4-1/2 minutes, followed by a count down from 190 seconds (which allows the power supply to warm up).
- 9. If a "TORCH ERROR" message appears, see section 5.2 of the instrument manual, correct, and clear. Verify a Hg line wavelength calibration. See 120.
- 10. When the wavelength calibration is complete, the CRT displays the Program Selection Menu.
- 11. Finally, remove the cassette from the cassette drive.

At this point, the torch may be ignited if desired. BEFORE IGNITING THE TORCH, connect the pump winding to the peristaltic pump. Make sure the capillary tubing is connected properly to the capillary and the pump winding. The pump winding should be disconnected when the IL Plasma-200 is shut down to extend its lifetime. The torch should be ignited and the system allowed to warm up for at least 20 minutes before use.

The following procedure is used for torch ignition:

- 1. To ignite the torch, press <ENABLE> <TORCH>. The information in Figure 3-3 then appears on the screen.
- 2. The ENABLE TORCH command ignites the torch and maintains it at power level 5. IL recommends that the system be warmed up at the power level which is to be used during analysis; if the power level for analysis is other than 5, change the power setting at this time by typing n POWER <RETURN> (where n is the desired power level). Most analysis is done at power level 3 or 4. Power level 6 is used for organics only. Refer to Section 3.10 of the instrument manual for operating instructions before using power level 6.
- 3. If the torch fails to ignite, and the CRT displays only the message "TORCH DIDN'T LIGHT," and does not display an error condition, key <ENABLE> <TORCH>. If the torch continually refuses to ignite, contact your IL service engineer. If there is an error condition displayed, see Section 5.2 of the instrument manual to troubleshoot and type in <CLEAR> <ENABLE> <TORCH>.
- 4. To end the torch ignition cycle (if necessary), key <ESC>.
- 5. While the torch is stabilizing, set the I/O Format and the required parameters; the torch should stabilize for at least 20 minutes.

Program Selection Menu

the sampler, and other peripheral devices. The I/O Format must be set up for each program, because it cannot be stored on the mini-cassette. The I/O Format Menu appears displaying the status of each peripheral device. A "#" appears on the screen, prompting a numeric keyboard entry. To activate a particular device, press the appropriate number followed by <RETURN>. If the device is accidentally accessed, keying a <RETURN> will return the # prompt. To turn the device on, type 1 <RETURN>. Keying anything except 1 turns the device off. Turn on the printer (leave paging off). Set operator ID, date, and time. The other devices are optional. #9 exits the I/O Format.

120 is the Wavelength Calibration Procedure Option. This command causes the system to plot the Hg wavelength curve. If the hash marks are more than 2.5 times their own length away from the curve, the optics are out of calibration. (IN THIS CASE, CALL YOUR SERVICE ENGINEER.)

130 is the EDIT Mode Option. The EDIT Mode is used to generate and/or modify methods programs. The full ASCII keyboard must be used when in the EDIT Mode. When in this mode, an asterisk (*) appears on the CRT to prompt keyboard entries.

140 is the Shutdown Procedure Option. The Shutdown Procedure Option describes how to prepare the instrument to shut down the power supply and eventually shut down the Plasma-200 instrument. To select and enter the Shutdown Procedure option, type 140 <RETURN>. The system displays the message "PRESS ENABLE THEN 0" on the screen. Press <ENABLE> and 0. "WAIT 3 MINUTES FOR SHUTDOWN" appears on the screen. (Note: Pressing <ENABLE> and 0 at anytime begins the Shutdown Procedure.) After three minutes the message "TURN OFF CIRCUIT BREAKER" appears on the CRT, and the circuit breaker can be tripped.

PROCEDURE

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See Instrument Operation to turn on the instrument. Put instrument in the EDIT Mode. To enter a new program, select the Program Number and Name Option by typing the number (from 1 through 99, inclusive) you wish to assign to the program; then, enter a space by pressing the space bar. Then, type the word ENTER followed by a space and program name (up to 18 characters); then press the RETURN key. To call up the program, type n SEE (RETURN).

Power Level Option

The Power Level of the plasma discharge is under computer control and can be changed as needed by the operator by using the ASCII keyboard. There are six power settings (1-6) that are available, with 1 being the lowest power, and 6 being the highest power. The default power level is 3.

To select a Power Level other than 3, press the desired setting (from 1 through 6, inclusive) and type PWR. For example, if the Power Level 4 is to be entered, type 4 PWR (RETURN). To override the existing PWR power setting, use the POWER command, which instantaneously changes the plasma power to the desired level. Then, when any new command causes the monochromator to move from rest, the plasma power returns to the PWR program power setting.

Repeat Analyses and Repeat Readings Option

The two commands *ANAL and *RDG are used to set the number of repeat analyses and repeat readings, respectively. Each analysis is one complete program cycle. If 3 *ANAL is chosen as the number of repeat analyses, the entire program is cycled through three times. If two readings of each element are required, then 2 *RDG would be entered into the program. With those selections, each element in the program would be read twice and then the cyclewould be repeated three times.

- 1. To enter the number of Repeat Analyses for the program, type the appropriate number followed by *ANAL <RETURN>. For example, if two analyses are desired, type 2 *ANAL <RETURN>. Consequently, the complete analysis for this program is repeated three times.
- 2. Now, to select the number of readings for each element, type the desired number and *RDG <RETURN>. For example, if three readings are required for each element, type 3 *RDG <RETURN>.

Element Selection Option

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- 1. Library of Elements. A library of useful analytical lines for 78 elements is available in memory. To access the possible line choices for these elements, type ELEMENT and the element symbol, then press <RETURN>. For example, if Copper is the element of interest, type ELEMENT CU <RETURN>.
- 2. Wavelength Selection. To select one of the wavelengths from the table, press the number of the desired line and type USE. For example, if the first Cu line is the one of choice, type 1 USE <RETURN>.
- 3. Alternate Wavelength Selection. To select a wavelength other than one of those displayed, type 1 USE <RETURN>. Then, type desired wavelength followed by NM. For instance, if 273.53 nm is desired, type 273.53 nm <RETURN>. As a result, the wavelength selected in step B is replaced by 273.53 nm.

Integration Time Option

To enter the desired Integration Time, type the desired integration time (from 0.1 seconds to 25.5 seconds, inclusive) followed by SEC. For example, if 2.0 sec is the Integration Time to be entered, type 2.0 SEC <RETURN>. The integration time can be increased to aid in achieving low detection limits if the increase in analysis time is justified.

Decimal Placement Option

To select the number of digits to the right of the decimal, use the #D command. To select the number of digits, type the desired number followed by #D. For example, for a format displaying two digits to the right of the decimal, type 2 #D <RETURN>. A high concentration curve (i.e., 1,000 ppm - 100 ppm) will not accept anything higher than 1 #D accuracy.

Generating a Calibration Curve Option

For generation of a Calibration Curve, the Plasma-200 accepts a reagent blank plus up to five standards. The "#" symbol denotes standard number; bottle number and concentration are defined by the operator. To enter the Calibration Standards, type the number of the element in the program followed by TH <RETURN>. For instance, for the first element of the program (assuming the current program has been accessed), type 1 TH <RETURN>. To enter the standard numbers, bottle numbers, and concentrations, perform the following steps. Type standard number, bottle number desired (1-99), and the concentration. For example, type 1 2 50 CONC <RETURN>.

Window Size Option

The peak search window can be varied for each element in the program. The three window sizes available are Narrow (N), Medium (M), and Wide (W). The sizes represent 0.033, 0.066, and 0.1 nm, respectively. The standard window size is Medium. If the Narrow window is to be used, type WS N <RETURN>. The smaller the window, the less chance for interfering peaks.

Trim Routine Option

Each wavelength chosen has a theoretical position stored in memory. The actual position is slightly different due to the mechanics of the monochromator.

To optimize the wavelength position, call up the desired program and line number, aspirate a test solution containing the element of interest and type TRIM (RETURN). (It is assumed that the desired program and line report have been called up.) Move the cursor to the center of the analyte peak by pressing L for left, R for right, U for up, and D for down. Only the horizontal location must be adjusted; the vertical displacement (U and D) is for operator convenience only. Then press (RETURN). To perform the TRIM routine for all lines of the program, call up the program, aspirate a solution containing all the elements in the program and type #TRIM (RETURN).

Torch Height Selection Option

The Torch Height observation is variable and can be optimized for each element in the program; the MM command changes the observation height for the element in the program. The observation heights must be even numbers between 0 and 48 mm. To select a Torch Height of 18 mm, type 18 MM (RETURN).. To determine the best viewing height, call up the line (n TH), aspirate a standard and type in TPROFILE (RETURN). Then aspirate the blank and type ASPIRATE ard and type in TPROFILE (RETURN). Then aspirate the blank and type ASPIRATE TPLOT (RETURN). The best observation height is usually the height at which a maximum intensity difference exists between sample and blank. Each "-" on the screen represents a change of 2 mm in observation height starting with 0

Restpeak Routine

The RESTPEAK routine can be used for any trimmed element in the program. If the spectral region around a peak needs to be investigated, use this command to direct the microcomputer to the analytical peak, scan a 0.25 nm (second order) region around a peak, and produce an image of the scan on the CRT.

To carry out the RESTPEAK command, first select the desired element of the program by typing the element number followed by TH and pressing <RETURN>. Next aspirate a standard containing the element of interest, then type RESTPEAK <RETURN>. After completing the RESTPEAK routine, a second emission scan at a given spectral line can be superimposed by the following steps.

- 1. Aspirate the sample.
- 2. Next, if the operator is changing bottles, it is recommended that the operator type ASPIRATE before PLOT. This causes the pump to operate at the fastpump rate for the time interval set by PDLY, flushing the sample introduction system of the original solution. Type ASPIRATE PLOT <RETURN>.
- 3. This process may be repeated as often as required to plot as many solutions as desired. Differences in baseline intensity between the standard and the sample indicate that background correction is needed at that wavelength.

Background Correction

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Background correctin is primarily used to compensate for baseline shift between standards and samples. To correct for background shift, background correction must be performed in a region of the spectrum which is free from matrix emission lines and which accurately represents the background under the analyte peak. For a more thorough discussion of background correction, consult the "Methods Manual for Inductively Coupled Plasma Emission Spectrometry."

To set the background correction position:

- 1. Select the line of interest by typing the line number and TH and pressing <RETURN>. For example, if the first line in the program is to be corrected, type 1 TH <RETURN>.
- Aspirate the sample and type BKG-TRIM <RETURN>.
- 3. Next, select and enter one of the following:

For no background correction, press N.

For correction to the left of the peak, press L.

For correction to the right of the peak, press R.

For correction to the right and left of the peak, press B.

