

Keywords: Tank Farm, Tank Closure, Tank 6F

Retention: Permanent

Analysis of the Tank 6F Final Characterization Samples-2012 (U)

**L. N. Oji, D.P. Diprete, C. J. Coleman,
M. S. Hay and E. P. Shine**

January 2013

Savannah River National Laboratory
Savannah River Nuclear Solutions
Aiken, SC 29808

Prepared for the U.S. Department of Energy under
contract number DE-AC09-08SR22470.



DISCLAIMER

This work was prepared under an agreement with and funded by the U.S. Government. Neither the U.S. Government or its employees, nor any of its contractors, subcontractors or their employees, makes any express or implied:

- 1. warranty or assumes any legal liability for the accuracy, completeness, or for the use or results of such use of any information, product, or process disclosed; or**
- 2. representation that such use or results of such use would not infringe privately owned rights; or**
- 3. endorsement or recommendation of any specifically identified commercial product, process, or service.**

Any views and opinions of authors expressed in this work do not necessarily state or reflect those of the United States Government, or its contractors, or subcontractors.

Printed in the United States of America

**Prepared for
U.S. Department of Energy**

REVIEWS AND APPROVALS

AUTHORS:

L. N. Oji, Author, Advanced Characterization & Processing Date

D. P. Diprete, Co-author, Analytical Development Date

C. J. Coleman, Co-author, Analytical Development Date

M.S. Hay, Co-author, Advanced Characterization & Processing Date

E. P. Shine, Co-author, Applied Comp. Engineering & Statistics Date

TECHNICAL REVIEW:

S. H. Reboul, Process Technology Programs Date

T. B. Edwards, Applied Comp. Engineering & Statistics Date

APPROVALS:

F. M. Pennebaker, Manager, Advanced Characterization & Processing Date

P. L. Lee, Manager, Applied Comp. Engineering & Statistics Date

S. L. Marra, Manager,
Environmental & Chemical Process Technology Research Programs Date

M. J. Mahoney, Closure & Waste Disposal Authority Date

A. J. Tisler, Manager, SRR Engineering Date

LIST OF REVISIONS		
Revision Number	Summary of Changes	Date
2.0	Notes on the application of the Dixon statistical test for outliers were added to the bottom of Tables 21 and 22.	1/31/13
2.0	A percent standard deviation column was added to Tables 19, 24, and 27.	1/31/13
1.0	Errors on percent relative deviation for elements B, Ba, Ca, Cr, and Si in the reference glass (last column in Appendix A-4, page 35) were corrected. Corrections were also made to section 3.2 of the report where those values were cited.	9/27/12
1.0	Error on percent relative deviation for element Cr in the reference Tank 8 simulant (last column in Appendix A-3, page 34) was corrected. Correction was also made to section 3.2 of the report where that value was cited. Typographical error for Na values in the Tank 8 simulant was corrected in Appendix A-3 and transcription error for Ti in Appendix A-4 was corrected.	9/27/12
1.0	In the reference ARG samples, elements (Ba, Cr, Cu, Sr and Zn) with concentrations less than 0.1 Wt% were not included in Appendix A-4 because their concentrations could be influenced by trace reagent impurities. Similarly, for the Tank 8 simulants, K was taken out of Appendix A-3.	9/27/12

EXECUTIVE SUMMARY

Characterization summary

The Savannah River National Laboratory (SRNL) was requested by Savannah River Remediation (SRR) to provide sample preparation and analysis of the Tank 6F final characterization samples to determine the residual tank inventory prior to grouting. Fourteen residual Tank 6F solid samples from three areas on the floor of the tank were collected and delivered to SRNL between May and August 2011.

These Tank 6F samples were homogenized and combined into three composite samples based on a proportion compositing scheme and the resulting composite samples were analyzed for radiological, chemical and elemental components. Additional measurements performed on the Tank 6F composite samples include bulk density and water leaching of the solids to account for water soluble components. The composite Tank 6F samples were analyzed and the data reported in triplicate.

Sufficient quality assurance standards and blanks were utilized to demonstrate adequate characterization of the Tank 6F samples. The main evaluation criteria were target detection limits specified in the technical task request document. While many of the target detection limits were met for the species characterized for Tank 6F some were not met. In a few cases, the relatively high levels of radioactive species of the same element or a chemically similar element precluded the ability to measure some isotopes to low levels. The isotopes whose detection limits were not met in all cases included Sn-126, Sb-126, Sb-126m, Eu-152, Cm-243 and Cf-249. SRNL, in conjunction with the customer, reviewed all of these cases and determined that the impacts of not meeting the target detection limits were acceptable.

Statistical review summary

Based on the analyses of variance (ANOVA) for the inorganic constituents of Tank 6F, all the inorganic constituents displayed heterogeneity. The inorganic results demonstrated consistent differences across the composite samples: lowest concentrations for Composite Sample 1, intermediate-valued concentrations for Composite Sample 2, and highest concentrations for Composite Sample 3. The Hg and Mo results suggest possible measurement outliers. However, the magnitudes of the differences between the Hg 95% upper confidence limit (UCL95) results with and without the outlier and the magnitudes of the differences between the Mo UCL95 results with and without the outlier do not appear to have practical significance. It is recommended to remove the potential measurement outliers. Doing so is conservative in the sense of producing a higher UCL95 for Hg and Mo than if the potential outliers were included in the calculations.

In contrast to the inorganic results, most of the radionuclides did not demonstrate heterogeneity among the three Tank 6F composite sample characterization results.

TABLE OF CONTENTS

1.0	INTRODUCTION	9
2.0	SAMPLING AND SAMPLE PREPARATION FOR CHARACTERIZATION. 12	
2.1	Blank Evaluations and Reference Materials	16
2.2	Leaching Characterization of Tank 6F Solids	16
3.0	RESULTS	16
3.1	Data Quality and Presentations for Routine Radionuclide Constituents	18
3.2	Data Quality and Presentations for Elemental Constituents	19
3.3	Data Quality and Presentations for Non-Routine Radionuclide Analytes.....	20
3.4	Statistical Analyses	31
4.0	CONCLUSIONS.....	31
5.0	QUALITY ASSURANCE	31
6.0	ACKNOWLEDGEMENTS.....	32
7.0	REFERENCES	32
	Appendix A-1 AD Tracking Numbers for Tank 6F Characterization	33
	Appendix A-2 AD Tracking Numbers for Tank 6F Characterizations -Continued.....	34
	Appendix A-3. Chemical Composition for Reference Tank 8 Simulant Sludge.....	34
	Appendix A-4. Chemical Composition of Analyzed Reference Glass.....	35
	Appendix A-5. ICPEs and ICP-MS Comparisons for Select Analytes.....	36
	Appendix B - Summary of Analytical Methods	38
	Appendix C Summary of Statistical Methods	45

LIST OF TABLES

Table 1	Tank 6 Sample ID Numbers and Composite Sample Proportions.....	13
Table 2	Tank 6F “As-Received” Sample Bulk Density*, g/mL	13
Table 3	Tank 6F “Homogenized” Sample Bulk Density, g/mL	14
Table 4	Tank 6F Composite Sample Bulk Density, g/mL.....	14
Table 5	Tank 6F Sample Compositions for Composite Samples 1, 2 and 3.	15
Table 6	Weight Percent Solids for Tank 6F Composite Samples, Wt%	15
Table 7	Weight Percent Anions Leached per gram of Tank 6F- Composite Sample #1	22
Table 8	Weight Percent Anions Leached per gram of Tank 6F- Composite Sample #2.....	22
Table 9	Weight Percent Anions Leached per gram of Tank 6F- Composite Sample #3.....	22
Table 10	Elemental Constituents in Tank 6F Composite Sample # 1, wt%	23
Table 11	Elemental Constituents in Tank 6F Composite Sample # 2, wt%	24
Table 12	Elemental Constituents in Tank 6F Composite Sample # 3, wt%	25
Table 13	Radiological Constituents for Tank 6F Composite Sample #1, $\mu\text{Ci/g}$	26
Table 14	Radiological Constituents for Tank 6F Composite Sample #2, $\mu\text{Ci/g}$	28
Table 15	Radiological Constituents for Tank 6F Composite Sample #3, $\mu\text{Ci/g}$	30
Table 16	Tank 6F Constituents for Statistical Evaluation	46
Table 17	Tests and Estimators for Density, Weight Percent, and Anions.....	57
Table 18	Anion and Tritium Concentrations less than their MDCs	60
Table 19	95% UCLs for Mean Density, Weight Percent Solids, and Anion Concentrations (mg/g).....	60

Table 20 Tests and Estimators for Inorganic Constituents	61
Table 21 Computations for the Mean, Standard Error, and the 95% Upper Confidence Limit for the Mean Hg Concentration Omitting the Result for Run 1 of Composite Sample 171	
Table 22 Computations for the Mean, Standard Error, and the 95% Upper Confidence Limit for the Mean Mo Concentration Omitting the Result for Run 1 of Composite Sample 3	72
Table 23 Inorganic Constituent Concentrations with All Results Less Than Their MDCs...	73
Table 24 95% UCLs for Mean Concentrations of Inorganic Constituents with All Results Above Their MDCs.....	74
Table 25 Tests and Estimators for Radionuclides.....	75
Table 26 Radionuclide Concentrations with All Results below Their MDCs.....	93
Table 27 95% UCLs for Mean Concentrations of Radionuclide Constituents with All Results above Their MDCs.....	94

LIST OF FIGURES

Figure 1: Tank 6F Sample Locations.....	10
Figure 2 Photo images of some “as-received” Tank 6F samples.....	11
Figure 3. Sequence of Goodness-of-Fit Tests to Identify a Distribution and Select an Estimation Method.....	49
Figure 4. Scatterplots for the Inorganic Constituents	52
Figure 5. Scatterplots for a Subset of the Radionuclides	54

LIST OF ABBREVIATIONS

AD	Analytical Development
ANOVA	Analyses of Variance
ARG	Analyzed Reference Glass
AQR	Aqua Regia Digestions
C&WDA	Closure and Disposal Authority
DL	Detection limit: As used in mass spectrophotometer analyses or ICP-ES; three times the standard deviation of the blank measurements.
ICP-ES	Inductively Coupled Plasma–Atomic Emission Spectroscopy
ICP-MS	Inductively Coupled Plasma–Mass Spectroscopy
LIMS	Laboratory Information Management System
LWO	Liquid Waste Operations
MDA	Minimum Detectable Activity: Minimum detectable activity is the value above which instrument signal can be considered real.
PF	Sodium Peroxide/Hydroxide Fusions
PMP	Polymethyl Pentane
PuTTA	Plutonium thenoyltrifluoro-acetone
UCL95	Upper 95% Confidence Limit
UL	Upper limit: Activity observed but biased high due to spectral interference or blank contamination.
SRNL	Savannah River National Laboratory
SRR	Savannah River Remediation
TTQAP	Task Technical Quality Assurance Plan
TTR	Technical Task Request

1.0 INTRODUCTION

Savannah River Remediation (SRR) is preparing Tank 6F for closure. The Savannah River National Laboratory (SRNL) was requested by SRR to provide sample preparation and analysis of the Tank 6F final characterization samples to determine the residual tank inventory prior to grouting. In all, fourteen floor samples from three areas in Tank 6F were provided by SRR. These Tank 6F samples were taken from the tank and made available to SRNL between May and August 2011. Figure 1 shows the three locations in the Tank where these samples were taken. A photo image of some of the “as-received” Tank 6F samples is shown in Figure 2.

The fourteen Tank 6F samples formed the basis for designing the three Tank 6F composite materials (Tank 6F-Composite sample # 1, Tank 6F-Composite sample # 2 and Tank 6F-Composite sample # 3). The volume of residual material in each of the Tank 6F regions was obtained by SRR and this information was used to estimate the strata volumes in the tank. These strata volumes were converted into volumetric proportions and subsequently to the mass of residual material to be obtained from each primary sample for each composite sample¹ as summarized in Table 1.

The Tank 6F samples were analyzed in accordance with TTR⁶, and TTQAP⁷, for the analysis of Tank 5F and 6F⁷ and Tank 6F Sampling analysis plan⁸. The Justification for Changes to the Tank 6 Sampling and Analysis Plan, SRR-CWDA-2011-00159, Nov., 2011, Rev.0.²

The scope of this work includes characterization of Tank 6F composite samples and statistical analyses of select data as specified in the TTR⁶.

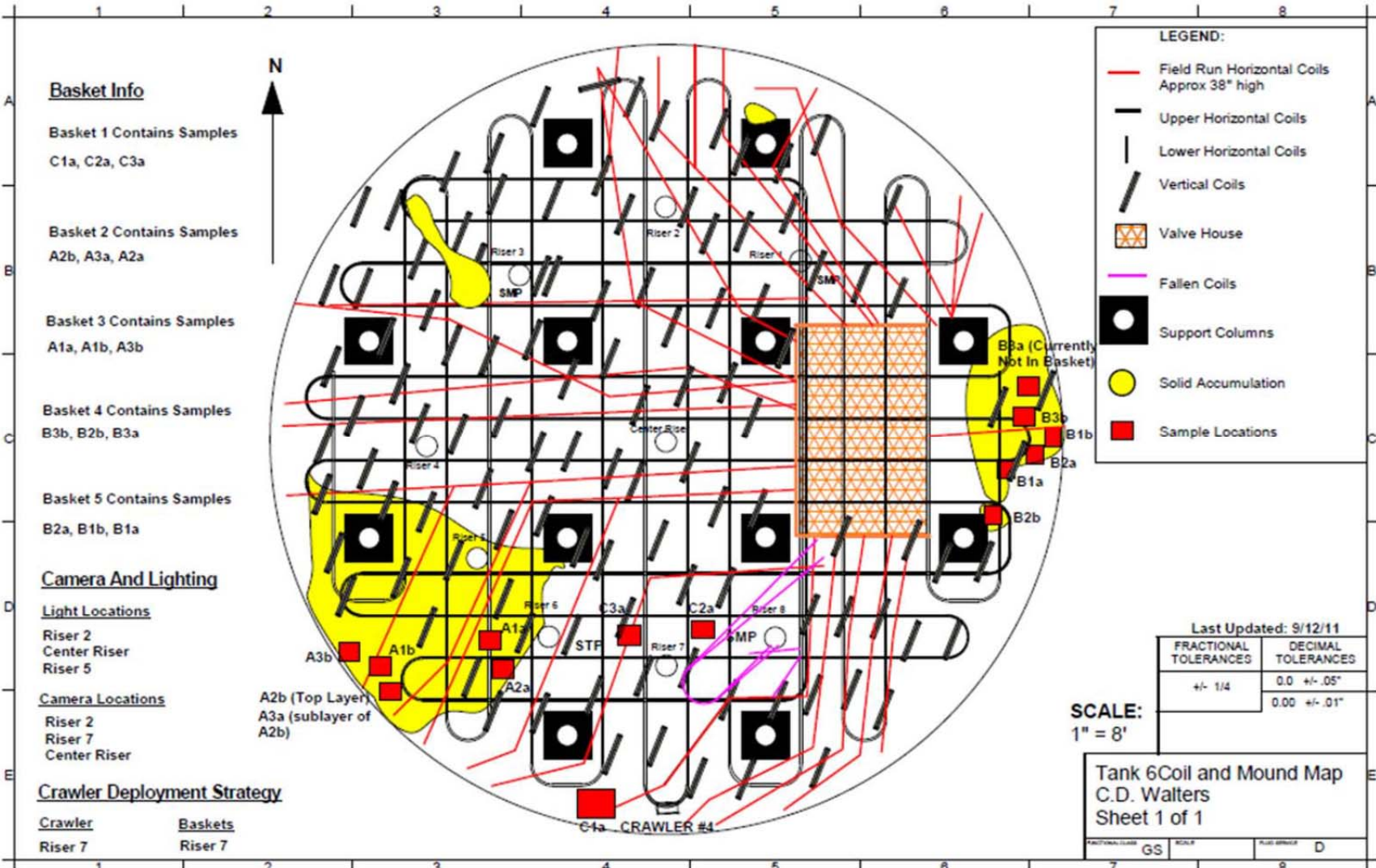


Figure 1 Tank 6F Sample Locations



Figure 2 Photo images of some “as-received” Tank 6F samples.

2.0 SAMPLING AND SAMPLE PREPARATION FOR CHARACTERIZATION

Samples from planned locations along the north side of the solids accumulation under riser 5 in Tank 6F were actually collected from the central/south region. This was determined by SRR to be acceptable because of process history and because the solids appearances in the tank photos indicate that the Tank 6F solids were well-mixed. Thus, actual samples are representative of the entire solids accumulation under Riser 5. Five of the planned six samples were collected from the solids accumulation along the east edge of Tank 6F because the sample crawler became hung up on a cooling coil and could not return the last sample to the collection basket for retrieval from the tank. As a solution to the unattained sample, SRR decided to take additional volume from one of the five samples to adequately represent the east accumulation in one of the three composite samples. The impact on analysis results uncertainty was assessed to be acceptable given the number of samples used for each composite and given that the single sample from the east accumulation is limited to only one of the three composite samples. Therefore, C&WDA and SRR Engineering determined that the minimal benefit of taking additional samples in Tank 6F did not warrant the potential worker exposure and risk of contamination.²

A few of the Tank 6F samples were moist and needed further air drying in the shielded cells before preparation for compositing. The individual “as-received” materials were weighed and their “as-received” dry bulk densities determined prior to preparing each sample for composition and characterization. Each Tank 6F sample was then homogenized to promote particle size reduction due to the presence of chunks of solids. Homogenizing each sample involved grinding with a mortar and pestle and then passing the powder through a sieve with 850 micron openings (mesh 18). Materials which did not go through the sieve were ground with mortar and pestle until it was small enough to go through the sieve. The bulk density of each homogenized sample was determined followed by the blending of proportional amounts of the samples by weight to form three composite Tank 6F samples. The bulk density of each of the three composite samples was then determined by the process described in Appendix B. A reference simulant sludge sample, based on Tank 8 sample chemistry [See Appendix A-3], was air-dried in a clean laboratory and the resulting sludge cake ground and homogenized with a mortar and pestle. The bulk density of this reference Tank 8 sludge was determined both inside the shielded cell along with the Tank 6F samples and outside the cell in a clean laboratory hood. These Tank 8 sludge simulant bulk density values were used to verify how well the reference bulk densities could be reproduced both inside (using remote handling via manipulators) and outside of the shielded cell.

SRR determined the composite sample volumetric percent as shown in Table 1, B. Dean, “Tank 6F Composite Sample Volumetric Proportions,” SRR-CWDA-2011-00067, Rev.1 April 20, 2011¹. All bulk density data for the “as-received”, homogenized and composited Tank 6F samples are presented in Tables 2 through 4. The weight percent solid determination method is described in Appendix B. These individual sample proportional location volumes, along with the homogenized sample bulk densities were used to calculate each sample’s mass per composite volume (Table 5). The total provided the composite density and the required weight from each of the fourteen Tank 6F sample material needed to make the three 70-gram composite Tank 6F samples as shown in Table 5. The weight percent solids in the three composite Tank 6F samples are summarized in Table 6.

Because of the inherent risk of cross-contamination of these samples in the shielded cells environment, certain actions were taken to minimize the risks. Actions taken to control cross-contamination in the cell included wiping down the cell (cell decontaminated), covering the entire cell floor with clean stainless steel plates, and changing manipulator fingers prior to initiating work.

Table 1 Tank 6 Sample ID Numbers and Composite Sample Proportions

Region	Location	Composite Sample					
		1		2		3	
		Vol.%	Sample ID	Vol.%	Sample ID	Vol.%	Sample ID
1	SW Accumulation	31%	6-A1a	27%	6-A2a	25%	6-A3a
		31%	6-A1b	27%	6-A2b	25%	6-A3b
2	East Accumulation	11.5%	6-B1a	13%	6-B2a	31%	6-B3b
		11.5%	6-B1b	13%	6-B2b		
3	Remainder of the Tank	15%	6-C1a	20%	6-C2a	19%	6-C3a
	Total	100%		100%		100%	

Table 2 Tank 6F “As-Received” Sample Bulk Density*, g/mL

Tank 6F Sample ID	Run-1	Run-2	Run-3	Average	Stdev.
TK6-A1a	1.17	1.19	1.18	1.18	0.01
TK 6-B1a	1.56	1.51	1.58	1.55	0.04
TK 6-B1b	1.66	1.65	1.56	1.62	0.06
TK 6-A1b	1.30	1.35	1.32	1.32	0.03
TK 6-C1a	1.07	1.09	1.07	1.08	0.01
TK 6-B2a	1.55	1.69	1.70	1.65	0.08
TK 6-A2a	1.69	1.58	1.62	1.63	0.06
TK 6-A2b	1.42	1.36	1.40	1.39	0.03
TK 6-B2b	1.09	1.28	1.20	1.19	0.10
TK 6-C2a	1.12	1.13	1.20	1.15	0.04
TK 6-B3a	No sample	No sample	No sample	No sample	
TK 6-B3b	0.87	0.85	0.84	0.85	0.02
TK 6-A3a	1.46	1.47	1.39	1.44	0.05
TK 6-A3b	1.52	1.51	1.47	1.50	0.03
TK 6-C3a	1.14	1.15	1.12	1.14	0.02
Tk 8 simulant sludge	1.40	1.45	1.43	1.43	0.03

*The “As-received” density values may in some cases have large uncertainty values. Problems were encountered in determining the volumes of these samples in calibrated PMP beakers. Most of the samples contained large chunky pieces, which made it difficult to determine acceptable sample volumes.

Table 3 Tank 6F “Homogenized” Sample Bulk Density, g/mL

Tank 6F Sample ID	Run-1	Run-2	Run-3	Average	Stdev.
TK6-A1a	1.12	1.16	1.29	1.19	<i>0.09</i>
TK 6-B1a	1.38	1.30	1.34	1.34	<i>0.04</i>
TK 6-B1b	1.17	1.15	1.16	1.16	<i>0.01</i>
TK 6-A1b	1.54	1.58	1.51	1.55	<i>0.04</i>
TK 6-C1a	1.07	1.09	1.07	1.08	<i>0.01</i>
TK 6-B2a	1.30	1.23	1.24	1.26	<i>0.03</i>
TK 6-A2a	1.50	1.41	1.42	1.44	<i>0.05</i>
TK 6-A2b	1.40	1.28	1.35	1.34	<i>0.06</i>
TK 6-B2b	1.35	1.32	1.30	1.32	<i>0.03</i>
TK 6-C2a	1.12	1.13	1.20	1.15	<i>0.04</i>
TK 6-B3a	No sample	No sample	No sample	No sample	
TK 6-B3b	1.29	1.31	1.30	1.30	<i>0.01</i>
TK 6-A3a	1.38	1.31	1.26	1.32	<i>0.06</i>
TK 6-A3b	1.50	1.37	1.46	1.44	<i>0.06</i>
TK 6-C3a	1.14	1.15	1.12	1.14	<i>0.02</i>
Tk 8 simulant sludge	1.34	1.47	1.41	1.41	<i>0.07</i>

Table 4 Tank 6F Composite Sample Bulk Density, g/mL

Tank 6F Sample ID	Run-1	Run-2	Run-3	Average	Stdev.
Tk 6 Composite No. 1	1.33	1.31	1.32	1.32	<i>0.01</i>
Tk 6 Composite No. 2	1.33	1.26	1.28	1.29	<i>0.04</i>
Tk 6 Composite No. 3	1.41	1.38	1.36	1.39	<i>0.02</i>
Tank 8 Simulant sludge#	1.40	1.41	1.42	1.41	<i>0.01</i>

Out of cell bulk density determination using the reference Tank 8 simulant sludge were within 5% of the cell values reported here for the Tank 8 simulant sludge.

Table 5 Tank 6F Sample Compositions for Composite Samples 1, 2 and 3.

Composite Sample #s	Material Available, g	Proportional Sample location volume, %	Homogenized Bulk density, g/mL	Wt. Fraction	Required wt. of material to make 70 g composite	Amount Weighed, g
Comp. Sample #1						
6-A1a	55.17	31	1.19	0.28	19.88	19.877
6-A1b	78.94	31	1.55	0.37	25.89	25.894
6-B1a	49.55	11.5	1.34	0.12	8.31	8.305
6-B1b	82.12	11.5	1.16	0.10	7.19	7.187
6-C1a	44.85	15	1.08	0.12	8.73	8.728
Mass sum, g	310.63	NA	NA	NA	70.00	69.991
Comp. Sample #2						
6-A2a	117.26	27	1.44	0.30	20.68	20.684
6-A2b	83.47	27	1.34	0.27	19.24	19.242
6-B2a	87.14	13	1.26	0.12	8.71	8.715
6-B2b	81.09	13	1.32	0.13	9.13	9.132
6-C2a	43.68	20	1.15	0.17	12.23	12.228
Mass sum, g	412.64	NA	NA	NA	70.00	70.001
Comp. Sample #3						
6-A3a	109.06	25	1.32	0.25	17.64	17.636
6-A3b	99.37	25	1.44	0.27	19.24	19.244
6-B3a	NA	NA	NA	NA	NA	NA
6-B3b	51.94	31	1.30	0.31	21.54	21.546
6-C3a	86.26	19	1.14	0.17	11.58	11.578
Mass sum, g	346.63	NA	NA	NA	70.00	70.004

NA Sample not available. See reference-2.

Table 6 Weight Percent Solids for Tank 6F Composite Samples, Wt%

Tank 6F Sample ID	Run-1	Run-2	Run-3	Average	Stdev.
Tk 6 Composite No. 1	87.8	87.4	87.8	87.7	0.23
Tk 6 Composite No. 2	89.3	89.7	89.9	89.6	0.31
Tk 6 Composite No. 3	91.3	91.3	91.1	91.2	0.13
Tank 8 Simulant sludge	91.2	91.2	91.0	91.1	0.14
*5% Reference NaCl Salt solution	4.9	4.7	4.8	4.8	0.10

*Reference target wt% NaCl solid = 4.9%

2.1 Blank Evaluations and Reference Materials

Two types of reference matrices were used during the characterization of Tank 6F samples. The first reference material was an analyzed reference glass (ARG) which was stored outside the shielded cells but processed in the shielded cells along with the samples during sample preparations. The second was a dried Tank 8 simulant sludge, which was exposed to the shielded cell radiological environment in which the Tank 6F radionuclide material was processed prior to analysis. The elemental chemical composition of the Tank 8 simulant sludge and analyzed reference glass are presented in Appendices A-3 and A-4. Distilled and de-ionized water was used as the liquid reagent media and blanks in all cell digestion cases.

The absence of radionuclides in these reference materials allowed the materials to additionally be utilized as blanks for radiochemical analyses.

Prior to the processing of the Tank 6F samples, which normally involved the opening of selected samples to be blended together, two in-cell reference Tank 8 simulant sludge samples in 250-mL capacity poly-bottles were placed at strategic locations in the shielded cell to ensure that these reference samples were exposed to the same cell environments as the Tank 6F samples. Each simulant sludge reference sample container held about 20 grams of Tank 8 simulant sludge. The containers were opened when the Tank 6F samples were being processed or air dried and closed at the end of each day of work in the cell. At the end of each Tank 6F sample preparations or digestion (aqua regia and peroxide fusion digestions), the Tank 8 simulant sludge reference material was also prepared in a manner similar to that for the preparation of Tank 6F samples and submitted for the same analyses as the actual samples from Tank 6F.

2.2 Leaching Characterization of Tank 6F Solids

Known quantities of homogenized Tank 6F composite solids were leached with distilled and de-ionized water and analyzed in triplicate. An average of 1.24 ± 0.04 grams of the composite solids was leached with an average of 50.01 ± 0.01 grams of distilled and de-ionized water. In this process each solid fraction was thoroughly mixed with the given amount of distilled and de-ionized water, and the mixture was hand agitated (shielded cell manipulator) for a total of about five minutes and left to stand for another 24 hours before another agitation and filtering of the mixture using a 0.45 micron Nalgene filter unit. The filtrate from the mixture was analyzed in triplicate for anion components as required. Thus, only surface-bound and water soluble constituents are assumed to be accounted for in the leachate analyses.

3.0 RESULTS

Appendix A (Appendices A-1 and A-2) contains the SRNL Analytical Development Laboratory Information Management System (LIMS) numbers for tracking the analytical data presented in this report. Details of most of the analytical methodologies including weight percent solids and density determinations applied in Tank 6F sample characterizations are summarized in Appendix B. It is worth pointing out that many digestion methods were performed in the shielded cells prior to taking representative sample aliquots out of the cells for analyses. Additionally, many of the initial separations for challenging radionuclide characterizations were performed in the Shielded Cells.

In the Tank 6F composite sample characterization results presented below, values preceded by “<” (less than sign) indicate values were below minimum detection limits, and values preceded by “≤” (less than or equal to sign) indicate that for replicates, at least one of the analysis values was above the instrument or method detection limit. Thus, where replicate analyses were both above and below the detection limit, the average of all replicates above and below the detection limit is given and a “≤” sign precedes the average value. The standard deviation values were calculated only for values that were above the detection limits. The minimum detectable activity (MDA) is defined as the value above which instrument signal can be considered real and the upper limit (UL) is defined as activity observed but biased high due to spectral interference or blank contamination. The detection limit (DL) as used in mass spectrometer or ICP-ES analyses is equivalent to three times the standard deviation of the blank measurements.

The one sigma percent uncertainty for each major radionuclide, as reported in the tables, is based on the pooled estimate derived from the individual uncertainties for each replicate measurement for that radionuclide [$\text{SQRT}((\text{SUMSQ}(x_i)/n))$], where n is the number of replicates and x_i is the individual uncertainty associated with each radionuclide for each run. Here it is assumed that the radio-analytical processes, be it counting or other techniques, are of the same precision for each individual measurement.

Occasionally, situations were encountered where the samples prepared and analyzed in triplicate gave mixed results with one or two of the triplicate analyses results being less than the MDA. In these cases, the reporting of the one sigma percent uncertainty is presented in a slightly different format. In this situation, the individual percent uncertainty associated with each run for that radionuclide is reported along with MDA or upper limit values as indicated by the analytical method. For example, under the one sigma percent uncertainty column for the isotope Np-239 in Table 14, the 21.7/MDA designation implies that the one sigma percent uncertainty for Np-239 in run 1 is reported with values above the detection limit and thus has a one sigma percent uncertainty of 21.7 percent. The measurements (runs 2 and 3) for Np-239 which were below the detection limit and thus not assigned percent uncertainty values are assigned an MDA. Similarly, in the analysis result for Eu-155 (runs 2 and 3, Table 13), the pooled statistics for the one sigma percent uncertainty is 5 and since the third run result of $<2.17\text{E}+00$ uCi/g was due to spectral interference the result is only reported as an upper limit. Thus, the one sigma percent uncertainty for that set of runs for Eu-155 is presented as 5/UL.

To monitor potential sample contamination during processing, analytical blank (reagent blanks and Tank 8 simulant sludge) results were compared to sample analytical results (See second column blank results for most radionuclides as presented in each Table). Although analyses of the ARG and Tank 8 simulant solids blanks both provided valid measures of potential radionuclide contamination, results for the Tank 8 simulant solids blank were judged more appropriate for two primary reasons: 1) the Tank 8 simulant solids aliquots were carried through the entire series of Shielded Cells preparation and digestion steps, just like the tank samples (while the ARG aliquots were prepared outside of the Shielded Cells and then only digested in the Shielded Cells); and 2) the dilution factors for the Tank 8 simulant solids aliquots were consistent with those of the tank samples (while the dilution factors for the ARG aliquots were approximately four times those of the tank samples). For these reasons, all blank values reported for radionuclide analyses were based on Tank 8 simulant data (instead of the ARG data).

It is worth noting that when reporting results in units of concentration (as opposed to straight activity), the impact of increased dilution is inflation in the apparent magnitude of detected contamination. For example, in the case of Pu-238 (where blank contamination was detected), the Pu-238 activity measured in the Tank 8 simulant blank was 7.3 - 9.7% of the Pu-238 measured in the samples, and the Pu-238 activity measured in the ARG blank was 5.4 - 7.1% of the Pu-238 measured in the samples. These levels of blank contamination were all deemed acceptable, based on the measurement performance criterion requiring that blank activity be less than 10% of the sample activity. In contrast, in terms of concentrations (activity per mass), the Pu-238 concentration in the Tank 8 simulant blank was 7.6 - 9.7% of the Pu-238 concentrations in the samples, while the Pu-238 concentration in the ARG blank was 23 - 29% of the Pu-238 concentrations in the samples. Clearly, the apparent inflation of contaminant concentrations for the ARG matrix is an artifact of adjusting the ARG data for 4x greater dilution than the sample data. Thus, taking all these into consideration the conclusion is that there were no significant cross contamination issues either from the environment of the shielded cell staging and operation areas or the reagents used in sample preparations.

The reporting units for all radionuclides including PF and AQR digestion analytical results are presented per gram of composite Tank 6F sample. Correction for water content as determined by sub-sample drying at 110 °C, if required (original “as received” basis to dry basis), can be accomplished through the use of the dry solid weight percent (wt %) values as shown in Table 6 for each composite sample. For example, $\mu\text{Ci/g dried solids} = [x \mu\text{Ci/g of “as-received solids”} * (100 \text{ g of “as-received solids”}/87.7 \text{ g dried solids})]$; using composite sample 1 in Table 6. Here x $\mu\text{Ci/g}$ represents the unknown activity of the “as-received” solids.

The one sigma analytical measurement uncertainty value for all of the anions and transition metals reported here is 20 percent. Leaching results are presented per gram of the “homogenized and composite” Tank 6F composite samples.

Tables 7 through 9 show the water soluble anion constituents for the Tank 6F composite sample, while Tables 10 through 12 contain inorganic constituent analytical results for the three composite Tank 6F samples. Tables 13 through 15 show the analytical results for the standard radiological constituents for the three composite Tank 6F samples. The following color codes are used for the Table contents: Green for blank values, red for less than values, pink for less than or equal to values, and bold for averages. All subsequent tables have similar color code meanings.

3.1 Data Quality and Presentations for Routine Radionuclide Constituents

The ICP-MS results are given for each atomic mass and in most cases each mass number represents only one isotope. An example of an exception is mass 238, since both uranium and plutonium are represented by this mass number. However, since the mass contribution of U-238 is significantly greater than that of Pu-238, the 238 signal is used to quantify U-238, not Pu-238. For this reason, Pu-238 was determined by PUTTA (chemical separation coupled with alpha spectroscopy). See Appendix B for summaries of the methods. In cases where ICP-MS and

radiochemistry data give similar results for a species, radiochemistry is typically selected due to better sensitivity and precision.

While many of the minimum detection limits (MDL), as specified in the TTR and TTQAP were met for the species characterized for Tank 6F composite samples, some were not met. In a number of cases, the relatively high levels of radioactive species of the same element or a chemically similar element precluded the ability to measure an isotope to lower levels. For example, the high activities of americium and curium isotopes in the sample matrix raised the instrumental backgrounds for Cm-243, having a detrimental effect on the detection limit for that isotope (Appendix A; Tables A5-1 through Tables A5-3). The 2.6 year half-life Pm-147 co-extracts with the 90 year half-life Sm-151. Both have overlapping beta spectra, with slightly higher continuum beta end-point energy for Pm-147. The Sm-151 levels in these composite Tank 6F samples were relatively high, substantially raising the detection limit achievable for Pm-147. A number of gamma emitting radionuclides were analyzed using a Cs-137 removed gamma analysis. Cesium-137 was expected to be the main contributor to background levels which would decrease the sensitivity of the gamma analysis for other species. While that was true, the samples also contained significant quantities of other gamma emitting isotopes (i.e. Co-60) which raised the background and thus the detection limits for other gamma emitting species. The minimum detection limits for Eu-152, Cm-243 and Cf-249 were not met because of spectral interferences.

