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PARALLEL CHANNEL FLOW EXCURSIONS (U)

by

Barry S. Johnston
Westinghouse Savannah River Company
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An invited paper proposed for presentation at
VPI in Blacksburg, VA on
January 22, 1990
(WSRC 1989-1990 Traveling Lecturer Program)

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PARALLEL CHANNEL FLOW EXCURSIONS (U)*

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Among the many known types of vapor-liquid flow instability is the flow excursion which may occur in heated parallel channels. Under certain conditions, the pressure drop requirement in a heated channel may increase with decreases in flow rate. This leads to an excursive reduction in flow. For channels heated by electricity or nuclear fission, this can result in overheating and damage to the channel. In the design of any parallel channel device, flow excursion limits should be established.

After a review of parallel channel behavior and analysis, a conservative criterion will be proposed for avoiding excursions. In support of this criterion, recent experimental work on boiling in downward flow will be described.

* The information contained in this article was developed during the course of work done under Contract No. DE-AC09-88SR18035 with the U. S. Department of Energy.

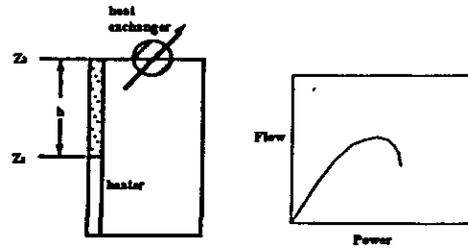
Parallel Channel Flow Excursions

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Barry S. Johnston
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 Savannah River Laboratory

SRL - Reactor Engineering Group

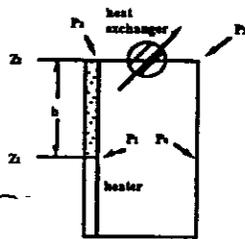
2-phase Natural Circulation



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2-phase Natural Circulation



$$P_1 - P_2 = \int_{Z_2}^{Z_1} \rho_m g dz$$

$$P_1 - P_2 = \int_{Z_2}^{Z_1} \rho_m g dz - \rho_m g h$$

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Simple Analysis

$$\int_{Z_2}^{Z_1} \left(\frac{dP}{dz} \right) dz = \rho_m g h - k_m \frac{G^2}{D^5}$$

$$\rho_m = \left(\frac{x}{\rho_g} + \frac{(1-x)}{\rho_l} \right)^{-1}$$

mixture density

$$x = \frac{\rho_l (z - z_0) D}{G A}$$

quality

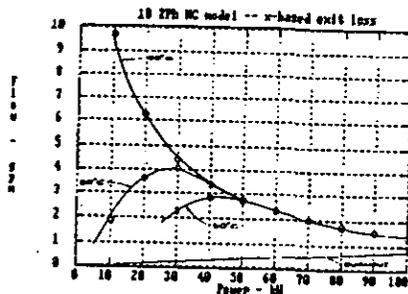
$$\frac{dP}{dz} = \left(\frac{dP}{dz} \right)_g + \left(\frac{dP}{dz} \right)_l + \left(\frac{dP}{dz} \right)_w$$

pressure gradient

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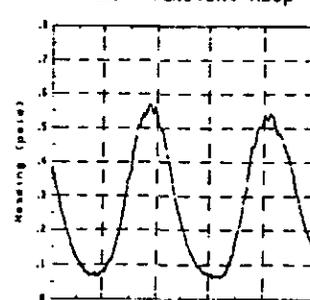
Model Predictions