When the cursor appears at its default location (-0.05 nm in second order), position it as desired by pressing the L key for left, R key for right, U key for up, and D key for down. The movement of the cursor in the left and right directions can be varied by using either the fine or coarse step sizes. The system defaults to the coarse step size, but if a finer movement is needed, the cursor can be made to move in much smaller steps by typing F. After positioning the cursor, key <RETURN>.

Interfering Element Correction Routine

The Interfering Element Correction routine should be used only as a last resort. The operator should first attempt to use a line without interferences. If this cannot be done, the Interfering Element Correction routine may be used. For a more complete discussion of the Interfering Element Correction, see the "Methods Manual for Inductively Coupled Plasma Emission Spectrometry."

An interfering element is any element other than the analyte of interest that emits at the chosen wavelength. Perform a restpeak routine of the element of interest followed by a plot of suspected interferences. If any part of a peak shows in the narrowest window, an erroneously large peak will result. It can be corrected in this way.

- 1. Select a known concentration of Fe (the interfering element). In this example, a standard concentration of 1,000 ppm Fe is used. The 1,000 ppm Fe standard is analyzed at the V wavelength (the analyte). The apparent V concentration due to the presence of Fe is 10 ppm.
- Then, compute a scale factor. The scale factor can be from 0.0001 to 3.0000.

Scale Apparent Analyte Concentration 10
Factor = Actual Interferent Concentration = 1000 = 0.0100

In this example, 0.0100 is used as the scale factor.

- 3. Add Fe to the program before V is added to the program. Follow standard procedures and select an Fe line. Enter the Fe line as any other line is entered in the program. The interfering element line must be in the program before the line being corrected; i.e., it must have a low line number. If the order of the interferent and analyte are reversed, the IMPROPERLY NESTED error message will appear on the screen.
- 4. Now select the analyte line requiring correction by typing the desired line number followed by TH. For example, if line 2 is desired, type 2 TH <RETURN>.
- 5. Enter the line number of the interfering element under one of the two I/E headings. For instance, if line 1 is the interfering element, type 1 1I/E <RETURN>. Line 1 is now entered as the interfering element line for line 2.
- To cancel a selected line, type 0 1I/E <RETURN>.
- 7. Next, enter the scale factor under the corresponding S/F heading. As an example, type 0.01 1S/F <RETURN>. A scale factor of 0.01 is now entered and the program will now correct for that interfering element.

The problem with using the interfering element correction is that the interference must either be fairly well resolved or be a near direct overlap. Direct overlaps are difficult to detect.

Side Line Indexing Method

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A standard feature of Revision 0 software is a program called SLIM (Side Line Indexing Method). This routine allows the operator to select a reference emission line as the "searched" peak near a difficult to detect analyte peak. The reference peak is first located by the conventional monochromator search routine and then the refractor plate moves directly to the analyte peak location. The reference peak can be an integral part of the matrix, or spiked into the sample, high standard, and blank by the operator. The SLIM routine is very useful for determinations of samples where the analyte peak is obscured by a partial spectral overlap, wing broadening, or when the

analyte peak is too small to determine under normal conditions. The reference peak has to be within 0.2 nm of the analyte peak. To use the SLIM routine, aspirate a solution containing analyte only and trim. Aspirate a solution containing analyte and spiked with suspected interfering reference peak and type SLIM <RETURN>. Trim the reference peak. Enter side for analyte peak (L or R). Trim the analyte peak. Enter background correction, if necessary.

The high standard, the blank, and all samples must contain some Al. The Al concentration does not have to be constant. Calibration is carried out in the standard manner.

If the use of the SLIM routine is no longer required for a particular line in a program, typing -SLIM <RETURN> will remove the routine for that particular line. If the position of the reference peak has to be changed, typing TRIM <RETURN> will allow the readjustment of the reference peak position. If the analyte peak position needs to be reset, typing SLIM <RETURN> will allow the operator to change the position of the analyte peak only.

Calibration

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After all options are optimized, calibrate the elements. Emission line intensities obtained during calibration and the corresponding concentration values are fit to a quadratic equation by a least squares method. During analysis, concentration values are calculated from intensities using this equation. This method is used to correct for any nonlinearity of the calibration curve.

To perform calibration, type CALIBRATE <RETURN>. The question *NO. OF READINGS TO STANDARDIZE?* appears on the CRT screen. Enter the number of readings (the number of readings must be between 1 and 10) by pressing the desired number and <RETURN>. For example, if three readings are to be used to standardize, type 3 <RETURN>. In response, the system displays the standard to be aspirated. Aspirate the standards as requested by the Plasma-200, then press <READ>.

Program Storage Routine

After a program is written, it can be stored on tape or disk. The information stored consists of each user program in memory with element information, the trimmed line positions for each element, and the latest calibration data. The user programs can either be stored by themselves or with the system program. To store system and user program, enter <ENABLE> <TAPE>, followed by 4 <RETURN>. To modify programs, refer to instrument manual.

Recalibration

After a calibration curve is entered, a slope recalibration may be performed using the reagent blank and the highest standard. This operation may be performed with either keyboard and is recommended each time a program is reentered from the cassette reader.

To perform recalibration on the full keyboard, type in the EDIT mode RECALIBRATE (RETURN). The question "NO. OF READINGS TO STANDARDIZE?" then appears on the CRT. Enter the desired number of readings (between 1 and 10)

by pressing the desired number of readings and <RETURN>. For example, if two readings are to be taken, press 2 <RETURN>. Next, aspirate the requested bottle number (the highest standard) and press <READ>. Finally, aspirate the blank as requested by the Plasma-200 and press the <READ> key.

REAGENTS

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The only reagents used are pure grade HNO₃ to digest (see digestion procedure) and make up the standard curves. Triton X-100 can be used if there is a problem matching sample and standard viscosity. It can also be used to aspirate through the spray chamber to keep the surface smooth and clean for top aspiration efficiency.

ANALYSIS

Recalibrate analyte and interfering elements of analyte following procedure. Return to operator mode <PROG>, aspirate sample, and type in <SAM#>, nnnnn (number has to be less than 67000), and <READ>.

Analysis Errors

OV FLOW Signal intensity exceeds dynamic range of the instrument (i.e., 25000 cts/25 ms)

OVRANGE Sample is greater than 125 percent of high standard

If either of these messages occurs, analyte can either be run diluted or on a less sensitive wavelength. Refer to manual or any table of atomic emissions.

INTERFERENCE

The main interference in plasma spectroscopy is spectral. An analyte may or may not be influenced by any interfering element. Using a narrow window helps to eliminate interference, but if the concentration of the interfering element is high, it will inevitably interfere with the analyte. The best procedure is to choose an alternate wavelength. If no alternate wavelength is suitable, then interfering element correction must be used (see procedure).

Baseline shift or a continuous spectrum interference must be background corrected (see procedure). Some elements may be corrected using the SLIM routine (see procedure). It is a good idea to inspect the spectral region of each analyte on a representative matrix. The best way of handling interferences must then be decided.

STANDARD PREPARATION

Depending upon the sensitivity of the wavelength chosen for the analyte, a blank and four standards are made up usually spreading the range 0, X, 2.5X, 5X, 10X. If several analytes do not interfere with each other, they may be mixed together in a cocktail. The matrix must match closely the samples; usually one to two percent HNO3.

SAMPLE PREPARATION

See digestion procedure.

QA/QC

A blank, standard, and duplicate are digested with every set of samples. The instrument, when warmed up properly, is very stable. A check standard (usually close in value to sample concentration) is read in the middle and end of the run. If you suspect drift or carryover, run the check standard more often. If the check standard is not satisfactory (within § *80 percent of true and/or mean value), a recalibration must be performed. If there is a lot of carryover, it is a good practice to aspirate blank water first so as to get a stable and accurate recalibration. The digested blank, standard, and duplicate are recorded and calculated into mean and standard deviation.

CALCULATION

Waters: Response (ug/ml) x concentration (ml/ml) x dilution (ml/ml)

Soils or solids: Response (ug/ml) x final volume (ml) x dilution (ml/ml) weight of sample (g)

DETECTION LIMIT

The detection limit for most metals is listed in the manual. Experimentally, they can be determined by calculating a value that is \$2 times the mean of a series of blank responses. Obviously, interferences (even if corrected), the use of a less sensitive line, or dilution will all raise the detection limit accordingly.

SAFETY

The drain line must be attached and full of water. The pump must be hooked up and aspirating solution while the torch is on. Do not attempt to work on instrument while voltages are on.

STANDARD OPERATING PROCEDURE CHEMICAL OXYGEN DEMAND

APPLICATION

This method applied to both wastewater and soils/sludges. The chemical oxygen demand (COD) is used as a measure of the oxygen equivalent of the organic matter content of a sample that is susceptible to oxidation by a strong chemical oxidant. For samples from a specific source, COD can be related empirically to biochemical oxygen demand (BOD), organic carbon, or organic matter. The test is useful for monitoring and control after correlation has been established. The dichromate reflux method is preferred over procedures using other oxidants because of superior oxidizing ability, applicability to a wide variety of samples, and ease of manipulation. Oxidation of most organic compounds is 95 to 100% of the theoretical value. Pyridine and related compounds resist oxidation and volatile organic compounds are oxidized only to the extent that they remain in contact with the oxidant. Ammonia, present either in the waste or liberated from nitrogen-containing organic matter, is not oxidized in the absence of significant concentration of free chloride ions.

Most types of organic matter are oxidized by a boiling mixture of chromic and sulfuric acids. A sample is refluxed in strongly acid solution with a known excess of potassium dichromate ($K_2Cr_2O_7$). After digestion, the remaining unreduced $K_2Cr_2O_7$ is titrated with ferrous ammonium sulfate to determine the amount of $K_2Cr_2O_7$ consumed and the oxidizable organic matter is calculated in terms of oxygen equivalent. Keep ratios of reagent weights, volumes and strengths constant when sample volumes other than 50 ml are used. The standard 2-hour reflux time may be reduced if it has been shown that a shorter period yields the same results.

PRODEDURE

1. Treatment of Water Samples with COD of >50 mg Oxygen Per Liter

Place 50 ml sample (for samples with CCD >900 mg O2/liter, use smaller sample portion diluted to 50 ml) in a 500 ml refluxing flask. Add 1 g HgSO4, several glass beads, and very slowly add 5.0 ml sulfuric acid reagent, with mixing to dissolve HgSO4. Cool while mixing to avoid possible loss of volatile materials. Add 10 ml of 0.2500 k2Cr2O7 solution and mix. Attach flask to condenser and turn on cooling water. Add remaining sulfuric acid reagent (25 ml) through open and of condenser. Continue swirling and mixing while adding the sulfuric acid reagent. CAUTION: Mix reflux mixture thoroughly before applying heat to prevent local heating of flask bottom and a possible blowout of flask contents. Reflux for 2 hours.