Data reported for Tank 6F composite samples on Am-241 and Am-243 are based on analytical result from Cs-removed gamma analyzes. However, a second set of confirmatory analytical results for Am-241 and Am-243 based on Am/Cm analytical methods which are used mainly to validate the first set of Cs-removed gamma data is also presented in Appendix A, Table A5-1. This second set of data for Am-241 and Am-243 overlaps the first set of data and are within 10% of the Cs-removed data.

While reviewing the data tables, one of the triplicate Cm-242 values was observed to be roughly an order of magnitude lower in concentration than the results of the other eight Cm-242 measured values in the other two triplicate groups as well as the remaining 2 values of the sample's triplicate group. The discrepancy led to a further review of the sample's Am/Cm alpha spectrum fit. The alpha spectrum was dominated by Cm-244, Am-241 and Am-243. The alpha peak corresponding to Cm-242 had ~0.1% of the alpha counts measured in the spectrum. The low statistics of the counts in the Cm-242 region of interest led to a poor spectral peak shape which proved to be challenging to the spectroscopy software peak fitting algorithm. The Cm-242 peak fitting region of interest had to be adjusted several times manually to finally provide a satisfactory fit to the Cm-242 region of interest. The resulting fit provided a Cm-242 value which fell right in line with the other 8 Tank 6 Cm-242 values.

3.2 Data Quality and Presentations for Elemental Constituents

The non-radioactive materials used for the elemental analyses results presented in Tables 10 through 12 were a reference glass standard, ARG and dried Tank 8 simulant sludge samples. Appendices A-3 and A-4 contain the elemental analytical results for the two reference materials in comparison to their known reference values.^{3,4} In the reference ARG samples, elements (Ba, Cr, Cu, Sr and Zn) with concentrations less than 0.1 Wt% were not included in Appendices A-

4. because their concentrations could be influenced by trace reagent impurities. Similarly, for the Tank 8 simulants, K was not included in Appendix A-3.

A comparison of the laboratory results for the cations present in the simulant sludge shows that the laboratory analytical results are not significantly different from the known reference values for these cations. The percent relative deviation (%RD defined as $[\text{difference}/\text{mean}] * 100$) for each of the 12 constituent cations of this simulant sludge material was less than 20%. Similarly, looking at the analytical results for the 13 elemental constituents of the ARG reference sample [Appendix A-4], the percent relative deviation for each of the 13 constituents was below 10%.

Analytical elemental results were also compared between different methods used for characterization of Tank 6F composite samples, specifically comparing results from inductively coupled plasma-mass spectrometer (ICP-MS) with results from inductively coupled plasma-emission spectroscopy (ICP-ES). The concentration of select cations (natural lanthanum, barium and lead) were calculated from ICP-MS information and the resulting concentration values compared with the ICP-ES corresponding results presented in this report. Typical calculations are shown in Appendix A-5 for La, Ba and Pb. The average percent relative deviation between ICP-MS and ICP-ES analytical results for La, Ba and Pb were between 3 and 15%. These comparison results are summarized in Appendix A-5 and show that ICP-ES analytical results are about the same order of magnitude as the ICP-MS data for these select cations.

Because of the low iodine concentration in the Tank 6F leachate samples, analyses for iodine by mass spectroscopy was preferred over analyses by IC. Leached Tank 6F composite sample analyses for iodine by mass spectroscopy for stable iodine, assuming 100% iodine natural abundance, was based on the assumption that all other elements with mass 127 (Xe-127, Sn-127, Cs-127, Ba-127, La-127, In-127 etc.) have relatively short half-lives ranging from milliseconds to a few days. Thus, the total stable iodine reported in Tables 7 through 9 for elemental iodine is based on mass spectroscopy data for mass-127. The sum of iodine in each Tank 6F composite sample is approximated by adding mass 127 stable iodine results with mass 129 radioactive iodine data.

3.3 Data Quality and Presentations for Non-Routine Radionuclide Analytes.

Some of the radionuclides are not present in easily measurable concentrations and in some cases there was significant sample matrix effect as in the cases of carbon-14 (C-14) analyses in the Tank 6F composite samples. Thus, existing standard methods are not sufficient in attaining the requested minimum detection limits. These cases required new method development to meet the low detection limit requirements and minimize spectral interferences. Isotopes measured for the Tank 6F composite samples which fall into this category of analyses also include Zr-93, Ac-227, Th-229/230, Pa-231, Ra-226, Nb-94, Sn-126, Sb-126 and Sb-126m. With the exception of the antimony and tin isotopes (Sn-126, Sb-126 and Sb-126m), most of the targeted minimum detection limits for these radionuclides were met.

Thorium-229/230 analyses blanks for all three composite Tank 6F samples showed “no- yields” for Th-229/Th-230. A no-yield implies that there was no activity observed in the sample. Only Tank 6F composite sample number 3, run 1 showed no measurable yield for Th-229. Tank 6F

composite sample number 3, run 1 result for Ac-227 showed a poor yield and thus no data is presented.

Difficulties encountered during the C-14 analyses in the Shielded Cells required repeated sets of sample preparations and re-engineered carbon isolation vessels to produce data of acceptable quality. The first set of Tank 6F C-14 determinations was performed using the same analytical method and labware successfully utilized in the Tank 5F C-14 analyses. Using this approach, sample aliquots were digested and processed in a manner that liberated C-14 in the form of gaseous carbon dioxide, and then captured the carbon dioxide in an aqueous solution conducive to liquid scintillation counting. C-14 standards and blanks were processed and analyzed along with the sample aliquots, to provide a measure of the relative carbon recoveries and the absence or presence of C-14 contamination. As in the case of the Tank 5F C-14 analyses, the first set of Tank 6F C-14 analyses utilized a series of "Mason jar-like" vessels to liberate and collect the carbon dioxide, prior to capturing it in a medium submitted to Analytical Development. In the Tank 5F analyses, the liberation vessels and the seals used to prevent loss of carbon dioxide gas were all new (never used before). In contrast, in the Tank 6 analyses, the vessels and seals were those previously used for the Tank 5F analyses, following cleaning and decontamination.

The first set of Tank 6F C-14 analytical results indicated that the vessel seals were ineffective, as evidenced by carbon dioxide losses and C-14 contamination of blanks. As a consequence, the first set of C-14 results was rejected. A second set of Tank 6F C-14 analyses was performed after cleaning the existing vessels and replacing the seals. Unfortunately, the results of the second set of Tank 6F analyses suffered one of the same problems as the first set of Tank 6F analyses -- carbon dioxide losses. Hence, the second set of C-14 results was also rejected.

Because of the problems encountered with the "Mason jar-like" vessels, new collection vessels generated from Erlenmeyer flasks were fabricated at SRNL glass shop. Utilizing the new vessels, the C-14 analyses were repeated once again for a new set of Tank 6F sample aliquots. This time, the results were considerably more consistent, with both effective carbon dioxide capture and insignificant blank contamination. Although the recoveries for the C-14 spiked simulant were slightly outside of the targeted range (67-133% versus the 75-125% target), the results were deemed acceptable, given the high level of resources that would have been needed to hone the method further. The reported results include this larger method uncertainty in the pooled calculations.

Composite Tank 6F samples contained significant quantities of other gamma emitting isotopes (i.e. Co-60, Eu-154, Eu-155, etc.), which raised the spectral background. Because of this raised background, the detection limits for other gamma emitting species with lower activities were not met (i.e. Sb-126, Sn-126, and Sb-126m).

Table 7 Weight Percent Anions Leached per gram of Tank 6F- Composite Sample #1

Anion	Run-1	Run-2	Run-3	Average	Std. Dev.	Unit
Fluoride, F ¹⁻	<0.04	<0.04	<0.04	<0.04		Wt%
Formate, CHO ₂ ¹⁻	<0.04	<0.04	<0.04	<0.04		Wt%
Chloride, Cl ¹⁻	<0.04	<0.04	<0.04	<0.04		Wt%
Nitrite, NO ₂ ¹⁻	3.07E+00	3.18E+00	3.19E+00	3.15E+00	7.0E-02	Wt%
Bromide, Br ¹⁻	<0.19	<0.22	<0.21	<0.21		Wt%
Nitrate, NO ₃ ¹⁻	3.23E+00	3.34E+00	3.35E+00	3.31E+00	7.0E-02	Wt%
Phosphate, PO ₄ ³⁻	<0.04	<0.04	<0.04	<0.04		Wt%
Sulfate, SO ₄ ²⁻	1.03E+00	1.07E+00	1.01E+00	1.03E+00	3.0E-02	Wt%
Oxalate, C ₂ O ₄ ²⁻	1.16E+00	1.13E+00	1.25E+00	1.18E+00	6.0E-02	Wt%
Iodine, I-127	1.39E-04	1.19E-04	1.39E-04	1.32E-04	1.20E-05	Wt%
Iodine, I-129	7.88E-05	6.69E-05	8.16E-05	7.57E-05	7.82E-06	Wt%
Total Iodine	2.18E-04	1.86E-04	2.21E-04	2.08E-04	1.93E-05	Wt%

Table 8 Weight Percent Anions Leached per gram of Tank 6F- Composite Sample #2

Anion	Run-1	Run-2	Run-3	Average	Std. Dev.	Unit
Fluoride, F ¹⁻	<0.04	<0.04	<0.04	<0.04		Wt%
Formate, CHO ₂ ¹⁻	<0.04	<0.04	<0.04	<0.04		Wt%
Chloride, Cl ¹⁻	<0.04	<0.04	<0.04	<0.04		Wt%
Nitrite, NO ₂ ¹⁻	3.08E+00	3.08E+00	3.09 E+00	3.08E+00	1.0E-02	Wt%
Bromide, Br ¹⁻	<0.19	<0.20	<0.20	<0.20		Wt%
Nitrate, NO ₃ ¹⁻	3.24E+00	3.27E+00	3.24E+00	3.25E+00	2.0E-02	Wt%
Phosphate, PO ₄ ³⁻	<0.04	<0.04	<0.04	<0.04		Wt%
Sulfate, SO ₄ ²⁻	1.03E+00	9.90E-01	1.04E+00	1.02E+00	3.0E-02	Wt%
Oxalate, C ₂ O ₄ ²⁻	1.00E+00	1.18E+00	1.16E+00	1.11E+00	1.0E-01	Wt%
Iodine, I-127	1.47E-04	3.51E-04	2.99E-04	2.66E-04	1.06E-04	Wt%
Iodine, I-129	9.12E-05	9.35E-05	8.22E-05	8.90E-05	6.00E-06	Wt%
Total Iodine	2.38E-04	4.44E-04	3.81E-04	3.55E-04	1.06E-04	Wt%

Table 9 Weight Percent Anions Leached per gram of Tank 6F- Composite Sample #3

Anion	Run-1	Run-2	Run-3	Average	Std. Dev.	Unit
Fluoride, F ¹⁻	<0.04	<0.04	<0.04	<0.04		Wt%
Formate, CHO ₂ ¹⁻	<0.04	<0.04	<0.04	<0.04		Wt%
Chloride, Cl ¹⁻	<0.04	<0.04	<0.04	<0.04		Wt%
Nitrite, NO ₂ ¹⁻	3.23E+00	3.32E+00	3.28E+00	3.28E+00	4.0E-02	Wt%
Bromide, Br ¹⁻	<0.20	<0.21	<0.20	<0.20		Wt%
Nitrate, NO ₃ ¹⁻	3.21E+00	3.41E+00	3.32E+00	3.31E+00	1.0E-01	Wt%
Phosphate, PO ₄ ³⁻	<0.04	<0.04	<0.04	<0.04		Wt%
Sulfate, SO ₄ ²⁻	1.01E+00	1.07E+00	1.01E+00	1.03E+00	4.0E-01	Wt%
Oxalate, C ₂ O ₄ ²⁻	1.42E+00	1.27E+00	1.40E+00	1.36E+00	8.0E-02	Wt%
Iodine, I-127	3.78E-04	4.37E-04	2.52E-04	3.56E-04	9.46E-05	Wt%
Iodine, I-129	1.04E-04	1.08E-04	1.07E-04	1.06E-04	2.29E-06	Wt%
Total Iodine	4.82E-04	5.45E-04	3.59E-04	4.62E-04	9.49E-05	Wt%

Table 10 Elemental Constituents in Tank 6F Composite Sample # 1, wt%

Analytes	Tank 6F, Run1, wt%	Tank 6F, Run 2, wt%	Tank 6F, Run 3, wt%	Average, wt%	STDEV
Ag	<1.12E-02	<1.13E-02	<1.13E-02	<1.13E-02	
Al	2.22E+00	2.20E+00	2.24E+00	2.22E+00	2.00E-02
As	<5.37E-04	<5.41E-04	<5.40E-04	<5.39E-04	
B	<1.58E-02	<1.59E-02	<1.59E-02	<1.59E-02	
Ba	1.11E-01	1.10E-01	1.05E-01	1.09E-01	3.21E-03
Be	<4.69E-04	<4.72E-04	<4.72E-04	<4.71E-04	
Ca	3.58E-01	3.62E-01	3.64E-01	3.61E-01	3.06E-03
Cd	1.03E-02	9.87E-03	9.90E-03	1.00E-02	2.40E-04
Ce	1.81E-01	1.81E-01	1.73E-01	1.78E-01	4.62E-03
Co	2.13E-02	1.99E-02	2.02E-02	2.05E-02	7.37E-04
Cr	5.05E-02	4.64E-02	4.71E-02	4.80E-02	2.19E-03
Cu	1.02E-01	9.65E-02	9.44E-02	9.76E-02	3.92E-03
Fe	2.03E+01	1.93E+01	1.83E+01	1.93E+01	1.00E+00
Gd	<1.68E-02	<1.69E-02	<1.69E-02	<1.69E-02	
Hg	4.19E-01	3.63E-01	3.51E-01	3.78E-01	0.036
K	7.21E-02	6.53E-02	6.43E-02	6.72E-02	4.24E-03
La	8.76E-02	8.42E-02	8.10E-02	8.43E-02	3.30E-03
Li	1.04E-01	9.98E-02	9.39E-02	9.92E-02	5.07E-03
Mg	4.89E-02	4.88E-02	4.75E-02	4.84E-02	7.81E-04
Mn	1.55E+00	1.56E+00	1.51E+00	1.54E+00	2.65E-02
Mo	6.45E-03	6.61E-03	6.83E-03	6.63E-03	1.91E-04
Na	1.32E+01	1.35E+01	1.36E+01	1.34E+01	2.08E-01
Ni	4.60E+00	4.45E+00	4.33E+00	4.46E+00	1.35E-01
P	3.22E-02	2.59E-02	1.41E-02	2.41E-02	9.19E-03
Pb	4.98E-02	4.91E-02	4.73E-02	4.87E-02	1.29E-03
S	3.75E-01	4.04E-01	4.30E-01	4.03E-01	2.75E-02
Sb	<9.98E-02	<1.01E-01	<1.00E-01	<1.00E-01	
Se	<1.07E-03	<1.08E-03	<1.08E-03	<1.08E-03	
Si	6.13E-01	5.97E-01	6.00E-01	6.03E-01	8.50E-03
Sn	5.09E-03	6.04E-03	4.51E-03	5.21E-03	7.72E-04
Sr	4.39E-02	4.69E-02	4.53E-02	4.54E-02	1.50E-03
Th	<1.25E-01	<1.26E-01	<1.26E-01	<1.26E-01	
Ti	1.89E-02	1.83E-02	1.76E-02	1.83E-02	6.51E-04
U	3.31E+00	3.55E+00	3.45E+00	3.44E+00	1.21E-01
V	<3.67E-03	<3.70E-03	<3.69E-03	<3.69E-03	
Zn	1.02E-01	9.59E-02	9.28E-02	9.69E-02	4.68E-03
Zr	1.56E-01	1.66E-01	1.20E-01	1.47E-01	2.42E-02

Table 11 Elemental Constituents in **Tank 6F Composite Sample # 2, wt%**

Analytes	Tank 6F, Run1, wt%	Tank 6F, Run 2, wt%	Tank 6F, Run 3, wt%	Average, wt%	STDEV
Ag	<1.15E-02	<1.12E-02	<1.15E-02	<1.14E-02	
Al	2.29E+00	2.35E+00	2.34E+00	2.33E+00	3.21E-02
As	<5.49E-04	<5.33E-04	<5.48E-04	<5.43E-04	
B	<1.61E-02	<1.57E-02	<1.61E-02	<1.60E-02	
Ba	1.14E-01	1.16E-01	1.16E-01	1.15E-01	1.15E-03
Be	<4.79E-04	<4.65E-04	<4.78E-04	<4.74E-04	
Ca	4.24E-01	4.16E-01	4.29E-01	4.23E-01	6.56E-03
Cd	1.04E-02	1.07E-02	1.08E-02	1.06E-02	2.08E-04
Ce	1.85E-01	1.88E-01	1.88E-01	1.87E-01	1.73E-03
Co	2.24E-02	2.23E-02	2.26E-02	2.24E-02	1.53E-04
Cr	4.75E-02	4.86E-02	4.77E-02	4.79E-02	5.86E-04
Cu	1.01E-01	1.01E-01	1.01E-01	1.01E-01	0.00
Fe	2.05E+01	2.03E+01	2.05E+01	2.04E+01	1.15E-01
Gd	<1.72E-02	<1.67E-02	<1.71E-02	<1.70E-02	
Hg	3.74E-01	3.69E-01	3.68E-01	3.70E-01	3.00E-03
K	7.50E-02	6.77E-02	7.21E-02	7.16E-02	3.68E-03
La	8.88E-02	8.97E-02	9.01E-02	8.95E-02	6.66E-04
Li	1.03E-01	9.98E-02	1.02E-01	1.02E-01	1.64E-03
Mg	5.16E-02	5.18E-02	5.24E-02	5.19E-02	4.16E-04
Mn	1.66E+00	1.68E+00	1.73E+00	1.69E+00	3.61E-02
Mo	6.72E-03	6.68E-03	6.69E-03	6.70E-03	2.08E-05
Na	1.22E+01	1.29E+01	1.25E+01	1.25E+01	3.51E-01
Ni	4.67E+00	4.65E+00	4.72E+00	4.68E+00	3.61E-02
P	3.73E-02	3.87E-02	2.64E-02	3.41E-02	6.73E-03
Pb	5.16E-02	4.98E-02	5.08E-02	5.07E-02	9.02E-04
S	3.53E-01	4.08E-01	3.76E-01	3.79E-01	2.76E-02
Sb	<1.02E-01	<9.90E-02	<1.02E-01	<1.01E-01	
Se	<1.10E-03	<1.07E-03	<1.10E-03	<1.09E-03	
Si	6.37E-01	6.43E-01	5.98E-01	6.26E-01	2.44E-02
Sn	5.13E-03	6.50E-03	5.43E-03	5.69E-03	7.20E-04
Sr	5.00E-02	5.03E-02	5.13E-02	5.05E-02	6.81E-04
Th	<1.28E-01	<1.24E-01	<1.28E-01	<1.27E-01	
Ti	1.89E-02	1.92E-02	1.92E-02	1.91E-02	1.73E-04
U	3.65E+00	3.58E+00	3.82E+00	3.68E+00	1.23E-01
V	<3.75E-03	<3.64E-03	<3.74E-03	<3.71E-03	
Zn	1.00E-01	1.00E-01	9.88E-02	9.96E-02	6.93E-04
Zr	2.43E-01	2.07E-01	2.25E-01	2.25E-01	1.80E-02

Table 12 Elemental Constituents in Tank 6F Composite Sample # 3, wt%

Analytes	Tank 6F, Run1, wt%	Tank 6F, Run 2, wt%	Tank 6F, Run 3, wt%	Average, wt%	STDEV
Ag	<1.14E-02	<1.15E-02	<1.12E-02	<1.14E-02	
Al	2.38E+00	2.41E+00	2.43E+00	2.41E+00	2.52E-02
As	<5.43E-04	<5.48E-04	<5.36E-04	<5.42E-04	
B	<1.60E-02	<1.61E-02	<1.58E-02	<1.60E-02	
Ba	1.26E-01	1.31E-01	1.30E-01	1.29E-01	2.65E-03
Be	<4.74E-04	<4.78E-04	<4.68E-04	<4.73E-04	
Ca	3.64E-01	3.77E-01	3.87E-01	3.76E-01	1.15E-02
Cd	1.08E-02	1.09E-02	1.13E-02	1.10E-02	2.65E-04
Ce	2.22E-01	2.30E-01	2.29E-01	2.27E-01	4.36E-03
Co	2.63E-02	2.65E-02	2.73E-02	2.67E-02	5.29E-04
Cr	5.26E-02	5.39E-02	5.42E-02	5.36E-02	8.50E-04
Cu	1.10E-01	1.10E-01	1.08E-01	1.09E-01	1.15E-03
Fe	2.11E+01	2.10E+01	2.17E+01	2.13E+01	3.79E-01
Gd	<1.70E-02	<1.71E-02	<1.68E-02	<1.70E-02	
Hg	3.97E-01	4.04E-01	4.02E-01	4.01E-01	4.00E-03
K	6.47E-02	6.61E-02	6.68E-02	6.59E-02	1.07E-03
La	1.03E-01	1.07E-01	1.07E-01	1.06E-01	2.31E-03
Li	1.08E-01	1.05E-01	1.14E-01	1.09E-01	4.58E-03
Mg	5.67E-02	5.75E-02	5.88E-02	5.77E-02	1.06E-03
Mn	1.82E+00	1.99E+00	1.96E+00	1.92E+00	9.07E-02
Mo	6.63E-03	7.55E-03	7.38E-03	7.19E-03	4.90E-04
Na	1.15E+01	1.13E+01	1.13E+01	1.14E+01	1.15E-01
Ni	5.35E+00	5.45E+00	5.51E+00	5.44E+00	8.08E-02
P	1.79E-02	3.03E-02	2.41E-02	2.41E-02	6.20E-03
Pb	5.46E-02	5.22E-02	5.46E-02	5.38E-02	1.39E-03
S	3.97E-01	3.73E-01	3.96E-01	3.89E-01	1.36E-02
Sb	<1.01E-01	<1.02E-01	<9.96E-02	<1.01E-01	
Se	<1.09E-03	<1.10E-03	<1.07E-03	<1.09E-03	
Si	6.84E-01	6.85E-01	6.72E-01	6.80E-01	7.23E-03
Sn	6.14E-03	5.36E-03	5.23E-03	5.58E-03	4.92E-04
Sr	5.12E-02	5.29E-02	5.40E-02	5.27E-02	1.41E-03
Th	<1.27E-01	<1.28E-01	<1.25E-01	<1.27E-01	
Ti	2.09E-02	2.07E-02	2.15E-02	2.10E-02	4.16E-04
U	4.42E+00	4.54E+00	4.49E+00	4.48E+00	6.03E-02
V	<3.72E-03	<3.74E-03	<3.66E-03	<3.71E-03	
Zn	1.08E-01	1.03E-01	1.11E-01	1.07E-01	4.04E-03
Zr	2.19E-01	1.68E-01	1.52E-01	1.80E-01	3.50E-02

Table 13 Radiological Constituents for Tank 6F Composite Sample #1, $\mu\text{Ci/g}$.

Analytes*	Blank	Run 1	Run 2	Run 3	Average	Stdev	%Uncert.	Targeted Minimum Detection Limits
Gross alpha	<1.92E-02	<2.10E+02	<2.26E+02	<2.00E+02	<2.12E+02		MDA	None
Non-volatile beta	6.88E-01	3.94E+04	3.76E+04	3.70E+04	3.80E+04	1.24E+03	10.0	None
H-3	<2.06E-02	<2.01E-02	<2.03E-02	<2.03E-02	<2.02E-02		MDA	1.0E-01
C-14	<7.34E-04	2.22E-02	1.22E-02	2.13E-02	1.86E-02	5.56E-03	48.7	1.0E-01
Ni-59	<3.91E-02	5.32E+00	2.71E+00	3.59E+00	3.87E+00	1.32E+00	10.0	9.0E-02
Ni-63	2.04E-01	2.83E+02	1.64E+02	3.64E+02	2.70E+02	1.00E+02	10.0	1.0E-01
Co-60	<1.02E-02	7.03E+00	7.12E+00	7.07E+00	7.07E+00	4.50E-02	5.0	1.0E-03
Se-79	<2.80E-04	1.15E-02	1.59E-02	1.50E-02	1.41E-02	2.31E-03	32.2	1.0E-03
Sr-90	<6.58E+00	1.57E+04	1.61E+04	1.54E+04	1.57E+04	3.83E+02	6.7	1.0E-03
Y-90	<6.58E+00	1.57E+04	1.61E+04	1.54E+04	1.57E+04	3.83E+02	6.7	1.0E-03
Zr-93	6.10E-03	8.40E-01	7.87E-01	6.26E-01	7.51E-01	1.11E-01	20	1.0E-03
Nb-94	<2.90E-04	<1.74E-03	<1.72E-03	<2.04E-03	<1.83E-03		MDA	3.0E-03
Tc-99	<1.45E-04	1.24E-01	1.18E-01	1.07E-01	1.17E-01	8.50E-03	6.8	1.0E-03
Sn-126	<2.46E-02	<7.30E-01	<7.30E-01	<7.30E-01	<7.30E-01		MDA	1.0E-03
Sb-126	<9.91E-03	<9.41E-02	<9.50E-02	<9.41E-02	<9.44E-02		MDA	1.0E-03
Sb-126m	<9.91E-03	<9.41E-02	<9.50E-02	<9.41E-02	<9.44E-02		MDA	1.0E-03
I-129	<5.27E-06	1.39E-04	1.18E-04	1.44E-04	1.33E-04	1.39E-05	7.5	1.0E-04
Cs-135	<2.27E-05	2.64E-03	2.77E-03	3.04E-03	2.82E-03	2.04E-04	20	5.0E-02
Cs-137	<2.74E-02	5.36E+02	5.32E+02	5.36E+02	5.35E+02	2.60E+00	5.0	1.0E-03
Ba-137m	<2.59E-02	5.07E+02	5.03E+02	5.07E+02	5.06E+02	2.46E+00	5.0	1.0E-03
Pm-147	<2.40E-02	<1.58E+02	<1.49E+02	<1.63E+02	<1.56E+02		UL	None
Sm-151	<3.07E-02	2.01E+02	2.05E+02	2.08E+02	2.05E+02	3.40E+00	16.9	3.0E+00
Eu-152	<2.73E-02	<1.46E-01	<1.47E-01	<1.49E-01	<1.47E-01		MDA	7.0E-03
Eu-154	<1.90E-02	1.60E+01	1.59E+01	1.59E+01	1.59E+01	4.50E-02	5	1.0E-03
Eu-155	<2.80E-02	3.16E+00	<2.17E+00	3.66E+00	<3.00E+00		5/UL	None
Ra-226**	No yield	<2.65E-03	<3.25E-03	<2.76E-03	<2.89E-03		MDA	5.0E-03
Ac-227	No yield	<7.21E-06	<1.50E-05	<7.34E-06	<9.83E-06		UL	1.30E-04
Th-229	No yield	6.53E-05	7.84E-05	5.59E-05	6.65E-05	1.13E-05	18.1	1.0E-03
Th-230	No yield	6.62E-04	7.16E-04	7.79E-04	7.19E-04	5.86E-05	18.1	1.0E-03
Pa-231	<9.17E-04	<4.08E-04	<6.82E-04	<8.15E-04	<6.35E-04		DL	1.0E-03
U-232	No activity	6.71E-05	6.13E-05	6.26E-05	6.37E-05	3.07E-06	16.30	1.0E-03
U-233	<1.21E-04	2.86E-03	2.86E-03	3.57E-03	3.10E-03	4.10E-04	20.0	1.0E-03
U-234	<7.81E-05	7.77E-03	7.81E-03	9.69E-03	8.42E-03	1.10E-03	20.0	1.0E-03
U-235	<2.72E-08	3.72E-04	3.69E-04	4.56E-04	3.99E-04	4.94E-05	20.0	1.0E-04
U-236	<8.13E-07	4.67E-04	4.68E-04	5.74E-04	5.03E-04	6.15E-05	20.0	1.0E-03
U-238	<8.17E-07	1.35E-02	1.28E-02	1.33E-02	1.32E-02	3.61E-04	20.0	1.0E-03
Np-237	<1.48E-04	1.50E-02	1.11E-02	1.49E-02	1.37E-02	2.22E-03	24.7	1.0E-03
Pu-238	2.73E-01	3.59E+00	3.49E+00	2.80E+00	3.29E+00	4.29E-01	9.9	1.0E-03
Pu-239	3.34E-02	2.89E+00	2.99E+00	2.95E+00	2.94E+00	5.03E-02	20	1.0E-03
Pu-240	<8.26E-03	1.77E+00	1.90E+00	1.81E+00	1.83E+00	6.66E-02	20	1.0E-03
Pu-239/240	<1.08E-01	4.64E+00	4.91E+00	4.77E+00	4.77E+00	1.35E-01	8.2	None
Pu-241	<9.50E-03	7.12E+00	6.53E+00	6.17E+00	6.61E+00	4.77E-01	15.5	1.0E-03
Pu-242	<1.43E-04	2.26E-03	2.20E-03	2.20E-03	2.22E-03	3.46E-05	20	1.0E-03
Pu-244	<6.66E-07	<7.89E-07	<7.72E-07	<6.62E-07	<7.41E-07		DL	1.3E-04
Am-241	<3.14E-02	5.68E+01	6.53E+01	5.77E+01	5.99E+01	4.7E+00	5	1.0E-03
Am-242m	<1.36E-02	1.00E-01	1.10E-01	1.09E-01	1.06E-01	5.63E-03	24.7	1.0E-03
Np-239	<3.34E-02	1.31E+00	<2.25E+00	1.15E+00	<1.57E+00		11.9/UL	None

Table 13 Continued. Radiological Constituents for Tank 6F Composite Sample #1, $\mu\text{Ci/g}$.

Am-243	<2.19E-02	1.22E+00	1.03E+00	1.23E+00	1.16E+00	<i>1.16E-01</i>	13.3	1.0E-03
Cm-242	<1.13E-02	8.24E-02	9.14E-02	9.01E-02	8.80E-02	<i>4.86E-03</i>	24.71	None
Cm-243	<3.05E-03	<5.18E-01	<6.31E-01	<8.87E-01	<6.79E-01		UL	2.0E-02
Cm-244	5.00E-01	4.91E+01	4.95E+01	4.86E+01	4.91E+01	<i>4.50E-01</i>	15.10	None
Cm-245	<1.27E-04	4.82E-03	4.91E-03	4.73E-03	4.82E-03	<i>9.01E-05</i>	20.0	2.0E-02
Cm-246	<6.35E-04	3.20E-02	3.30E-02	3.36E-02	3.29E-02	<i>7.97E-04</i>	20.00	None
Cm-247	<5.23E-08	<1.62E-07	<2.05E-07	<2.36E-07	<2.01E-07		UL	1.3E-04
Bk-247	<5.86E-04	<1.81E-03	<2.28E-03	<2.63E-03	<2.24E-03		UL	None
Cm-248	<9.23E-06	<1.49E-05	<1.36E-05	<1.26E-05	<1.37E-05		UL	1.3E-04
Cf-249	<7.84E-04	<5.27E-03	<4.95E-03	<5.90E-03	<5.38E-03		MDA	5.0E-03
Cf-250	<7.97E-05	<3.82E-05	<3.10E-05	<6.35E-05	<4.42E-05		UL	None
Cf-251	<1.73E-03	<1.41E-02	<1.32E-02	<1.56E-02	<1.43E-02		MDA	None
Cf-252	<1.13E-02	<8.24E-02	<9.14E-02	<9.01E-02	<8.80E-02		UL	None

** While analysis of these isotopes is needed, meeting the detection limits for these isotopes is a lower priority than meeting detection limits for the other specified isotopes.

Table 14 Radiological Constituents for Tank 6F Composite Sample #2, $\mu\text{Ci/g}$.

Analytes	Blank	Run 1	Run 2	Run 3	Average	Stdev	%Uncert.	Targeted Minimum Detection Limits
Gross alpha	<1.92E-02	<2.07E+02	<2.13E+02	<2.17E+02	<2.12E+02		MDA	None
Non-volatile beta	6.88E-01	4.24E+04	4.12E+04	3.92E+04	4.09E+04	1.59E+03	10.0	None
H-3	<2.06E-02	<2.06E-02	<2.00E-02	<2.06E-02	<2.04E-02		MDA	1.0E-01
C-14	<7.34E-04	1.55E-02	2.36E-02	2.38E-02	2.10E-02	4.73E-03	48.6	1.0E-01
Ni-59	<3.91E-02	3.98E+00	4.59E+00	3.32E+00	3.96E+00	6.40E-01	10.0	9.0E-02
Ni-63	2.04E-01	3.03E+02	2.54E+02	3.09E+02	2.88E+02	3.02E+01	10.0	1.0E-01
Co-60	<1.02E-02	7.39E+00	7.25E+00	6.80E+00	7.15E+00	3.07E-01	5	1.0E-03
Se-79	<2.80E-04	3.40E-02	1.37E-02	1.63E-02	2.13E-02	1.11E-02	47.6	1.0E-03
Sr-90	<6.58E+00	1.67E+04	1.61E+04	1.48E+04	1.58E+04	9.69E+02	6.7	1.0E-03
Y-90	<6.58E+00	1.67E+04	1.61E+04	1.48E+04	1.58E+04	9.69E+02	6.7	1.0E-03
Zr-93	6.10E-03	1.37E+00	1.22E+00	1.39E+00	1.33E+00	9.29E-02	20	1.0E-03
Nb-94	<2.90E-04	<1.86E-03	<1.52E-03	<1.01E-03	<1.46E-03		MDA	3.0E-03
Tc-99	<1.45E-04	9.82E-02	1.23E-01	8.56E-02	1.02E-01	1.93E-02	6.4	1.0E-03
Sn-126	<2.46E-02	<7.52E-01	<6.40E-01	<6.26E-01	<6.73E-01		MDA	1.0E-03
Sb-126	<9.91E-03	<9.64E-02	<1.10E-01	<1.08E-01	<1.05E-01		MDA	1.0E-03
Sb-126m	<9.91E-03	<9.64E-02	<1.10E-01	<1.08E-01	<1.05E-01		MDA	1.0E-03
I-129	<5.27E-06	1.61E-04	1.65E-04	1.45E-04	1.57E-04	1.03E-05	6.3	1.0E-04
Cs-135	<2.27E-05	2.80E-03	2.67E-03	2.68E-03	2.72E-03	7.23E-05	21.8	5.0E-02
Cs-137	<2.74E-02	5.50E+02	5.90E+02	5.32E+02	5.57E+02	3.00E+01	5.0	1.0E-03
Ba-137m	<2.59E-02	5.20E+02	5.58E+02	5.03E+02	5.27E+02	2.84E+01	5.0	1.0E-03
Pm-147	<2.40E-02	<1.66E+02	<1.59E+02	<1.46E+02	<1.57E+02		UL	None
Sm-151	<3.07E-02	2.11E+02	2.03E+02	1.86E+02	2.00E+02	1.31E+01	16.7	3.0E+00
Eu-152	<2.73E-02	<1.48E-01	<1.75E-01	<1.71E-01	<1.64E-01		MDA	7.0E-03
Eu-154	<1.90E-02	1.68E+01	1.65E+01	1.59E+01	1.64E+01	4.87E-01	5.0	1.0E-03
Eu-155	<2.80E-02	3.91E+00	5.41E+00	4.68E+00	4.67E+00	7.46E-01	6.3	None
Ra-226**	No yield	<2.78E-03	<3.10E-03	<2.55E-03	<2.81E-03		MDA	5.0E-03
Ac-227	No yield	<3.91E-05	<2.23E-05	<4.59E-05	<3.58E-05		UL	1.30E-04
Th-229	No yield	2.99E-05	8.33E-05	1.18E-04	7.71E-05	4.44E-05	13.0	1.0E-03
Th-230	No yield	8.24E-04	7.07E-04	1.00E-03	8.45E-04	1.50E-04	13.0	1.0E-03
Pa-231	<9.17E-04	<7.42E-04	<4.72E-04	<8.72E-04	<6.95E-04		DL	1.0E-03
U-232	No activity	7.30E-05	9.14E-05	5.14E-05	7.19E-05	2.01E-05	20.7	1.0E-03
U-233	<1.21E-04	3.20E-03	3.28E-03	3.24E-03	3.24E-03	4.00E-05	20.0	1.0E-03
U-234	<7.81E-05	9.09E-03	9.05E-03	9.36E-03	9.17E-03	1.69E-04	20.0	1.0E-03
U-235	<2.72E-08	4.25E-04	4.25E-04	4.22E-04	4.24E-04	1.73E-06	20.0	1.0E-04
U-236	<8.13E-07	5.14E-04	5.40E-04	5.25E-04	5.26E-04	1.31E-05	20.0	1.0E-03
U-238	<8.17E-07	1.35E-02	1.35E-02	1.16E-02	1.29E-02	1.10E-03	20.0	1.0E-03
Np-237	<1.48E-04	2.41E-02	1.59E-02	1.42E-02	1.81E-02	5.29E-03	24.7	1.0E-03
Pu-238	2.73E-01	3.19E+00	3.05E+00	3.44E+00	3.23E+00	1.97E-01	9.2	1.0E-03
Pu-239	3.34E-02	2.66E+00	2.65E+00	2.94E+00	2.75E+00	1.65E-01	20.0	1.0E-03
Pu-240	<8.26E-03	1.63E+00	1.67E+00	1.86E+00	1.72E+00	1.23E-01	20.0	1.0E-03
Pu-239/240	<1.08E-01	4.29E+00	4.32E+00	4.82E+00	4.48E+00	2.98E-01	7.8	None
Pu-241	<9.50E-03	6.26E+00	6.31E+00	7.12E+00	6.56E+00	4.82E-01	15.4	1.0E-03
Pu-242	<1.43E-04	2.01E-03	2.01E-03	2.25E-03	2.09E-03	1.39E-04	20.0	1.0E-03
Pu-244	<6.66E-07	<6.24E-07	<5.75E-07	<6.68E-07	<6.22E-07		DL	1.3E-04
Am-241	<3.14E-02	6.71E+01	6.44E+01	6.08E+01	6.41E+01	3.16 E+00	5	1.0E-03
Am-242m	<1.36E-02	8.92E-02	1.29E-01	1.42E-01	1.20E-01	2.76E-02	24.1	1.0E-03
Np-239	<3.34E-02	9.19E-01	<7.07E-01	<7.52E-01	≤7.93E-01		21.7/MDA	None

Table 14 Continued. Radiological Constituents for Tank 6F Composite Sample #2, $\mu\text{Ci/g}$.