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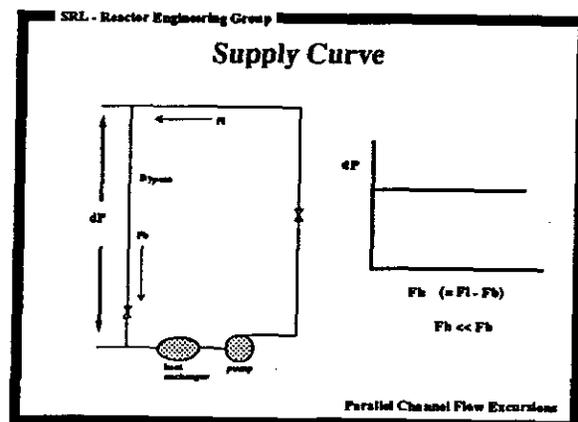
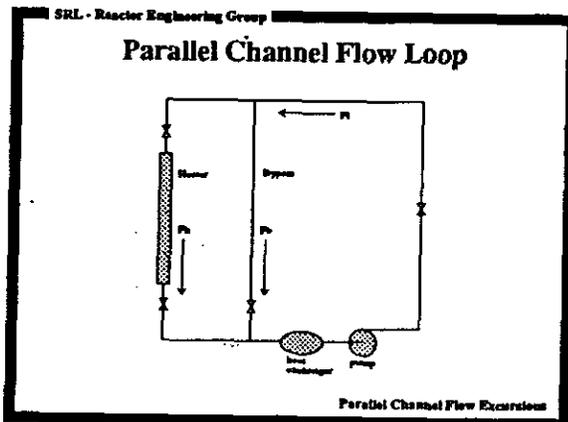
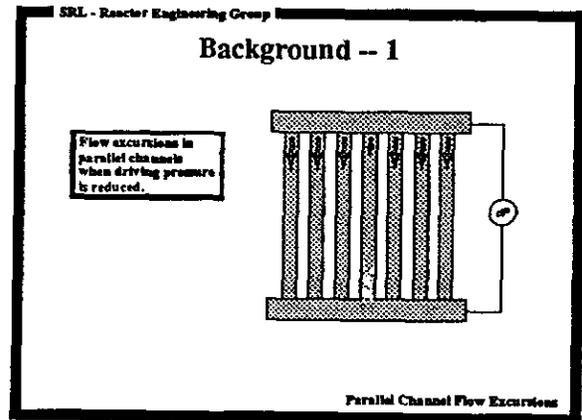
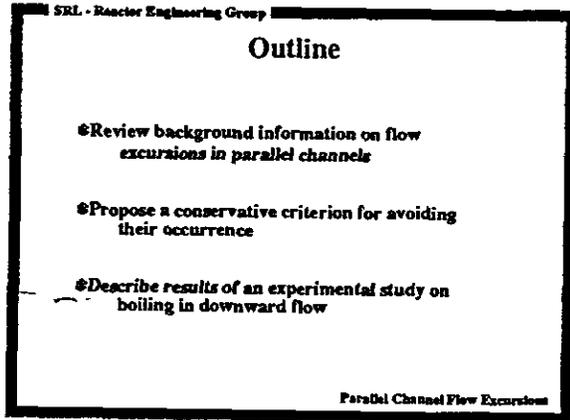
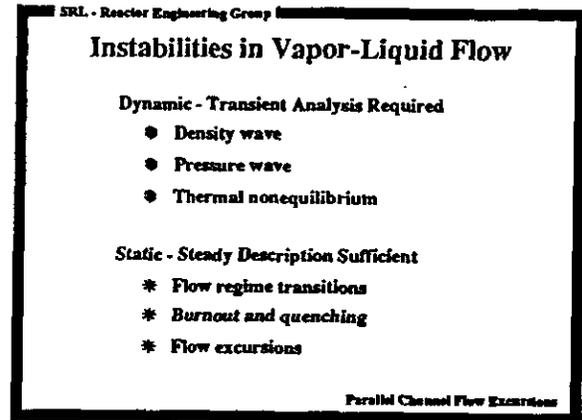
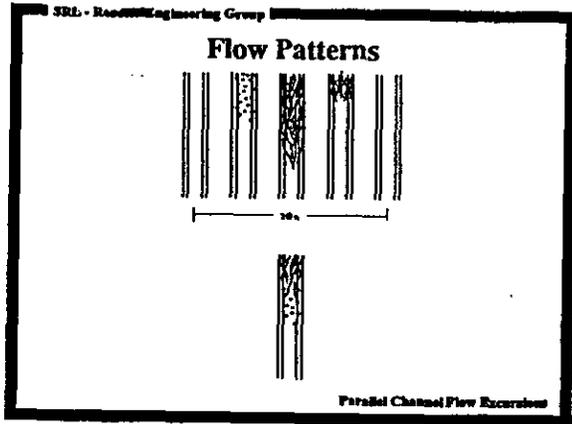
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What Happened...