Cool and wash down condenser with distilled water. Disconnect reflux condenser and dilute mixture to about twice its volume with distilled water. Cool to room temperature and titrate excess K2Cr2O7 with FAS, using 0.10 to 0.15 ml (2 to 3 drops) ferroin indicator. Although the quantity of ferroin indicator is not critical, use the same volume for all titrations. Take as the end point of the titration the first sharp color change from blue-green to reddish brown. The blue-green may reappear. In the same manner, reflux and titrate a blank containing the reagents and a volume of distilled water equal to that of sample.

2. Alternate Procedure for Low-COD Samples

Follow Procedure 1 with two exceptions: 1) use 10 ml of 0.025N $K_{\rm 2Cr_2O_7}$, and 2) titrate with 0.025M FAS. (CAUTION: Exercise extreme care with this procedure because even a trace of organic matter on the glassware or from the atmosphere may cause gross errors.) If a further increase in sensitivity is required, concentrate a larger volume of sample before digesting under reflux as follows: add all reagents to a sample larger than 50 ml and reduce total volume to 150 ml by boiling in the refluxing flask open to the atmosphere without the condenser attached. Compute amount of HgSO4 to be added (before concentration) on the basis; of a weight ratio of 10:1, HgSO4:Cl-, using the amount of Cl- present in the original volume of sample. Carry a blank reagent through the same procedure. This technique has the advantage of concentrating the same with out significant losses of easily digested volatile Hard-to-digest volatile materials such as volatile acids are lost, but an improvement is gained over ordinary evaporative concentration methods.

3. Determination of Standard Solution

Evaluate the technique and quality of reagents by conducting the test on a standard potassium hydrogen phthalate solution.

4. Alternate Procedure for Soil Samples

Follow Procedure 1 with the following exceptions: 1) accurately weigh 0.2 to 0.5 g that will consume one-half of the $K_2Cr_2O_7$, and 2) add 20 ml of distilled water to each flask. Add HgSO₄ and H₂SO₄ according to Procedure 1.

All glassware can be cleaned with 1:1 HNO_3 with plenty of distilled water rinse to remove traces of HNO_3 .

A blank and standard must be run with each set.

INSTRUMENT OPERATION

The reflex apparatus consist of 500 or 250 ml Erlenmeyer flasks with ground-glass 24/40 neck and 300 mm jacket Liebig, West or equivalent condenser with 24/40 ground-glass joint, and a hot plate having sufficient power to produce at least 1.4 W/cm² of heating surface, or equivalent. Turn hot plate on ahead of time. Turn on condenser cooling water.

REAGENTS

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Standard Potassium Dichromate Solution, 0.0417M/0.2500N

Dissolve 12.259 g $K_2Cr_2O_7$, primary standard grade, previously dried at 103°C for 2 hours in distilled water and dilute to 1000 ml.

2. Sulfuric Acid Reagent

Add Ag_2SO_4 , reagent or technical grade, crystals or powder, to concentrated H_2SO_4 at the rate of 5.5 g Ag_2SO_4/kg H_2SO_4 . Let stand 1 to 2 days to dissolve Ag_2SO_4 .

3. Ferroin Indicator Solution

Dissolve 1.485 g 1,10-phenanthroline monohydrate and 695 mg $FeSO_4.7H_2O$ in distilled water and dilute to 100 ml. This indicator solution may be purchased already prepared.

4. Standard FAS Titrant, Approximately 0.25M

Dissolve 98 g Fe(NH₄)₂(SO₄)₂.6H₂O in distilled water. Add 20 ml concentrated H₂SO₄, cool, and dilute to 100 ml. Standardize this solution daily against standard K₂Cr₂O₇ solution as follows. Dilute 10 ml standard K₂Cr₂O₇ to about 100 ml; add 30 ml concentrated H₂SO₄ and cool while samples are on hot plate. Titrate with FAS titrant using 0.10 to 0.15 ml (2 to 3 drops) ferroin indicator before titrating samples.

Normality of FAS Solution = Volume $K_2Cr_2O_7$ solution titrated, ml × 0.25N Volume FAS used in titration, ml $K_2Cr_2O_7$

5. Mercuric Sulfate ~

HgSO4, crystals or powder.

6. Sulfamic Acid

Required only if the interference of nitritesis to be eliminated

7. Potassium Hydrogen Phthalate (KHP) Standard

Lightly crush and then dry potassium hydrogen phthalate (HOCCC6H4COOK) to constant weight at 120°C. Dissolve 425 mg in distilled water and dilute to 1000 ml. KHP has a theoretical COD of 1.176 mg O_2/mg and this solution has a theoretical COD of 500 ug O_2/ml . This solution is stable when efrigerated for up to 3 months in the absence of visible biological growth.

INTERFERENCE

Volatile straight-chain aliphatic compounds are not oxidized to any appreciable extent. This failure occurs partly because volatile organics are present in the vapor space and do not come in contact with the oxidizing liquid. Straight-chain aliphatic compounds are oxidized more effectively when Ag₂SO₄ is added as a catalyst. However, Ag₂SO₄ reacts with chloride, bromide and iodide to produce precipitates that are oxidized only partially. The difficulties caused by the presence of the halides can be overcome largely, though not completely, by complexing with HgSO₄ before the refluxing procedure. Although 1 g HgSO₄ is specified by 50 ml sample, a lesser amount may be used where sample chloride concentration is known to be less than 2000 mg/l, as long as a 10:1 ratio of HgSO₄:Cl⁻ is maintained. Do not use the test for samples containing more than 2000 mg Cl-/l. Techniques designed to measure COD in saline water are available.

 NO_2^- exerts a COD of 1.1 mg O_2/mg NO_2^-N . Because concentrations of NO_2^- in waters rarely exceed 1 or 2 mg NO_2^-N/l , the interference is considered insignificant and usually is ignored. To eliminate a significant interference due to NO_2^- , add 10 mg sulfamic acid for each mg NO_2^-N present in the sample volume used; add the same amount of sulfamic acid to the reflux vessel containing the distilled water blank.

Reduced inorganic species such as ferrous iron, sulfide, manganous manganese, etc., are oxidized quantitatively under the test conditions. For samples containing significant levels of these species, stoichiometric oxidation can be assumed from known initial concentration of the the interferring species and corrections can be made to the COD value obtained.

STANDARD PREPARATION

A 500 mg/l KHP standard is analyzed on the high method COD (see Procedures 1 and 3, and Reagent 7.

A 50 mg/l KHP standard is analyzed on the low method COD (Procedure 2). Dilute 5 ml of Reagent 7 to 50 ml in flask and analyze.

SAMPLE PREPARATION

Samples must be preserved by acidification to pH ≤ 2 with concentrated H₂SO₄.

QUALITY ASSURANCE/QUALITY CONTROL

A blank and standard are analyzed with every ten samples. The standard must be within 2 standard deviations of the mean value. If the standard fails to be within the limits, the run must be reanalyzed.

CALCULATION

COD as mg $O_2/1 = \frac{(A - B) \times N \times 8000}{ml \text{ sample}}$

where A = ml FAS used for blank
B = ml FAS used for sample

DETECTION LIMIT

High Level Water: 50 mg/l anything; <50 mg/l should be rerun on low level

High Levl Soil: 2500 ug/g Low Level Water: 5 mg/l

SAFETY

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- 1. Slowly add concentrated H2SO4 reagent with plenty of swirling.
- 2. Make sure that ${\rm H}_2{\rm SO}_4{\rm -water}$ mixture is well mixed and cooling water is sufficient to condense organic vapors.
- Used titration mixture is classified as hazardous waste and must be diluted and stored in labeled plastic containers to be treated later.

DATA SHEET

Sample copy of data sheet attached.



ENVIRODYNE ENGINEERS

19161 Lectional Road, St. Laurs, Missauri 63146 (314) 434-6960

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COD DETERMINATIONS

Flask Bo.	Lab No.	Sample	Sample (m1)	Titrant (ml)	94ff. : (m1)	COD (mg/1)
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 						<u> </u>
	STAN	MAD			N -	

COD mg/1 = (Diff)(n)(8,000)

mi Sample

m a Marmality of Titrant

STANDARD OPERATING PROCEDURES CYANIDE

APPLICATION

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This method is applicable to the determination of cyanide in drinking, surface and saline waters, domestic and industrial wastes.

The colorimetric procedure is used for concentrations below 1 mg/l of cyanide and is sensitive to about 0.02 mg/l. The cyanide as hydrocyanic acid (HCN) is released from cyanide complexes by means of a reflux-distillation operation and absorbed in a scrubber containing sodium hydroxide solution. The cyanide ion in the absorbing solution is then determined.

In the colorimetric measurement the cyanide is coverted to cyanogen chloride, CNCl, by reaction with chloramine-T at a pH less than eight without hydrolyzing to the cyanate. After the reaction is complete, color is formed on the addition of pyridine-barbituric acid reagent. The absorbance is read at 578 nm for pyridine-barbituric acid. To obtain colors of comparable intensity, it is essential to have the same salt content in both the sample and the standards.

Cyanide is defined as cyanide ion and complex cyanides converted to hydrocyanic acid (HCN) by reaction in a reflux system of a mineral acid in the presence of magnesium ion.

PROCEDURE

Samples Without Sulfide

- 1. Place 500 ml of sample, or an aliquot diluted to 500 ml in the 1 liter boiling flask. (Add a few boiling beads to flask prior to adding sample. Make sure water is running through cold finger at a reasonable rate.) Add 50 ml of sodium hydroxide to the absorbing tube and dilute if necessary with distilled water to obtain an adequate depth of liquid in the absorber. Connect the boiling flask, condenser, absorber and trap in the train.
- 2. Start a slow stream of air entering the boiling flask by adjusting the vacuum source. Adjust the vacuum so that approximately one bubble of air per second enters the boiling flask through the air inlet tube. (CAUTION: The bubble rate will not remain constant after the reagents have been added and while heat is being applied to the flask. It will be necessary to readjust the air rate occasionally to prevent the solution in the boiling flask from backing up into the air inlet tube.)
- 3. Slowly add 25 ml concentrated sulfuric acid through the air inlet tube. Rinse the tube with distilled water and allow the airflow to mix the flask contents for 3 minutes. Pour 20 ml of magnesium chloride into the air inlet and wash down with a stream of water.
- 4. Heat the solution to boiling, taking care to prevent the solution from backing up into and overflowing from the air inlet tube. Reflux for one hour. Turn off heat and continue the airflow for at least 15 minutes. After cooling the boiling flask, disconnect absorber and close off the vacuum source.