Am-243	<2.19E-02	1.52E+00	1.35E+00	1.36E+00	1.41E+00	9.52E-02	13.1	1.0E-03
Cm-242	<1.13E-02	7.39E-02	1.07E-01	1.18E-01	9.97E-02	2.30E-02	24.1	None
Cm-243	<3.05E-03	<1.10E+00	<9.59E-01	<8.11E-01	< 9.58E-01		UL	2.0E-02
Cm-244	5.00E-01	4.77E+01	5.68E+01	5.50E+01	5.32E+01	4.77E+00	15.07	None
Cm-245	<1.27E-04	4.59E-03	5.68E-03	5.27E-03	5.18E-03	5.46E-04	20.00	2.0E-02
Cm-246	<6.35E-04	3.23E-02	3.76E-02	3.85E-02	3.61E-02	3.37E-03	20.00	None
Cm-247	<5.23E-08	<1.66E-07	<2.16E-07	<2.62E-07	< 2.15E-07		UL	1.3E-04
Bk-247	<5.86E-04	<1.85E-03	<2.41E-03	<2.92E-03	< 2.39E-03		UL	None
Cm-248	<9.23E-06	<9.23E-06	<1.14E-05	<2.39E-05	< 1.48E-05		UL	1.3E-04
Cf-249	<7.84E-04	<4.38E-03	<4.82E-03	<9.95E-03	< 6.38E-03		MDA	5.0E-03
Cf-250	<7.97E-05	<2.68E-05	<2.35E-05	<1.40E-04	< 6.33E-05		UL	None
Cf-251	<1.73E-03	<9.50E-03	<1.05E-02	<2.18E-02	< 1.39E-02		MDA	None
Cf-252	<1.13E-02	<7.39E-02	<1.07E-01	<1.18E-01	< 9.96E-02		UL	None

** While analysis of these isotopes is needed, meeting the detection limits for these isotopes is a lower priority than meeting detection limits for the other specified isotopes.

Table 15 Radiological Constituents for Tank 6F Composite Sample #3, $\mu\text{Ci/g}$.

Analytes	Blank	Run 1	Run 2	Run 3	Average	Stdev	%Uncert.	Targeted Minimum Detection Limits
Gross alpha	<1.92E-02	<4.55E+02	<2.91E+02	<2.36E+02	<3.27E+02		MDA	None
Non-volatile beta	6.88E-01	4.28E+04	4.39E+04	4.22E+04	4.30E+04	8.46E+02	10.0	None
H-3	<2.06E-02	<2.17E-02	<2.06E-02	<2.01E-02	<2.08E-02		MDA	1.0E-01
C-14	<7.34E-04	1.26E-02	1.92E-02	1.02E-02	1.40E-02	4.62E-03	48.7	1.0E-01
Ni-59	<3.91E-02	5.32E+00	5.23E+00	5.63E+00	5.39E+00	2.13E-01	10.0	9.0E-02
Ni-63	2.04E-01	3.39E+02	5.00E+02	3.49E+02	3.96E+02	9.01E+01	10.0	1.0E-01
Co-60	<1.02E-02	8.42E+00	8.78E+00	8.15E+00	8.45E+00	3.16E-01	5	1.0E-03
Se-79	<2.80E-04	1.25E-02	9.41E-03	8.15E-03	1.00E-02	2.22E-03	24.4	1.0E-03
Sr-90	<6.58E+00	1.68E+04	1.50E+04	1.76E+04	1.65E+04	1.34E+03	6.4	1.0E-03
Y-90	<6.58E+00	1.68E+04	1.50E+04	1.76E+04	1.65E+04	1.34E+03	6.4	1.0E-03
Zr-93	6.10E-03	1.03E+00	8.25E-01	8.10E-01	8.88E-01	1.23E-01	27.1	1.0E-03
Nb-94	<2.90E-04	<2.15E-03	<1.31E-03	<1.59E-03	<1.68E-03		MDA	3.0E-03
Tc-99	<1.45E-04	1.21E-01	1.07E-01	8.15E-02	1.03E-01	1.99E-02	6.3	1.0E-03
Sn-126	<2.46E-02	<6.62E-01	<7.97E-01	<6.44E-01	<7.01E-01		MDA	1.0E-03
Sb-126	<9.91E-03	<1.17E-01	<1.06E-01	<1.13E-01	<1.12E-01		MDA	1.0E-03
Sb-126m	<9.91E-03	<1.17E-01	<1.06E-01	<1.13E-01	<1.12E-01		MDA	1.0E-03
I-129	<5.27E-06	1.83E-04	1.91E-04	1.88E-04	1.87E-04	4.30E-06	5.7	1.0E-04
Cs-135	<2.27E-05	2.62E-03	2.83E-03	2.64E-03	2.70E-03	1.16E-04	20	5.0E-02
Cs-137	<2.74E-02	5.41E+02	5.41E+02	5.27E+02	5.36E+02	7.80E+00	5.0	1.0E-03
Ba-137m	<2.59E-02	5.11E+02	5.11E+02	4.99E+02	5.07E+02	7.38E+00	5.0	1.0E-03
Pm-147	<2.40E-02	<1.64E+02	<1.70E+02	<1.64E+02	<1.66E+02		UL	None
Sm-151	<3.07E-02	2.07E+02	2.16E+02	2.08E+02	2.10E+02	5.12E+00	16.7	3.0E+00
Eu-152	<2.73E-02	<1.91E-01	<1.60E-01	<1.78E-01	<1.76E-01		MDA	7.0E-03
Eu-154	<1.90E-02	2.05E+01	2.14E+01	2.00E+01	2.06E+01	7.28E-01	5.0	1.0E-03
Eu-155	<2.80E-02	5.59E+00	4.59E+00	3.63E+00	4.60E+00	9.80E-01	7.7	None
Ra-226**	No yield	<3.57E-03	<3.19E-03	<4.35E-03	<3.70E-03		MDA	5.0E-03
Ac-227	No yield	Poor yield	<3.41E-05	<4.39E-05	<3.90E-05		UL	1.30E-04
Th-229	No yield	Poor yield	9.05E-05	1.25E-04	1.08E-04	2.45E-05	12.9	1.0E-03
Th-230	No yield	1.18E-03	8.38E-04	1.18E-03	1.07E-03	1.98E-04	10.61	1.0E-03
Pa-231	<9.17E-04	<1.02E-03	<5.23E-04	<9.69E-04	<8.37E-04		DL	1.0E-03
U-232	No activity	8.87E-05	4.55E-05	8.92E-05	7.45E-05	2.51E-05	21.60	1.0E-03
U-233	<1.21E-04	3.56E-03	3.20E-03	3.77E-03	3.51E-03	2.88E-04	20.0	1.0E-03
U-234	<7.81E-05	1.01E-02	9.38E-03	1.11E-02	1.02E-02	8.64E-04	20.0	1.0E-03
U-235	<2.72E-08	4.70E-04	4.29E-04	5.09E-04	4.69E-04	4.00E-05	20.0	1.0E-04
U-236	<8.13E-07	5.61E-04	5.16E-04	6.20E-04	5.66E-04	5.22E-05	20.0	1.0E-03
U-238	<8.17E-07	1.57E-02	1.60E-02	1.63E-02	1.60E-02	3.00E-04	20.0	1.0E-03
Np-237	<1.48E-04	2.56E-02	2.38E-02	3.37E-02	2.77E-02	5.27E-03	24.0	1.0E-03
Pu-238	2.73E-01	3.52E+00	3.57E+00	3.16E+00	3.42E+00	2.21E-01	9.5	1.0E-03
Pu-239	3.34E-02	3.29E+00	2.99E+00	2.88E+00	3.05E+00	2.12E-01	20.0	1.0E-03
Pu-240	<8.26E-03	2.05E+00	1.86E+00	1.78E+00	1.90E+00	1.39E-01	20.0	1.0E-03
Pu-239/240	<1.08E-01	5.32E+00	4.86E+00	4.64E+00	4.94E+00	3.44E-01	7.6	None
Pu-241	<9.50E-03	7.48E+00	7.03E+00	6.62E+00	7.04E+00	4.28E-01	15.4	1.0E-03
Pu-242	<1.43E-04	2.41E-03	2.23E-03	2.09E-03	2.24E-03	1.60E-04	20.0	1.0E-03
Pu-244	<6.66E-07	<6.44E-07	<7.76E-07	<5.75E-07	<6.65E-07		DL	1.3E-04
Am-241	<3.14E-02	8.02E+01	8.56E+01	7.84E+01	8.14E+01	3.75E+00	5	1.0E-03
Am-242m	<1.36E-02	1.26E-01	1.14E-01	1.33E-01	1.24E-01	9.76E-03	30.3	1.0E-03
Np-239	<3.34E-02	1.56E+00	1.13E+00	1.62E+00	1.44E+00	2.67E-01	11.4	None

Table 15 Continued. Radiological Constituents for Tank 6F Composite Sample #3, $\mu\text{Ci/g}$.

Am-243	<2.19E-02	1.88E+00	1.77E+00	1.88E+00	1.85E+00	6.12E-02	11.2	1.0E-03
Cm-242	<1.13E-02	1.04E-01	9.41E-02	1.10E-01	1.03E-01	8.17E-03	30.32	None
Cm-243	<3.05E-03	<1.25E+00	<1.45E+00	<1.32E+00	< 1.34E+00		UL	2.0E-02
Cm-244	5.00E-01	6.62E+01	6.26E+01	6.35E+01	6.41E+01	1.88E+00	15.03	None
Cm-245	<1.27E-04	6.40E-03	6.17E-03	6.71E-03	6.43E-03	2.72E-04	20.00	2.0E-02
Cm-246	<6.35E-04	4.37E-02	4.17E-02	4.23E-02	4.25E-02	1.04E-03	20.00	None
Cm-247	<5.23E-08	<2.39E-07	<2.76E-07	<2.16E-07	< 2.44E-07		UL	1.3E-04
Bk-247	<5.86E-04	<2.67E-03	<3.08E-03	<2.41E-03	< 2.72E-03		UL	None
Cm-248	<9.23E-06	<8.33E-06	<9.10E-06	<1.42E-05	< 1.06E-05		UL	1.3E-04
Cf-249	<7.84E-04	<6.53E-03	<5.45E-03	<8.56E-03	< 6.85E-03		MDA	5.0E-03
Cf-250	<7.97E-05	<3.49E-05	<2.34E-05	<6.17E-05	< 4.00E-05		UL	None
Cf-251	<1.73E-03	<1.69E-02	<1.19E-02	<2.26E-02	< 1.71E-02		MDA	None
Cf-252	<1.13E-02	<1.04E-01	<9.41E-02	<1.10E-01	< 1.03E-01		UL	None

** While analysis of these isotopes is needed, meeting the detection limits for these isotopes is a lower priority than meeting detection limits for the other specified isotopes.

3.4 Statistical Analyses

All statistical data manipulation, conclusions and recommendations on select radionuclide and inorganic components of Tank 6F analyses results are presented in Appendix C.

4.0 CONCLUSIONS

Tank 6F composite samples were analyzed for radiological, elemental and chemical constituents. Where analytical methods yielded additional contaminants other than those requested by the customer, these results are also reported.

The target detection limits for isotopes analyzed were based on customer desired detection limits as specified in the technical task request documents. While many of the target detection limits, as specified in the Technical Task Request and Task Technical and Quality Assurance Plans were met for the species characterized for Tank 6F composite samples, some were not met. In a number of cases, the relatively high levels of radioactive species of the same element or a chemically similar element precluded the ability to measure some isotopes to low levels. The isotopes whose minimum detection limits were not met in all cases included the following: Sn-126, Sb-126, Sb-126m, Eu-152, Cm-243 and Cf-249. However, SRNL, in conjunction with the customer, reviewed the few cases where the detection limit goals were not met and determined that the impacts were acceptable⁵.

All of the inorganic constituents displayed heterogeneity as evidenced by the ANOVA results. The inorganic results demonstrated consistent differences across the composite samples: lowest concentrations for Composite Sample 1, intermediate-valued concentrations for Composite Sample 2, and highest concentrations for Composite Sample 3. The Hg and Mo results suggest possible measurement outliers. However, the magnitudes of the differences between the Hg UCL95 results and the magnitudes of the differences between the Mo UCL95 results not appear to have practical significance. It is recommended to remove the potential measurement outliers. Doing so is conservative in the sense of producing a higher UCL95 for Hg and Mo than if the potential outliers were included in the calculations.

In contrast to the inorganic results, most of the radionuclides did not demonstrate heterogeneity among the composite sample results.

5.0 QUALITY ASSURANCE

The Task Technical and Quality Assurance Plan details the planned activities and associated quality assurance implementing procedures for the characterization of Tank 6F (TTQAP⁹). Laboratory Notebooks SRNL-NB-2011-00125, SRNL-NB-2011-00089, WSRC-NB-2001-00142 and various AD notebooks contain the experimental and analytical data.

6.0 ACKNOWLEDGEMENTS

The authors thank Analytical Development Section personnel, in particular, Mark Jones, and Cecilia Diprete, for performing actinide and other metal analyses. We also thank the shielded cell operations personnel, in particular, Linda Bush, Carl Black and Kevin Reid for their work with the Tank 6F samples in the shielded cells.

7.0 REFERENCES

1. B. Dean, "Tank 5 Composite Sample Volumetric Proportions," SRR-CWDA-2011-00067, Rev.1 April 20, 2011
2. B. Martin, "Justification for Adjustments to the Tank 6 Sample Plan" SRR-CWDA-2011-00159, Revision 0, October 2011.
3. C. J Coleman, R. A. Dewberry, M. F. Bryant and J.J Gemmill," SRL's Performance in Round Robin #6-Analyses of Simulated Defense Waste Glass', WSRC-TR-91-187, Rev. 0, May 31, 1991.
4. D. Koopman,"Tank 8, Drum 1, Sludge simulant, SRTC mobile Lab. ID # 20000616," July 26, 2000
5. A. W. Wiggins, Jr., "Detection Limit Acceptability for Tank 6 Residual Sample Analysis" SRR-CWDA-2012-00091, June 7, 2012.
6. Technical Task Request number HLE-TTR-2010-004, Rev 7
7. Task Technical Quality Assurance Plan for the Analysis of the Tank 5F and Tank 6F Final Characterization Samples-SRNL-RP-2010-01695, Rev. 1
8. Tank 6F Sampling and Analysis Plan-SRR-LWE-2010-00285, Nov. 2011, Rev. 6
9. Task Technical Quality Assurance Plan and Characterization Plan for Tanks 18F and 19F Solid Fraction Analysis – 2008, SRNL-RP-2008-01202, Rev. 1, July 10, 2009

APPENDIX A-1 AD TRACKING NUMBERS FOR TANK 6F CHARACTERIZATION

Analytes	Method (s)	SRNL AD Tracking Number (LIMS)
Total Alpha	Rad Screen	300295756-300295758 300295762-300295764
Non-volatile Beta	Rad Screen	300295765-300295767 300295768-300295770
Sr-90	Sr90	300295756-300295764 300295766-300295769
Pu-238	Pu-238/241	300295756-300295769
Pu-241	Pu-238/241	300295756-300295769
Cs-137	GAMMA SPEC	300295756- 300295766
U-232	U-232	300295756-300295767
U-233	U-233, U-234, U-235, U-236	300295756-300295767
U-234	U-233, U-234, U-235, U-236	300295756-300295767
U-235	U-233, U-234, U-235, U-236	300295756-300295767
U-236	U-233, U-234, U-235, U-236	300295756-300295767
U-238	ICp-MS	300295756-300295767
Co-60	GAMMA SPEC Cs REMOVED	300295762-300295766
Sb-126	GAMMA SPEC Cs REMOVED	300295762-300295766
Eu-154	GAMMA SPEC Cs REMOVED	300295762-300295766
Eu-155	GAMMA SPEC Cs REMOVED	300295762-300295766
Am-241	Gamma Spec.	300295762-300295766
Cm-242	Am/Cm	300295762-300295766
Cm-244	Am/Cm	300295762-300295766
Pu-239		300295756-300295768
Pu-240		300295756-300295768
Pu-242	Pu-242/244	300295756-300295768
Pu-244	Pu-242/244	300295756-300295768
Pu-239/240	Pu-TTA	300295756-300295769
PM-147/ SM-151	Pm-147/Sm-151	300295756-300295767
Tritium	TRITIUM	300295771-300295780
Ni-59	Ni-59,63	300295771-300295783
Ni-63	Ni-59,63	300295771-300295783
Tc-99	Tc-99	300296139-300296151
I-129	I-129	300296467-300296477
Cs-135	Cs-135	300295756-300295768
Carbon-14	Carbon-14	300299257-300299386
Carbon-14, blank	Carbon-14	300299268 & 300299387
Se-79	Se-79	300297058-300297067
Zr-93	Zr-93	300295756-300295764
Zr-93 blank	Zr-93	300295765 & 300295768
Am/Cm	Am/Cm	300296591-300296599
Am/Cm	Am/Cm	300296600-300296601

**APPENDIX A-2 AD TRACKING NUMBERS FOR TANK 6F CHARACTERIZATIONS -
CONTINUED**

Analytes	Method (s)	SRNL AD Tracking Number (LIMS)	Comments
Nb-94	Nb-94	300295756-300295768	
Cs-removed gamma	Cs-removed gamma	300295756-300295766	
Am/Cm	Am/Cm	300296591-3002966601	
Ra-226	Ra-226	300297708-300297726	
Th-229/230	Th-229/230	30029750-300297869	
Ac-227	Ac-227	300297850-300297867	
Pa-231	Pa-231	300297206-300297224	
I-127 (stable)	Mass spect.	300297358-300297367	
Np-237		300295756-300295770	
Hg	CVAA Hg	300295771-300295779	Hg in Samples
		300295782-300295783	Hg Blank
Se	AASe	300295771-300295779	
		300295780-300295785	Se Blank
As	AASe	300295771-300295779	As in Samples
		300295780-300295785	As Blank
Cations	ICP-ES	300295771-300295779	AQR digestions
		300295783-300295785	AQR digestions-ARG
		300295780-300295782	AQR digestions-simulant
Cations	ICP-ES	300295756-300295767-	PF digestions
		300295768-300295770	PF digestions-ARG
		300295765-300295767	PF digestions-simulant

**APPENDIX A-3. CHEMICAL COMPOSITION FOR REFERENCE TANK 8 SIMULANT
SLUDGE**

	Analytical Results for Tank 8 Simulant Sludge	Standard deviation	Nominal Recipe for Tank 8 Simulant Sludge@	Percent Relative Deviation
	Average			%RD
Constituent	wt. %		wt. %	
Al	8.85E+00	1.46E-01	9.28	4.7
Ba	2.20E-01	3.21E-03	0.20	9.5
Ca	1.96E+00	3.51E-02	2.22	12.4
*Cr	2.28E-01	4.04E-03	0.22	3.6
Cu	1.19E-01	3.21E-03	0.13	8.8
Fe	2.25E+01	3.51E-01	26.23	15.3
Mg	1.15E-01	1.73E-03	0.12	4.3
Mn	2.45E+00	4.58E-02	2.55	4.0
Na	5.24E+00	8.02E-02	5.97	13.0
Ni	2.55E+00	4.04E-02	2.81	9.7
*Si	7.47E-01	5.03E-03	0.89	17.5
Pb	1.20E-01	1.73E-03	0.10	18.2

* Peroxide fusion digestion data; all other data from aqua regia digestions.

@ Reference values for the Tank 8 simulant are reported to the number of digits given in the original citation

APPENDIX A-4. CHEMICAL COMPOSITION OF ANALYZED REFERENCE GLASS

	Analytical Results for Reference Glass (ARG)	Standard deviation	Nominal Recipe for Reference Glass # (ARG)	Percent Relative Deviation
	Average			%RD
Constituent	wt. %		wt. %	
Al	2.48E+00	4.51E-02	2.50E+00	0.8
B	2.62E+00	4.58E-02	2.69E+00	2.6
Ca	1.06E+00	2.08E-02	1.02E+00	3.8
Fe	9.89E+00	1.94E-01	9.79E+00	1.0
Li	1.49E+00	3.00E-02	1.49E+00	0.0
K	2.11E+00	3.61E-02	2.26E+00	6.9
Mg	5.11E-01	8.74E-03	5.2E-01	1.7
Mn	1.46E+00	2.52E-02	1.46E+00	0.0
Na	8.40E+00	1.45E-01	8.52E+00	1.4
Ni	8.40E-01	1.23E-02	8.27E-01	1.6
P	1.13E-01	5.29E-03	1.1E-01	2.7
*Si	2.30E+01	3.06E-01	2.24E+01	2.6
*Ti	6.85E-01	8.72E-03	6.9E-01	0.7

* Peroxide fusion digestion data; all other data from aqua regia digestions.

Reference values for ARG are reported to the number of digits given in the original citation

APPENDIX A-5. ICPES AND ICP-MS COMPARISONS FOR SELECT ANALYTES.

Natural Lanthanum concentration by MS

Main stable La isotope used for calculations is mass 139

[Sum of MS signals from mass 139]
Tank 6F Composite No. 1, unit of ug/g sample

Mass 139 911 ug/g = 0.911 mg/g

	300295756 COMPOSITE 1- 1-PF, mg/g	300295757 COMPOSITE 1-2-PF, mg/g	300295758 COMPOSITE 1-3-PF, mg/g	Averages
La by ICP-MS	0.911	0.912	0.904	0.909
La by ICP-ES	0.841	0.856	0.830	0.842
%RD	8.0	6.3	8.5	7.6

The average percent relative deviation for lanthanum concentrations based on ICP-MS and ICP-ES is 7.6%.

Natural barium concentration by MS

Main stable Ba isotopes used for calculations are masses, 138, 137, 135

[Sum of MS signals from masses 138, 137,135]
Tank 6F Composite No. 1, unit of ug/g sample

Mass 138 942 ug/g = 0.942 mg/g
Mass 137 132 ug/g = 0.132 mg/g
Mass 135 4.34 ug/g = 0.0043 mg/g

	300295756 COMPOSITE 1- 1-PF, mg/g	300295757 COMPOSITE 1-2-PF, mg/g	300295758 COMPOSITE 1- 3-PF, mg/g	Averages
Ba by ICP-MS	1.08	1.08	1.07	1.08
Ba by ICP-ES	1.11	1.11	1.10	1.11
%RD	2.7	2.7	2.8	2.7

The average percent relative deviation for barium concentrations based on ICP-MS and ICP-ES is 2.7%.

Natural lead concentration by MS

Main stable Pb isotopes used for calculations are masses, 204, 206, 207, 208

[Sum of MS signals from masses 204, 206, 207, 208]
Tank 6F Composite No. 1, unit of ug/g sample

Mass 204 43.1ug/g = 0.043 mg/g
Mass 206 118 ug/g = 0.118 mg/g
Mass 207 108 ug/g = 0.108 mg/g
Mass 208 243 ug/g = 0.243

	300295756 COMPOSITE 1- 1-PF, mg/g	300295757 COMPOSITE 1-2-PF, mg/g	300295758 COMPOSITE 1- 3-PF, mg/g	Averages
Pb by ICP-MS	0.512	0.540	0.523	0.525
Pb by ICP-ES	0.645	0.507	0.674	0.609
%RD	23.0	6.3	25.2	14.8

The average percent relative deviation for lead concentrations based on ICP-MS and ICP-ES is 14.8%.

Table A5-1 AVERAGED CESIUM REMOVED GAMMA AND AM/CM FOR AM-241 AND AM-243.

AD LIMS #	Radiological Constituents for Tank 6F Composite Sample #1, $\mu\text{Ci/g}$.							pooled stat.	Comments
300-		Blank	Run-1	Run-2	Run-3	Average	Stdev.		
295756-295758	Am-241	<3.14E-02	5.68E+01	6.53E+01	5.77E+01	5.99E+01	4.7E+00	5	Cs-removed
296591-296593	Am-241	6.62E-02	6.35E+01	6.39E+01	6.17E+01	6.30E+01	1.19E+00	5	Am/Cm
	Am-241	\leq 4.88E-02	6.02E+01	6.46E+01	5.97E+01	6.15E+01	2.74E+00	5	Average
295756-295758	Am-243	<2.19E-02	1.22E+00	1.03E+00	1.23E+00	1.16E+00	1.16E-01	13.3	Cs-removed
296591-296593	Am-243	<2.82E-03	1.14E+00	1.14E+00	1.12E+00	1.13E+00	1.19E-02	6.3	Am/Cm
	Am-243	<1.24E-02	1.18E+00	1.09E+00	1.18E+00	1.15E+00	5.35E-02	9.8	Average
	Radiological Constituents for Tank 6F Composite Sample #2, $\mu\text{Ci/g}$.								
295759-295761	Am-241	<3.14E-02	6.71E+01	6.44E+01	6.08E+01	6.41E+01	3.16E+00	5	Cs-removed
296594-296596	Am-241	6.62E-02	6.71E+01	7.61E+01	6.40E+01	6.91E+01	6.31E+00	5	Am/Cm
	Am-241	\leq 4.88E-02	6.71E+01	7.03E+01	6.24E+01	6.66E+01	3.95E+00	5	Average
295759-295761	Am-243	<2.19E-02	1.52E+00	1.35E+00	1.36E+00	1.41E+00	9.52E-02	13.1	Cs-removed
296594-296596	Am-243	<2.82E-03	1.20E+00	1.38E+00	1.15E+00	1.2E+00	1.21E-01	6.3	Am/Cm
	Am-243	<1.24E-02	1.36E+00	1.365E+00	1.26E+00	1.33E+00	6.21E-02	9.7	Average
	Radiological Constituents for Tank 6F Composite Sample #3, $\mu\text{Ci/g}$.								
295762-295764	Am-241	<3.14E-02	8.02E+01	8.56E+01	7.84E+01	8.14E+01	3.75E+00	5	Cs-removed
296597-296599	Am-241	6.62E-02	8.74E+01	8.78E+01	8.24E+01	8.59E+01	3.00E+00	5	Am/Cm
	Am-241	\leq 4.88E-02	8.38E+01	8.67E+01	8.04E+01	8.37E+01	3.15E+00	5	Average
295762-295764	Am-243	<2.19E-02	1.88E+00	1.77E+00	1.88E+00	1.85E+00	6.12E-02	11.2	Cs-removed
296597-296599	Am-243	<2.82E-03	1.59E+00	1.59E+00	1.49E+00	1.56E+00	6.00E-02	6.5	Am/Cm
	Am-243	<1.24E-02	1.74E+00	1.68E+00	1.69E+00	1.71E+00	3.04E-02	8.9	Average

APPENDIX B - SUMMARY OF ANALYTICAL METHODS

Aqua Regia Digestions (AQR)

Samples were digested according to procedure L16.1, ADS-2226. In a typical digestion, ~0.5 g of Tank 6F composite sample was placed into a Teflon[®] digestion vessel. Then, 9 mL (hydrochloric acid) HCl, and 3 mL (nitric acid) HNO₃ were added to the Teflon[®] vessel. The Teflon[®] vessel was sealed and heated for a period of no more than 4 hours at 115 °C. The sample was then cooled and diluted to 100 mL. Three samples, in total, from each composite sample were digested by aqua regia.

Sodium Peroxide/Hydroxide Fusions (PF)

Samples were digested according to procedure L16.1, ADS 2502. In a typical digestion, ~2 grams of composite Tank 6F sample (as received) was placed into a nickel (Ni) crucible with a known weight. The remaining material in the crucible was fused at 675 °C using a mixture of sodium peroxide (6.0 grams) and sodium hydroxide (4.0 grams). After the sample was cooled, water was added to dissolve the fused material and the solution was acidified by the addition of 25 mL HCl. The sample was diluted to 25 mL. Three samples, in total, from each composite sample were digested by sodium peroxide fusion.

Inductively Coupled Plasma – Atomic Emission Spectroscopy (ICP-ES)

Samples are diluted as necessary to bring analytes within the instrument range. A scandium internal standard is added to all samples after dilution at a concentration of 2 mg/L. The instrument is calibrated daily with a blank and two standards: 5 and 10 mg/L NIST traceable multi-element standards in dilute acid. Background and internal standard correction were applied to the results.

Ion Chromatography for Anions (IC-Anions)

For IC Anions, samples were diluted with a carbonate/bicarbonate diluent as necessary to bring analytes to within instrument calibration. A 3-point calibration curve is run daily on the instrument with concentrations of 10, 25 and 50 µg/mL.

Atomic Absorption Spectroscopy (AA)

Arsenic, selenium, and mercury are analyzed by AA. The mercury was determined using the cold vapor technique. Samples were diluted as necessary to bring analytes within the instrument calibration range. A 3-point calibration curve is run daily on the instrument with concentrations of 0.025, 0.05 and 0.075 mg/L for arsenic and mercury and 0.005, 0.0075, and 0.01 mg/L for selenium. An instrument blank is performed daily and a calibration check standard is run for each element at the beginning of the day, after each five sample runs, and at the end of the day.

Inductively Coupled Plasma – Mass Spectroscopy (ICP-MS)

Samples were run concurrently with a laboratory control standard (LCS) containing V, Co, As, Sr, Mo, Ru, Ag, Cd, Sb, Cs, Ba, La, Eu, Ho, Yb, Tl, Pb, Th, and U. This LCS provided a mass response covering most of the mass range of interest. The following describes the calculation of the analytes of interest from the mass values:

Co	mass 59
⁹⁹ Tc	mass 99. Subject to interference when Ru is present in the sample.
Ag	mass 107, 109
Pb	mass 206, 207, 208
Sn	mass 117, 118, 120, 122, 124
²³³ U	mass 233
²³⁴ U	mass 234
²³⁵ U	mass 235
²³⁶ U	mass 236
²³⁸ U	mass 238
²³⁷ Np	mass 237
²³⁹ Pu	mass 239
²⁴⁰ Pu	mass 240
²⁴² Pu	mass 242.

Gross Alpha/Gross Beta

The solid material was too concentrated to be analyzed directly. Aliquots of peroxide fusion dissolution were added to liquid scintillation cocktail and analyzed for gross alpha and gross beta activity using liquid scintillation analysis. Alpha/beta spillover was determined for each aliquot analyzed, and subsequently used for accurately determining alpha and beta activity, via the addition of a known amount of plutonium to an identical aliquot of each sample.

Other Specialty Separations and Preparations

Ni-59/63

Aliquots of dissolution from the aqua regia digestion were aliquoted and spiked with an elemental nickel carrier. The nickel species were extracted from the matrix using dimethylglyoxime (DMG) based extractant. Ni-59 concentrations were measured using low energy photon/x-ray, thin-windowed, semi-planar high purity germanium spectrometers. Ni-63 concentrations were measured by liquid scintillation analysis. Elemental nickel carrier yields were measured by ICP-ES, and were used to correct the radioactive nickel species' analyses for any nickel losses from the radiochemical separations.

Cs-137/Cs-134

Aliquots of peroxide fusion dissolution and AQR were analyzed by coaxial high purity germanium gamma-ray spectrophotometers to measure Cs-137 and Cs-134.

Sr-90

Aliquots of peroxide fusion and AQR dissolutions were spiked with an elemental strontium carrier. The strontium species were extracted from the matrix using a crown-ether-based solid

phase extractant. Sr-90 concentrations were measured by liquid scintillation analysis. Elemental strontium carrier yields were measured by neutron activation analysis, and were used to correct the Sr-90 analyses for any strontium losses from the radiochemical separations.

Pm-147/Sm-151

Aliquots of peroxide fusion and AQR dissolution were spiked with an elemental samarium carrier. The promethium and samarium species were extracted from the matrix using a combination of Octylphenyl-N,N-di-isobutyl carbamoylphosphine oxide/tri-n-butyl phosphate (one CMPO/TBP) and di(2-ethylhexyl) orthophosphoric acid (one HDEHP based). Sm-151 and Pm-147 concentrations were measured by liquid scintillation analysis. The matrix was high in Sm-151, but the short-lived Pm-147 component of the material had decayed below noise levels of the analysis. Elemental samarium carrier yields were measured by neutron activation analysis, and were used to correct the analyses for any samarium losses from the radiochemical separations. The separation was designed to extract both Sm and Pm together; a Pm spike was run with the samples to confirm this.

Co-60, Nb-94, Sb-126, Sn-126, Sb-126m, Eu-152, Eu-154, Eu-155, Am-241, Ac-227

Aliquots of peroxide fusion were subjected to a Cs-removal process utilizing Bio Rad AMP-1 resin. The Cs-removed digestates were analyzed by coaxial high purity germanium spectrophotometers to measure the gamma-emitting radionuclides listed above.