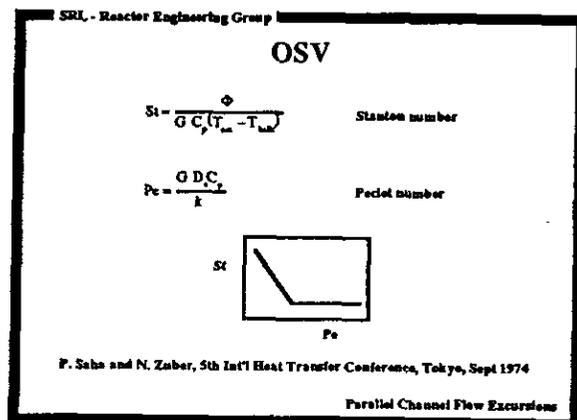
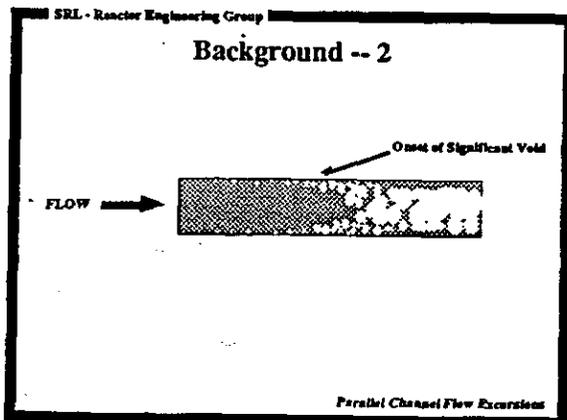
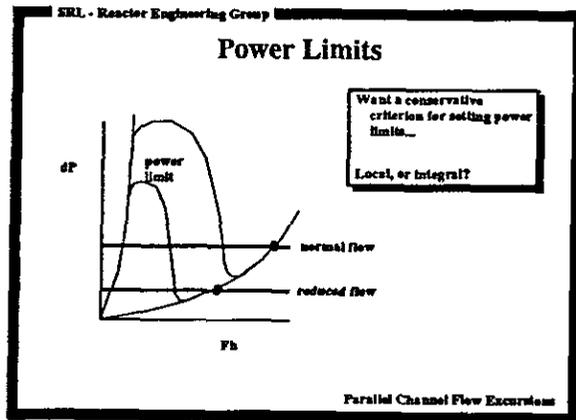
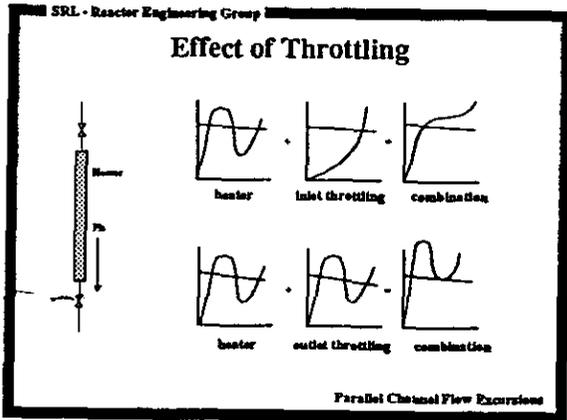
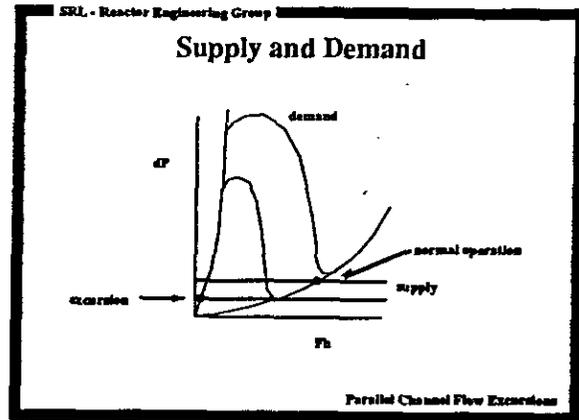
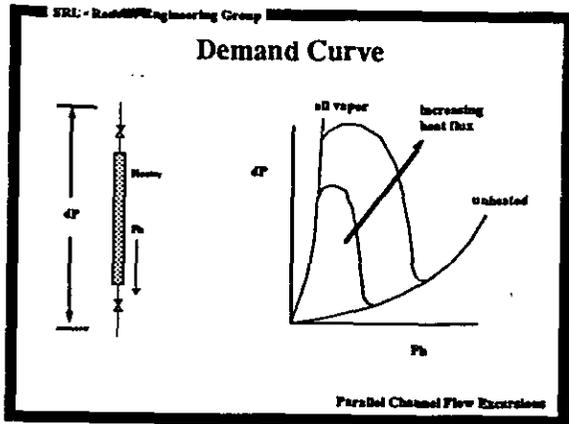