5. Drain the solution from the absorber into a 250 ml volumetric flask and bring up to volume with distilled water washings from the absorber tube.

Samples With Sulfide

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- 1. Place 500 ml of sample, or an aliquot diluted to 500 ml in the 1 liter boiling flask. Pipet 50 ml of sodium hydroxide to the absorbing tube. Add 25 ml of lead acetate to the sulfide scrubber. Connect the boiling flask, condenser, scrubber and absorber in the train. The flow meter is connected to the outlet tube of the cyanide absorber.
- 2. Start a stream of air entering the boiling flask by adjusting the vacuum source. Adjust the vacuum so that approximately 1.5 liters per minute enters the boiling flask through the air inlet tube. The bubble rate may not remain constant while heat is being applied to the flask. It may be necessary to readjust the air rate occasionally.
- 3. If samples contain NO3 and/or NO2 add 2 g of sulfamic acid solution after the air rate is set through the air inlet tube. Mix for three minutes prior to addition of H_2SO_4 .
- 4. Slowly add 50 ml 18N sulfuric acid through the air inlet tube. Rinse the tube with distilled water and allow the airflow to mix the flask contents for three minutes. Pour the tube with distilled water and allow the airflow to mix the flask contents for three minutes. Pour 20 ml of magnesium chloride into the air inlet and wash down with a stream of water.
- 5. Heat the solution to boiling. Reflux for one hour. Turn off heat and continue the airflow for at least 15 minutes. After cooling the boiling flask, disconnect absorber and close off the vacuum source.

Analysis can be stopped at this point, coloring can be done next day (time not factor, solution is very stable at this point).

Coloring Procedure

Withdraw 25 ml or less of the solution from the flask and transfer to 50~ml volumetric flask. If less than 25 ml is taken, dilute to 25~ml with 0.25~N sodium hydroxide solution. Add 15.0~ml of sodium phosphate solution and mix.

1. Pyridine - Barbituric Acid Method: Add 2 ml of chloramine T and mix. After one to two minutes, add 5 ml of pyridine-barbituric acid solution and mix. Dilute to mark with distilled water and mix again. Allow eight minutes for color development then read absorbance at 578 nm in a 1 cm cell within 15 minutes.

QA/QC

Prepare a series of standards by pipeting suitable volumes of standard solution into 250 ml volumetric flasks. To each standard add 50 ml of 1.25N sodium hydroxide and dilute to 250 ml with distilled water. Prepare as follows:

ml of Standard Solution (1.0 = 5 ug CN)	Concentrate mgCN per 250 ml
0	Blank
1.0	5
2.0	10
5.0	25
10.0	50
15.0	75
20.0	100

INSTRUMENT OPERATION

Apparatus

Reflux distillation apparatus such as shown in Figure 2. The boiling flask should be of 1 liter size with inlet tube and provision for condenser. The gas absorber may be a Fisher-Milligan scrubber. Spectrophotometer suitable for measurements at 578 nm or 620 nm with a 1.0 cm cell or larger.

Reflux distillation apparatus for sulfide removal. The sulfide scrubber may be a Wheaton Bubber #709682 with 29 42 joints, size 100 ml. The air inlet tube should not be fritted. The cyanide absorption vessel should be the same as the sulfide scrubber. The air inlet tube should be fritted. Flow meter, such as Lab Crest with stainless steel float (Fisher 11-164-50).

REAGENTS

- 1. Sodium hydroxide solution, 1.25N: Dissolve 50 g of NaOH in distilled water, and dilute to 1 liter with distilled water.
- Cadmium carbonate: powdered.
- 3. Ascorbic acid: crystals.
- 4. Dilute sodium hydroxide solution, 0.25N: Dilute 200 ml of sodium hydroxide solution to 1,000 ml with distilled water.
- 5. Sulfuric acid: concentrated.
- 6. Sodium dihydrogenphosphate, 1 M: Dissolve 138 g of $NaH_2PO_4H_2O$ in 1 liter of distilled water. Refrigerate this solution.
- 7. Stock cyanide solution: Dissolve 2.51 g of KCN and 2 g KOH in 1 liter of distilled water. Standardize with 0.0192 n $AgNO_3$. Dilute to appropriate concentration so that 1 ml = 1 mg CN.
- 8. Standard cyanide solution, intermediate: Dilute 50.0 ml of stock (1 ml = 1 mg CN) to 1000 ml with distilled water (1 ml = 50.0 ug).
- 9. Standard cyanide solution: Prepare fresh daily by diluting 100.0 ml of intermediate cyanide solution to 1,000 ml with distilled water and store in a glass stoppered bottle [1 ml = 5.0 ug CN(5.0 mg/l)].

- 10. Standard silver nitrate solution, 0.0192 N: Prepare by crushing approximately 5 g AgNo₃ crystals and dryig to constant weight at 40° C. Weigh out 3.2647 g of dried AgNO₃, dissolve in distilled water, and dilute to 1,000 ml (1 ml = 1 mg CN).
- 11. Chloramine T solution: Dissolve 1.0 g of white, water soluble Chloramine T in 100 ml of distilled water and refrigerate until ready to use. Prepare fresh weekly.
- 12. Color Reagent: Pryidine-Barbituric Acid Reagent: Place 15 g of barbituric acid in a 250 ml volumetric flask and add just enough distilled water to wash the sides of the flask and wet the barbituric acid. Add 75 ml of pyridine and mix. Add 15 ml of HCl, mix, and cool to room temperature. Dilute to 250 ml with distilled water and mix. This reagent is stable for approximately six months if stored in a cool, dark place.
- 13. Magnesium chloride solution: Weigh 510 g of $MgCl_2$ $6H_2O$ into a 1,000 ml flask, dissolve and dilute to 1 liter with distilled water.
- 14. Sulfamic acid.

ANALYSIS

See Procedure

INTERFERENCE

- 1. Inteferences are eliminated or reduced by using the distillation.
- 2. Sulfides adversely affect the colorimetric procedure. Samples that contain hydrogen sulfide, metal sulfides or other compounds that may produce hydrogen sulfide during the distillation should be distilled by the optional procedure.
- 3. High results may be obtained for samples that contain nitrate and/or nitrite. During the distillation nitrate and nitrite will form nitrous acid which will react with some organic compounds to form oximes. These compounds formed will decompose under test conditions to generate HCN. The interference of nitrate and nitrite is eliminated by pretreatment with sulfamic acid.

STANDARD PREPARATION

Standard Curve for Samples Without Sulfide

1. Prepare a series of standards by pipeting suitable volumes of standard solution into 250 ml volumetric flasks. To each standard add 50 ml of 1.25 N sodium hydroxide and dilute to 250 ml with distilled water. Prepare as follows:

ml of Working Standard Solution (1 ml = 10 ug CN)	Concentrate ug e per 250 ml
0	Blank
1.0	10
2.0	20
5.0	50
10.0	100
15.0	150
20.0	200

CN

- 2. It is not imperative that all standards be distilled in the same manner as the samples. It is recommended that at least two standards (a high and low) be distilled and compared to similar values on the curve to insure that the distillation technique is reliable. If distilled standards do not agree within $\pm 10\%$ of the undistilled standards the analyst should find the cause of the apparent error before proceeding.
- 3. Prepare a standard curve by plotting absorbance of standard vs. cyanide concentrations.
- 4. To check the efficiency of the sample distillation, add an increment of cyanide from either the intermediate standard or the working standard to 500 ml of sample to insure a level of 20 ug/1. Proceed with the analysis.

Standard Curve for Samples With Sulfide

- 1. It is imperative that all standards be distilled in the same manner as the samples. Standards distilled by this method will give a linear curve, but as the concentration increases, the recovery decreases. It is recommended that at least three standards be distilled.
- 2. Prepare a standard curve by plotting absorbance of standard vs. cyanide concentrations.

SAMPLE PREPARATION

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The sample should be collected in plastic or glass bottles of 1 liter or larger size. All bottles must be thoroughly cleansed and thoroughly rinsed to remove soluble material from containers.

Oxidizing agents such as chlorine decompose most of the cyanides. Test a drop of the sample with potassium iodide-starch test paper (KI-starch paper); a blue color indicates the need for treatment. Add ascorbic acid, a few crystals at a time, until a drop of sample produces no color on the indicator paper. Then add an additional 0.6 g of ascorbic acid for each liter of sample volume.

Samples must be preserved with 2 ml of 10 N sodium hydroxide per liter of sample $(pH \ge 12)$ at the time of collection. Samples should be analyzed as rapidly as possible after collection. If storage is required, the samples should be stored in a refrigerator or in an ice chest filled with water and ice to maintain temperature at 4° C.

- 1. Alternatively, if the sample contains more than 1 mg of CN transfer the distillate, or a suitable aliquot diluted to 250 ml, to a 500 ml Erlenmeyer flask. Add 10-12 drops of the benzalrhodanine indicator.
- 2. Titrate with standard silver nitrate to the first change in color from yellow to brownish-pink. Titrate a distilled water blank using the same amount of sodium hydroxide and indicator as in the sample.
- 3. The analyst should familiarize himself with the end point of the titratio and the amount of indicator to be used before actually titrating the samples. A 5 to 10 ml microburet may be conveniently used to obtain a more precise titration.

CALCULATION

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1. If the colorimetric procedure is used, calculate the cyanide, in ug/l, in the original sample as follows:

$$CN_{r} ug/1 = \frac{A \times 1,000}{B} \times \frac{25}{C}$$

where:

A = ug CN read from standard curve

B = ml of original sample for distillation

C = ml taken for colorimetric analysis

2. Using the titrimetric procedure, calculate concentration of CN as follows:

CN,
$$mg/l = \frac{(A - B)1,000}{ml \text{ original sample}} \times \frac{250}{ml \text{ of aliquot titrated}}$$

where:

A = volume of AgNO₃ for titration of sample

 $B = volume of AgNO_3$ for titration of blank

DETECTION LIMIT

5 ug/1

SAFETY

Use caution while refluxing samples and adding acid. Follow all safety regulations.

CYANIDE DATA FORM EPA METHOD 335.2

DATE/TIME DISTILLED EPA METHOD 335.2	PROJECT
NETHOD OF ANALYSIS	ANALYST

	25	1 1000	D: CN Ha/Z :	COLORMETRIC METHOD: CH		0 1 0	0001 1 (8-4) . 1/be		METHOD: C	TRIMETRIC	TIONS: TI	CALCULA	NOTES AND CALCULATIONS: TITRIMETRIC METHOD: CN
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STANDARD OPERATING PROCEDURE TOTAL AND DISSOLVED ORGANIC CARBON

APPLICATION

This method is applicable to drinking and surface waters, and sewage and industrial waste effluents.