Pu-238, 239/240, 241

Aliquots of peroxide fusion and AQR dissolutions were spiked with Pu-236 tracer. The plutonium was extracted from the matrix using thenoyltrifluoroacetone (TTA) following a series of oxidation-state adjustments. The TTA extracts were mounted on stainless steel counting plates and counted for Pu-238 and Pu-239/240 using PIPs detectors. Each separation was traced based on the Pu-236 recovery. Aliquots of sample were also subjected to Cs-removal with Bio-Rad Ammonium Molybdophosphate (AMP) resin and extracted using TEVA columns (TEVA Brand name for one of Eichrom's resins). The Pu-containing extracts were measured by liquid scintillation analysis to determine Pu-241 concentration.

Am-241, 242m, 243, Cm-242, 243, 244, 245, 247, 248, Cf-249, 251, 252

Samples of composite Tank 6F materials were digested using a sodium peroxide fusion. Additionally, a matrix blank and matrix blank spiked with Am-241 and Cm-244 were prepared using Tank 8 simulated sludge. The americium, curium and californium species were extracted from aliquots of peroxide fusion using a CMPO/TBP based solid phase extractant and purified further with an HDEHP based solid phase extractant. Am-241, 243, Cm-243, 245, 247, Cf-249 and 251 concentrations were measured using low energy photon/x-ray, thin-windowed, semi-planar high purity germanium spectrometers. Am-241, Am-242m, Cm-242, 244, Cf-252 concentrations were measured using passivated, implanted, planar silicon (PIPS) alpha spectrometers. Some of the Am, Cm and Cf isotopes were also measured using ICP-MS. Am-241 quantities had been measured from the gamma analyses, all Am, Cm, and Cf results were traced with the Am-241 present in the sample matrix.

U-232

Aliquots of peroxide fusion were spiked with a U-233 radioactive tracer, additional aliquots were run through the method with no tracer added. Uranium was extracted from the matrix using two stages of a diamyl, amyolphosphonate (DAAP)-based solid phase extraction and purified further via co-precipitation with cerium. U-232, U-233, and U-238 activities were measured using passivated, implanted, planar silicon (PIPS) alpha spectrometers. The Tank 6F composite samples were very high in U-234. Hence, U-233 tracers for U-234 (which have the same alpha energy as U-234) were swamped out. U-232/U-238 activity ratios were generated and were multiplied to U-238 activities measured with the ICP-MS to determine U-232 activities in the samples.

Np-237

Aliquots of peroxide fusion dissolution were traced with Np-239 (the daughter of Am-243 which was measured by Cs-removed gamma) and then purified with a quaternary amine based solid phase extraction. The purified aliquots were analyzed by low energy photon/x-ray, thin-windowed, semi-planar high purity germanium spectrometers to yield the Np-239 recoveries and by the ICP-MS to measure Np-237. The Np-237 values were corrected with the decay-corrected Np-239 recoveries.

Tritium

Aliquots of dissolution from the aqua regia digestion were subjected to tritium separations via steam distillation, and aliquots of the tritium-containing distillate were analyzed by liquid scintillation analysis.

Se-79

Samples of composite Tank 6F materials were weighed out, spiked with an elemental selenium carrier and digested in concentrated acid. The selenium species were extracted from the matrix using a combination of resin decontamination, selenium metal precipitation, and TBP-based liquid-liquid extractions. The purified selenium products were analyzed by liquid scintillation to measure Se-79, and by neutron activation analysis to measure elemental selenium carrier yields. The selenium carrier yields were used to correct the Se-79 analyses for any selenium losses from the radiochemical separations.

Tc-99

Tank 6F composite samples were digested in a combination of concentrated nitric and hydrochloric acids. Several matrix blanks were prepared using Tank 8 simulated sludge spiked with a Tc-99 standard. The dissolutions were subjected to a number of resin treatments to reduce dose prior to removal from the shielded cells. The treated samples were then spiked with Tc-99m and the technetium species were extracted from the matrix using an Aliquat-336 based solid phase extractant. Tc-99 concentrations were measured by liquid scintillation analysis. Tc-99m yields were measured with a NaI-well gamma spectrometer, and were used to correct the Tc-99 analyses for any technetium losses from the radiochemical separations. The average recovery of the Tc-99 spiked matrix blank was applied to the entire set of samples to correct for any losses from the decontamination steps used in the shielded cells.

Ra-226

Tank 6F composite samples were digested using a sodium peroxide fusion. Each replicate was prepared in duplicate with the duplicate containing a Ra-224 tracer. Additionally, a matrix blank and matrix spiked blank were prepared using Tank 8 simulated sludge. The Ra-226 was extracted from the matrix using a combination of resin decontamination and ion exchange. The purified Ra-226 was sealed in polypropylene tubes and stored for several daughter Rn-222 half-lives. The Ra-226 progeny daughter isotope Pb-214 was then analyzed for using a high purity germanium well gamma ray spectrophotometer and results were corrected for the tracer Ra-224 recoveries.

Pa-231

Tank 6F composite samples were digested using a sodium peroxide fusion. Each replicate was prepared in duplicate with the duplicate containing a Pa-233 tracer. Additionally, a matrix blank and matrix spiked blank were prepared using Tank 8 simulated sludge. The dissolutions were decontaminated with AMP and quaternary amine based resins. Protactinium species were then extracted from the matrix using a CMPO/TBP based extractant. Pa-233 tracer concentrations were measured using high purity germanium spectrometers to determine separation yields. Pa-231 was measured using the ICP-MS. The Pa-233 tracer yields were decay corrected and then used to correct the Pa-231 analyses for any losses from the radiochemical separations.

I-129

Tank 6F composite samples were dissolved in concentrated acid with an added KI carrier. A matrix blank and matrix blank containing an I-129 spike were also prepared using Tank 8 simulated sludge. Actinide and AMP resins were then added to the mixture to facilitate removal of interfering isotopes. Sodium sulfite is added to the material to reduce the iodine. Silver nitrate is added to the solution to precipitate the iodine as AgI, which is separated via filtration. The filtrate is analyzed for I-129 content using low energy photon/x-ray, thin-windowed, semi-planar, high purity germanium spectrometers. Elemental iodine yields were measured by neutron activation analysis, and were used to correct the I-129 analyses for any iodine losses from the radiochemical separation.

C-14

The solid Tank 6F composite material was used for the C-14 separation and analysis. The material was added to a mixture of sodium hydroxide, and sodium carbonate/sodium hydroxide. A series of oxidation and reduction steps designed to liberate C-14 containing carbon dioxide were carried out, which selectively trapped the C-14 in a basic solution. Finally, C-14 containing carbon dioxide was captured in Carbosorb E and measured by liquid scintillation analysis.

Th-229/230, Ac-227

Tank 6F composite samples were digested using a sodium peroxide fusion. Each replicate was prepared in duplicate with the duplicate containing a Th-229 tracer. Additionally, a matrix blank and matrix spiked blank were prepared using Tank 8 simulated sludge. The matrix spiked blank contained both a Th-228 and Th-229 spike. Thorium was extracted from the matrix using two stages of a quaternary amine based solid phase extraction and purified further via coprecipitation with cerium. Th-227, Th-229 and Th-230 concentrations were measured using passivated, implanted, planar silicon (PIPS) alpha spectrometers. The Th-229 tracer yields were used to correct the various analytes analyses for any thorium losses from the radiochemical separations. Ac-227 activities were calculated from the Th-227 results

Nb-94

Aliquots of peroxide fusion dissolution were spiked with Nb-95 and then purified with an anion exchange. The purified aliquots were analyzed by high purity germanium spectrometers to measure Nb-94 and to measure Nb-95 tracer recoveries. The Nb-94 values were corrected with the stable Nb-95 recoveries.

Zr-93

Zr was extracted from aliquots of peroxide fusion dissolution. Zr-93 levels were measured using the ICP-MS, and the results were yielded from sample stable Zr recoveries as measured by the ICP-MS.

Cs-135

Aliquots of dissolved material (alkali fusion digestion) were purified using a solvent-solvent caustic side solvent extraction-based (CSSX) extraction system. The purified Cs-containing aliquots were analyzed using ICP-MS to measure Cs-135/Cs-133 mass ratios. The Cs-133 and Ba-corrected Cs-135 ratios from the aliquots of separated material were used along with the associated Cs-133 ICP-MS result from the analysis of non-separated material to obtain a value for Cs-135. The Cs-135 result was then converted from ug/g to uCi/g using the specific activity of Cs-135.

Weight Fraction Solids Measurement

The weight percent total solids in each Tank 6F sample were measured in the Shielded Cells using a conventional drying oven at 110 °C. An aliquot of each composite sample was placed in a container. The container was placed in the oven. The weights of the dried sample were checked periodically over 72 hours until two consecutive weights yielded comparable results. The weight fraction solid was calculated by dividing the dry weight of the sample by the initial weight of the sample. A 5% sodium chloride salt solution prepared by dissolving 5 grams of dried sodium chloride in distilled water was used as the reference matrix for weight percent determinations as described above.

Density Measurement

The bulk densities of the “as-received” granular Tank 6F solids were measured using a calibrated syringe tube assembly with graduation markings. With the syringe plunger removed, the syringe was loaded with Tank 6F solids with the help of a spatula to a level of about 2-mL. The plunger was then inserted into the syringe until the tip of the plunger touched the sample matrix, taking care not to excessively compress the sample. The plunger was then slightly pulled back and tapped to ensure the granular solid was uniformly distributed around the internal circumference of the tube. The volume of samples in the tube was read and the weight of the whole syringe assembly including the plunger was determined. A subtraction of the weight of the assembly without the granular samples provided the weight of the granular sample inside the syringe tube. Using the same syringe unit, the plunger was carefully removed and more granular sample was added to the syringe and the new volume and weight of the granular samples determined again. Using different syringe assemblies, this process was repeated three times for each Tank 6F sample.

Appendix C Summary of Statistical Methods

1.0 INTRODUCTION

Sampling has been completed for the characterization of the residual material on the floor of Tank 6F in the F-Area Tank Farm at the Savannah River Site (SRS), near Aiken, SC. The sampling was performed by Savannah River Remediation LLC (SRR) using a stratified random sampling plan with volume-proportional compositing, Broaden¹². The plan consisted of partitioning the residual material on the floor of Tank 6F into three non-overlapping strata: an area of accumulation under Riser 5, a North Area, and a South Area.

Each of three composite samples was constructed from five primary samples of material. A total of 15 primary samples were planned, but one sample, 6-B3a, could not be obtained. The replacement material for the unavailable sample was described by Martin¹⁴. The volume of residual material in each of the three strata was estimated along with an uncertainty of the volume estimate. A separate set of strata volumes was randomly generated for each composite sample from the volume uncertainty distributions, Dean¹. All three strata volumes were converted into volumetric proportions, and subsequently to the mass of residual material to be used from each primary sample for its corresponding composite sample. This procedure directly incorporates the volume uncertainty into the variation among the analyte concentrations in the composite samples, Shine¹⁶. Each composite sample was measured three times for all but a few radionuclide concentrations.

A remote-controlled crawler was designed to collect the sample material. Tank 6F contains an extensive network of cooling coils that fettered movement of the crawler across the tank floor. Consequently, sample locations within strata were selected based on their accessibility to the crawler. However, it is assumed that earlier stages of cleaning/mixing of the material in the tank raised particles off the tank floor, and then deposited them in random locations, so the sample collection was effectively based on random sampling.

2.0 OBJECTIVE AND SCOPE

The objective of this appendix is to perform a statistical analysis of the chemical and isotopic concentration results for the residual material on the floor of Tank 6F. The approach is to use samples representative of the material from the tank floor to estimate the concentrations of analytes in the remaining residual material. The concentration results are summarized by the means and standard deviations of the composite sample concentrations. Upper 95% confidence limits (UCL95s) are calculated for the actual mean concentration of each analyte.

The statistical analyses are applied to a subset of the measured analytes. Table 16 from SRR¹³ lists the analytes to be considered in these analyses.

Table 16 Tank 6F Constituents for Statistical Evaluation

Density	Eu-152	Sb-126	Ag	Mn
Ac-227	Eu-154	Sb-126m	Al	Mo
Am-241	H-3	Se-79	As	Ni
Am-242m	I-129	Sm-151	B	NO ₂ ⁻¹
Am-243	Nb-94	Sn-126	Ba	NO ₃ ⁻¹
Ba-137m	Ni-59	Sr-90	Cd	Pb
C-14	Ni-63	Tc-99	Cl ⁻¹	PO ₄ ⁻³
Cf-249	Np-237	Th-229	Co	Sb
Cm-243	Pa-231	Th-230	Cr	Se
Cm-244	Pu-238	U-232	Cu	SO ₄ ⁻²
Cm-245	Pu-239	U-233	F	Sr
Cm-247	Pu-240	U-234	Fe	U
Cm-248	Pu-241	U-235	Hg	Zn
Co-60	Pu-242	U-236	I	Wt% Solids
Cs-135	Pu-244	U-238		
Cs-137	Ra-226	Y-90		
		Zr-93		

3.0 STATISTICAL METHODS

The material in each composite sample is considered to be representative of all of the residual material on the floor of Tank 6F, and thus the measured concentration for any analyte in a composite sample is considered to be an independent estimate of the actual mean concentration of the analyte in the residual material on the entire tank floor. Three concentration measurements were performed for each analyte on each composite sample. The statistical measurement error model for a concentration measurement result Y_{ij} is

$$Y_{ij} = \mu + s_i + \varepsilon_{ij}, \quad (1)$$

where Y_{ij} is the j -th measured concentration for an analyte in composite sample i , μ is the actual mean analyte concentration for all of the residual material on the floor of Tank 6F, s_i , the sampling error, is a random effect, the difference between the actual mean concentration in composite sample i and the actual mean concentration for all of the residual material on the tank floor that arises from heterogeneity, sampling, sample preparation, and volumetric proportion errors, and ε_{ij} , distributed with mean zero and standard deviation σ , is the difference between concentration measurement j on sample i and the actual mean concentration in composite sample i , $i = 1, 2, 3; j = 1, 2, 3$.

A test for heterogeneity of measurement variance was performed prior to other analyses in order to verify the assumption that the composite sample material is well-mixed and the measurement variance σ^2 is the same for all composite samples. The test procedure is the Levene's test with a Type I family-wise error rate $\alpha = 0.05$. Since the sample sizes are small (no more than three

measurement results per composite sample), a Bonferroni procedure is used to control for spuriously significant results by dividing the 0.05 family-wise¹ error rate by the number of comparisons to obtain the Type I error rate per comparison. The Bonferroni criteria for individual analyte test are $\alpha = 0.05/5 = 0.0100$ for anions, $\alpha = 0.05/18 = 0.0028$ for inorganics, and $\alpha = 0.05/36 = 0.0014$ for radionuclides. If the P-value for an individual constituent test is less than the Bonferroni α , then it is concluded that the laboratory variances are not the same for all of the composite samples.

An analysis of variance (ANOVA) F test was performed in order to determine whether the random effect s_i is warranted in Eqn (1). If the F test results indicate a statistically significant sampling error s_i at a level of significance $\alpha = 0.05$, then Eqn (1) becomes the basis for estimating the true mean concentration in the residual material; if the ANOVA F test result is not statistically significant, then the random effect s_i is not needed and Eqn (1) reduces to the following:

$$Y_{ij} = \mu + \varepsilon_{ij}, \quad (2)$$

where there is no sampling error term s_i in the model.

If all of the concentration measurements for an analyte are above detection, then the ANOVA F test can be performed, and a decision made to use the model in Eqn (1) with the random effect if $F \geq F_{0.95,2,6} = 5.14325$, and to use the model in Eqn (2) without the random effect if $F < F_{0.95,2,6} = 5.14325$. When $F \geq F_{0.95,2,6} = 5.14325$, the UCL95 for the actual mean tank concentration is given by

$$UCL_{95\%} = \bar{Y}_{..} + t_{0.95,2df} \cdot \sqrt{\frac{MS_{Sample}}{9}}, \quad (3)$$

where $\bar{Y}_{..}$ is the sample mean concentration of the nine concentration measurement results, and MS_{Sample} is the estimate of the mean square for the random effect s_i in the model in Eqn (1), where

$$MS_{Sample} = \frac{\sum_{i=1}^3 \frac{Y_i^2}{3} - \frac{Y_{..}^2}{9}}{6}, \quad (4)$$

and Y_i and $Y_{..}$ are the total of the three measured concentration results for composite sample i , $i = 1, 2, 3$ and the total of the nine measured concentration results for all three composite samples.

¹ A family-wise error rate refers to the error rate of making at least one Type I error (rejecting the null hypothesis when it is true) in a prescribed family or set of tests, where family refers to all analytes in the set of all inorganic constituents, the set of all radionuclides, or the set of all anions. Controlling the family-wise error rate means that the probability of making at least one Type I error for individual analytes in a family will be no more than a stated α probability.

The estimated standard error of the mean concentration is the square root of the $(MS_{Sample}/9)$ when all composite samples have three measurements. Tables 21 and 22 provides a more general formula for the estimated standard error of the mean when the composite samples have been measured different numbers of times.

When $F < F_{0.95,2,6} = 5.14325$, the UCL95 for the actual mean tank concentration is given by

$$UCL_{95\%} = \bar{Y}_{..} + t_{0.95,9-1df} \cdot \sqrt{\frac{s^2}{9}}, \quad (5)$$

where s is the sample standard deviation of all nine measured concentration results.

The above procedures are appropriate if the data or a transform of the data approximately follow the normal distribution. Figure 3 presents a sequence of goodness-of-fit tests to identify a distribution consistent with the measurement results and select an estimation method for the mean, standard deviation, and UCL95. Studies by Singh, Singh, and Englehardt¹⁷ demonstrated that using the coefficient of variation (the percent standard deviation) is much less effective than using a formal goodness-of-fit test to determine whether the concentration measurements are consistent with a particular distribution such as the normal distribution. Consequently, the normal distribution assumption is tested by the Wilk-Shapiro (W-S) goodness-of-fit test at an $\alpha = 5\%$ level of significance. If the W-S statistic is less than the W-S critical value, then normality is rejected; if there is no statistically significant departure from normality, the mean, standard deviation, and UCL95 are estimated based on a normal distribution.

If the normal distribution assumption is rejected by the W-S test, then the measurements are tested to determine whether they are consistent with a skewed distribution. This report adopts the strategy in Singh, Armbya, and Singh¹⁸ to test for the gamma distribution prior to the lognormal distribution. The gamma distribution assumption is tested using Anderson-Darling (A-D) goodness-of-fit statistic. If the A-D statistic exceeds the A-D critical value then the gamma distribution assumption is rejected; if there is no statistically significant departure from the gamma distribution, the mean, standard deviation, and UCL95 are determined based on a gamma distribution. If the gamma distribution is rejected, but a plot of the concentration results versus the theoretical gamma quantiles displays a linear pattern with high correlation (over 95%), then the results are said to follow an approximate gamma distribution. The mean, standard deviation, and UCL95 are estimated assuming a gamma distribution, according to Singh, Armbya, and Singh¹⁸.

Finally, if the gamma distribution is rejected and the gamma quantile plot does not exhibit high correlation (>95%), then the W-S goodness-of-fit test is used to determine if the measurements are consistent with the lognormal distribution. If the W-S statistic is less than the W-S critical value, then the lognormal assumption is vacated and a nonparametric approach to estimation is adopted; if the W-S test determines that the lognormal distribution is plausible, then the lognormal distribution is adopted. Appropriate UCL95s based on the lognormal distribution and the nonparametric Chebyshev UCL95 for use when the lognormal distribution is rejected are documented by Singh, Singh, and Englehardt¹⁷.

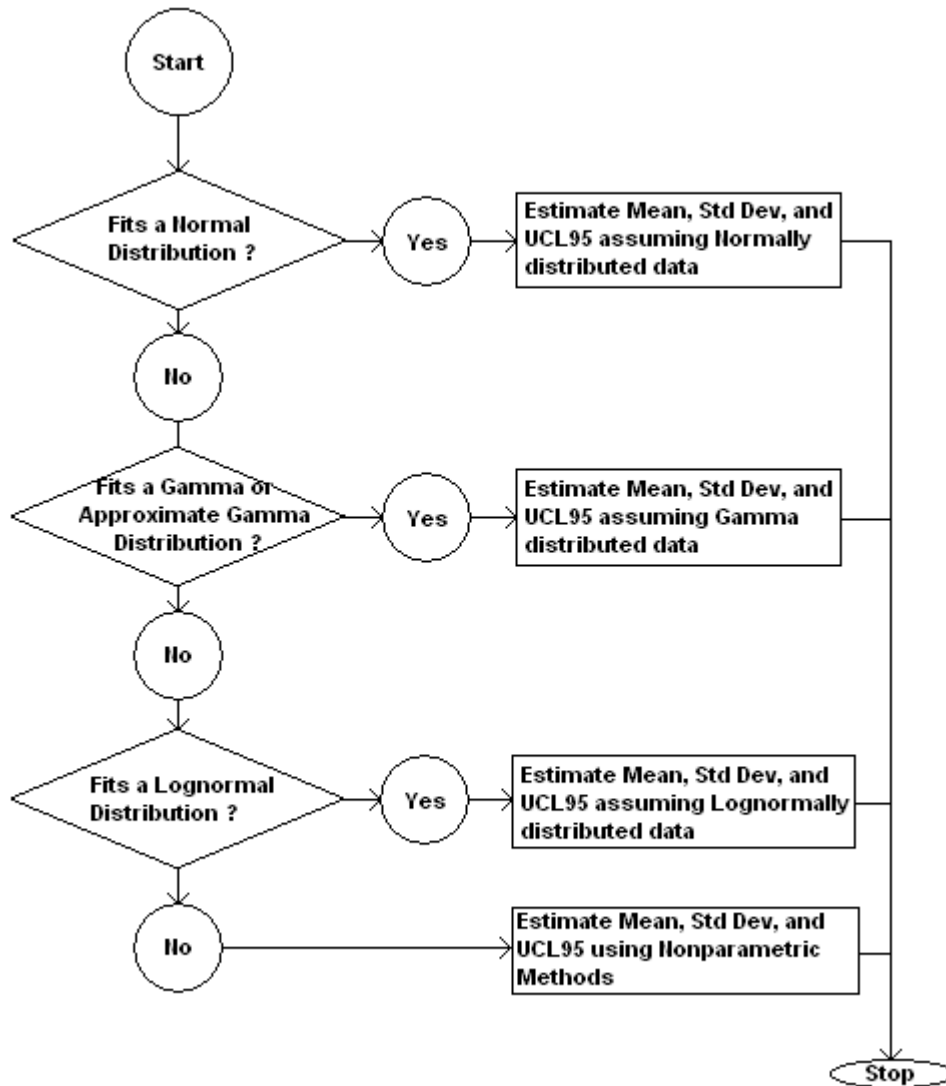


Figure 3. Sequence of Goodness-of-Fit Tests to Identify a Distribution and Select an Estimation Method

Heterogeneity and ANOVA tests were performed in SAS JMP® 9.0.0 software from SAS Institute, Inc.¹⁵, and distribution plotting, goodness-of-fit tests, and parameter estimation were performed in ProUCL 4.1.01¹⁸ software developed by Singh, Armbya, and Singh¹⁸. P-values for the Wilk-Shapiro goodness-of-fit tests were obtained from SAS JMP® 9.0.0 software. Software validation and verification for SAS JMP® 9.0.0 and ProUCL 4.1.01 are documented by Baker and Others¹¹.

The examination of the data for outliers is highly important. This can be done visually by examining graphs, but a statistical test can provide a good basis for deciding whether a concentration result conforms to the pattern of the rest of the data. Outliers were assessed graphically and by the Dixon Q test, Steel and Torrie, applied to the concentration data. The

Dixon Q test was performed by the ProUCL 4.1 software application written by Singh, Armbya, and Singh, A.K. [2010]. The null hypothesis of the Q test is that there is no outlier. Rejecting the null hypothesis at a 5% level of significance is evidence that a concentration result does not appear to conform to the general pattern of the rest of the concentration data. When the model contains a sampling term, the Dixon test is applied to the Studentized residuals from the sampling model¹⁹.

4.0 STATISTICAL ANALYSIS

The statistical analyses are based on the measurement results presented in Tables 7, 8, and 9 for anions, Tables 10, 11, and 12 for inorganic constituents, and in Tables 13, 14, and 15 for radionuclides. Composite Sample Bulk Densities (g/mL) were obtained from Table 4 and Weight Percent Solids (Wt%) were obtained from Table 6. The following subsections describe the application of the statistical methods described in Section 3.0. None of these measurement results were below their minimum detectable concentrations (MDCs).

4.1 Analysis of Density, Weight Percent Solids, and Anion Concentrations

Density, Weight Percent Solids, and six anions were included in the key list of constituents for statistical analyses. Detailed tables are presented in Appendix C Table 17.

Results for anions Cl-1, F, and PO4-3 were below their MDCs. The minimum and maximum MDCs for each of these analytes is reported in Table 18.

Levene's test for heterogeneity of variance was applied to the density, weight percent solids, and anion results with family-wise $\alpha = 0.05$. Referring to Table 17, the Levene's test is not statistically significant ($P\text{-value} > \alpha = 0.0100$) for density, weight percent solids, or any anion concentration. Therefore, the tests to determine whether there is variance among the composite samples will be performed using an ANOVA (which assumes a constant measurement error variance). The ANOVA F-test was statistically significant ($P\text{value} < \alpha = 0.05$) for density, weight percent solids, and NO2-1. Consequently, the model in Eqn (1) with the sampling error was adopted for those measurements. Their UCL95s are based on the one-sided upper Student's t confidence interval. The ANOVA F-Test was not statistically significant for NO3-1 and SO4-2. ProUCL 4.1 software was used to determine an appropriate distribution and UCL95 NO3-1 and SO4-2. Table 19 summarizes the results for the UCL95s.

4.2 Analysis of Inorganic Constituents

The inorganic constituents that are analyzed in this report are listed in Table 16. Figure 4 displays scatterplots of all pairs of inorganic constituents with Composite Samples 1, 2, and 3 shown as red, blue, and black circles, respectively. The three replicate measurements for each composite sample are identified by their run number (1, 2, or 3) in Figure 4. An overall picture emerges across all inorganic constituents that Composite Sample 1 tends to exhibit the lowest concentrations, Composite Sample 3 tends to show the highest concentrations, while Composite Sample 2 tends to have intermediate concentrations.

In Section 7.2 Statistical Tables for the Inorganic Constituents, Levene's test for heterogeneity of variance was applied to each inorganic constituent with $\alpha = 0.0028$. Based on Bonferroni's procedure, Alt¹⁰, this yields a tolerance of no more than 0.05 for the probability of at least one Type I error. The P-values for Levene's test are given in Table 20. None of these constituents have a statistically significant test result for heterogeneity of variance. Therefore, the following test to determine whether there is a variance among the composite samples will be performed using an ANOVA (which assumes a constant measurement error variance).

Each inorganic constituent was also subjected to an ANOVA test to determine if a sampling variance should be included in the model. As seen by the ANOVA P-values in Table 20, all inorganic constituents except Hg and Mo have statistically significant sampling variances.

The only potential outliers in the set of inorganic measurements appear to be one Hg measurement on Run 1 of Composite Sample 1 and one Mo measurement on Run 1 of Composite Sample 3. They do not align along the linear path traced by the other measurements in Figure 4 plots. The other two Hg measurements on Composite Sample 1 are consistent with all of the other Hg measurements on Composite Samples 2 and 3, and the other two Mo measurements on Composite Sample 3 are consistent with all of the other Mo measurements on composite Samples 1 and 2. The magnitudes of the differences among the Hg and MO results may not have practical significance. No numerical correlations are shown since there are only three composite samples.

Removing both of these potential outliers from the database, reduces the variability and results in statistically significant sampling variances, as was the case for all other inorganics. The computations for UCL95s for Hg and Mo when the potential outliers are omitted are detailed in Tables 21 and 22, respectively. It is recommended to remove the Hg and Mo outliers. Doing so results in more conservative (larger) UCL95s, and all inorganic results with measurements above their MDCs exhibit heterogeneity.

Several inorganics, Ag, As, B, Sb, and Se, had all measurements reported below their MDCs. Their minimum and maximum MDCs are given in Table 23. Table 24 provides a listing of UCL95s for the inorganics with results above their MDCs. The UCL95 results for Hg and Mo with and without their potential outliers are given in Table 24. It is recommended that the results without the potential outliers be used, since (1) those results are about the same or more conservative (higher UCLs) than those with all of the data and (2) the sampling error model obtained without the potential outliers is consistent with all of the other inorganics.

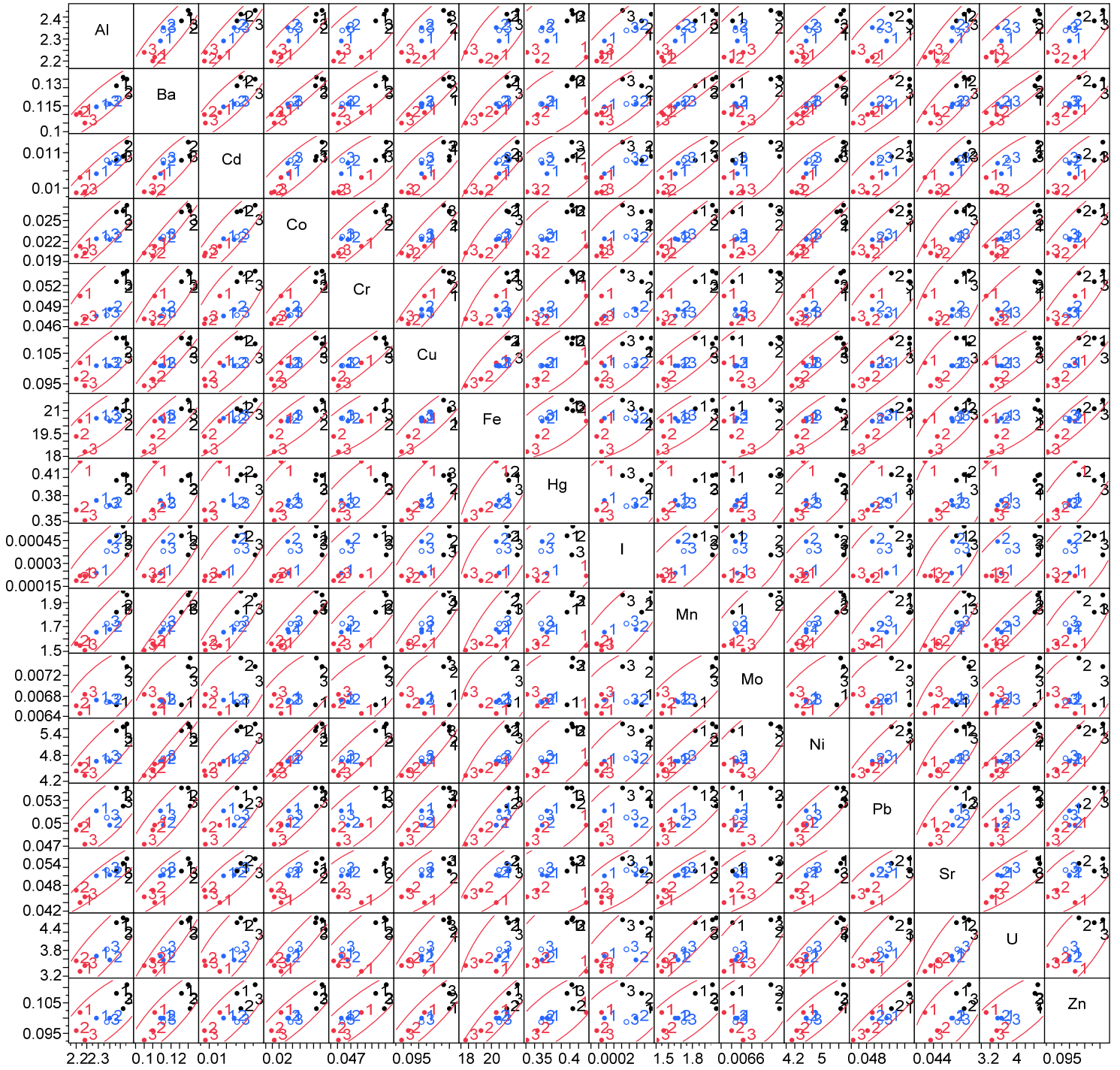


Figure 4. Scatterplots for the Inorganic Constituents
(Legend: Composite Samples 1 = red, 2 = blue, and 3 = black)

4.3 Analysis of Radionuclides

The radionuclides that are analyzed in this report are listed in Table 16. Figure 5 displays scatterplots of a subset of all pairs of radionuclides since there were too many to effectively plot. Composite Samples 1, 2, and 3 are shown as red, blue, and black circles, respectively. The three replicate measurements for each composite sample are not uniquely identified in Figure 5. Sample 3 has the highest measured concentrations of radionuclides as well as for inorganic constituents. There is no consistent pattern of higher and lower concentrations for Composite Samples 1 and 2 as was seen with the inorganic constituents.

In Table 25, Levene's test for heterogeneity of variance was applied to each radionuclide with an $\alpha = 0.0014$ for each comparison. Using the Bonferroni's approach to multiple comparisons in Alt¹⁰, this yields a tolerance of no more than 0.05 for the probability of at least one Type I error among the radionuclides. The P-values for Levene's test are given in Table 25 for each of the radionuclides. None of these radionuclides has a statistically significant test result for heterogeneity of variance. Therefore, each radionuclide was also subjected to an ANOVA test to determine if a sampling variance should be included in the model. As seen by the ANOVA P-values in Table 25, only ten radionuclides have statistically significant sampling variances.

Twelve radionuclides had all measurements below their MDCs. The minimum and maximum MDCs for each of these radionuclides is given in Table 26. The estimated mean, estimated standard error of the mean, and the UCL95 for all radionuclides with measurements above their MDCs is given in Table 27. The UCL95s for those radionuclides that had the No Sampling Error model type were computed in ProUCL 4.1 software. Table 27 lists the resulting distribution and values for the UCLs.