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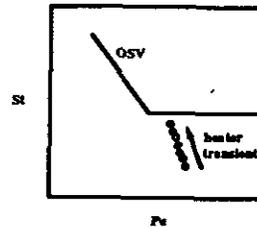
Proposal

- Set power limits to avoid flow excursions
- Use OSV as an indicator of flow excursions
- Get conditions for OSV from accepted correlations
- Calculate these conditions with thermo-hydraulic code

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OSV in Limits Calculation



But does OSV predict the minimum?

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Experimental Study

- Generate demand curves for steady flow in a heated annulus
- Cover a range of heat flux and inlet temperature
- Compare the demand curve minima to criteria for OSV

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Findings

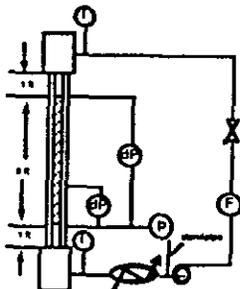
- For conditions studied, OSV is a good predictor of flow excursion
- but...
- OSV correlation needs to be modified for downward flow at low velocity

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Equipment

DI = 1.0 in, heated
 Do = 1.5 in
 L/D = 744
 no ribs
 TI = 25 - 90 C
 F = 1 - 15 gpm
 P = 20 psia
 q = 0 - 87 kBTU/hrft²



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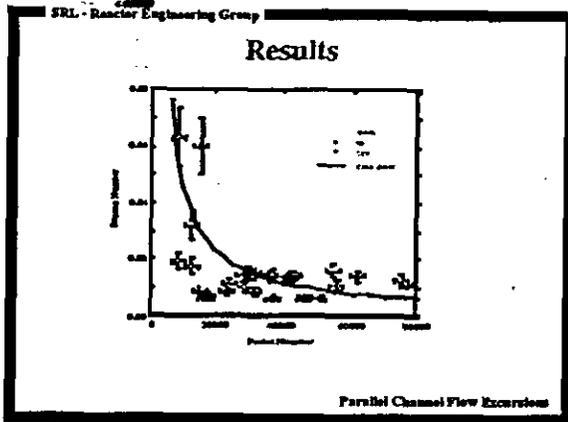
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Data



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- ### In Conclusion
- * Expect FE at minimum of demand curve.
 - * Use OSV as conservative predictor.
- however...
- Need a special OSV correlation for restricted geometry?
 - Is the steady analysis appropriate for rapid change in pressure?
- Parallel Channel Flow Excursions