PROCEDURE

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For Total Organic Carbon (TOC) acidified samples are analyzed as received. Dissolved Organic Carbon (DOC) samples are analyzed using the same procedure except the samples are filtered through a 0.45 micron filter prior to analysis.

An acidified persulfate reagent is continuously pumped from an external reservoir to the injection port and then into the bottom of UV reactor. The reactor is a constant volume design; the excess liquid is pumped to waste from a drain port.

The reactor liquid is continuously sparged and this sparge/carrier gas flows out on the top of the reactor to a non-dispersive infra-red detector (NDIR). When a sample is injected, it is carried into the reactor by the reagent flow. The oxidation of organics occurs rapidly, and the resultant carbon dioxide is sparged from the liquid and carried to the NDIR. The NDIR produces an electrical output (peak) which is integrated and sealed by the number processor and then displayed and printed. The concentration of the sample injected is displayed and printed directly in the concentration units for which the instrument has been calibrated.

The instrument is designed for three levels of carbon analysis. High level samples are run with the detector module set on 40 ul, and 40 ul samples are injected into the reaction module. Low level carbon samples are run with the detector module set on 1 ml, and 1 ml samples are injected into the reaction module. We do not generally use the mid-range carbon setting of 200 ul.

INSTRUMENT OPERATION

- 1. Fill the reactor with persulfate reagent by temporarily lifting the lamp and cap assembly up and pouring the reagent in. Fill to about 1 inch below the recycle port.
- 2. Add clean water to the "U" tube trap until the level is just at the bottom of the bulb section on the right.
- 3. Turn on oxygen gas tank; regulator reads 30 psi.
- 4. Turn on switches:
 - a. Main power on EM-2 microprocessor
 - b. Power, pump and lamp on UV-persulfate reaction module

- Let instrument warm up for at least one-half hour to ensure complete sparging of the persulfate solution and stabilization of all electronics and the UV lamp.
- Calibrate the instrument, if necessary, following the instructions on pages 3-6 to 3-9 in the instrument manual. The instrument, once calibrated, retains its calibration (even when shut-off) until it is erased manually. Check the calibration by running a standard after the instrument is warmed
- 7. The samples and standards are purged for a few minutes with oxygen to drive off any inorganic carbon prior to analysis.
- 8. Standards, blanks and samples are injected into the injection port with 40 ul or 1 ml aliquots using glass syringes. Rinse the syringe 10-12 times with water and 10-12 times with standard or sample to be analyzed before filling the syringe to inject into the instrument. Repeat for each sample.

Instrument Maintenance

- Reaction vessel is cleaned with chromic acid cleaning solution once a week.
- 2. The tin scrubber which traps any chlorine generated is changed every 3-4 weeks.
- 3. Change pump tubing as necessary, usually every 2-3 weeks.

Instrument Troubleshooting

The instrument will print error messages when not operating properly. Table I, page 3-10, in the instrument manual.

REAGENTS

Potassium Persulfate Solution: Dissolve 20 grams of reagent grade potassium persulfate and 1 ml of reagent grade concentrated nitric acid in 1 liter of the purest water available.

INTERFERENCE

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High Chloride: See Appendix B of instrument manual.

STANDARD PREPARATION

- 2,000 ppm Carbon Standard: Weigh 425 mg of potassium hydrogen phthalate (C8H5O4K), KHP, dried to a constant weight. Transfer the KHP quantitatively with the purest water available to a 100 ml flask, dissolve, add 0.1 ml of concentrated nitric acid (HNO3) and dilute to volume with water. Store this solution in dark glass under refrigeration. Replace monthly.
- 10 ppm Carbon Standard: 1.00 ml of the 2000 ppm standard is diluted to 200 ml with pure water in a volumetric flask.

SAMPLE PREPARATION

Sulfuric acid is used to preserve the samples to a pH of less than 2. If the samples are unpreserved, add acid prior to analysis. (DOC samples are generally received unpreserved.) Acidify DOC samples after filtering through a 0.45 micron filter and prior to analysis.

QA/QC

A blank of the purest water available, a standard, and a duplicate are run per every ten samples analyzed.

CALIBRATION

When calibrated properly (as described previously), the instrument display and printer will read directly in concentration units.

DETECTION LIMIT

0.1 mg/1

SAFETY

Safety glasses, gloves and lab coat are worn in the laboratory. Special care is taken when working with syringes to avoid injury.

DATA SHEET

Sample copy of Data Sheet attached.

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TOC/DOC (Instrumental)

NAME

S PROJECT NUMBER: DATE WORK IN: Page_ ្ទ

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				,	-					
(mg/L)	(mg/L)	000	700	800	700	DOC	700	SET	SAMPLE NO.	LAB NO.
DOC (119/9)	TOC (119/9)	DILUTION FACTOR	DILUTIOI (C) NECTED	VOL. 13	(A) (C) INSTR. READING VOL. INJECTED	INSTR.	(B)		
		,			1					

(A) INSTRUMENT READING

(B) INSTRUMENT VOLUME SETTING

(C) VOLUME INJECTED
(D) DILUTION FACTOR
(Sample Volume / Total Volume)

TOC = AR B

anion exchange column. Plutonium is eluted with sulfurous acid, the eluate evaporated to dryness and dissolved for electrodeposition on stainless steel discs. Quantitation and chemical recovery are determined from alpha spectroscopy counting.

1.2 Soil

1.2.1 Gamma Spectroscopy

One-hundred grams of dried and pulverized sample is placed in a Marinelli beaker and counted for eight hours, on a Ge(Li) Detector, which is coupled to a 2048 computer based, multi-channel analyzer (Northern Scientific). The resulting spectrum is fed into a computer and specific nuclides, if present, are identified and quantized in terms of energy and net count rate with the aid of the computer.

1.2.2 Gross Alpha and Gross Beta

A suitable aliquot of prepared sample is muffled, dissolved in acid, nitrated, evaporated and transferred to a tared two-inch stainless steel planchet. The planchet is counted for Gross Alpha and Gross Beta activity as in Method 3.1.1.

1.2.3 Radium (total)

Preparation of the soil for analysis requires that it first be dried, muffled to remove carbon, and pulverized. Aliquots for sample and sample spike with added radium-226 tracer are leached in dilute nitric acid, filtered, and the leachate evaporated to dryness. The residue is dissolved in nitric acid, insoluble residue filtered off and sulfuric acid added as an anion source for the precipitate. The samples are heated and barium carrier added, precipitating the barium/radium as a sulfate. Samples and corresponding spikes are alpha counted. Chemical recovery is determined from radium-226 tracer spike recovery.

1.2.4 Strontium-89/90

Strontium-90

A ten-gram aliquot is spiked with Strontium-85 tracer and dissolved in HNO3 - HF mixture. After dissolution of the soil, the solution is evaporated to dryness several times with HCl. Oxalic acid is added and the solution adjusted to a pH of 5.5 - 6.0 with NH4OH. The solution is allowed to stand for several hours and is then stirred and filtered. The filtrate is discarded.

The precipitate and paper are transferred to a dish and dried overnight at 110°C. The oxalate precipitate is ignited in a muffle furnace at 400-500°C for two hours. The temperature is raised slowly to about 700°C and heating continued for two hours. The precipitate is cooled and transferred to an appropriate size beaker and dissolved in 1:1 HNO3. About six drops of H2O2 (30%) is added to facilitate dissolution, and then the solution is gently heated to boiling. The solution is cooled to room temperature.

The solution is transferred to a suitable size beaker and evaporated to dryness.

The residue is dissolved in 25 ml of 0.08 \underline{N} HCl and transferred to a 125 ml separatory funnel using two 5 ml rinses of 0.08 \underline{N} HCl.

After the 14-day ingrowth period is established, the Yttrium-90 is extracted with 5% di-2-ethylhexyl phosphoric acid (D2EHPA) in toluene, back extracted into an aqueous phase, precipitated as the oxalate and counted in a low background internal gas flow proportional counter (Beckman Low Beta II) to determine the Strontium-90 content of the sample. The Strontium-85 tracer is counted on the Gamma Spectrometer to determine the percent recovery of the method.

Strontium-89

A ten-gram aliquot of sample containing standardized stable Strontium carrier is dried at 110°C for twenty-four hours, ashed in a muffle furnace with the addition of concentrated fuming nitric acid. The Strontium is precipitated with concentrated fuming nitric acid, redisssolved is water, made basic with dilute ammonium hydroxide and precipitated as the oxalate. The dried oxalate precipitate is counted in a low-background proportional counter, which has 60% Strontium, Yttrium-90 efficiency. The Strontium-89 activity is determined by subtracting the previously measured Strontium-90 activity and its corresponding Yttrium-90 ingrowth from the measured Gross Strontium activity.

1.2.5 Isotopic Uranium

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CEP uses the following analytical method for analyzing Uranium-234, 235, 238 in soil: A ten-gram aliquot is spiked with Uranium-232 tracer. Total dissolution of the soil is performed using a hydrofluoric-nitric acid mixture, nitrated and evaporated to dryness. The residue is dissolved in concentrated nitric acid and again taken to dryness and redissolved in dilute acid. The sample is purified with an ion exchange resin column. The Uranium is electroplated and the discs counted on a solid state alpha spectrometer and the chemical recovery is determined from the Uranium-232 tracer peak.

1.2.6 Uranium, total

The soil sample is dried, muffled to remove carbon and pulverized. An aliquot is taken, leached in nitric acid, filtered, and brought to a known volume with deionized water. Analysis is then performed according to Method 1.1.8.

1.2.7 Cesium-137

See method 1.2.1, Gamma Spectrometry in Soil

1.2.8 Isotopic Plutonium

The soil sample is totally dissolved using a 40% solution of HF and Pu-242 tracer is added before dissolution. The sample is fumed with HF and converted to sulfate and then brought up with HNO3. The Plutonium is separated using an ion exchange resin. The Plutonium is eluted off the column and electroplated on a stainless steel disc. The disc is counted on a solid state alpha spectrometer and chemical recovery is determined from the tracer peak.

1.3 Vegetation

1.3.1 Gamma Spectroscopy

The wet sample is placed in a Marinelli beaker and counted with a multichannel analyzer equipped with an intrinsic detector which is coupled to a 4096 channel, computer-based, multichannel analyzer (Northern Scientific TN4500). The resulting spectrum is analyzed by computer, and specific nuclides, if present, identified and quantified on a dry weight basis.

1.3.2 Gross Alpha and Gross Beta

A suitable aliquot of the sample is dried at 110°C for twenty-four hour, ashed in a muffle furnace, dissolved in dilute acid and transferred to a tared planchet. The Alpha and Beta radioactivity are determined using a low-background gas flow, proportional counter (Beckman Wide Beta II). The activity is corrected for counter efficiency and self absorption.