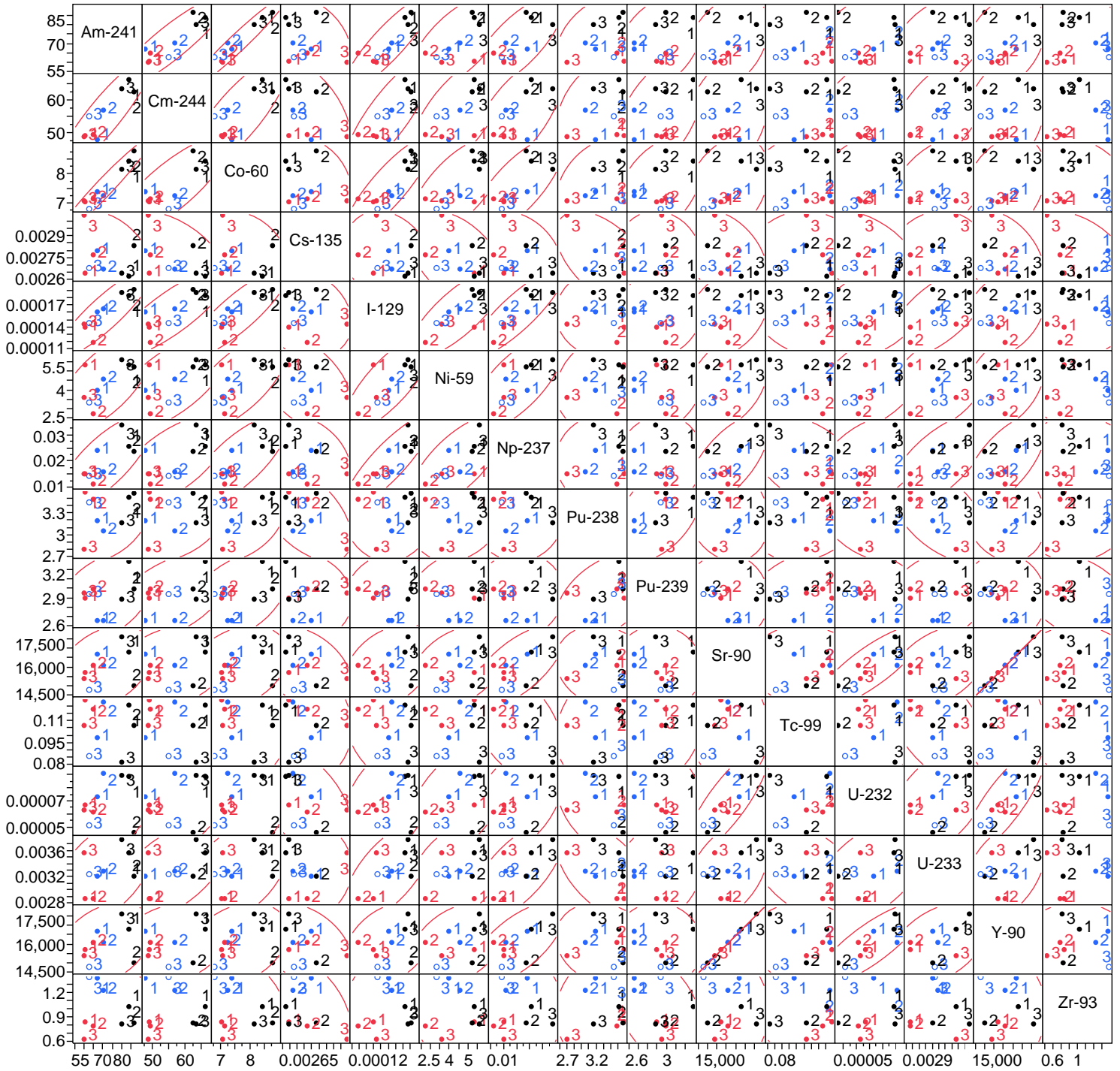


Figure 5. Scatterplots for a Subset of the Radionuclides
(Legend: Composite Samples 1 = red, 2 = blue, and 3 = black)

5.0 CONCLUSIONS AND RECOMMENDATIONS FOR THE STATISTICAL APPENDIX

This appendix documents the statistical summary of the Tank 6F floor composite sample results.

The estimated mean concentration, the estimated standard error of the mean concentration, and the UCL95 for the bulk densities, the weight percent solids, and the anion concentrations with measurements above their MDCs are summarized in Table 19. Those anions without results above their MDCs were listed in Table 18 along with their minimum and maximum MDCs.

All of the inorganic constituents displayed heterogeneity as evidenced by the ANOVA results. The inorganic results demonstrated consistent differences across the composite samples: lowest concentrations for Composite Sample 1, intermediate-valued concentrations for Composite Sample 2, and highest concentrations for Composite Sample 3. The Hg and Mo results suggest possible measurement outliers. However, the magnitude of the difference between the Hg UCL95 results with and without the Hg outlier and the magnitude of the difference between the Mo UCL95 results with and without the Mo outlier do not appear to have practical significance. It is recommended to remove the potential measurement outliers. Omitting the outliers is conservative in the sense of producing a higher UCL95 for Hg and Mo than if the potential outliers were included in the calculations. The estimated mean, estimated standard deviation, and the UCL95 for each inorganic constituent are summarized in Table 24.

In contrast to the inorganic results, most of the radionuclides did not demonstrate heterogeneity among the composite sample results. The estimated mean concentrations, the estimated standard errors of the mean concentrations, and the UCL95s for the radionuclide mean concentrations are summarized in Table 27.

6.0 REFERENCES FOR THE STATISTICAL APPENDIX

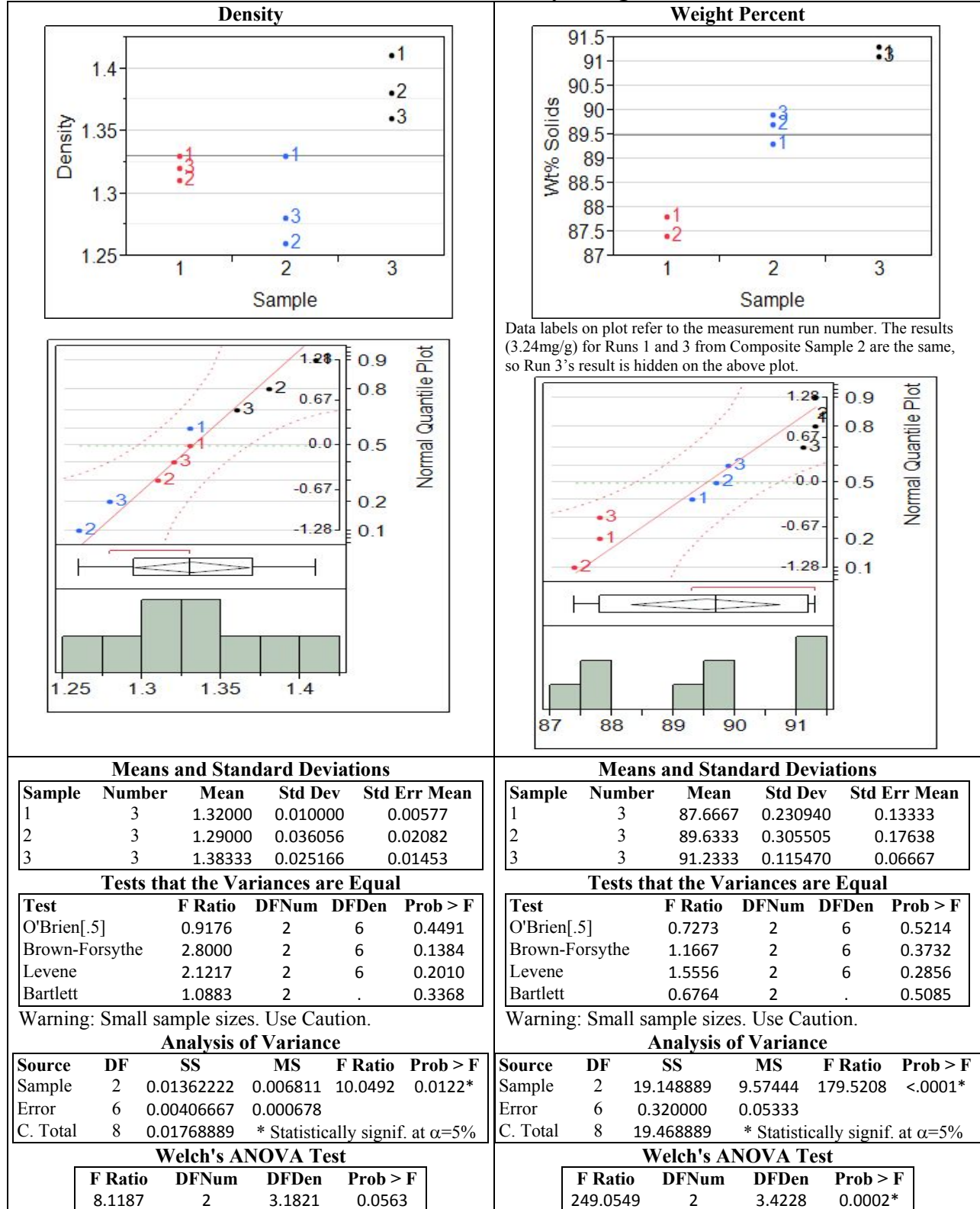
- [1982] Alt, F.B. "Bonferroni Inequalities and Intervals," in Kotz, S. and Johnson, N.L. **Encyclopedia of Statistical Sciences**, John Wiley and Sons, NY.
- [2012] Baker, R.A.; Edwards, T.B.; Harris, S.P.; Harvel, C.D.; and Shine, E.P. "Verification and Validation for Commercial Statistical Packages Utilized by Applied Computational engineering and Statistics," B-VVR-A-00002, Revision 1 (May).
- [2011] Broaden, D.A. "Tank 6F Sampling and Analysis Plan," Savannah River Remediation LLC SRR-LWE-2010-00300, Revision 1 (January 5).
- [2012] SRR. "Tanks 5 and 6 – TTR, Rev. 7 (June 7, 2012)
- [2011] Martin, B.A. *Justification for Adjustments to the Tank 6F Sample Plan*, Revision 0, SRR-CWDA-2011-00159, Aiken, SC, October 2011.
- [2010] SAS Institute, Inc. **Basic Analysis and Graphing**, JMP 9.0.0 On-line Help Books, Cary, NC.
- [2011] Shine, E.P. "Technical Review of the Method of Constructing Composite Samples with Uncertain Volumetric Proportions," SRNL-STI-2011-00323, May 24.

17. [1997] Singh, A.K.; Singh, A; and Englehardt, M. “The Lognormal Distribution in Environmental Applications,” EPA/600/S-97/006 (December).
18. [2010] Singh, A.; Armbya, N.; and Singh, A.K. “ProUCL Version 4.100 Technical Guide (Draft)” US EPA/600/R-07/041 (May).
19. [1980] Steel, R.D. and Torrie, J.H. **Principles and Procedures of Statistics: a Biometrical Approach**, Second Edition, McGraw-Hill Publishers.

7.0 SUPPORTING STATISTICAL TABLES

The statistical tables supporting the results discussed in Section 4 are presented in Section 7.

APPENDIX C: STATISTICAL RESULTS FOR ANIONS
Table 17 Tests and Estimators for Density, Weight Percent, and Anions



APPENDIX C: STATISTICAL RESULTS FOR ANIONS

Table 17 Tests and Estimators for Density, Weight Percent, and Anions

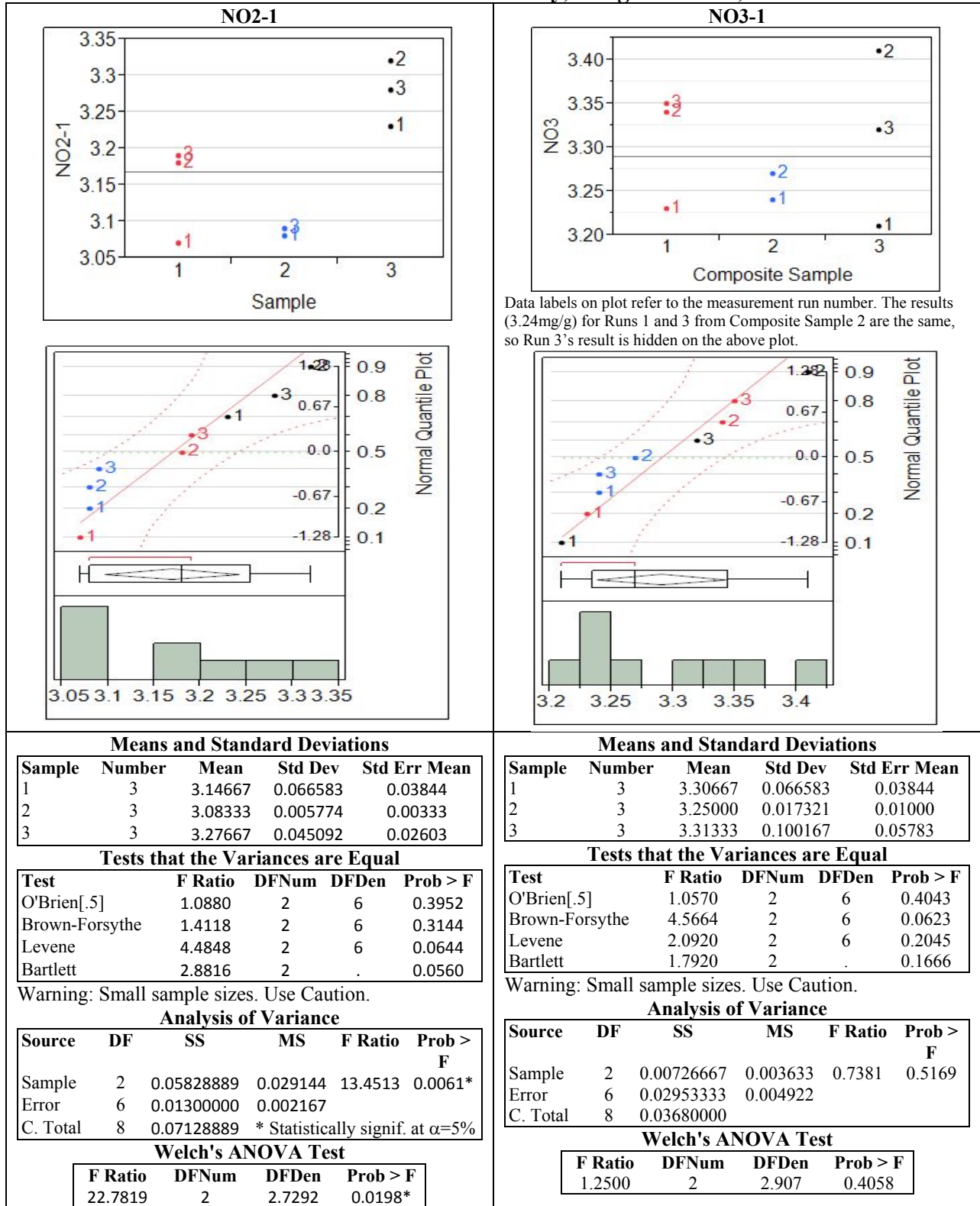
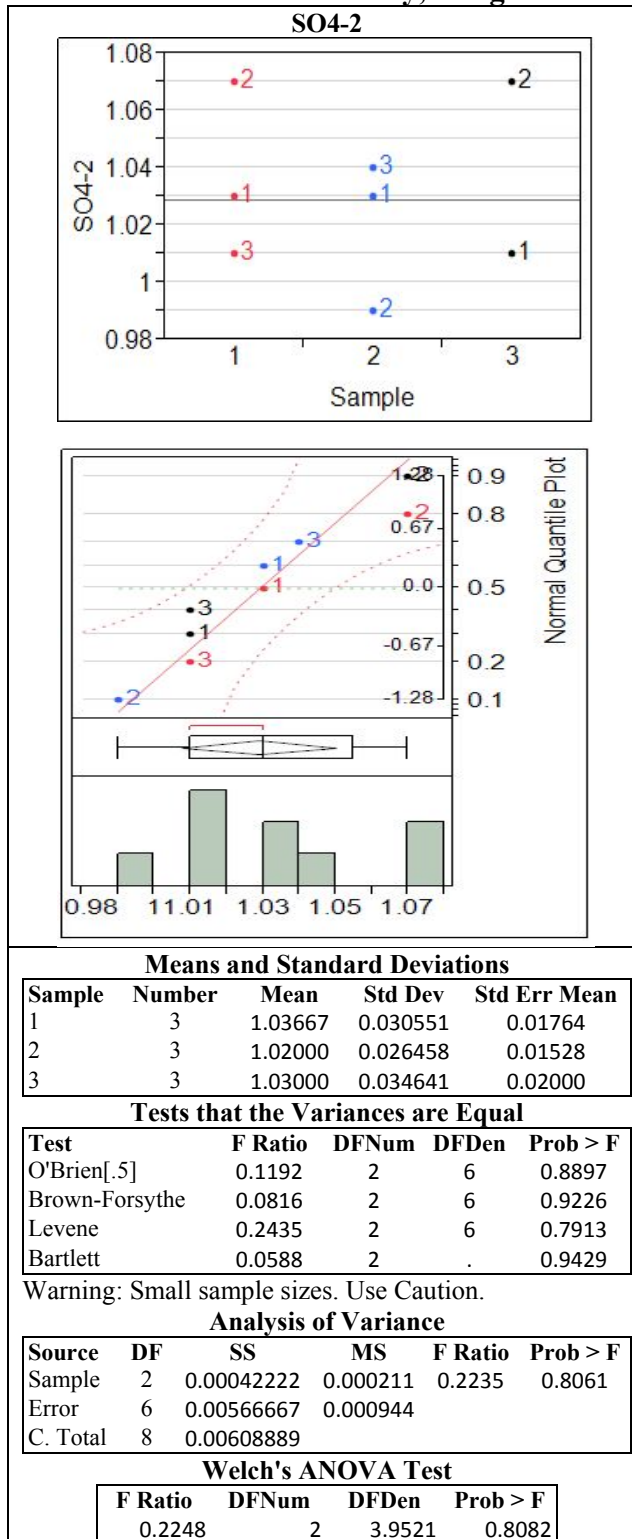


Table 17 Tests and Estimators for Density, Weight Percent, and Anions



APPENDIX C: STATISTICAL RESULTS FOR DENSITY, WEIGHT PERCENT, AND ANIONS

Table 18 Anion and Tritium Concentrations less than their MDCs

	MDCs	
	Min	Max
Cl-1	4.00E-02	4.00E-02
F-1	4.00E-02	4.00E-02
PO4-3	4.00E-02	4.00E-02

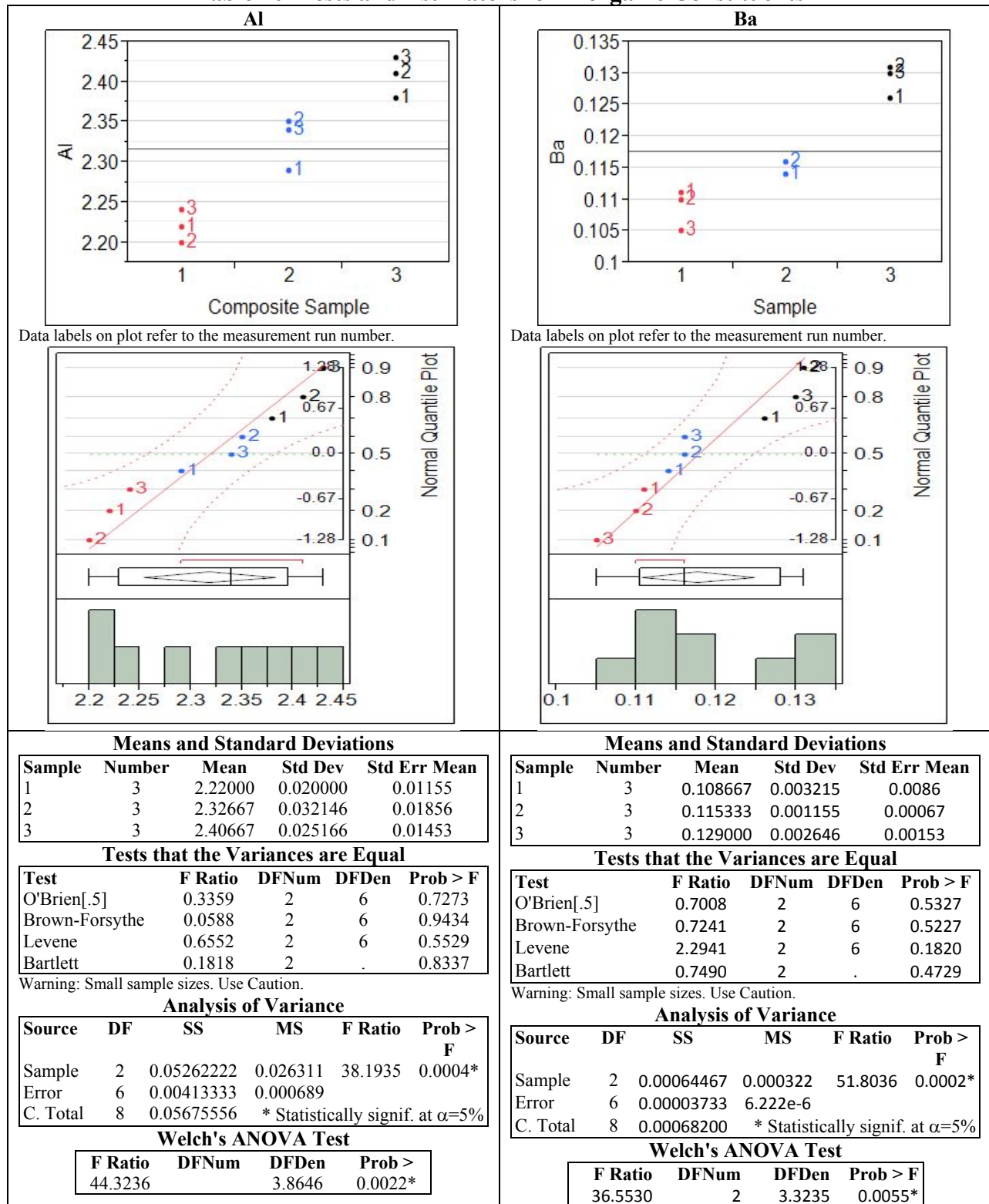
Table 19 95% UCLs for Mean Density, Weight Percent Solids, and Anion Concentrations (mg/g)

Anion	Model Type	N	Mean	Standard Deviation	Percent Std Deviation	UCL95	Notes
Density	Sampling Error	9	1.331e+0	5.217e-2	3.9%	1.411e+0	Normal
Weight % Solids	Sampling Error	9	8.951e+1	1.796e+0	2.0%	9.252e+1	Normal
NO2-1	Sampling Error	9	3.169e+0	1.056e-1	3.3%	3.335e+0	Normal
NO3-1	No Sampling Error	9	3.290e+0	6.782e-2	2.1%	3.332e+0	Normal: Student's t
SO4-2	No Sampling Error	9	1.029e+0	2.759e-2	2.7%	1.046e+0	Normal: Student's t

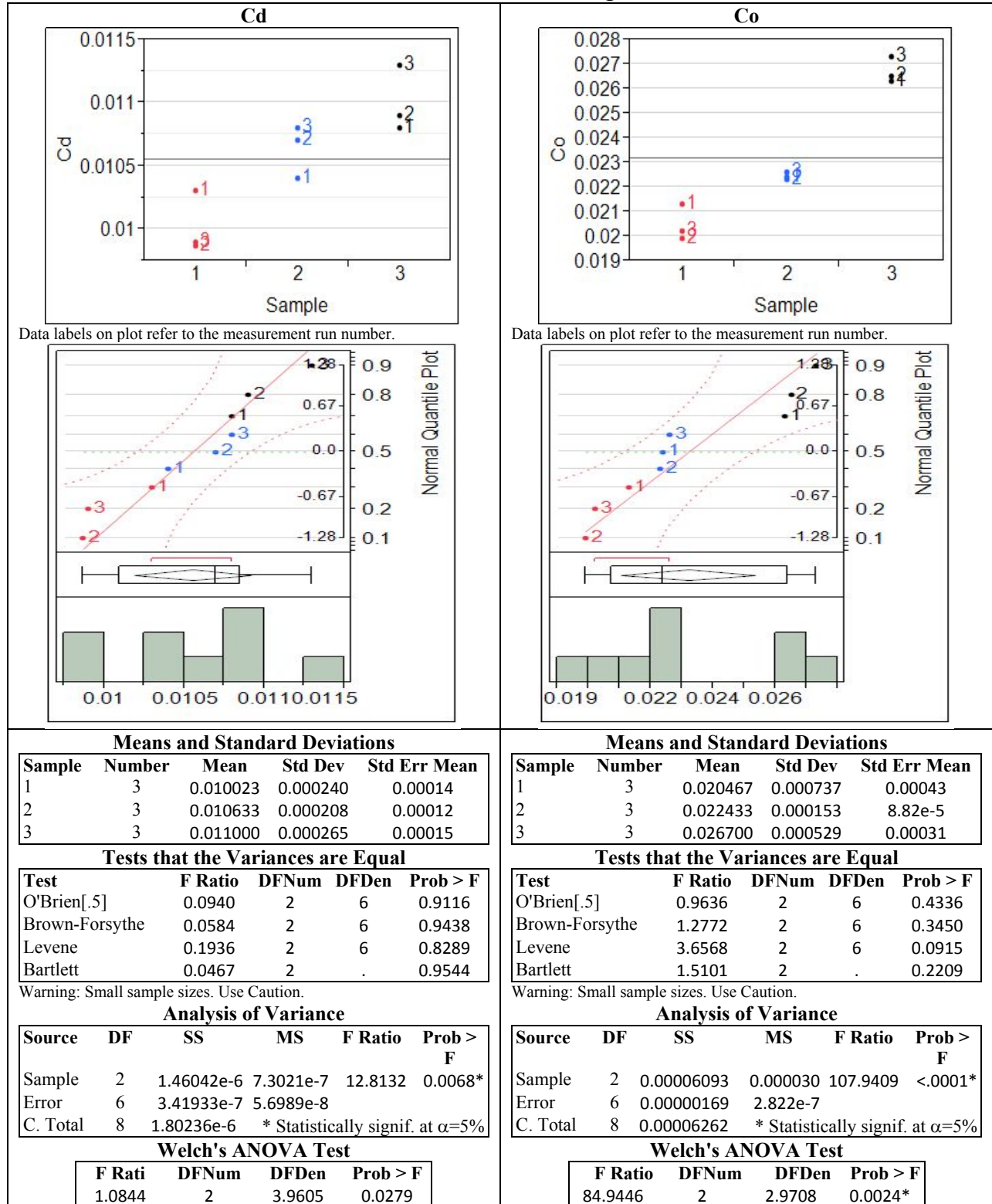
Notes: The distribution of NO3 conforms to a normal distribution based on a Wilk-Shapiro goodness of fit test (P-value = 0.3982 > α = 0.05). The UCL95 was based on a Student's t confidence limit as recommended in the ProUCL software guidance.

APPENDIX C: STATISTICAL RESULTS FOR INORGANIC CONSTITUENTS

Table 20 Tests and Estimators for Inorganic Constituents

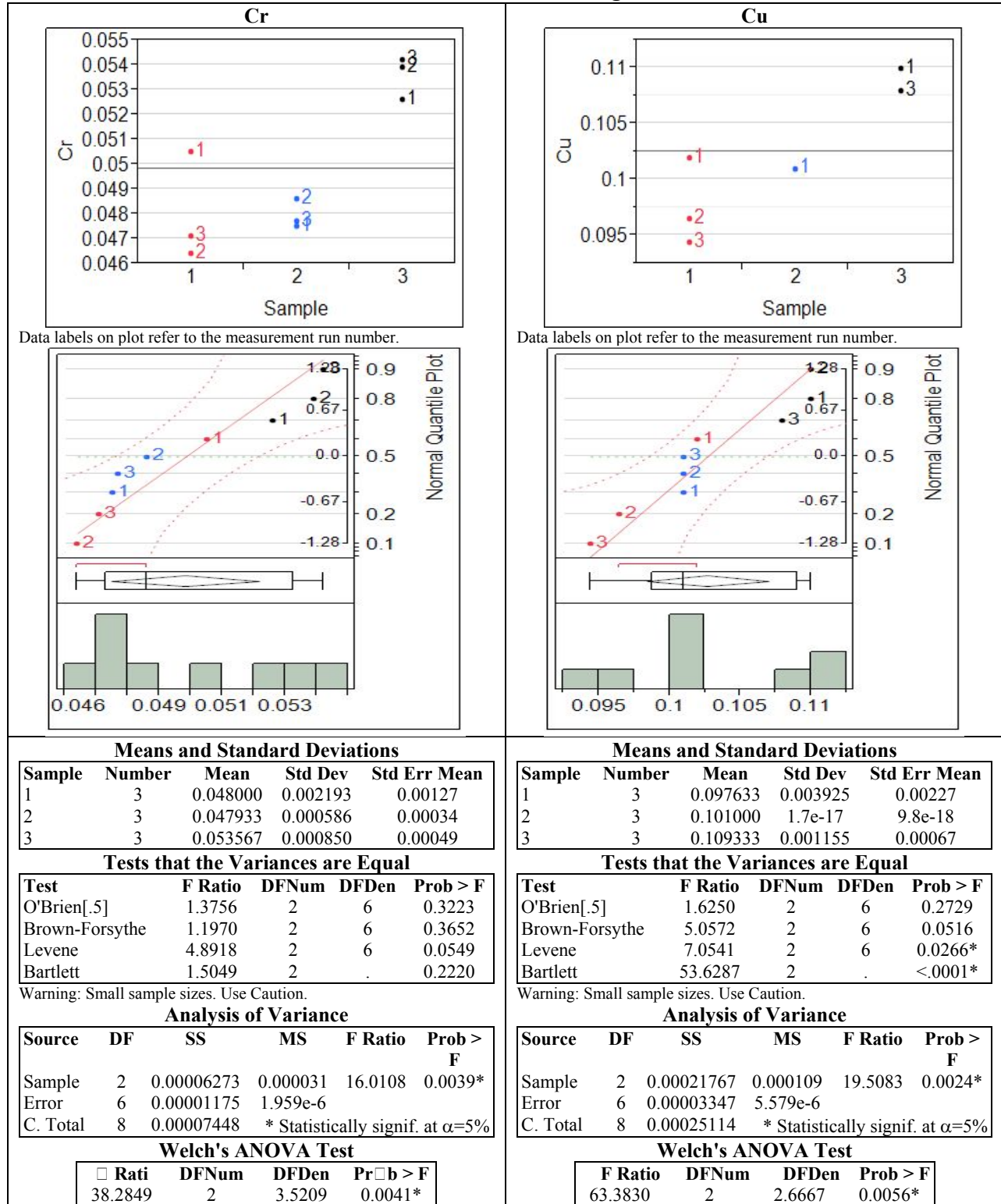


APPENDIX C: STATISTICAL RESULTS FOR INORGANIC CONSTITUENTS
Table 20 Tests and Estimators for Inorganic Constituents

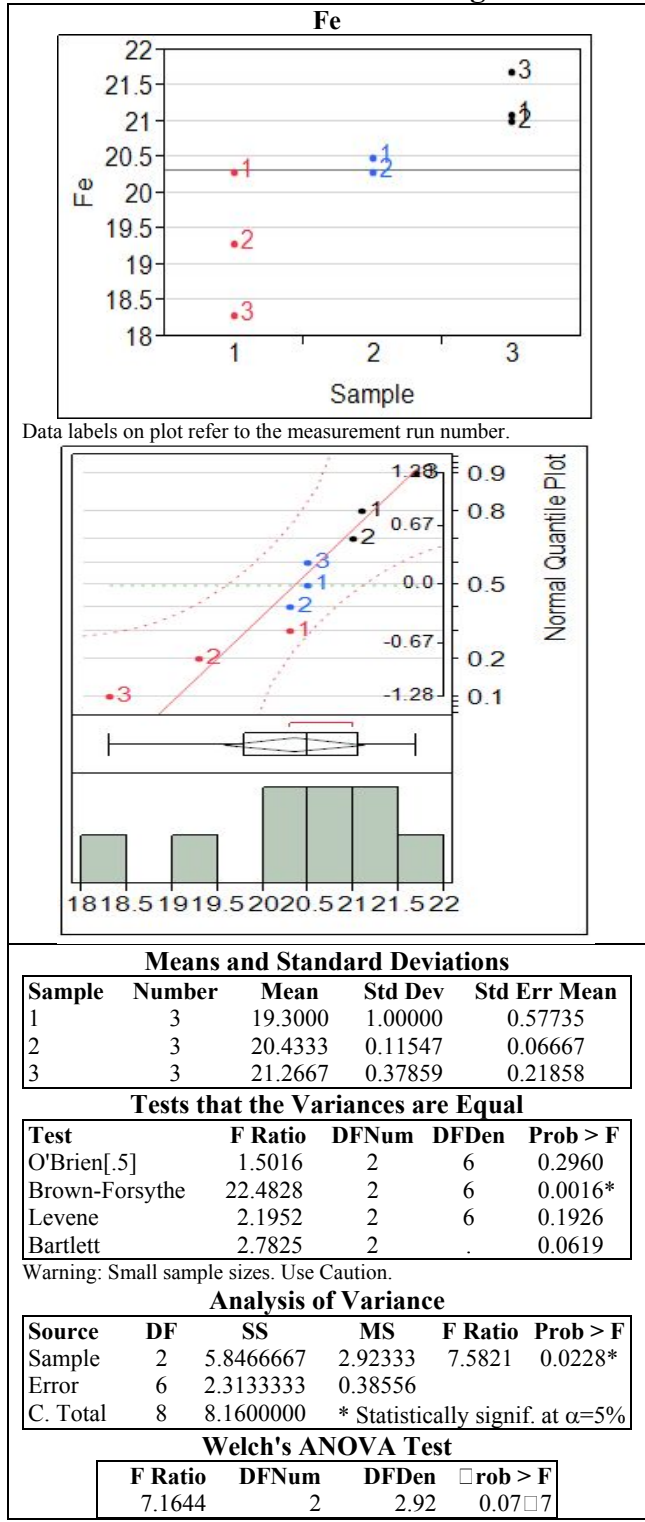


APPENDIX C: STATISTICAL RESULTS FOR INORGANIC CONSTITUENTS

Table 20 Tests and Estimators for Inorganic Constituents

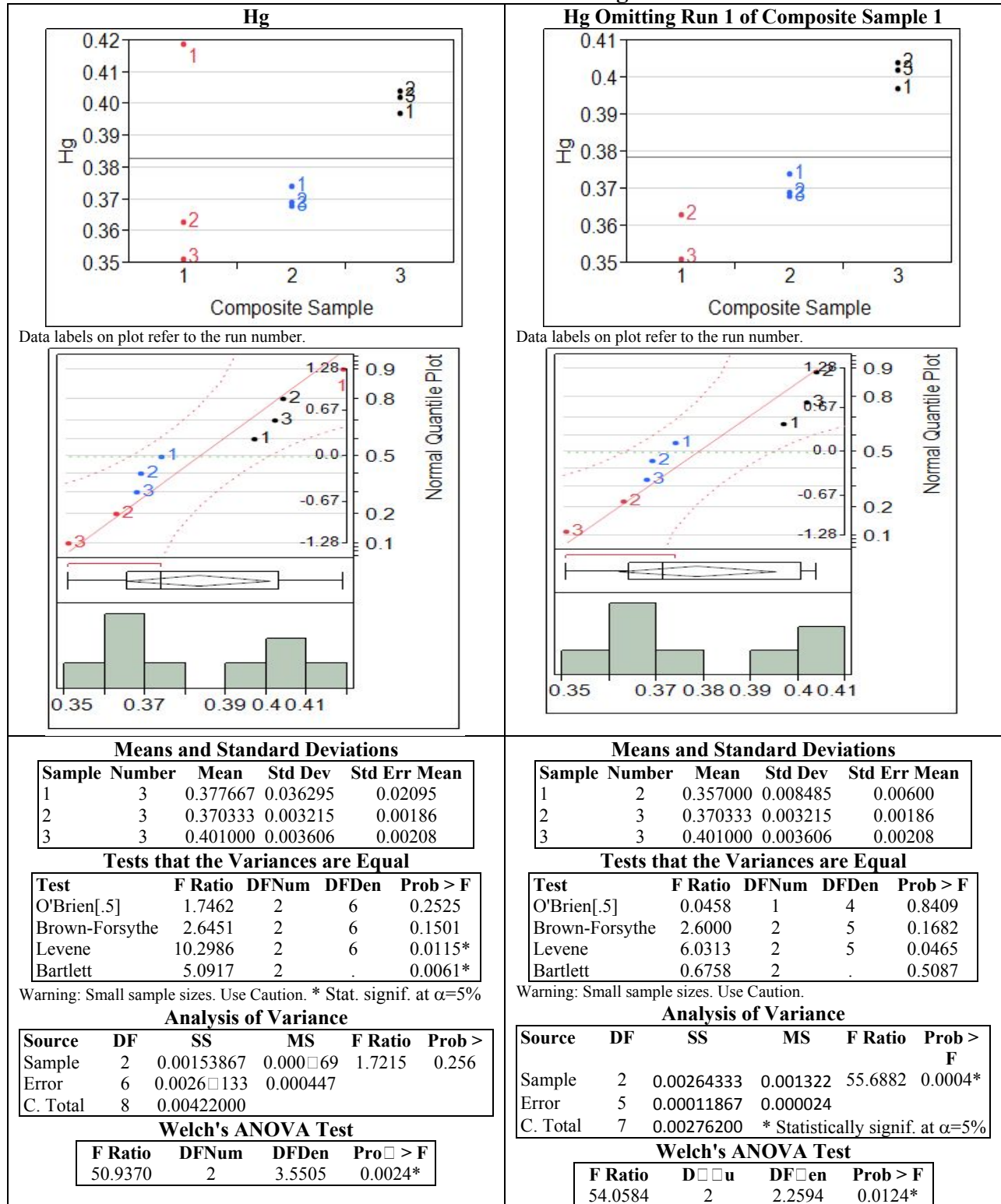


APPENDIX C: STATISTICAL RESULTS FOR INORGANIC CONSTITUENTS
Table 20 Tests and Estimators for Inorganic Constituents



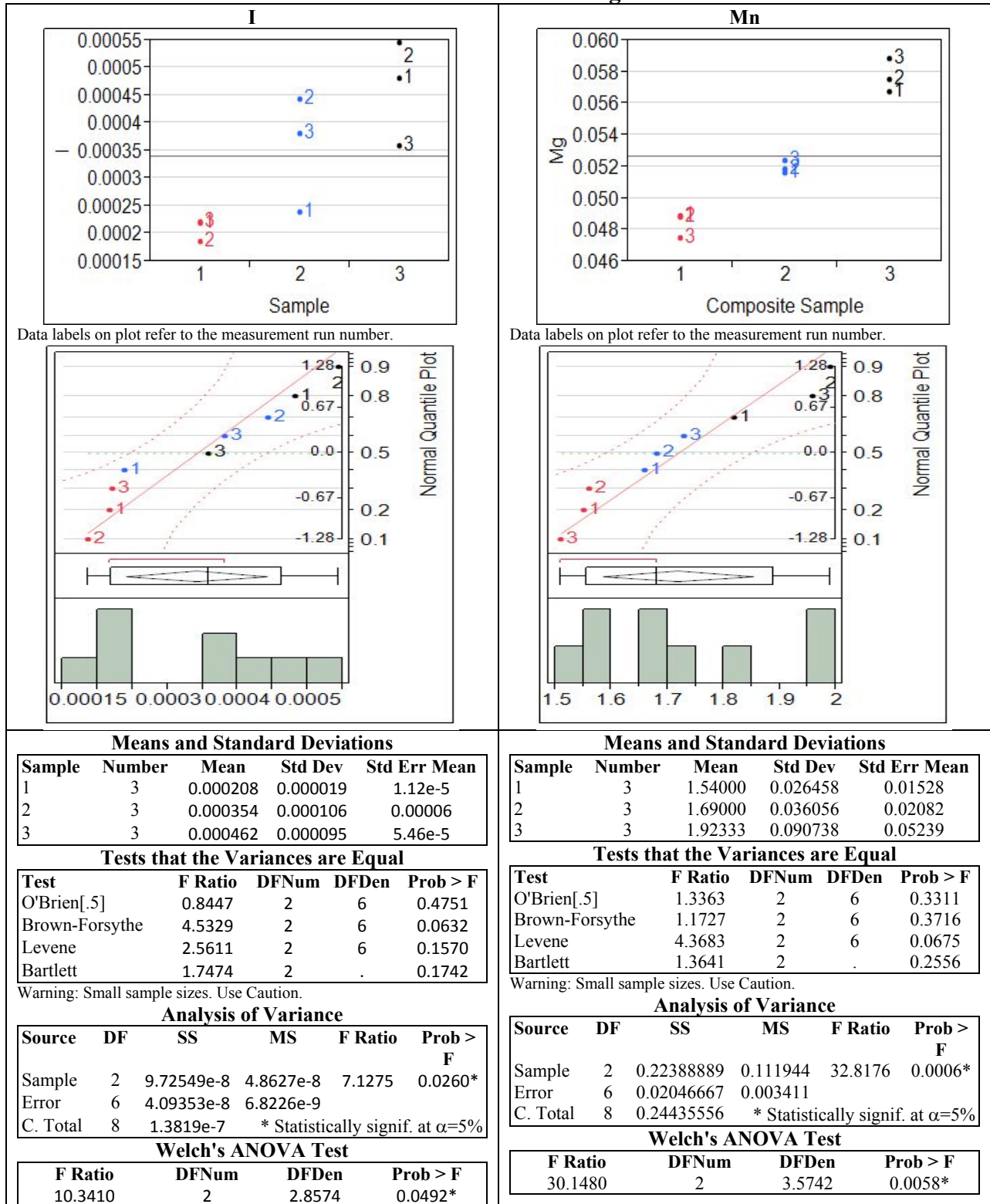
Appendix C: Statistical Results for Inorganic Constituents

Table 20 Tests and Estimators for Inorganic Constituents



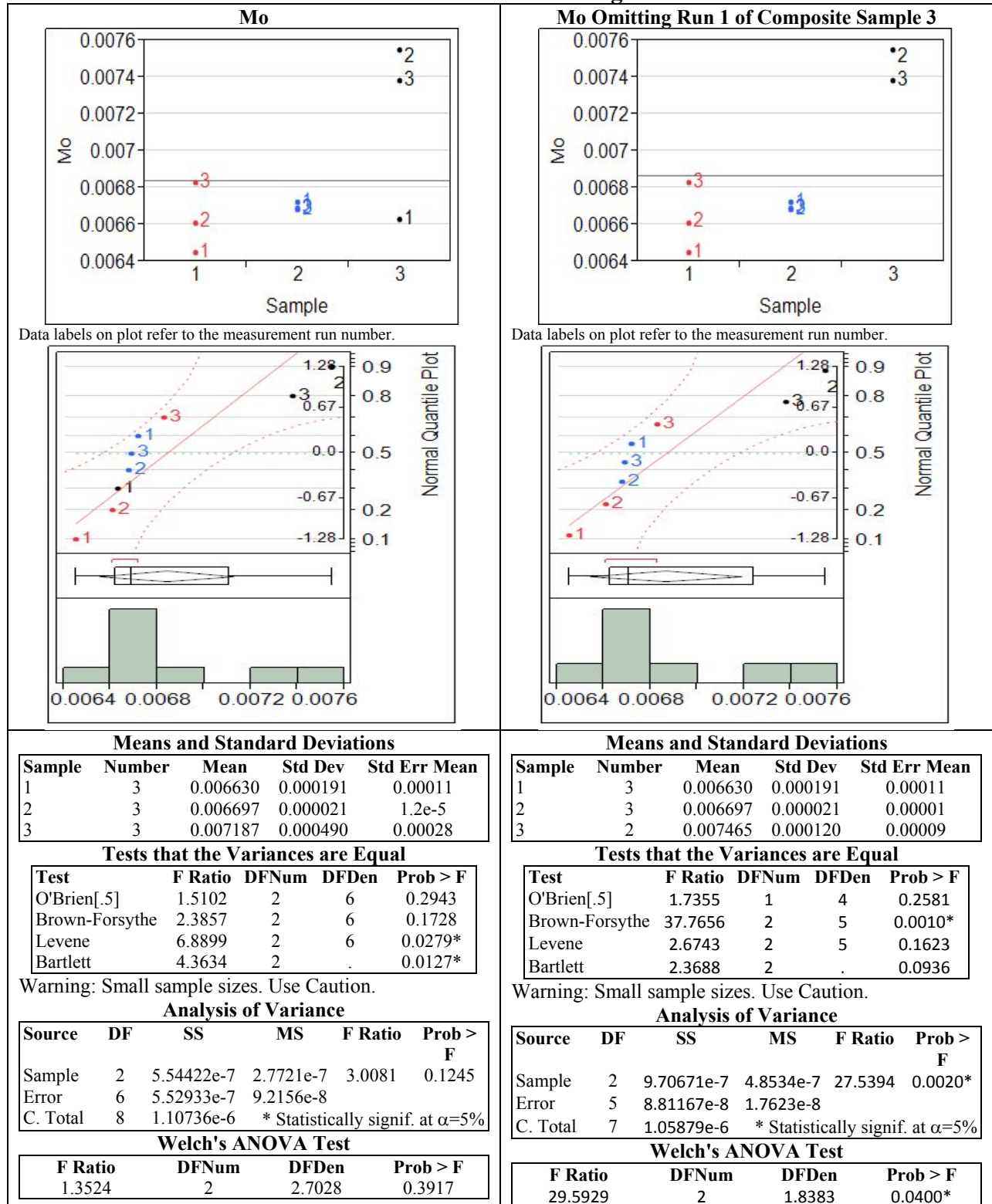
Appendix C: Statistical Results for Inorganic Constituents

Table 20 Tests and Estimators for Inorganic Constituents



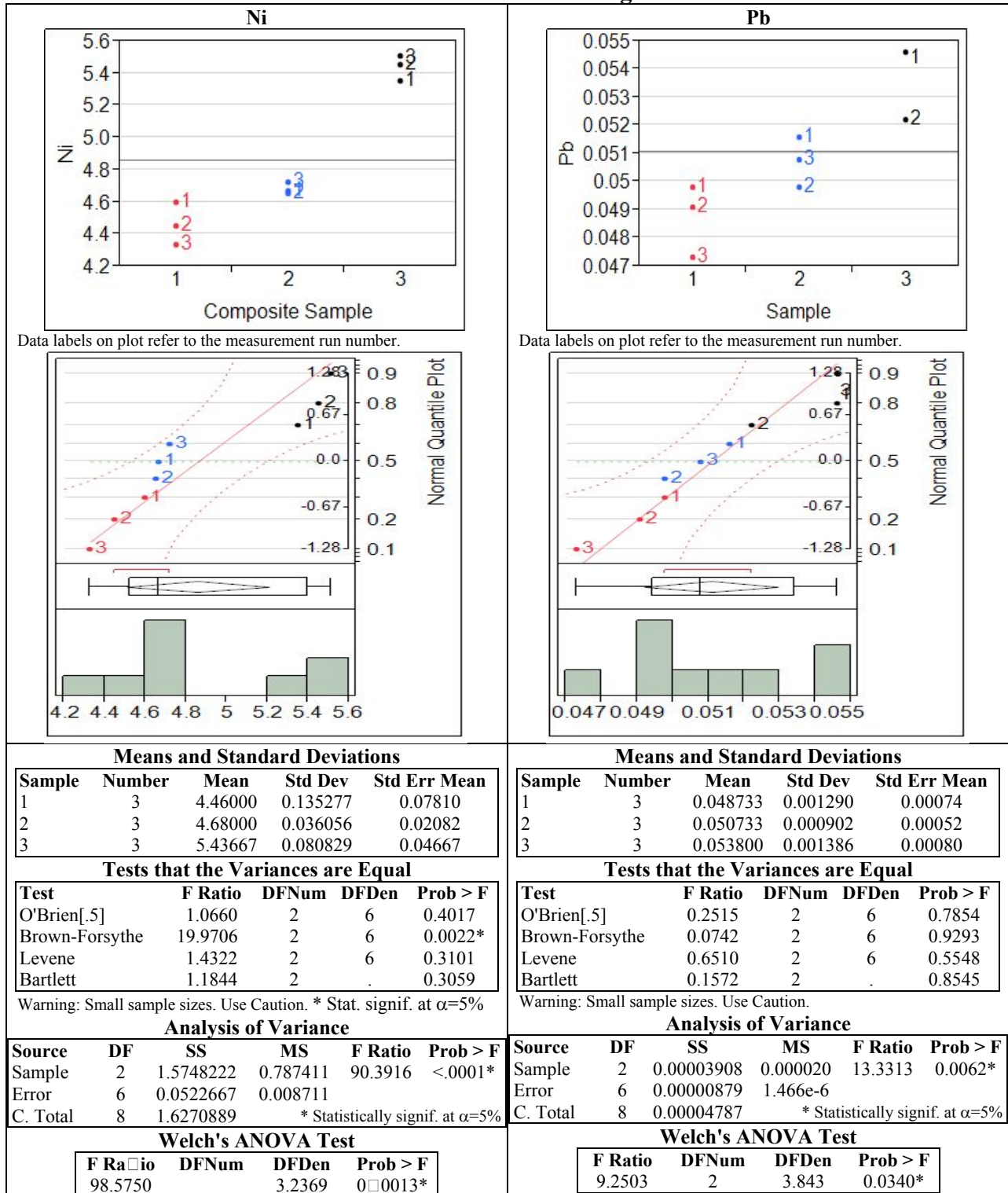
Appendix C: Statistical Results for Inorganic Constituents

Table 20 Tests and Estimators for Inorganic Constituents

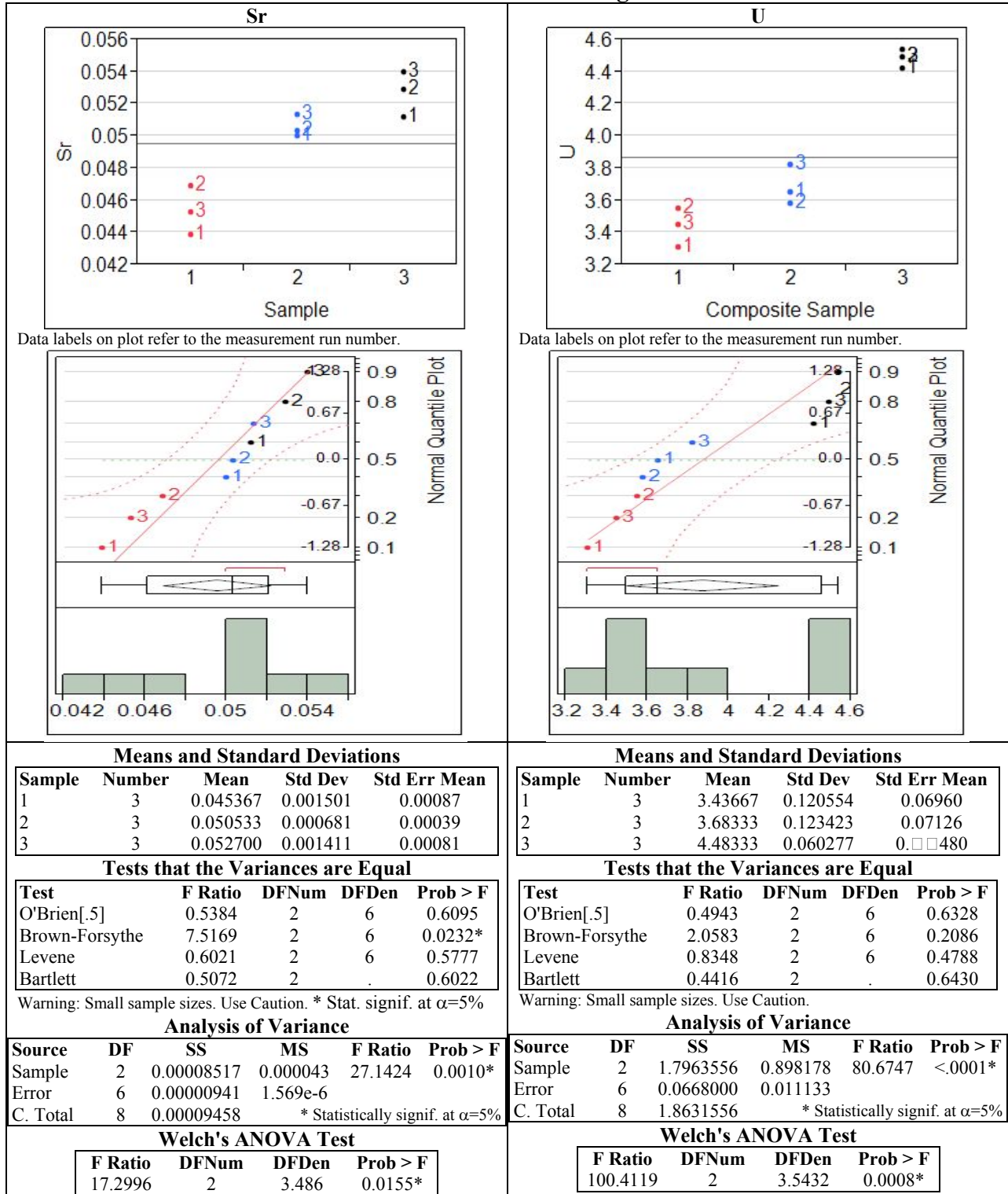


Appendix C: Statistical Results for Inorganic Constituents

Table 20 Tests and Estimators for Inorganic Constituents

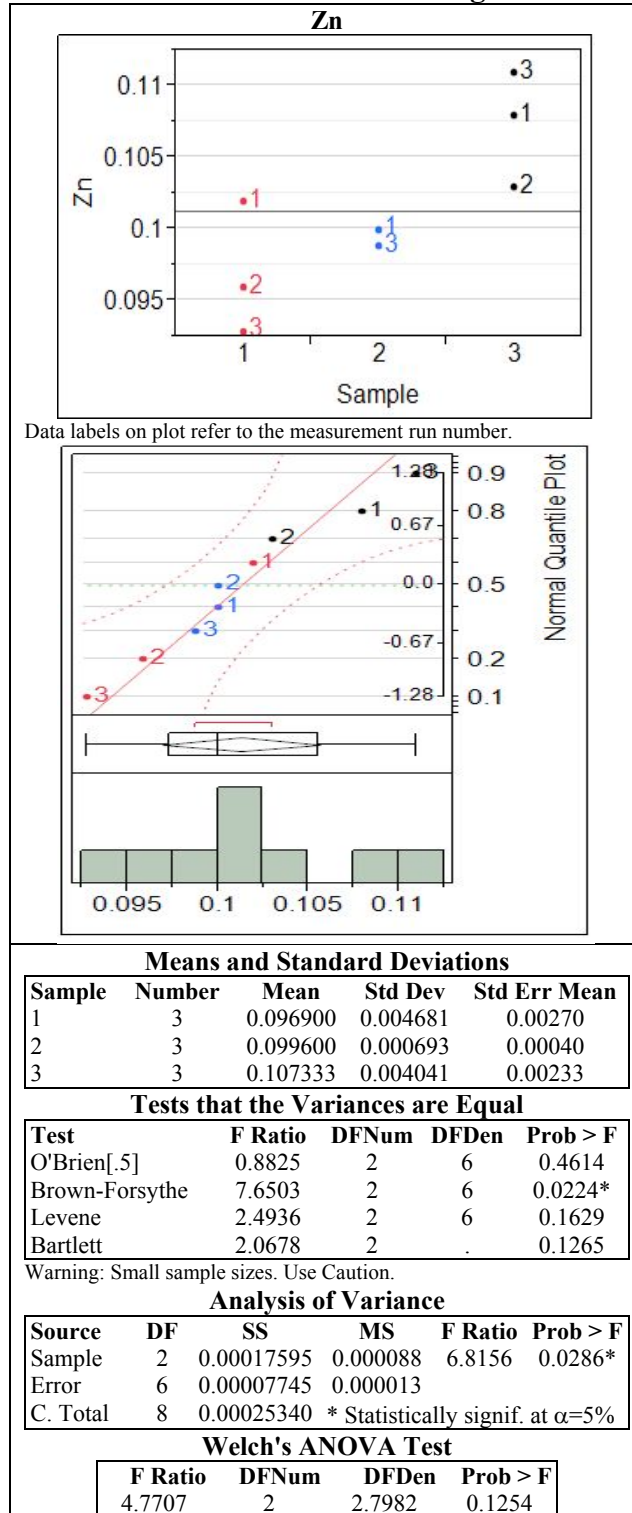


APPENDIX C: STATISTICAL RESULTS FOR INORGANIC CONSTITUENTS
Table 20 Tests and Estimators for Inorganic Constituents



APPENDIX C: STATISTICAL RESULTS FOR INORGANIC CONSTITUENTS

Table 20 Tests and Estimators for Inorganic Constituents



Appendix C: Statistical Results for Inorganic Constituents

Table 21 Computations for the Mean, Standard Error, and the 95% Upper Confidence Limit for the Mean Hg Concentration Omitting the Result for Run 1 of Composite Sample

1

ANOVA Summary without Run 1 from Composite 1 of Hg Results		
Source	df	Mean Square
BS=Between Samples	2	$MS_{Sample} = 0.0013216667$
WS=Within Samples	5	$MS_{Error} = 0.0000237333$

When the composite samples having differing numbers of measurements, Eqn (4) must be

$$n_0 = \left[n - \left(\sum_{i=1}^m n_i^2 \right) / n \right] / (m-1) = \left[8 - (2^2 + 3^2 + 3^2) / 8 \right] / (3-1) = 5.25 / 2 = 2.625, \text{ where}$$

$m = 3$ composite samples, $n_1 = 2$, $n_2 = 3$, and $n_3 = 3$ measurements for composite samples 1, 2, 3, respectively, $n = n_1 + n_2 + n_3 = 8$ total measurements, and $E\{MS_{Sample}\} = n_0 \sigma_{BS}^2 + \sigma_{WS}^2$.

Then $\tilde{V}_{BS} = (MS_{Sample} - MS_{Error}) / n_0 = (0.001321667 - 0.0000237333) / 2.625 = 0.001297934 / 2.625 = 0.000494451$
and $\tilde{V}_{WS} = MS_{Error} = 0.0000237333$

Estimated Mean, Estimated Std Error of the Mean, and UCL95

$$\bar{X} = \sum_{i=1}^m \bar{X}_i / m = (0.357000 + 0.370333 + 0.401000) / 3 = 1.128333 / 3 = 0.376111 \text{ mg/g}$$

$$V\{\bar{X}\} = (V\{\bar{X}_1\} + V\{\bar{X}_2\} + V\{\bar{X}_3\}) / 3^2 = ((V_{BS} + V_{WS} / n_1) + (V_{BS} + V_{WS} / n_2) + (V_{BS} + V_{WS} / n_3)) / 9$$

$$= (3V_{BS} + (1/2 + 1/3 + 1/3)V_{WS}) / 9 = 0.3333V_{BS} + 0.12963V_{WS}$$

$$= 0.3333(0.000494451) + 0.12963(0.000023775) = 0.000164815 + 0.000003082$$

$$= 0.000167897$$

Est. std err of the mean $= \sqrt{V\{\bar{X}\}} = \sqrt{0.000167897} = 0.01296$

Satterthwaite's $df = V\{\bar{X}\}^2 / (a_{BS}^2 V_{BS}^2 / df_{BS} + a_{WS}^2 V_{WS}^2 / df_{WS})$

$$= 0.000167897^2 / ((0.33333)^2 (0.000494451)^2 / 2 + (0.12963)^2 (0.000023775)^2 / 5) = 2.08$$

Note: The 95-th percentile of the t distribution with 2.08 df was calculated in JMP® 9.0.0.

$$UCL95 = \bar{X} + t_{0.95, 2.08} \sqrt{V\{\bar{X}\}} = 0.376111 + 2.84481924 \sqrt{0.000167897} = 0.41297 \text{ mg/g}$$

Note on the Outlier Test for Hg Results

All inorganics except for Hg and Mo had a statistically significant composite sampling variance. Plots of the Hg and Mo results in Table 20 suggest an outlier issue exists for those two constituents. Direct application of the Dixon test to the Hg concentration data ignores the sampling structure observed in the data in the top left plot of Table 20 on page 65 and does not indicate that any outliers exist. Application of the Dixon test to the largest positive Studentized residual from the sampling model produces a Dixon test statistic value of 0.673 which indicated that Composite Sample 1 Run 1 is a statistically significant outlier an observed significance level (P-value) less than 1%. A model without the Hg outlier was adopted, yielding a conservatively higher UCL95 than would have been obtained with all of the Hg concentration results.

Appendix C: Statistical Results for Inorganic Constituents

Table 22 Computations for the Mean, Standard Error, and the 95% Upper Confidence Limit for the Mean Mo Concentration Omitting the Result for Run 1 of Composite Sample 3

ANOVA Summary without Run 1 from Composite 1 of Hg Results		
Source	df	Mean Square
BS=Between Samples	2	$MS_{Sample} = 4.8533542e-7$
WS=Within Samples	5	$MS_{Error} = 1.7623333e-8$

When the composite samples having differing numbers of measurements, Eqn (4) must be

$$n_0 = \left[n - \left(\sum_{i=1}^m n_i^2 \right) / n \right] / (m-1) = \left[8 - (3^2 + 3^2 + 2^2) / 8 \right] / (3-1) = 5.25 / 2 = 2.625, \text{ where}$$

$m = 3$ composite samples, $n_1 = 3$, $n_2 = 3$, and $n_3 = 2$ measurements for composite samples 1, 2, 3, respectively, $n = n_1 + n_2 + n_3 = 8$ total measurements, and $E\{MS_{Sample}\} = n_0\sigma_{BS}^2 + \sigma_{WS}^2$.

Then $\tilde{V}_{BS} = (MS_{Sample} - MS_{Error}) / n_0 = (4.8533542e-7 - 1.7623333e-8) / 2.625 = 4.677121e-7 / 2.625 = 1.781760e-7$
and $\tilde{V}_{WS} = MS_{Error} = 1.7623333e-8$

Estimated Mean, Estimated Std Error of the Mean, and UCL95

$$\bar{X} = \sum_{i=1}^m \bar{X}_i / m = (0.006630 + 0.006697 + 0.007465) / 3 = 0.020792 / 3 = 0.006931 \text{ mg/g}$$

$$V\{\bar{X}\} = (V\{\bar{X}_1\} + V\{\bar{X}_2\} + V\{\bar{X}_3\}) / 3^2 = ((V_{BS} + V_{WS} / n_1) + (V_{BS} + V_{WS} / n_2) + (V_{BS} + V_{WS} / n_3)) / 9$$

$$= (3V_{BS} + (1/3 + 1/3 + 1/2)V_{WS}) / 9 = 0.3333V_{BS} + 0.12963V_{WS}$$

$$= 0.3333(1.781760e-7) + 0.12963(1.7623333e-8) = 5.938607e-8 + 2.284513e-9$$

$$= 6.167058e-8$$

Est. std err of the mean = $\sqrt{V\{\bar{X}\}} = \sqrt{6.167058e-8} = 0.000248336$

Satterthwaite's $df = V\{\bar{X}\}^2 / (a_{BS}^2 V_{BS}^2 / df_{BS} + a_{WS}^2 V_{WS}^2 / df_{WS})$

$$= (6.167058e-8)^2 / ((0.33333)^2 (1.781760e-7)^2 / 2 + (0.12963)^2 (1.7623333e-8)^2 / 5) = 2.16$$

Note: The 95-th percentile of the t distribution with 2.08 df was calculated in JMP® 9.0.0.

$$UCL95 = \bar{X} + t_{0.95, 2.08} \sqrt{V\{\bar{X}\}} = 0.006931 + 2.777697 \sqrt{6.167058e-8} = 0.0076208 \text{ mg/g}$$

Note on the Outlier Test for Mo Results

All inorganics except for Hg and Mo had a statistically significant composite sampling variance based on the entire set of results. Plots of the Hg and Mo results in Table 20 suggest an outlier issue exists for those two constituents. Direct application of the Dixon test to the Mo concentration data ignores the sampling structure observed in the data in the top left plot of Table 20 on page 65 and does not indicate that any outliers exist. However, application of the Dixon test to the largest positive Studentized residual from the sampling model produces a Dixon test statistic value of 0.498 which indicated that Composite Sample 3 Run 1 is a statistically significant outlier with an observed significance level (P-value) between 5 and 10%. A model without the Mo outlier was adopted though the P-value was not less than 5%, producing a common sampling model for all inorganics and producing a conservatively higher UCL95 than would have been obtained with all of the Mo concentrations results.

Appendix C: Statistical Results for Inorganic Constituents

Table 23 Inorganic Constituent Concentrations with All Results Less Than Their MDCs

Inorganic	MDC	
	Min	Max
Ag	1.12E-02	1.15E-02
As	5.33E-04	5.49E-04
B	1.57E-02	1.61E-02
Sb	9.90E-02	1.02E-01
Se	1.07E-03	1.10E-03

Appendix C: Statistical Results for Inorganic Constituents

Table 24 95% UCLs for Mean Concentrations of Inorganic Constituents with All Results Above Their MDCs

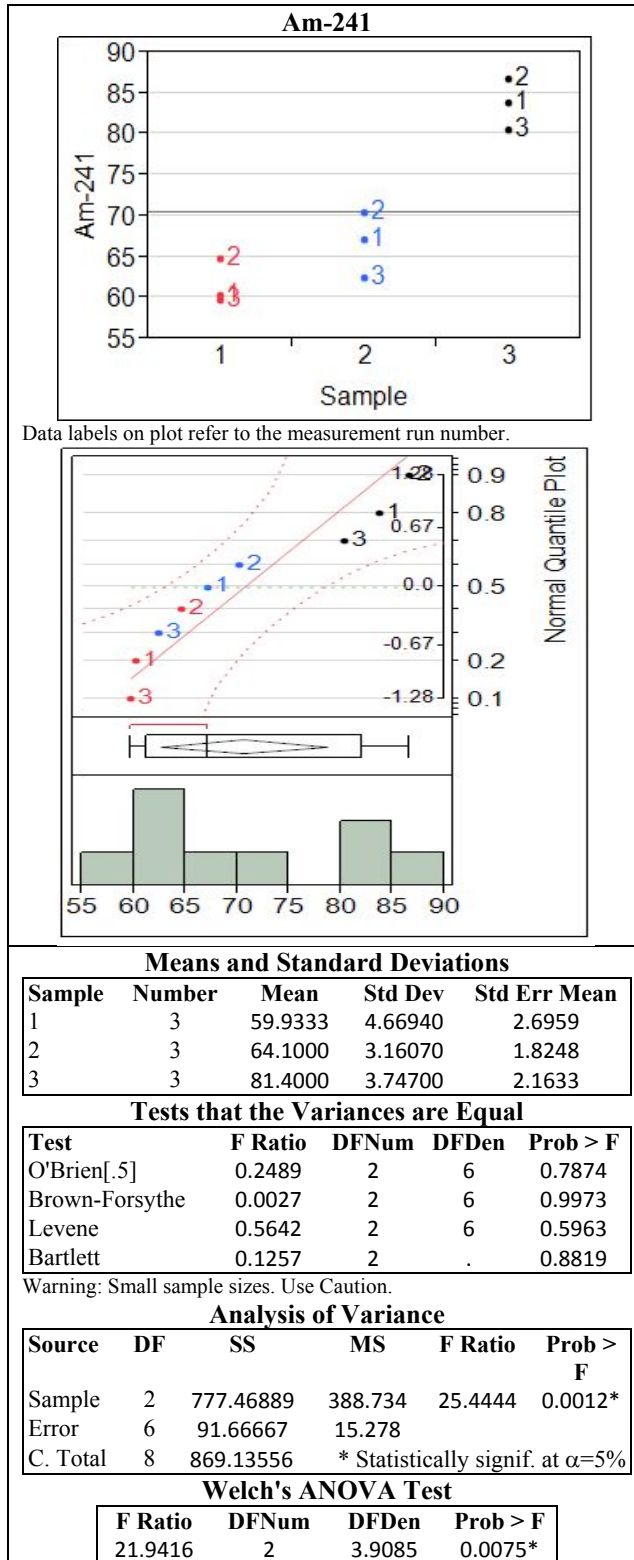
Inorganic	Model Type	N	Mean	Standard Deviation	Percent Standard Deviation	UCL95
Al	Sampling Error	9	2.318e+0	9.607e-2	4.1%	2.476e+0
Ba	Sampling Error	9	1.177e-1	1.056e-2	9.0%	1.351e-1
Cd	Sampling Error	9	1.055e-2	5.305e-4	5.0%	1.138e-2
Co	Sampling Error	9	2.320e-2	3.216e-3	13.9%	2.857e-2
Cr	Sampling Error	9	4.983e-2	3.429e-3	6.9%	5.528e-2
Cu	Sampling Error	9	1.027e-1	6.324e-3	6.2%	1.128e-1
Fe	Sampling Error	9	2.033e+1	1.110e+0	5.5%	2.200e+1
Hg	No Sampling Error	9	3.830e-1	2.297e-2	6.0%	3.972e-1
Hg [♦]	Sampling Error	8	3.761e-1	2.276e-2	6.1%	4.130e-1
I	Sampling Error	9	3.416e-4	1.441e-4	42.2%	5.562e-4
Mn	Sampling Error	9	1.718e+0	1.990e-1	11.6%	2.043e+0
Mo	No Sampling Error	9	6.838e-3	3.720e-4	5.4%	7.068e-3
Mo [♦]	Sampling Error	8	6.931e-3	4.425e-4	6.4%	7.621e-3
Ni	Sampling Error	9	4.859e+0	5.180e-1	10.7%	5.723e+0
Pb	Sampling Error	9	5.109e-2	2.737e-3	5.4%	5.539e-2
Sr	Sampling Error	9	4.953e-2	3.904e-3	7.9%	5.588e-2
U	Sampling Error	9	3.868e+0	5.539e-1	14.3%	4.790e+0
Zn	Sampling Error	9	1.013e-1	6.159e-3	6.1%	1.104e-1

♦ Hg calculations in this row omitted a potential outlier associated with Run 1 from Composite Sample 1.

♦ Mo calculations in this row omitted a potential outlier associated with Run 1 from Composite Sample 3.