1.3.3 Strontium-89/90

The sample is prepared according to method 1.3.2 above and then analyzed according to method 1.2.4 Strontium-89 and 90 in Soil.

STANDARD OPERATING PROCEDURE BULK CHEMISTRY

APPLICATION

This method is applicable for soils and sediments. This method is suitable for extraction of metal complexes. The assumption is made that the oxide form is preferred by most metals in soil.

PROCEDURE

The nitric acid digestion is used for all bulk metals with the exception of silica, aluminum, calcium and iron. Calcium is extracted by DI because of its high solubility rate. Silica, aluminum and iron are extracted by the following procedure.

Transfer 10 ml of NaOH solution measured with a plastic graduated cylinder to each of two nickle crucibles, and evaporate the solution to dryness on a hot plate. (A small amount of spattering can be ignored.) Except for addition of no soil, carry one of the crucibles through the entire procedure described below to obtain the reference blank solution. To the other crucible, add a sample of about 0.05 g of 100-mesh soil that has been weighed to the nearest 0.1 mg. Cover crucible, and heat to dull redness for about 5 minutes. Grasp the crucible with nickel or platinum-tipped tongs, and rotate it so that the melt is spread over the sides of the lower half of the crucible. Allow the melt to cool, add approximately 50 ml of water, cover the crucible, and let it stand overnight. Transfer the contents of the crucible to a 600 ml beaker containing about 400 ml of water and 20 ml of 6N HCl. (Do not allow the nickel crucible to come in contact with the acid solution.) Scrub the crucible well with a rubber policeman, and wash any remaining residue or solution into the beaker. Transfer the solution to a 1-liter volumetric flask, add distilled water to make 1-liter, and mix the contents well. (This is referred to as the sample solution.)

INSTRUMENT OPERATION

See ICP Methods. Silica was determined spectrophotometrically as follows.

Color Development

Withdraw 10 ml of the sample solution with a pipette, and transfer the aliquot to a 100-ml volumetric flask. Treat a 10 ml aliquot of the reference blank solution in the same manner as the sample solution. Add 1 ml of the ammonium molybdate reagent solution, swirling the contents of the flask during addition. Mix the solutions wells, and allow the flask to stand for 10 minutes. Now add 4 ml of the tartaric acid solution while swirling contents of the flask, and mix the solution well. Add 1 ml of reducing solution while swirling the contents of the flask, add distilled water to make 100 ml, mix the contents well, and allow the flask to stand at least 30 minutes. Determine the percent transmission at 650 mu, setting the reference blank solution at 100. Calculate the concentration of silicon from the standard curve.

Standard Curve

Pipette 0, 1, 2, 3, 4, 5, 6, 7 and 8 ml of the standard silicon solution into 100 ml volumetric flasks. Add sufficient reference blank solution to each flask so that the volume of silicon standard plus reference blank totals 10 ml. Develop the color as described above, starting with "add 1 ml of the ammonium molybdate reagent solution...." Plot the percent transmission versus silicon concentration on semilogarithmic graph paper.

Results were calculated as follows:

mg Si/liter (from standard x liter/g sample x 10 (d.f.) = mg Si/g sample curve) (as per procedure)

See ICP Methods for Al and Fe determinations.

REAGENTS

Reagents are specific for each extraction procedure.

ANALYSIS

See ICAP Methods.

QA/QC

Normal QA/QC procedures to be followed.

DETECTION LIMIT

See ICAP Methods.

SAFETY

Use normal Laboratory safety procedures.

APPENDIX XI ANALYTICAL RESULTS "LABORATORY AND FIELD"

NOTE

Laboratory Rodinacias Data

from CED are givery poor & alix.



CONSIN (RADECLOGICAL LASCRATORY PESULTS)

THIS DATA IS IN 8-BIL ASCHI FORMAT. THE FORMAT BY THE DISK IS AS FOLLOWS:

BYTE

ITEM

FORTRAN FERMAT SCOE

RECORD #1 (ONCE FOR EACH LBC #)

1-4

LBC #

441

5-6

NUMBER OF INTERVALS 12

RECORD #2 (REPEATED FOR EACH INTERVAL)

1-5

INCHES

5A1

6-10

SAMPLE #

5A1

11-12

OF ELEMENTS IN SAMPLE 12

RECORD #3 (REPEATED N TIMES FOR EACH ELEMENT FOUND IN INTERVAL)

1-5

NUCLIDE

5A1

10-17

Pci/q

841

18-24

+/- ERROR

7**A**1

RECORD #4 (CONTAINS 2 80-BYTE RECORDS FOR EACH INTERVAL)

1-11

Pu238

1:A1

12-23

Pu239/240

12A1

24-33

Sr89

13A1

34-44

Sr 90

1141

```
LBCS 6
 0-5 76953 9
          1130.0
 83137
                    3.0
           2.72
 08134
                    0.3
           2070.0
 0060
                   4.0
 LA140
           7330.0 1590.0
 IR95
            29.7
                  1.7
 NB95
            6.05
                  1.46
 NA22
            39.6
                  1.0
 EU152
           65.4
                  2.0
 CD109
           388.0 11.0
          0.08 0.03 <0.04
 0.09 0.04
                               12.3 1.0
 <0.05
                  <0.05
           <0.05
                               11.3 1.5
 3-6 76954 9
 ZR95
           47.4 3.0
 CS134
           4.61 1.45
 NB95
            7.91 2.56
 CD109
           419.0
                 13.0
 NA22
           62.8
                  1.9
 EU152
           152.0 29.0
 LA140
          8050.0 2790.0
 CS137
         1130.0 4.0
           160.0 8.0

<0.05 <0.05

<0.05 <0.06
 0040
          7160.0
 <0.05
                              51.5 9.0
 <0.05
                               49.1 2.5
 6-9 7685510
 EU152
           472.0
                  3.0
 ZN65
           270.0
                  8.0
 08137
           560.0
                  3.0
 NA22
           81.3
                  1.9
 0403
         10200.0
                 68.0
 CD109
         412.0
                 12.0
                  0.5
 09134
            5.81
 LA140
         17400.0 3090.0
 ZR95
           63.1 3.8
           11.2 1.0
 NB95
          <0.05 <0.06 1426.0 17.0
 5.74 0.48
-_7-1276956 P
 G9109
          639.0
                 18.0
 ZR95
           104 0
                  5.0
 NAZ2
           117.0
                  2.0
09137
           366.0
                  2.0
08134
           7.42
                 0.8
0360
         27300.0 12.0
NB95
         14.0 1.0
LA:40
        15300.0 3370.0
E0152
        10:0.: 5.0
0.35 0.12 0.04 0.13 00.06 12.5 4.6
 10-1575957 9
13109 134,0
                 1913
         124.0
19<sup>4</sup>/1
 EU152
                 3.0
 - <u>- - -</u>
       749.70
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7050.0 2660.0
LA140
ZR75
NA22
            15.9
                    2.3
            20.4
                    1.0
98134
             3.48
                   0.4
NB95
            7.02 0.8
1.22 0.1
            7.09 0.3 <0.06
                                   1.0 0.4
1.07 0.1
            7.05 0.27 (0.06
                                   1.4 0.6
15-187695810
NA22
            14.4
                   1.0
09134
            3.47
                    0.4
NB95
            6.79
                    0.8
           21.9
ZR95
                    1.0
CD109
           82.9
                    6.7
8857
             2.41
                    0.93
EU152
           114.0
                    2.0
CS137
          108.0
                   2.0
0060
         3870.0
                   4.)
ZN45
           79.2
                    5.0
3.52 0.13 29.79 3.0
                       12.3 0.6 2.3 1.0
2.56 0.12
          22.69 2.3
                      12.3 0.8 2.9 1.4
```

14421. EDITZ. DATA (LAB1)

E-AREARDIL & CHEMICAL BASIN REAS RESULTS METALS, PETAGLESM, MYDROSDAPSONS AND BIL & GREASE)

THIS DATA IS IN SHBIT ASCIL FORMAT. THE FORMAT ON THE DISK IS AS FOLLOWS:

BYTE ITEM

FORTRAN FORMAT CODE

RECORD #1 (ONCE FOR EACH (BC 4)

1-4 LBC #

461

NUMBER OF INTERVALS

RECORD #2 (REPEATED 3% FOR EACH INTERVAL) DOMINING I SO-BYTE RECORDS EACH

1-5	INCHES	531
á- 10	SAMPLE #	5A1 - Envirodyne Lab ID SA1
11-14	,Sb	GAI Some Late ?
17-21	As	SAI SAI
22-25	Be	441
26-29	Cd	44:
30-35	©r	á f. l
35-40	Pa	541
41-45	Нg	541
46-51	53 - 53 - 19 4	£ &1
52-5a	Se	5 4 :
57-61	Ag	SAI
62-67	<u>. </u>	\$A1
5 8-73	Z m	8A1
74-90	*8C	761
1-5	cas	5A1
3-10	CN	EA:
11-15	PETROL HYDROCARBONS	541
15-20	GREASE & DIL	541