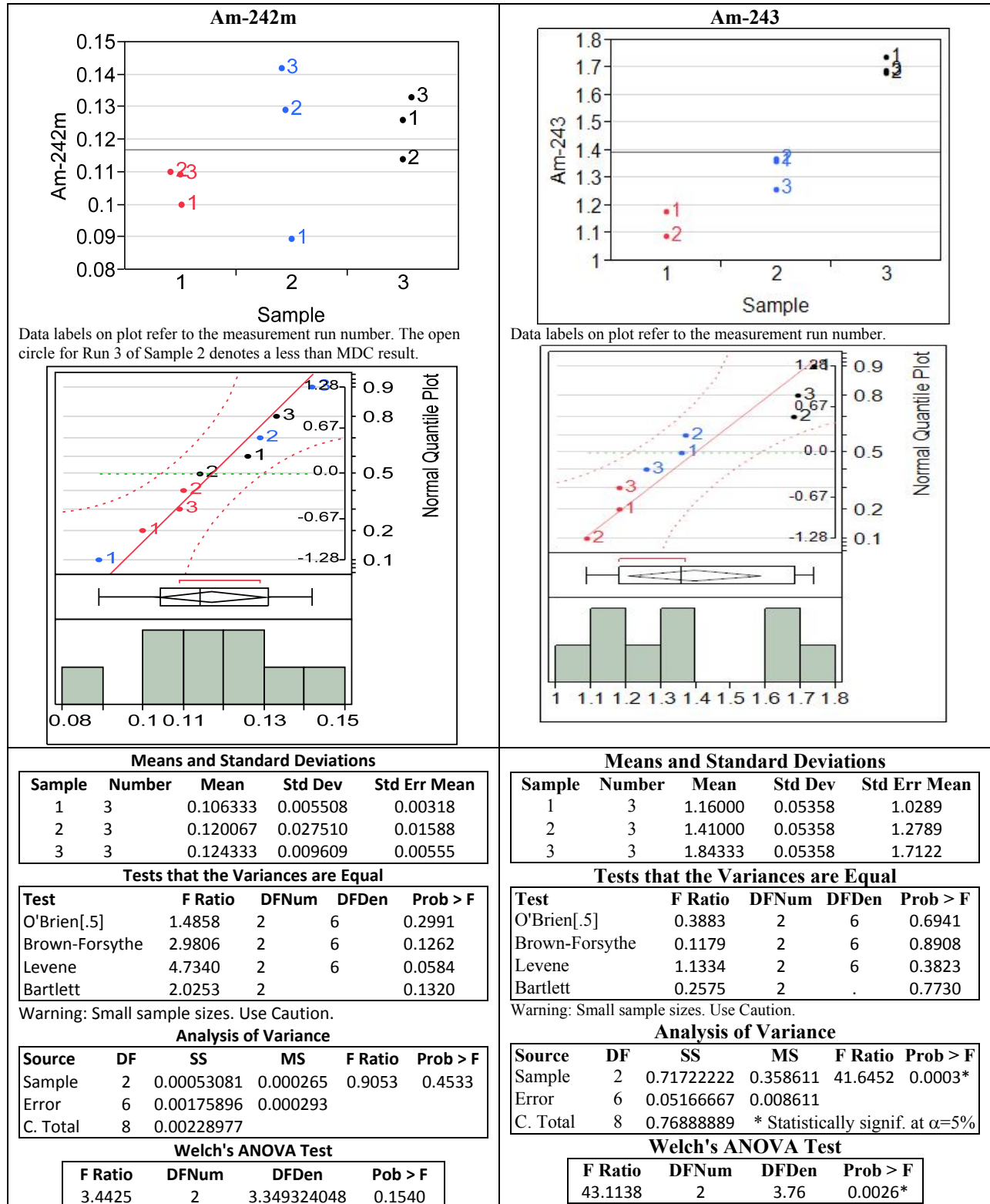
Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides



Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides



Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides

Ba-137m					C-14																																																						
Data labels on plot refer to the measurement run number.					Data labels on plot refer to the measurement run number.																																																						
<p align="center">Means and Standard Deviations</p> <table border="1"> <thead> <tr> <th>Sample</th> <th>Number</th> <th>Mean</th> <th>Std Dev</th> <th>Std Err Mean</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>3</td> <td>505.667</td> <td>2.3094</td> <td>1.333</td> </tr> <tr> <td>2</td> <td>3</td> <td>527.000</td> <td>28.1603</td> <td>16.258</td> </tr> <tr> <td>3</td> <td>3</td> <td>507.000</td> <td>6.9282</td> <td>4.000</td> </tr> </tbody> </table>					Sample	Number	Mean	Std Dev	Std Err Mean	1	3	505.667	2.3094	1.333	2	3	527.000	28.1603	16.258	3	3	507.000	6.9282	4.000	<p align="center">Means and Standard Deviations</p> <table border="1"> <thead> <tr> <th>Sample</th> <th>Number</th> <th>Mean</th> <th>S² Dev</th> <th>Std Err Mean</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>3</td> <td>0.018567</td> <td>0.005532</td> <td>0.00319</td> </tr> <tr> <td>2</td> <td>3</td> <td>0.020967</td> <td>0.004735</td> <td>0.00273</td> </tr> <tr> <td>3</td> <td>3</td> <td>0.014000</td> <td>0.004660</td> <td>0.00269</td> </tr> </tbody> </table>					Sample	Number	Mean	S ² Dev	Std Err Mean	1	3	0.018567	0.005532	0.00319	2	3	0.020967	0.004735	0.00273	3	3	0.014000	0.004660	0.00269										
Sample	Number	Mean	Std Dev	Std Err Mean																																																							
1	3	505.667	2.3094	1.333																																																							
2	3	527.000	28.1603	16.258																																																							
3	3	507.000	6.9282	4.000																																																							
Sample	Number	Mean	S ² Dev	Std Err Mean																																																							
1	3	0.018567	0.005532	0.00319																																																							
2	3	0.020967	0.004735	0.00273																																																							
3	3	0.014000	0.004660	0.00269																																																							
<p align="center">Tests that the Variances are Equal</p> <table border="1"> <thead> <tr> <th>Test</th> <th>F Ratio</th> <th>DFNum</th> <th>DFDen</th> <th>Prob > F</th> </tr> </thead> <tbody> <tr> <td>O'Brien[.5]</td> <td>1.6579</td> <td>2</td> <td>6</td> <td>0.2672</td> </tr> <tr> <td>Brown-Forsythe</td> <td>6.8952</td> <td>2</td> <td>6</td> <td>0.0279*</td> </tr> <tr> <td>Levene</td> <td>5.7299</td> <td>2</td> <td>6</td> <td>0.0406*</td> </tr> <tr> <td>Bartlett</td> <td>3.8503</td> <td>2</td> <td>.</td> <td>0.0213*</td> </tr> </tbody> </table> <p>Warning: Small sample sizes. Use Caution.</p>					Test	F Ratio	DFNum	DFDen	Prob > F	O'Brien[.5]	1.6579	2	6	0.2672	Brown-Forsythe	6.8952	2	6	0.0279*	Levene	5.7299	2	6	0.0406*	Bartlett	3.8503	2	.	0.0213*	<p align="center">Tests that the Variances are Equal</p> <table border="1"> <thead> <tr> <th>Test</th> <th>F Ratio</th> <th>DFNum</th> <th>DFDen</th> <th>Prob > F</th> </tr> </thead> <tbody> <tr> <td>O'Brien[.5]</td> <td>0.0681</td> <td>2</td> <td>6</td> <td>0.9349</td> </tr> <tr> <td>Brown-Forsythe</td> <td>0.0490</td> <td>2</td> <td>6</td> <td>0.9526</td> </tr> <tr> <td>Levene</td> <td>0.1529</td> <td>2</td> <td>6</td> <td>0.8614</td> </tr> <tr> <td>Bartlett</td> <td>0.0303</td> <td>2</td> <td>.</td> <td>0.9702</td> </tr> </tbody> </table> <p>Warning: Small sample sizes. Use Caution.</p>					Test	F Ratio	DFNum	DFDen	Prob > F	O'Brien[.5]	0.0681	2	6	0.9349	Brown-Forsythe	0.0490	2	6	0.9526	Levene	0.1529	2	6	0.8614	Bartlett	0.0303	2	.	0.9702
Test	F Ratio	DFNum	DFDen	Prob > F																																																							
O'Brien[.5]	1.6579	2	6	0.2672																																																							
Brown-Forsythe	6.8952	2	6	0.0279*																																																							
Levene	5.7299	2	6	0.0406*																																																							
Bartlett	3.8503	2	.	0.0213*																																																							
Test	F Ratio	DFNum	DFDen	Prob > F																																																							
O'Brien[.5]	0.0681	2	6	0.9349																																																							
Brown-Forsythe	0.0490	2	6	0.9526																																																							
Levene	0.1529	2	6	0.8614																																																							
Bartlett	0.0303	2	.	0.9702																																																							
<p align="center">Analysis of Variance</p> <table border="1"> <thead> <tr> <th>Source</th> <th>DF</th> <th>SS</th> <th>MS</th> <th>F Ratio</th> <th>Prob > F</th> </tr> </thead> <tbody> <tr> <td>Sample</td> <td>2</td> <td>856.8889</td> <td>428.444</td> <td>1.5187</td> <td>0.2926</td> </tr> <tr> <td>Error</td> <td>6</td> <td>1,692.6667</td> <td>282.111</td> <td></td> <td></td> </tr> <tr> <td>C. Total</td> <td>8</td> <td>2,549.5556</td> <td></td> <td></td> <td></td> </tr> </tbody> </table>					Source	DF	SS	MS	F Ratio	Prob > F	Sample	2	856.8889	428.444	1.5187	0.2926	Error	6	1,692.6667	282.111			C. Total	8	2,549.5556				<p align="center">Analysis of Variance</p> <table border="1"> <thead> <tr> <th>Source</th> <th>DF</th> <th>SS</th> <th>MS</th> <th>F Ratio</th> <th>Prob > F</th> </tr> </thead> <tbody> <tr> <td>Sample</td> <td>2</td> <td>0.00007515</td> <td>0.000038</td> <td>1.5081</td> <td>0.2947</td> </tr> <tr> <td>Error</td> <td>6</td> <td>0.00014949</td> <td>0.000025</td> <td></td> <td></td> </tr> <tr> <td>C. Total</td> <td>8</td> <td>0.00022464</td> <td></td> <td></td> <td></td> </tr> </tbody> </table>					Source	DF	SS	MS	F Ratio	Prob > F	Sample	2	0.00007515	0.000038	1.5081	0.2947	Error	6	0.00014949	0.000025			C. Total	8	0.00022464					
Source	DF	SS	MS	F Ratio	Prob > F																																																						
Sample	2	856.8889	428.444	1.5187	0.2926																																																						
Error	6	1,692.6667	282.111																																																								
C. Total	8	2,549.5556																																																									
Source	DF	SS	MS	F Ratio	Prob > F																																																						
Sample	2	0.00007515	0.000038	1.5081	0.2947																																																						
Error	6	0.00014949	0.000025																																																								
C. Total	8	0.00022464																																																									
<p align="center">Welch's ANOVA Test</p> <table border="1"> <thead> <tr> <th>F Ratio</th> <th>DFNum</th> <th>DFDen</th> <th>Prob > F</th> </tr> </thead> <tbody> <tr> <td>0.729</td> <td>2</td> <td>2.9463</td> <td>0.5528</td> </tr> </tbody> </table>					F Ratio	DFNum	DFDen	Prob > F	0.729	2	2.9463	0.5528	<p align="center">Welch's ANOVA Test</p> <table border="1"> <thead> <tr> <th>F Ratio</th> <th>DFNum</th> <th>DFDen</th> <th>Prob > F</th> </tr> </thead> <tbody> <tr> <td>1.4526</td> <td>2</td> <td>3.9789</td> <td>0.3360</td> </tr> </tbody> </table>					F Ratio	DFNum	DFDen	Prob > F	1.4526	2	3.9789	0.3360																																		
F Ratio	DFNum	DFDen	Prob > F																																																								
0.729	2	2.9463	0.5528																																																								
F Ratio	DFNum	DFDen	Prob > F																																																								
1.4526	2	3.9789	0.3360																																																								

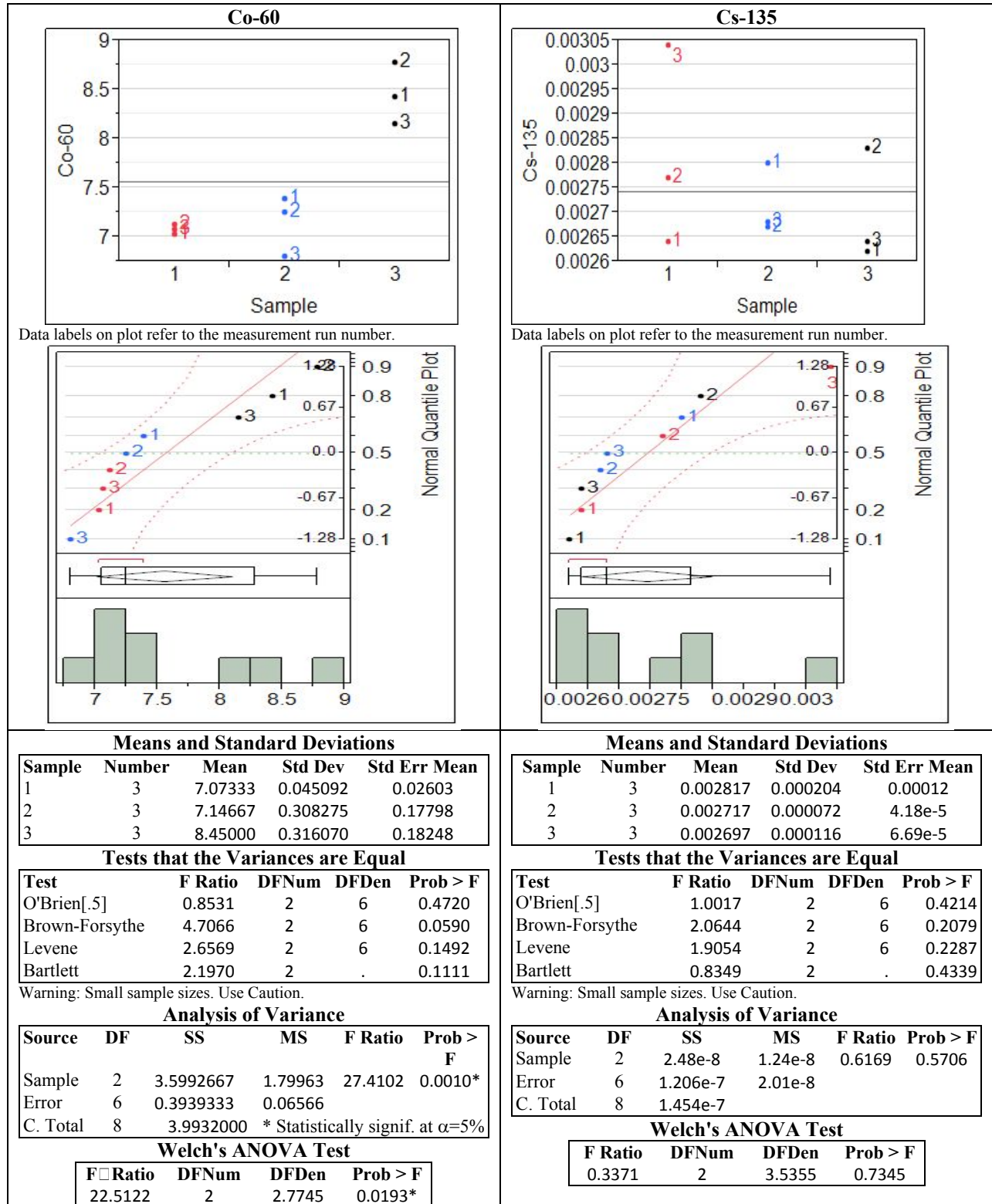
Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides

Cm-244					Cm-245																																																																				
Data labels on plot refer to the measurement run number.					Data labels on plot refer to the measurement run number.																																																																				
<p align="center">Means and Standard Deviations</p> <table border="1"> <thead> <tr> <th>Sample</th> <th>Number</th> <th>Mean</th> <th>Std Dev</th> <th>Std Err Mean</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>3</td> <td>49.0667</td> <td>0.45092</td> <td>0.2603</td> </tr> <tr> <td>2</td> <td>3</td> <td>53.1667</td> <td>4.81906</td> <td>2.7823</td> </tr> <tr> <td>3</td> <td>3</td> <td>64.1000</td> <td>1.87350</td> <td>1.0817</td> </tr> </tbody> </table>					Sample	Number	Mean	Std Dev	Std Err Mean	1	3	49.0667	0.45092	0.2603	2	3	53.1667	4.81906	2.7823	3	3	64.1000	1.87350	1.0817	<p align="center">Means and Standard Deviations</p> <table border="1"> <thead> <tr> <th>Sample</th> <th>Number</th> <th>Mean</th> <th>Std Dev</th> <th>Std Err Mean</th> </tr> </thead> <tbody> <tr> <td>1</td> <td>3</td> <td>0.004820</td> <td>0.000090</td> <td>5.2e-5</td> </tr> <tr> <td>2</td> <td>3</td> <td>0.005180</td> <td>0.000551</td> <td>0.00032</td> </tr> <tr> <td>3</td> <td>3</td> <td>0.006427</td> <td>0.000271</td> <td>0.00016</td> </tr> </tbody> </table>					Sample	Number	Mean	Std Dev	Std Err Mean	1	3	0.004820	0.000090	5.2e-5	2	3	0.005180	0.000551	0.00032	3	3	0.006427	0.000271	0.00016																								
Sample	Number	Mean	Std Dev	Std Err Mean																																																																					
1	3	49.0667	0.45092	0.2603																																																																					
2	3	53.1667	4.81906	2.7823																																																																					
3	3	64.1000	1.87350	1.0817																																																																					
Sample	Number	Mean	Std Dev	Std Err Mean																																																																					
1	3	0.004820	0.000090	5.2e-5																																																																					
2	3	0.005180	0.000551	0.00032																																																																					
3	3	0.006427	0.000271	0.00016																																																																					
<p align="center">Tests that the Variances are Equal</p> <table border="1"> <thead> <tr> <th>Test</th> <th>F Ratio</th> <th>DFNum</th> <th>DFDen</th> <th>Prob > F</th> </tr> </thead> <tbody> <tr> <td>O'Brien[.5]</td> <td>1.4976</td> <td>2</td> <td>6</td> <td>0.2968</td> </tr> <tr> <td>Brown-Forsythe</td> <td>2.1397</td> <td>2</td> <td>6</td> <td>0.1989</td> </tr> <tr> <td>Levene</td> <td>6.6186</td> <td>2</td> <td>6</td> <td>0.0303*</td> </tr> <tr> <td>Bartlett</td> <td>3.0901</td> <td>2</td> <td>.</td> <td>0.0455*</td> </tr> </tbody> </table> <p>Warning: Small sample sizes. Use Caution.</p>					Test	F Ratio	DFNum	DFDen	Prob > F	O'Brien[.5]	1.4976	2	6	0.2968	Brown-Forsythe	2.1397	2	6	0.1989	Levene	6.6186	2	6	0.0303*	Bartlett	3.0901	2	.	0.0455*	<p align="center">Tests that the Variances are Equal</p> <table border="1"> <thead> <tr> <th>Test</th> <th>F Ratio</th> <th>DFNum</th> <th>DFDen</th> <th>Prob > F</th> </tr> </thead> <tbody> <tr> <td>O'Brien[.5]</td> <td>1.3155</td> <td>2</td> <td>6</td> <td>0.3359</td> </tr> <tr> <td>Brown-Forsythe</td> <td>14.4754</td> <td>2</td> <td>6</td> <td>0.0051*</td> </tr> <tr> <td>Levene</td> <td>2.7153</td> <td>2</td> <td>6</td> <td>0.1446</td> </tr> <tr> <td>Bartlett</td> <td>2.0117</td> <td>2</td> <td>.</td> <td>0.1338</td> </tr> </tbody> </table> <p>Warning: Small sample sizes. Use Caution.</p>					Test	F Ratio	DFNum	DFDen	Prob > F	O'Brien[.5]	1.3155	2	6	0.3359	Brown-Forsythe	14.4754	2	6	0.0051*	Levene	2.7153	2	6	0.1446	Bartlett	2.0117	2	.	0.1338														
Test	F Ratio	DFNum	DFDen	Prob > F																																																																					
O'Brien[.5]	1.4976	2	6	0.2968																																																																					
Brown-Forsythe	2.1397	2	6	0.1989																																																																					
Levene	6.6186	2	6	0.0303*																																																																					
Bartlett	3.0901	2	.	0.0455*																																																																					
Test	F Ratio	DFNum	DFDen	Prob > F																																																																					
O'Brien[.5]	1.3155	2	6	0.3359																																																																					
Brown-Forsythe	14.4754	2	6	0.0051*																																																																					
Levene	2.7153	2	6	0.1446																																																																					
Bartlett	2.0117	2	.	0.1338																																																																					
<p align="center">Analysis of Variance</p> <table border="1"> <thead> <tr> <th>Source</th> <th>DF</th> <th>SS</th> <th>MS</th> <th>F Ratio</th> <th>Prob > F</th> </tr> </thead> <tbody> <tr> <td>Sample</td> <td>2</td> <td>362.34889</td> <td>181.174</td> <td>20.1778</td> <td>0.0022*</td> </tr> <tr> <td>Error</td> <td>6</td> <td>53.87333</td> <td>8.979</td> <td></td> <td></td> </tr> <tr> <td>C. Total</td> <td>8</td> <td>416.22222</td> <td></td> <td></td> <td>* Statistically signif. at $\alpha=5\%$</td> </tr> </tbody> </table> <p align="center">Welch's ANOVA Test</p> <table border="1"> <thead> <tr> <th>F Ratio</th> <th>DFNum</th> <th>DFDen</th> <th>Prob > F</th> </tr> </thead> <tbody> <tr> <td>74.4642</td> <td>2</td> <td>2.84</td> <td>0.0036*</td> </tr> </tbody> </table>					Source	DF	SS	MS	F Ratio	Prob > F	Sample	2	362.34889	181.174	20.1778	0.0022*	Error	6	53.87333	8.979			C. Total	8	416.22222			* Statistically signif. at $\alpha=5\%$	F Ratio	DFNum	DFDen	Prob > F	74.4642	2	2.84	0.0036*	<p align="center">Analysis of Variance</p> <table border="1"> <thead> <tr> <th>Source</th> <th>DF</th> <th>SS</th> <th>MS</th> <th>F Ratio</th> <th>Prob > F</th> </tr> </thead> <tbody> <tr> <td>Sample</td> <td>2</td> <td>4.26516e-6</td> <td>2.1326e-6</td> <td>16.6333</td> <td>0.0036*</td> </tr> <tr> <td>Error</td> <td>6</td> <td>7.69267e-7</td> <td>1.2821e-7</td> <td></td> <td></td> </tr> <tr> <td>C. Total</td> <td>8</td> <td>5.03442e-6</td> <td></td> <td></td> <td>* Statistically signif. at $\alpha=5\%$</td> </tr> </tbody> </table> <p align="center">Welch's ANOVA Test</p> <table border="1"> <thead> <tr> <th>F Ratio</th> <th>DFNum</th> <th>DFDen</th> <th>Prob > F</th> </tr> </thead> <tbody> <tr> <td>38.9921</td> <td>2</td> <td>2.9904</td> <td>0.0072*</td> </tr> </tbody> </table>					Source	DF	SS	MS	F Ratio	Prob > F	Sample	2	4.26516e-6	2.1326e-6	16.6333	0.0036*	Error	6	7.69267e-7	1.2821e-7			C. Total	8	5.03442e-6			* Statistically signif. at $\alpha=5\%$	F Ratio	DFNum	DFDen	Prob > F	38.9921	2	2.9904	0.0072*
Source	DF	SS	MS	F Ratio	Prob > F																																																																				
Sample	2	362.34889	181.174	20.1778	0.0022*																																																																				
Error	6	53.87333	8.979																																																																						
C. Total	8	416.22222			* Statistically signif. at $\alpha=5\%$																																																																				
F Ratio	DFNum	DFDen	Prob > F																																																																						
74.4642	2	2.84	0.0036*																																																																						
Source	DF	SS	MS	F Ratio	Prob > F																																																																				
Sample	2	4.26516e-6	2.1326e-6	16.6333	0.0036*																																																																				
Error	6	7.69267e-7	1.2821e-7																																																																						
C. Total	8	5.03442e-6			* Statistically signif. at $\alpha=5\%$																																																																				
F Ratio	DFNum	DFDen	Prob > F																																																																						
38.9921	2	2.9904	0.0072*																																																																						

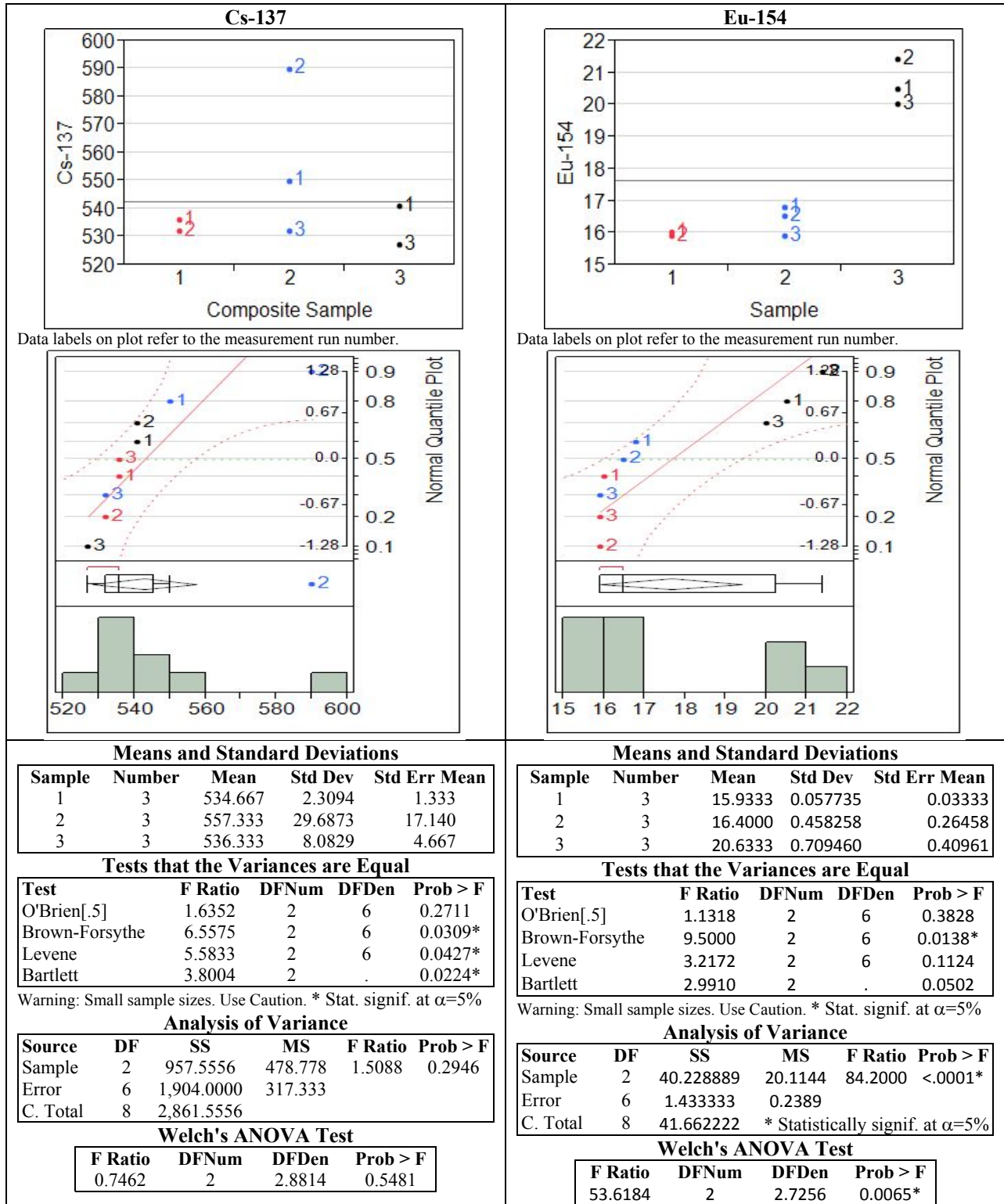
Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides



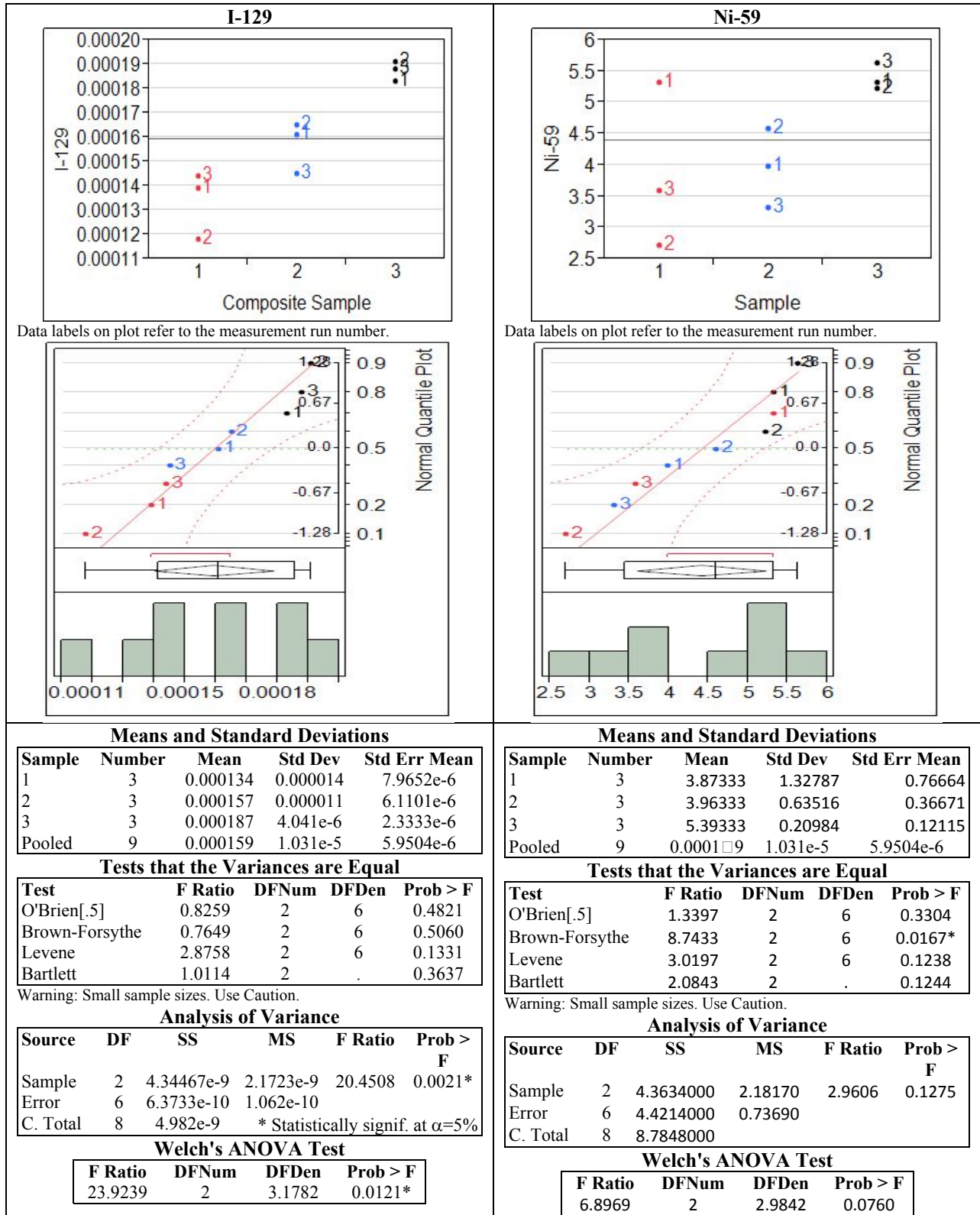
Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides



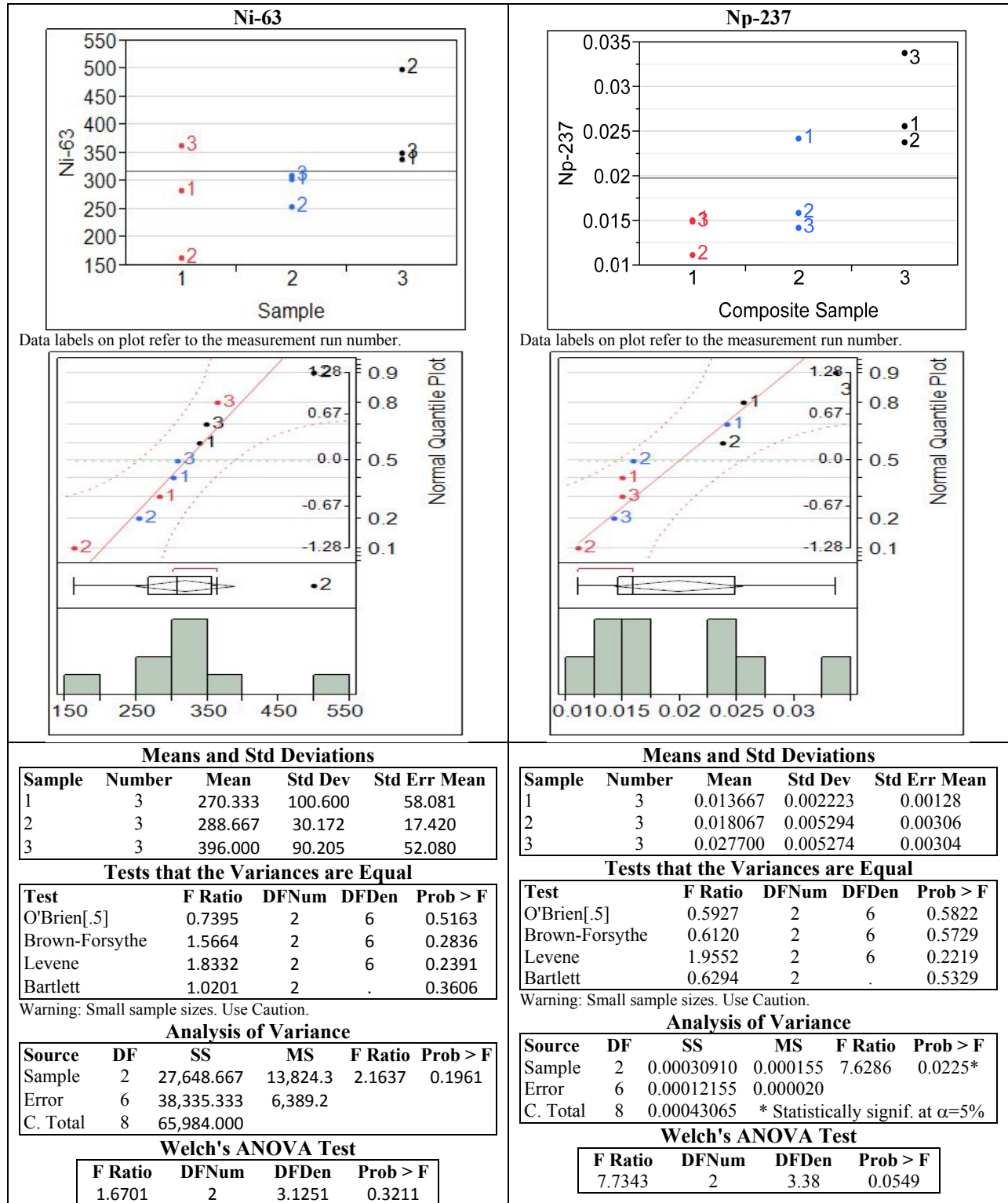
Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides



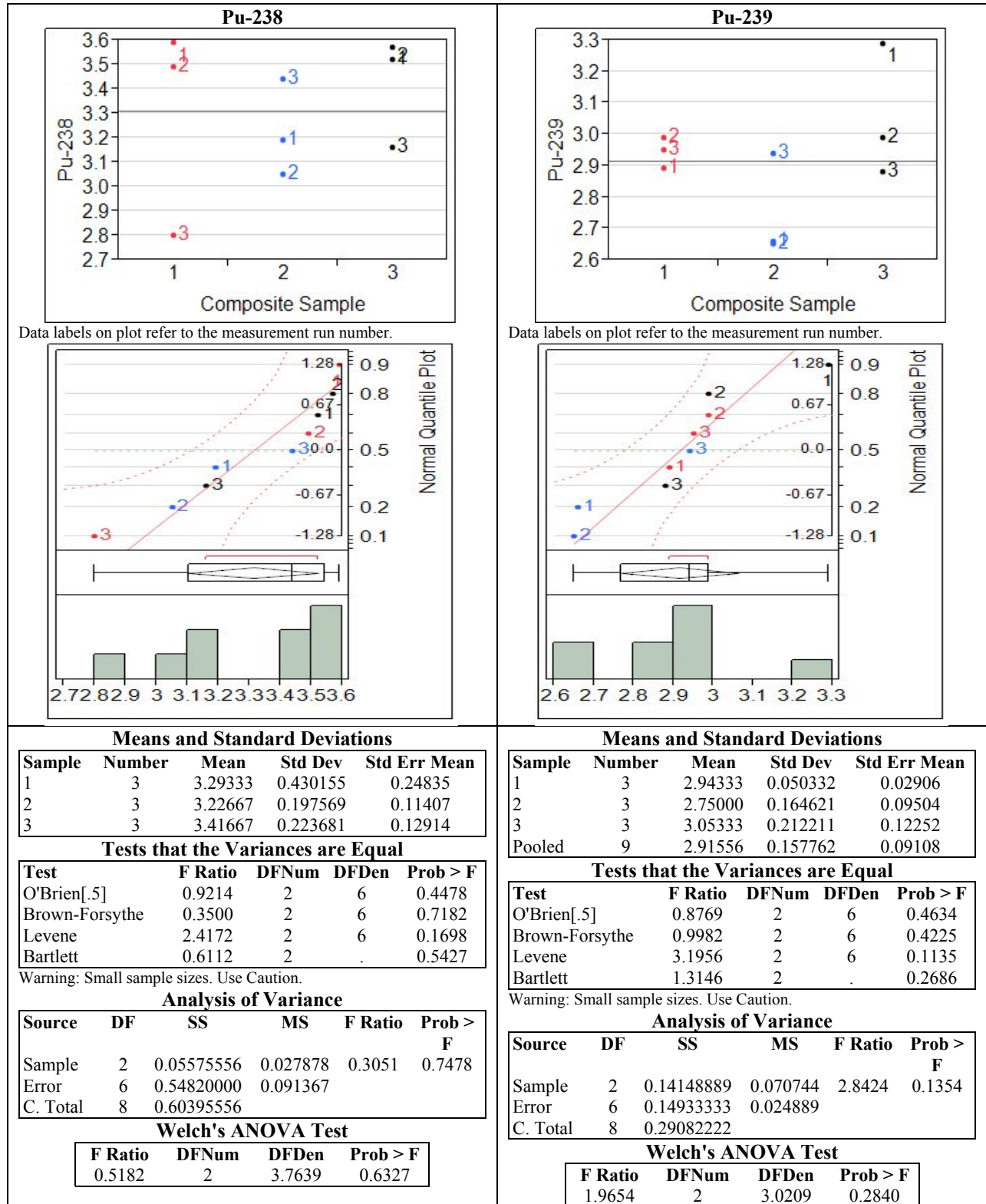
Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides



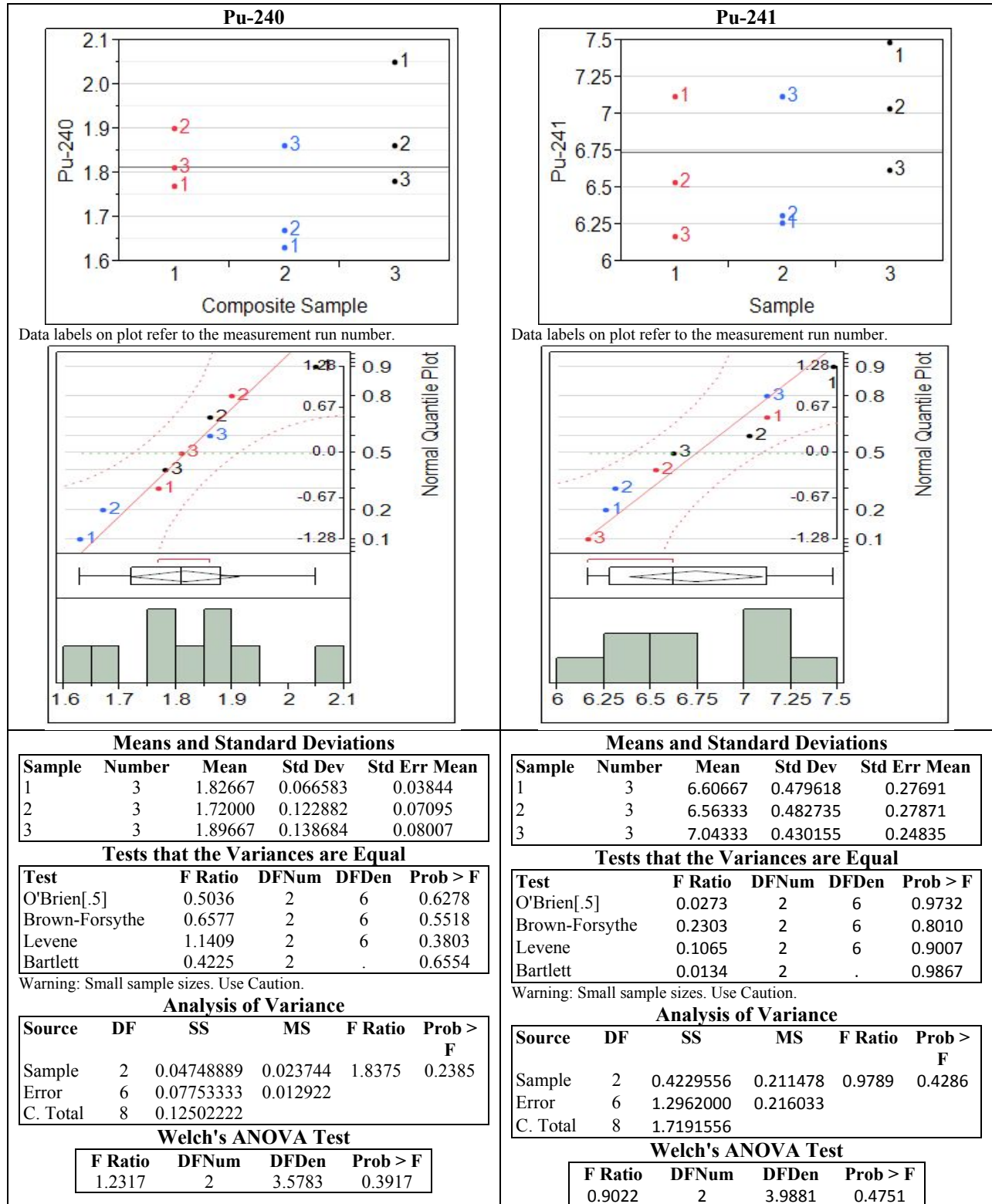
Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides



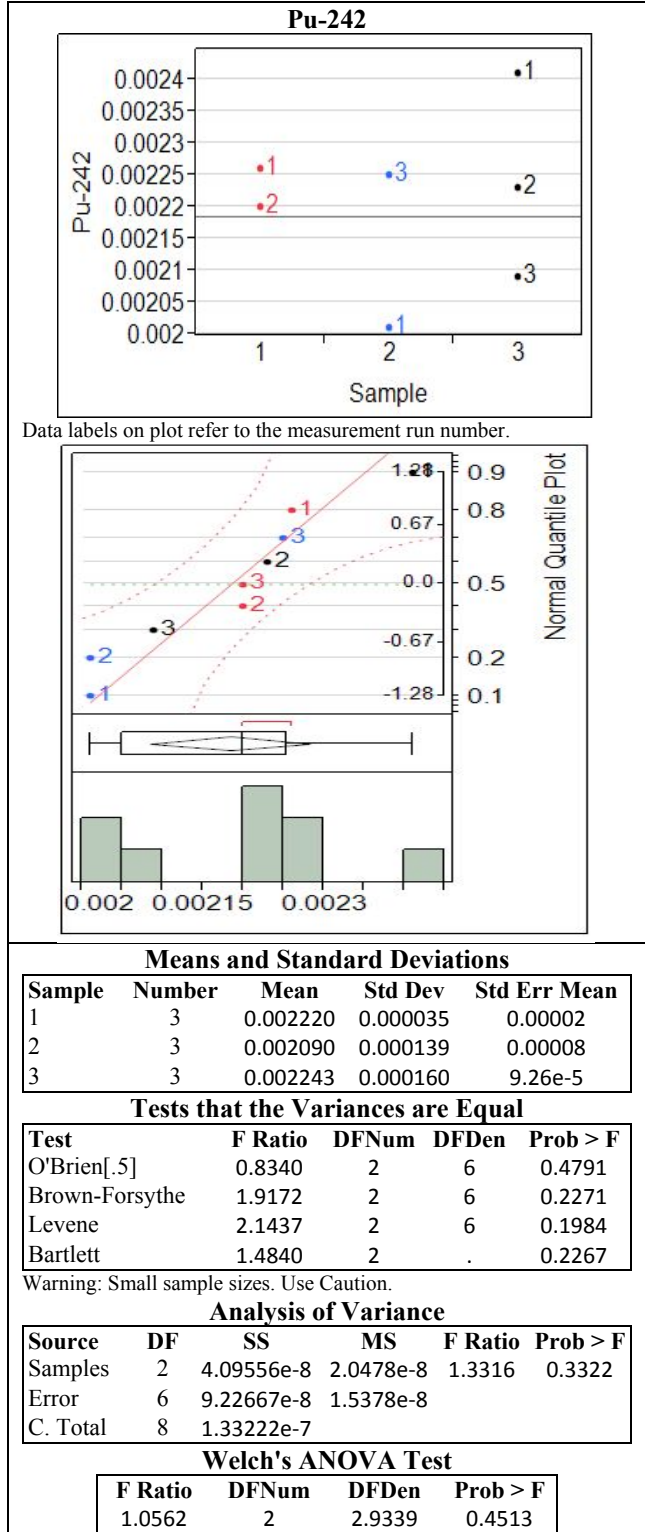
Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides



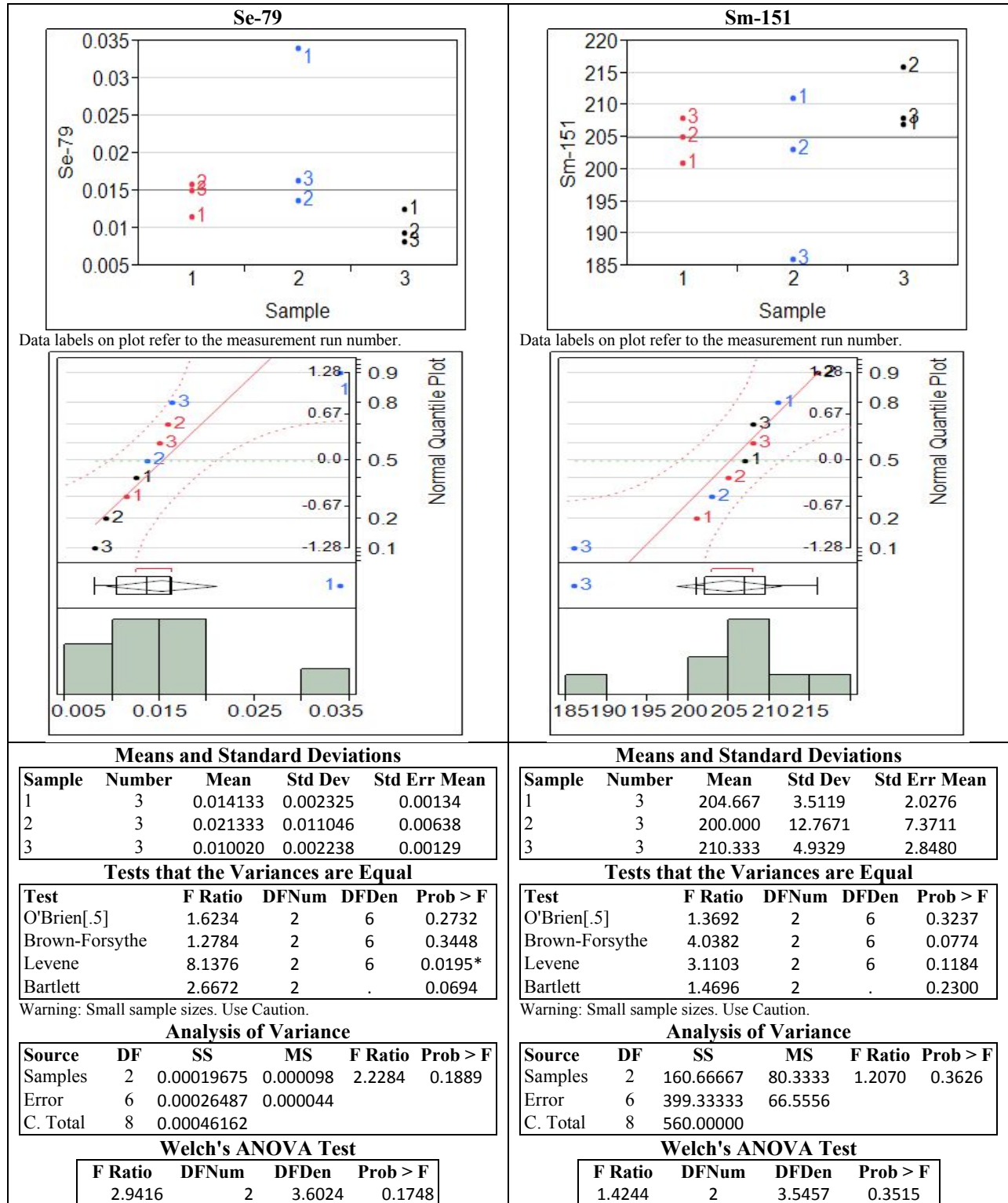
Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides



Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides



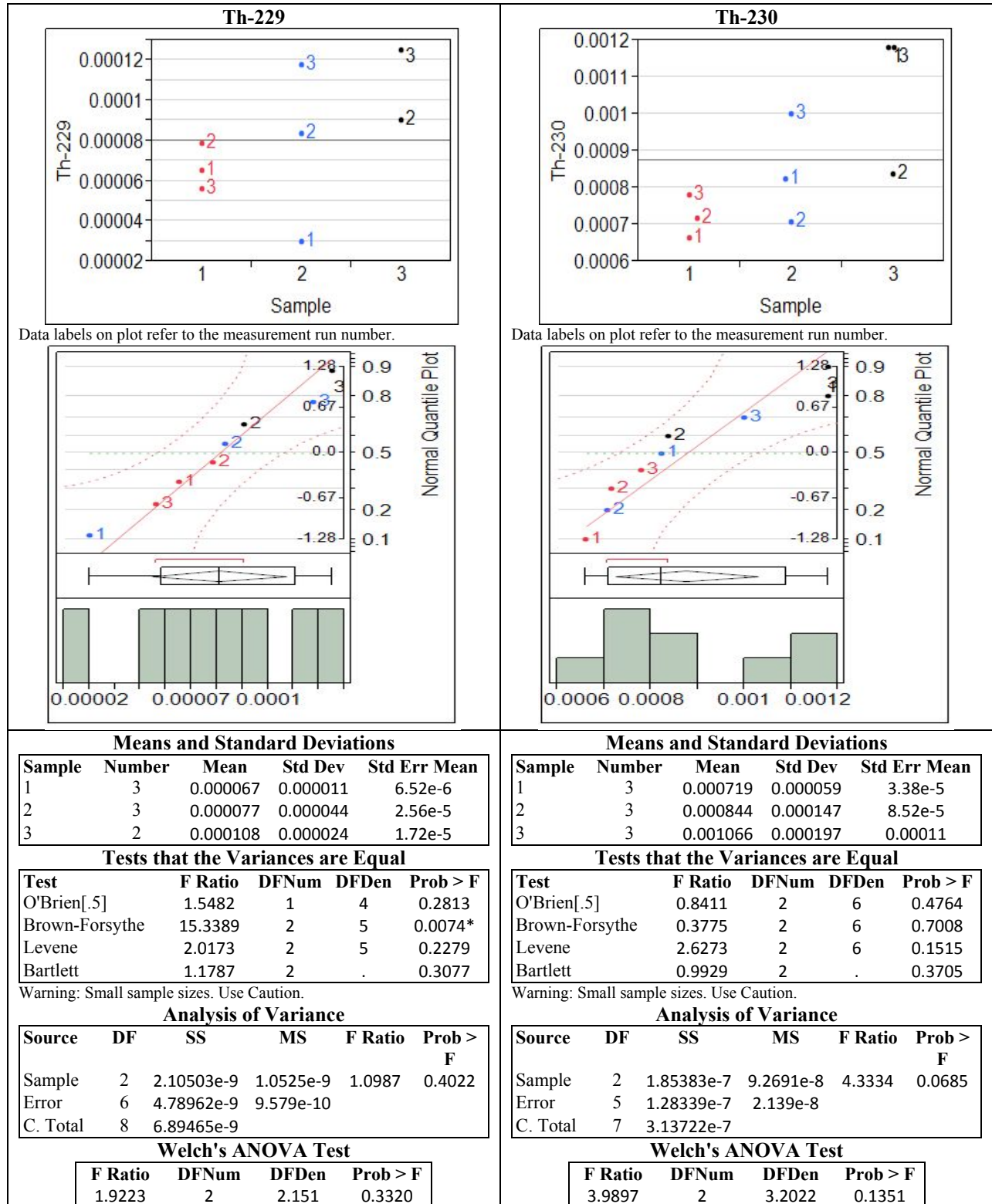
Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides

Sr-90					Tc-99						
Data labels on plot refer to the measurement run number.					Data labels on plot refer to the measurement run number.						
Means and Standard Deviations					Means and Standard Deviations						
Sample	Number	Mean	Std Dev	Std Err Mean	Sample	Number	Mean	Std Dev	Std Err Mean		
1	3	15,733.3	351.19	202.76	1	3	0.116333	0.008622	0.00498		
2	3	15,866.7	971.25	560.75	2	3	0.102267	0.019029	0.01099		
3	3	16,466.7	1,331.67	768.84	3	3	0.103167	0.020027	0.01156		
Tests that the Variances are Equal					Tests that the Variances are Equal						
Test	F Ratio	DFNum	DFDen	Prob > F	Test	F Ratio	DFNum	DFDen	Prob > F		
O'Brien[.5]	0.8964	2	6	0.4564	O'Brien[.5]	0.5709	2	6	0.5929		
Brown-Forsythe	2.9400	2	6	0.1288	Brown-Forsythe	2.7304	2	6	0.1435		
Levene	2.2231	2	6	0.1895	Levene	1.0486	2	6	0.4069		
Bartlett	1.1568	2	.	0.3145	Bartlett	0.5734	2	.	0.5636		
Warning: Small sample sizes. Use Caution.					Warning: Small sample sizes. Use Caution.						
Analysis of Variance					Analysis of Variance						
Source	DF	SS	MS	F Ratio	Prob > F	Source	DF	SS	MS	F Ratio	Prob > F
Samples	2	915,555.6	457,778	0.4836	0.6387	Sample	2	0.00037204	0.000186	0.6663	0.5479
Error	6	5680000.0	946,667			Error	6	0.00167502	0.000279		
C. Total	8	6595555.6				C. Total	8	0.00204706			
Welch's ANOVA Test					Welch's ANOVA Test						
F Ratio	DFNum	DFDen	Prob > F		F Ratio	DFNum	DFDen	Prob > F			
0.3590	2	3.1201	0.7239		0.8841	2	3.4261	0.4902			

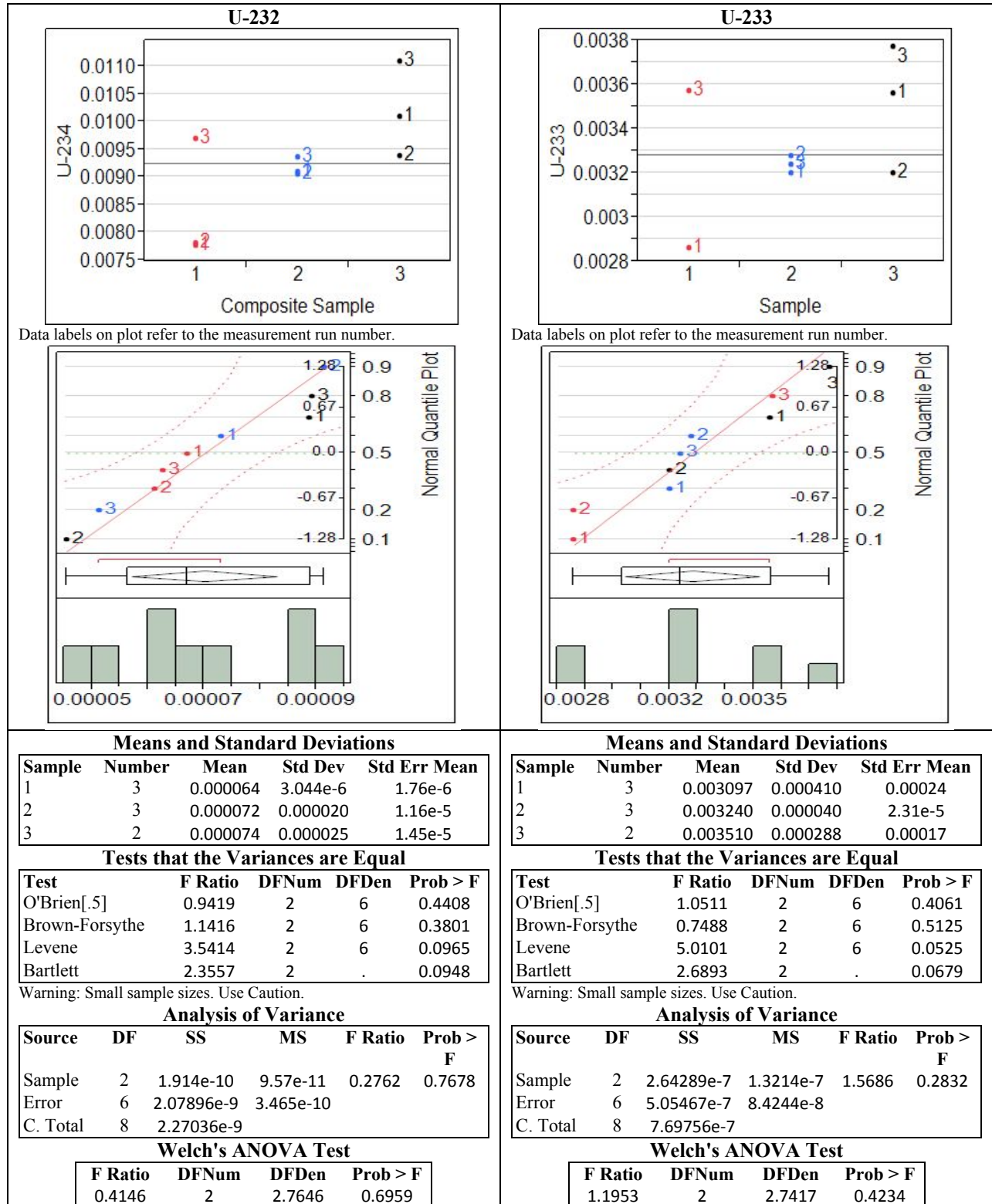
Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides



Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides



Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides

U-234					U-235						
Data labels on plot refer to the measurement run number.					Data labels on plot refer to the measurement run number.						
Means and Standard Deviations					Means and Standard Deviations						
Sample	Number	Mean	Std Dev	Std Err Mean	Sample	Number	Mean	Std Dev	Std Err Mean		
1	3	0.008423	0.001097	0.00063	1	3	0.000399	0.000049	2.85e-5		
2	3	0.009167	0.000169	0.0001	2	3	0.000424	1.732e-6	1e-6		
3	3	0.010193	0.000864	0.00050	3	3	0.000469	0.000040	2.31e-5		
Tests that the Variances are Equal					Tests that the Variances are Equal						
Test	F Ratio	DFNum	DFDen	Prob > F	Test	F Ratio	DFNum	DFDen	Prob > F		
O'Brien[.5]	0.9329	2	6	0.4438	O'Brien[.5]	0.9598	2	6	0.4348		
Brown-Forsythe	1.0223	2	6	0.4149	Brown-Forsythe	1.6631	2	6	0.2663		
Levene	3.5555	2	6	0.0958	Levene	4.0315	2	6	0.0777		
Bartlett	1.9788	2	.	0.1382	Bartlett	4.3707	2	.	0.0126*		
Warning: Small sample sizes. Use Caution.					Warning: Small sample sizes. Use Caution.						
Analysis of Variance					Analysis of Variance						
Source	DF	SS	MS	F Ratio	Prob > F	Source	DF	SS	MS	F Ratio	Prob > F
Sample	2	4.73949e-6	2.3697e-6	3.5936	0.0942	Sample	2	7.62689e-9	3.8134e-9	2.8301	0.1362
Error	6	3.9566e-6	6.5943e-7			Error	6	8.08467e-9	1.3474e-9		
C. Total	8	8.69609e-6				C. Total	8	1.57116e-8			
Welch's ANOVA Test					Welch's ANOVA Test						
F Ratio	DFNum	DFDen	Prob > F		F Ratio	DFNum	DFDen	Prob > F			
2.2526	2	2.8235	0.2601		1.8485	2	2.6749	0.3132			

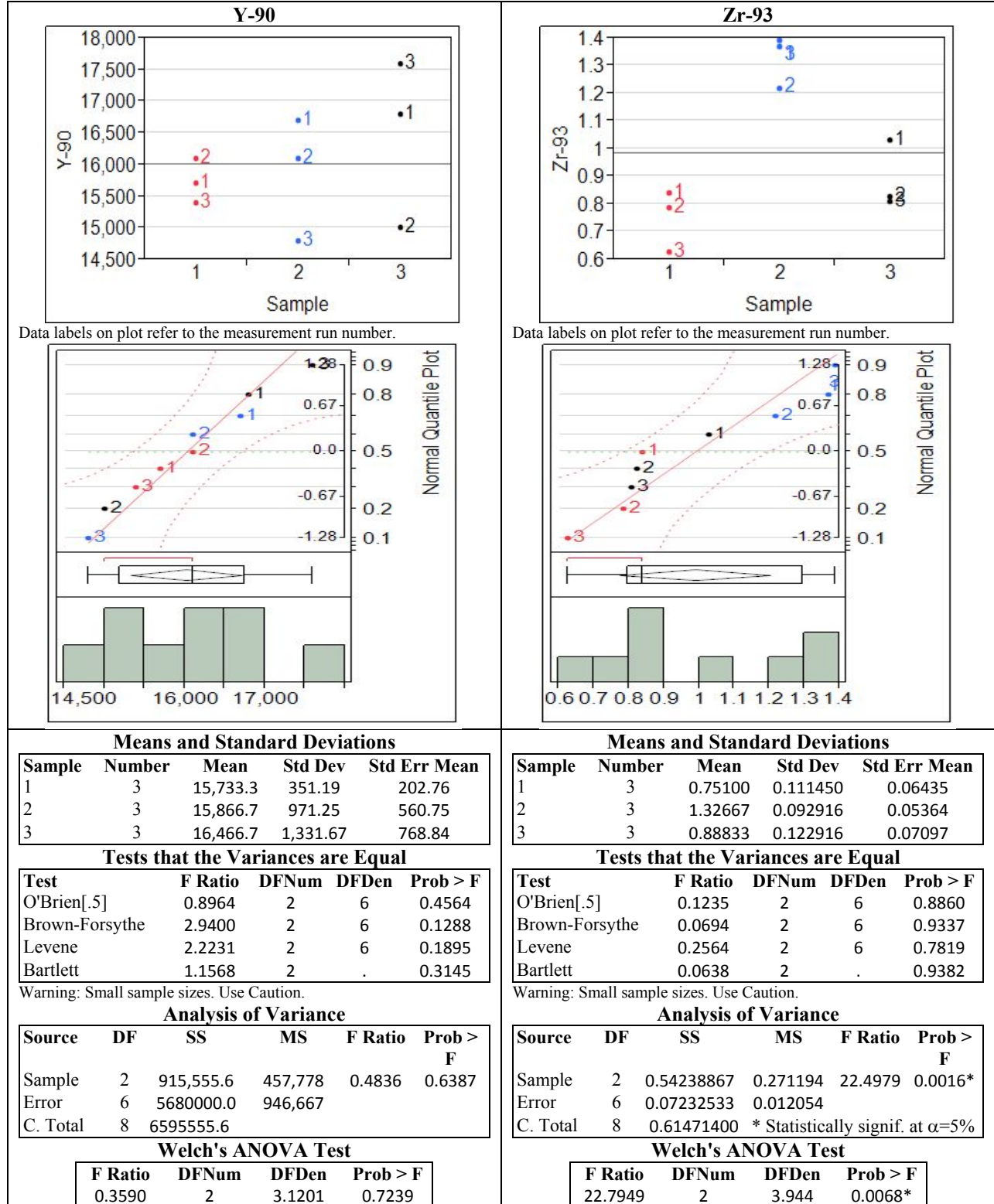
Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides

U-236					U-238						
Data labels on plot refer to the measurement run number.					Data labels on plot refer to the measurement run number.						
Means and Standard Deviations					Means and Standard Deviations						
Sample	Number	Mean	Std Dev	Std Err Mean	Sample	Number	Mean	Std Dev	Std Err Mean		
1	3	0.000503	0.000061	3.55e-5	1	3	0.013200	0.000361	0.00021		
2	3	0.000526	0.000013	7.54e-6	2	3	0.012867	0.001097	0.00063		
3	3	0.000566	0.000052	0.00003	3	3	0.016000	0.000300	0.00017		
Tests that the Variances are Equal					Tests that the Variances are Equal						
Test	F Ratio	DFNum	DFDen	Prob > F	Test	F Ratio	DFNum	DFDen	Prob > F		
O'Brien[.5]	0.8455	2	6	0.4748	O'Brien[.5]	1.4442	2	6	0.3076		
Brown-Forsythe	0.8573	2	6	0.4705	Brown-Forsythe	0.2703	2	6	0.7720		
Levene	2.8555	2	6	0.1345	Levene	6.0436	2	6	0.0365*		
Bartlett	1.5030	2	.	0.2225	Bartlett	1.6578	2	.	0.1906		
Warning: Small sample sizes. Use Caution.					Warning: Small sample sizes. Use Caution.						
Analysis of Variance					Analysis of Variance						
Source	DF	SS	MS	F Ratio	Prob > F	Source	DF	SS	MS	F Ratio	Prob > F
Sample	2	6.01867e-9	3.0093e-9	1.3532	0.3273	Sample	2	0.00001777	8.8844e-6	18.7260	0.0026*
Error	6	1.33433e-8	2.2239e-9			Error	6	0.00000285	4.7444e-7		
C. Total	8	1.9362e-8				C. Total	8	0.00002062			* Statistically signif. at α=5%
Welch's ANOVA Test					Welch's ANOVA Test						
F Ratio	DFNum	DFDen	Prob > F		F Ratio	DFNum	DFDen	Prob > F			
0.8580	2	2.9306	0.5089		49.1135	2	3.6145	0.0024*			

Appendix C: Statistical Results for Radionuclide Constituents

Table 25 Tests and Estimators for Radionuclides



Appendix C: Statistical Results for Radionuclide Constituents

Table 26 Radionuclide Concentrations with All Results below Their MDCs

	MDCs	
	Min	Max
Ac-227	7.21E-06	4.59E-05
Cf-249	4.38E-03	9.95E-03
Cm-243	5.18E-01	1.45E+00
Cm-247	1.62E-07	2.76E-07
Cm-248	8.33E-06	2.39E-05
Eu-152	1.46E-01	1.91E-01
H-3	2.00E-02	2.17E-02
Nb-94	1.01E-03	2.15E-03
Pa-231	4.08E-04	1.02E-03
Pu-244	5.75E-07	7.89E-07
Ra-226	2.55E-03	4.35E-03
Sb-126	9.41E-02	1.17E-01
Sb-126m	9.41E-02	1.17E-01
Sn-126	6.26E-01	7.97E-01

Appendix C: Statistical Results for Radionuclide Constituents

Table 27 95% UCLs for Mean Concentrations of Radionuclide Constituents with All Results above Their MDCs

Radionuclide	Model Type	N	Mean	Standard Deviation	Percent Std Dev	UCL95	Notes
Am-241	Sampling Error	9	6.848e+1	1.182e+1	17.3%	8.767e+1	Normal
Am-242m	No Sampling Error	9	1.169e-1	1.692e-2	14.5%	1.274e-1	Normal: Student's t UCL
Am-243	Sampling Error	9	1.471e+0	3.539e-1	24.1%	2.054e+0	Normal
Ba-137m	No Sampling Error	9	5.132e+2	1.785e+1	3.5%	5.243e+2	No discernable dist: Student's t UCL
C-14	No Sampling Error	9	1.784e-2	5.299e-3	29.7%	2.113e-2	Normal: Student's t UCL
Cm-244	Sampling Error	9	5.544e+1	8.147e+0	14.7%	6.855e+1	Normal
Cm-245	Sampling Error	9	5.476e-3	8.924e-4	16.3%	6.897e-3	Normal
Co-60	Sampling Error	9	7.557e+0	8.023e-1	10.6%	8.862e+0	Normal
Cs-135	No Sampling Error	9	2.743e-3	1.348e-4	4.9%	2.827e-3	Normal: Student's t UCL
Cs-137	No Sampling Error	9	5.428e+2	1.891e+1	3.5%	5.545e+2	No discernable dist: Student's t UCL
Eu-154	Sampling Error	9	1.766e+1	2.620e+0	14.8%	2.202e+1	Normal
I-129	Sampling Error	9	1.593e-4	2.819e-5	17.7%	2.047e-4	Normal
Ni-59	No Sampling Error	9	4.410e+0	1.048e+0	23.8%	5.060e+0	Normal: Student's t UCL
Ni-63	No Sampling Error	9	3.183e+2	9.082e+1	28.5%	3.746e+2	Normal: Student's t UCL
Np-237	Sampling Error	9	1.981e-2	8.064e-3	40.7%	3.191e-2	Normal
Pu-238	No Sampling Error	9	3.312e+0	2.748e-1	8.3%	3.483e+0	Normal: Student's t UCL
Pu-239	No Sampling Error	9	2.916e+0	1.907e-1	6.5%	3.034e+0	Normal: Student's t UCL
Pu-240	No Sampling Error	9	1.814e+0	1.250e-1	6.9%	1.892e+0	Normal: Student's t UCL
Pu-241	No Sampling Error	9	6.738e+0	4.636e-1	6.9%	7.025e+0	Normal: Student's t UCL
Pu-242	No Sampling Error	9	2.184e-3	1.290e-4	5.9%	2.264e-3	Normal: Student's t UCL

Appendix C: Statistical Results for Radionuclide Constituents

Table 27 Continued. 95% UCLs for Mean Concentrations of Radionuclide Constituents with All Results above Their MDCs

Radionuclide	Model Type	N	Mean	Standard Deviation	UCL95	Percent Standard Deviation	Notes
Se-79	No Sampling Error	9	1.516e-2	7.596e-3	2.028e-2	50.1%	Gamma: Gamma UCL
Sm-151	No Sampling Error	9	2.050e+2	8.367e+0	2.102e+2	4.1%	Normal: Student's t UCL
Sr-90	No Sampling Error	9	1.602e+4	9.080e+2	1.659e+4	5.7%	Normal: Student's t UCL
Tc-99	No Sampling Error	9	1.073e-1	1.600e-2	1.172e-1	14.9%	Normal: Student's t UCL
Th-229	No Sampling Error	8	8.079E-5	3.138e-5	1.018e-4	38.8%	Normal: Student's t UCL
Th-230	No Sampling Error	9	8.762e-4	1.980e-4	9.990e-4	22.6%	Normal: Student's t UCL
U-232	No Sampling Error	9	7.002e-5	1.685e-5	8.046e-5	24.1%	Normal: Student's t UCL
U-233	No Sampling Error	9	3.282e-3	3.102e-4	3.474e-3	9.5%	Normal: Student's t UCL
U-234	No Sampling Error	9	9.261e-3	1.043e-3	9.907e-3	11.3%	Normal: Student's t UCL
U-235	No Sampling Error	9	4.308e-4	4.432e-5	4.582e-4	10.3%	Normal: Student's t UCL
U-236	No Sampling Error	9	5.317e-4	4.920e-5	5.622e-4	9.3%	Normal: Student's t UCL
U-238	Sampling Error	9	1.402e-2	1.810e-3	1.692e-2	12.9%	Normal
Y-90	No Sampling Error	9	1.602e+4	9.080e+2	1.659e+4	5.7%	Normal: Student's t UCL
Zr-93	Sampling Error	9	9.887e-1	3.137e-1	1.496e+0	31.7%	Normal

Notes: All sampling error models were fitted in JMP® statistical software. The no sampling error models were fit in ProUCL 4.1