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LBC5 4
 0 - 3 2
 0-3
 3-6 76950
          34.3 49800
 3-6 76960
 3-6
 6-9 7695145.92 8.5 <2.0 9.7 1782. 0421. 040.2 90.9 <0.490.62 175.0 1155.0 100000
 6-9 76961
 6-9
 9-147695235.99 7.1 (2.0 7.78039.0202.0 0.85 373.0 0.680.37 177.0 334.0 32000
1090000.25
 9-1476962
 9-14
LBC419
 0-3 76953
 0-3 76963
 0-3
 3-5 76954
 3-6 76964
 3-6
 5-9 76955
         <4.8 48000
 5-9 76965
 9-1276956 -- -
          <4.8 5090
 9-1276966
9-12
12-1576957 3.5 4.7 (2.0 4.42365.0 66.3(0.2 115.0 0.640.056 b).T 41.5
1050040.2544.5 1330
11-1576967 4.04 5.2 K2.0 4.72489.0 67.5k0.1 126.0 0.690.078 60.1 45.1
1050040,2544,8
12-15
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	15-187 6958 10200(0.25			2011.0	54.1(0.2	77.5 0.62	e State		
				19 8 8.0	38.4 0 74	98.2 0.52	0.04 -7 3	γ. 	
	1000000.25	<4.8	,210		2072 017	, , , , , , , , , , , , , , , , , , , ,	2. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.		
	15-18	**					•	5	
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1							2	-
•	18-2176110	1.4792.72	2 <2.0<2.0	474.0	36.8<0.2	9 .200.5	1689 L 12. 3		: <u>=</u> <u>-</u>
	3400<0.25	(4.42 270)					v a s	
	18-2175123			463.0	33.2 0.2	8.0<0.5		1.	1012
٠		(4.42 125				0. 0.0.0.0		4 1 5	2
	18-21	0.8502.76	<2.0<2.0.	462.0	24.1<0.2	5.800.5	5. 97 3		
	500 0 702	CA AT							* •
1	21-2476111	1.0092.30	<2.0<2.0	117.0	31.3(0.2	< 2.0(0.5	0.079(<u>2.</u>)		5.4
	< 600<0.25<	4.42 188			•				
	21-2475124	1.0562.29	<2.0<2.0	110.0	28,3<0.2	< 2.0<0.5	0.085 < 2.0 :		
	500(0,250	4.42	•	•	•		:	• • •	- ·
	21-24	0.88 2.23	,<2.0<2.0	108.0	27.440.2	< 2.0<0.5	0.071	1 - 1 1	ء ۽ ۽
	< 400<0.25<	4.42		•			the second		-
	24-2776112	2.7491.35	<2.0<2.0	320.0	33.2<0.2	14.5(0.5	0.133 7.29	9.8	1276
	1200<0,25<	(4,42 200		•		•,			
	24-2776125			315.0	29.3<0.2	16.2<0.5	0.128	4.3	1142
	29 00<0.25<					•	*		
	24-27		<2.0<2.0	311.0	57.5 <q.2< td=""><td>18.8/0.5</td><td>0.127</td><td>10.7</td><td>1137</td></q.2<>	18. 8 /0.5	0.127	10.7	1137
	2300(0.250								
,	27-3078113	4.0220.70	3<2.0<2.0	259.0	35.2(0.2)	13.5<0.5	0.132	5.5	1114
	1500(Q.25)	•							
	27-3076126		⟨2.0⟨2.0	254.0	42.8(0.2	14.800.5	0.181	9 . É	:224
	2400(0. 25 (
	27-30 1600<0.25<		352.052.0	∠33.0	27.250.2	13.6<0.5	3.125	÷ = =	1251
	30-3378114		20 820 8	**** *	56 4 6 5		A 497/ 5 4		
	< 600/0.25<			23.0	20.1\0.2	4.5(0.5	0.03TK 2.0	1.1	7.1.3
	30+3376127			77 7	76 275 7	E 3/3 E :	·	i A	
	< 400(0.25k		12.012.0	نورن	20.0/0.2	G# 444 J# G1 3	0.031 v	3 4 6	Ĭ.7
	30-33		72 A72 A	राग छ	19 1/6 5	4.7(0.5	n wee)	-::
	<pre>400<0,25</pre>		12101210	9217	* 1 * * / / / * =	4837080	9.29 22	- १ ४	
	33-3676115		(2.0(2.0	30.3	20.740.7	4 4.0 5	0.025 3.19k	1 .74	1030
	< 600<0.250	4.42 84			2017 1012	910,010	04V26 041:5	* * *	. 966
				28.2	20.000.2	£.5<0.5 (0.034 (1.4	2 ° 5
	< 400<0.2 5 <	4.42						• • •	
	33 -36	0.4091.78	(2.0(2.0	27.3	13.7<0.2	5,80,5	0.035	1 2	
	500(0 .25 (4.42						•	
	36-3976116	0.5231.23	<2.0<2.0	15.1	15.640.2	< 2.000.5	0.031/1 E.O 1	1.0	:
	< 500<0.2 5 <	4.42 154							
	36-3976129	0.6361,22	<2.0<2,0	14.1	19.900.1	3.4√Q.5 :).JIA/ 2.0	1.0	Īta
	<pre>< 400<0.25</pre>	4.8						·	
	კ ე ლეზ - ოკი ო ————	0.7541.3	<2.0<2.0	13.7	19.7.0.2	2.000.E	0.021	4:3	± ∄a
	<pre>410:3.25</pre>	# : 급			and the second	.			
							9.041< 2.0 ×		
) 		
	-730(0,25)	andakinda. Ala:	.N.≰ + V 5 ⊈ + V	ā.:	_1,30,0,1	ေကြးေရးသည္သည်။	. > 12.7	. د سد	-
	THEOREM : A STATE OF THE STATE	प्राथी प्राप्तिक्रिक्ति चला			7: 5 · ·	. •),) T\$		_
	9 3 28.98.48. 2 23.1		james si meris	<i>3</i> € ₹	AT FAST SE	in Explosion 5			

48-5176118 0.6350.913<2.0<2.0 < 600<0.25<4.42 48-5176131	4.2 11.9(0.2	Land the state of	3 🖫
		1000 1100 1100 1100 1100 1100 1100 110	•
- 48-51 - 110, year and a final of the control of			.
54-5776119 0.5340.799<2.0<2.0 < 600<0.25<4.42 212 54-5776132	4,4 17,446.2	. 2.5.0.5 0.0210 Z.V + 1.V	471
54-57			
60-6376120 0.3170.554<2.0<2.0 <	4.0 12.340.2	₹ 2.0₹0.5,0.031₹ 2.0 ₹ 1.0	44 =
< 500<0.25<4.42 60-6376130	•		
60-63			
66-6976121 1.7200.709(2.0(2.0) (600(0.25(4.42 825 66-6976134	4.5 20.0<0.2	4.5<0.5 0.044< 2.0 < 1.0	o28
56-69			. 7
72-7576122 1.0580.985<2.0<2.0 < 500 <4.42 72-7576135	.5.9 24.1kg.2	3.9<0.5 0.024< 2.0 < 1.0	727

72-75

THUZI · EDIT 2 · DATH (FIELD)

THAREA DIE & CREMICAL BASIN FREEZ LAS STELLS

THIS BATA HE LIM BOBIT ASETE FIRMAT. HOTHER FIRMAT IN THE DEEK TRASSES TRASSES TO ASETE THE

EYTER STEWN FORMAL FORM

PECORS #1 (CNOS FOR EACH LEG #)

1-4 LSC # 44. .S-6 [NUMBER OF INTERVALS II

REDORD #2 (REPEATED FOR EACH INTERVAL)

1-10	To all office and the second	
1 - 1 0	INCHES	1041
11-18	Ca-60	ā∂1
19-20	€a-60 +/-	2 A 1
21-23	55-125	Jai
24-26	S5-125 +/-	JA:
27-30	0s-137	74:
34-36	Cs-137 +/- `	3A1
37-43	Eu-152	741
44-47	Eu-152 +/-	4A1
48-52	Eu-154	5 <u>8</u> 1
53 -5 8	Eu-154 +/-	3A:
54-59	Eu-155	-ê:
60-62	Eu-155 +/-	3A1
4I-4E	SROSS ALPHA	341
56-59	GROSS ALPHA +/-	4è1
70-75	38388 BETA	681
75-77	SA053 BETA +/-	241

MOISTURE

78-80

```
LBC-1 2
    9-15 13400.0 1 690.0 2 430.0 3 240.0 12 52 8 8500 1 6)
3-38 19.0 5 20.0 4 1 100 57 6 7
     24
0-3 2720.0 2 1180.0 3 100.0 8 7 22 760 2 72
3-6 2510.0 2 1040.0 2 104.0 20 266 27 37 10 2026 2 84
     6-9 5140.0 1 77 22 1430.0 2 250.0 4 195.0 17 130:13 17 :15 3660 1 82
    9-11 7160.0 1 1710.0 2 130.0 18 230.0 13:100.14 47 9 3830 1 30 11-17 4500.0 1 440.0 2 180.0 11 130.0 16 92 8 73 3 7920 1 53
                                                                  170 5 17
                                                            1 100
          120.0 2
                        60.0 3
    17-20
                                                                  140 5 17
                                                            1 100
                        63.0 3
            86.03
    20-23
                                                            1 100
                                                                    130 5 19
    23-26 160.0 2
                        66.0 3
                                                                    100 6 18
                         62.0 3
                                                            1 100
          140.0 2
    28-29
           47.0 4
                                                                    39 5 17
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                         56.0 3
    29-32
                                                                    36 6 17
                                                            1 100
            38.0 4
                          44.0 3
    32-35
                                                                    85 6 17
                                                            1 100
          34.0 4
                          42.0 4
    35-38
                                                                   49 7 15
                                                            1 100
                          32.0 4
           37.0.4
    38-41
                                                                   63 7 16
                                                            1 100
                          29.0 4
    41-44 29.0.5
                                                                    73 6 13
                                                            1 100
                        27.0 4
     44-47 . 35.0 4
                                                                    70 6 16
                                                            1 100
                          24.0 4
             32.0 4
     47-50
                                                                    72 6 15
                                                            1 100
                           18.0 5
          39.0 4
     50-53
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                          18.0 5
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     53-56
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     62-65
                                                                    70 6 16
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     65-68
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                                                            1 100
                           9.6 7
     68-71
            21.0 5
                                                                    61 5 9
                                                             1 100
                          12.0 7
            25.0 5
     71-74
LBC-314
                                                            7 20
                                                                    910 2 82
      3-6 960.0 2 700.0 2 68.0 8
6-9 3260.0 1 620.0 2 140.0 5
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                                                            8 21 1260 1 31
                                                                  2040 1 67
                                                          40 10
     9-11 8180.0 1105 14 450.0 3 420.0 5 310.0 2 182 6 40 10
                                                                   5280 1 59
                         210.0 4 250.0 8 170.0 3 140 5 11 18
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    11-15 7360.0 1
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     15-18 360.0 2
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                                                             1 100
            63.0 3
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            160.0 2
                          64.0 3
     21-24
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                                                             1 100
                           46.0 3
           120.0 2
     24-27
                                                                    120 5 17
                                                             1 100
                           33.0 4
           120.0 2
     27-30
                                                                    120 5 16
                                                             1 100
                           28.0 4
     30-33
           110.0 2
     33-36 100 0 2
36-39 700 3
                                                                   100 6 16
                                                            1 100
               2 21.0 5
20.0 5
                                                           . 1 100
                                                                    93 6 16
                                                                     87 5 15
     39-44 -43 3
                                                             1 100
                           18.0 5
LBC-412
       0-3 2 00 2 54 70 3160.0 1 230.0 4 210.0 8
                                                            33 11 2720 2 84
       3-6 7 1 99 24 1560.0 2 300.0 4 175.0 13 73 17 27 12 7290 1 30
6-9 21300.0 1135 18 780.0 3 1110.0 2 430.0 8 57 8 15100 1 76
S(BL) 9-15 9500.0 1 240.0 4 390.0 8 110.0 14 17 14 10400 1 50
                                                                    660 J 26
                                                            3 30
                                    11.0 11
                          77.0 3
CS(CL) 9-15 390.0 2
                          54.0 3
                                                                    260 4 20
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           88.0 3
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                                                             1 45
           43.0 4
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     18-21
                                                                    130 5 18
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                          . 26.0 4
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                                  5514 95400,011 | 570.0 4
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    14-17
                         220.7 4
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                                  |65.2 | 51.0 | 5 | C6/13
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    20-23
           450.0 2
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           410.0 I
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    25-29
           230.0 2
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    29-32
           340.0 2
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      3-5. 530.0 i
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                                                               3820 1 88
      7-12 204(0.0 1 59 33 290.0 6 880.0 2 270.0 15
                                                        . 12-15, 3300.0 ; 20 ]1 1:0.0 5 140.0 3 60.) 14 
- 18-18 3200.0 ; 100.0 5 120.0 4 27.0 28
                                                        10 19
                                                               3400 1 49
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                                                                3100 1 48
   13-21
          Z10.0 2
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                                  9.2 10
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    21-24
           77.303
                       - 50.0 D
                                                                 100 5 le
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    24-27
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           430.0 1
                         44.0 4
                                  14.0 8
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    27-59
           340.0 2
                          33.0 5
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                                                                ZEO 4 21
                                           10.0 12
    30-33
           58.0 3
                         15.0 16
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                                                                209 4 LE
    33-36
           76.0 3
                          7.1 9
                                  1.9 20
                                                           →7
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  36-39
          30.0 4
                          2.7 14
                                                         1 50
                                                                 72 8 14
    39-43
            12.0 7
                          3.1 10
                                                         1 100
                                                                 82 B 10
    42-45
            72.0 3
                          3.8 20
                                                                120 5 18
                                                         1 100
    45-48
            50.0 3
                                                                 72 = 10
                          3.2 16
                                                         1 100
    48-51
            4.98
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                                                                 35 8 .3
            5.010
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    54-57
                                                         1 100
                                                                 14 9 13
    57-60
            6.311
                                                         1 100
    30-43
            4.1 9
                                                                 27 € .1
                                                         1 100
                                                                 32 3 .4
            3,09
    53-65
                                                         1 100
          5.010
                                                         t_{\ell}(\ell,1-1)
                                                                 29 8 .9
   55-57
    69-71
                                                                  12 8 12
            4.111
                                                         1 100
    72-75
            4.112
                                                           (i, j)
165-714
     4-31 14000 3 72 40
                        915., 1
                                 Notes of
                                         55.0 .a
                                                               1373 1 85
                                                           ; :
      3-4 6020:0 . 74 00
                        11...
                                          --1, 50 --- 41 15 28
                                  2:0.0 4
                                                           2 A
     ±-10 (20%) 1.9 (11 ° 12
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                        d 1 au
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                                 1 <u>1 1</u> 1
    14-12 1510 0 1
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			وق) 4	42.0						_			
•					22.								2		170 1	
	7	· 1			8.8			1.0					4	50 53		-
	77-16	\$ J			. 4.								: -{	100 100	110 5 73 6	•
	30-3					10							•	100	75 G 30 7	4 ⁷
	33-36	5.4	10	•		30								100		16
	36-39	7.2	10			• •							•	45	52 7	
	39-42				4,4	12	·						ì	100	225 2	
LBC-8	313												-			`•
	0-3	2100.0	2 41	30	870.0	2	115.0	16	110.0	13	66	20	20	10	1126 1	34
	3-8	18500.0	1160	20	700.0	3	1140.0				240				3 4 00 1	- 3
	9-11	1360 0	" "		105.6	3	73.0	9	53.0	15	98	25	3	20		<u> </u>
		229.0			11.0	3	7.0	27	7.5	3			1	4.9	130 4	27
RED	11-14		2		68.0			20	16.0	30	40	30	1	40	200 4	20
	14-17				55.0								1	100	90 £	14
		32.0			25.0									100	120 á	
		40.0			28.0			55						100	160 5	
	17-20-	· · · · ·			39.0	_								100	60 B	
		10.0			17.0									100	100 6	
	23-26				6.1									100	40 7	
	26-29	- 7				10								100	40 8	
LBC-9	29-32	5.4	10		2.5	10							1	100	4010 ⁻	14
LDG-7	0-3	1840.0	2 50	25	790.0	· 	130.0	1.5	100 0	10	~~	* 15	-		040.0	2.7
	3-9	5650.0				-			240.0		47 90			15	940 2	
	6-12	1450.0		20	95.0				41.0		18		13	7 17	3000 1 2080 1	
	12-15	72.0			58.0		02.0	7.0	1.1		10	7		100		3€ 20
	15-18	73.0			43.0		1.5	33	1.1					100		4 7 1 7
	18-21	58.0			21.0	_			***	00				100		ie i
	21-24				18.0									100	50 7	18
	24-27	32.0			13.0									100	50 7	
	27-31	38.0	4		9.5									100		18
															=	



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TY421. EDET 2 DATA (LAB2)

HENIERE BASIN (LAS RESULTS, EPA TOXICITY, AND BULL CHEMISTRY)

THIS DATA IS IN BEBIT ASCII FORMAT. THE FORMAT ON THE DIEK IS AS FOLLOWS:

BYTE

FORTRAN FORMAT CODE

RECORD #1 (ONCE FOR EACH LBC #)

NUMBER OF INTERVALS 12

RECORD #2 (REPEATED 3% FOR EACH INTERVAL) SONTAINS 2 86-BYTE RECORDS EACH

1-5	INCHES	5A1
6-10	SAMPLE #	54:
11-16	As	AA1
17-22	Ba	áAí
23-28	Ed	6A1
29-34	€r	5 A1
35-40	Pb ·	AA1 EP# TOXIGITY
41-45	Hg	5A1 /
46-51	Sa	éA1
52-38	Ag	7A1
59-61	8102	3A1
62-64	A1203	3 A1 -
5 5-53	Fe203	4A1
69-7 3	MgO	541
74-73	CaO	5A1
1-3	Na2B	3A: BULK CHEMISTRY
4-7	K20	441
8-12	7 i 02	5A1
13-18	P205	åA:
19-25	MnO	761

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D-3 76949 ₩
0-3
3-4.74950
3-6 76960
3-6
                                                         . 247499123.763.0657.0
6-9 76951
5282.60 69.051.4 12460.0
6-9 76961
6-9
9-1476952
3532.15 48.039.3 4070.0
LBC619
0-3 76953
0-3 76963
0 - 3
3-6 76954
3-6 76964
3-6
 5-9 76955<0.002 0.09
 6-9 76965
                             0.013<0.004<0.20<0.002<0.45
 9-12
12-1576957(0.002 0.023(0.002 0.005(0.004(0.20(0.002(0.45 69526371.8167.0 79.0
1321.13 68.012.2
                    346.0
                                                            68929778.6172.0 91.0
12-1576967
1191.19 45.012.2
                    399.0
15-1876959<0.002 0.022<0.002 0.004<0.004<0.20<0.002<0.45 69727768.0129.0 64.0
1191.03 35.013.1
                    271.0
                                                            69926462.3163.0 69.0
15-1876968
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741.03 45.012.1
                    276.0
 15-18
 18-2176110k0.002k0.004k0.002(0.004(0.004(0.004)0.60k0),001 0.010884928185.1.71.1.1.1.1.1
  .331.02 8.3 3.73 45.0
 18-2176123
                                                         63735755.8146.30 J.5
 572.752 6.7 3.96
                     45.0
 19-21
                                                         57424854.Cipa.3 1.3
 640.884 J.B 0.73
                   49.0
 21-2475;10k0.002.0.004(0.002k0.004+0.004-0.50(0.002k0.000551601057.2-44-0.-2.5
 21-2475124
                                                        5653.050.5 70.9 2.0
 1431.24, 1.7 2.32
                     7.5
21-24
                                                         45128949.2 69.0 1.4
1261.20 2.8 2.27
                     9.0
24-277611260.002 0.01060.002 0.00460.004 0.2160.002 0.000772528825.3053.70 0.70
1151.324 1.7 2.35 65.0
24-2776125
                                                        74426725.8133.0% 1.5
1151.310 1.7 3.01
                     63.0
24-27
                                                        75726230.9274.0< 1.5
1651.75 16.0 2.91 59.0
27-3076113(0.002(0.004(0.002 0.004(0.004 0.24(0.002 0.000870229424.8139.0( 1.5
1201.61< 1.7 2.81 53.0
27-3076126
                                                        72125426.5174.0 1.8
1501.55 1.8 2.74
                  49.0
27-30
                                                        75723048.6101.00 1.5
1141.58( 1.7 2.53 52.9
30-337611440.002 0.00940.00240.00440.004 0.5640.002 0.000975522551.2 33.3 1.5
 911.58 7.0 1.83 . 11.0
30-3376127
                                                        67124050.0 70.00 1.5
1071.58 2.8 1.73
30-33
                                                        30922047.5 35.0 2.0
841.51 2.2 1.67
                    8.4
03-3676115(0.002 0.011(0.002(0.004 0.014 0.32(0.002 0.001083)21450.7 20.00 0.5
1191.56 2.3 0.979 . 7.6
35-3676128
                                                        77224449.9 28.00 1.5
871.51 6.8 0.889
                     7.0
33-35
                                                        74723248.9 14.0K 2.E
                    7.5
1101.54 2.3 0.847
36+3976116<0.002 0.016<0.002<0.004<0.004<0.20<0.002<0.00057662253B.3 40.3< 1.3
841.79( 1.7 0.399 5.2
36-3976129
                                                        81520130.b 48.00 1.3
1251.86 4.5 0.399
                     4.9
36-37
                                                      1073722319.2 60.00 0.5
771.93 7.0 0.353 5.4
39-4376117<0.002<0.004<0.002<0.004<0.004<0.20<0.032<0.000569522929.4 65.0 5.3
1882.46 3.0 0.422 4.3
39-4373130
                                                       83020428.9 85.0 3.4
2151.45 5.0 0.399
                     4.5
19-40
                                                       83422636.0 50.00 1.5
1901.811 1.7 0.399 4.4
48-517511900.002 0.03400.00200.00400.004 0.7100.00200.000580817528.9 40.00 i.u
20±1,99 1,7 U,274 5.4
48-517-171
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49-51

54-5 2212 54-52

0.014<0.004 0.73<0.002<0.000582315129.7 25.0 [.]

54-57

60-6376120<0.002 0.020<0.002 0.007<0.004 0.28<0.002 0.000892510618.0 g.s< 1.5 1281.56 1.8 0.188 6.5 60-6376133

60-63

66-6976121<0.002 0.023<0.002<0.004<0.004 0.30<0.002<0.000585013319.8 45.0< 1.5 1701.94 3.3 0.165 3.6 66-6976234

66-69

72-7576122<0-002 0.042<0.002<0.004<0.004 1.38<0.002<0.000580417823.7 45.04 1.5 1982.02 4.0 0.284 8.3 72-7576135

72-75