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**THREE-DIMENSIONAL SIMULATION OF GROUNDWATER FLOW AND TRANSPORT  
OF CHEMICAL AND LOW-LEVEL RADIOACTIVE CONSTITUENTS WITHIN  
TWO PRODUCTION AREAS OF THE SAVANNAH RIVER PLANT**

by

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#### INTRODUCTION

To assist in the assessment of the impacts of waste management activities at the Savannah River Plant (SRP), modeling of transport in the environmental media was performed. Predicting the future performance of any waste site or facility and postulated actions in terms of migration of potential hazardous materials requires mathematical models capable of simulating flow and transport in the groundwater. Three-dimensional groundwater flow and transport models were developed to simulate the groundwater movement and contaminant transport in two specific production areas, the Raw Materials Fabrication Area and the Separations Area, on SRP (Figures 1 and 2). The overall objective of the analysis was to develop groundwater flow models that could be used to quantify the rate and direction of the groundwater movement from the waste sites to points of discharge.

The USGS Modular 3D model (McDonald & Harbaugh, 1984) uses the strongly implicit procedure to solve sets of simultaneous finite-difference equations that represent the groundwater flow process. The transport functions, which are the concentration or mass flux at time  $t$  due to continuous injection starting at time  $t'$ , were obtained by solving the three-dimensional advection-dispersion equations using the Sandia Waste Isolation Flow & Transport (SWIFT) model (Reeves & Cranwell, 1981).

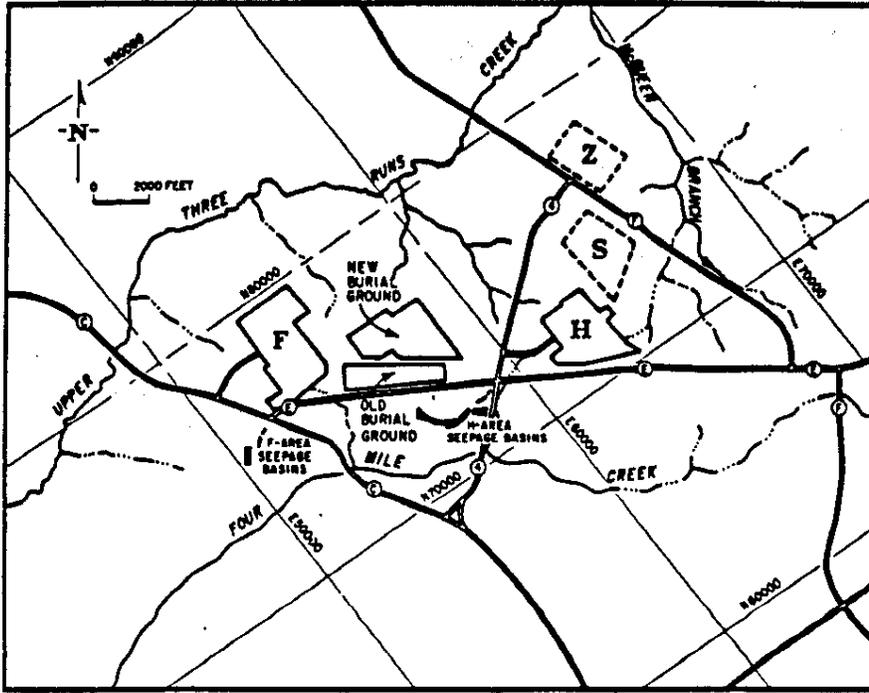


FIGURE 1. Location Map of General Separation Area, SRP

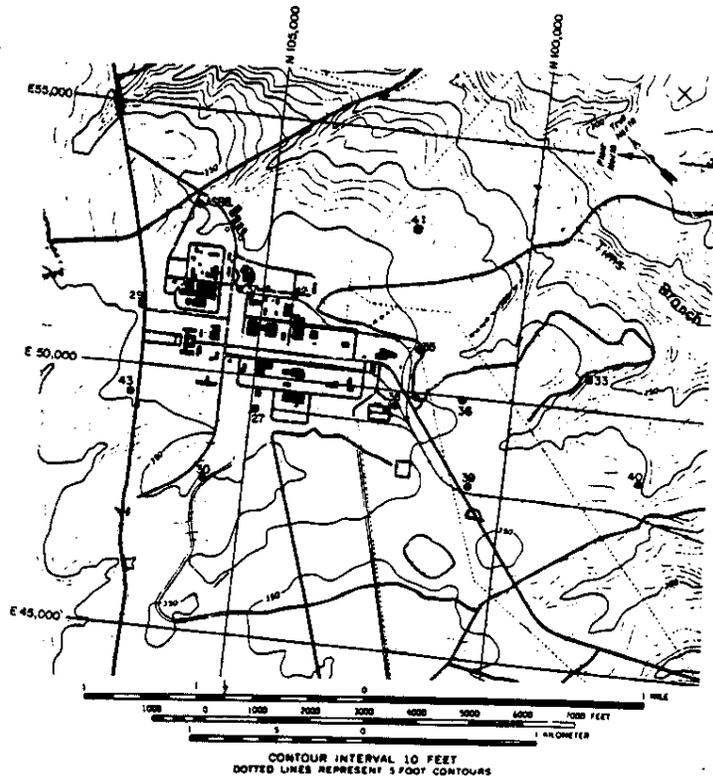


FIGURE 2. Location Map of Raw Materials Fabrication Area

## CONCEPTUAL MODEL OF THE SITE AREAS

A compilation and review of the available hydrogeologic data was performed to provide the framework for the conceptual model of the sites. This information primarily included geologic data, well locations, water levels, water quality, and pumping rates for production wells.

From these data conceptual models of the groundwater flow systems were developed to generate the relevant properties and conditions of the real flow systems in a form suitable for treatment by mathematical models. The development of the conceptual model requires a knowledge of the hydrology and geology of the physical system. Simplifying assumptions were carefully selected to accommodate data uncertainties and the complex spatially and temporally variable hydrologic parameters. Boundary conditions are chosen to represent accurately the system and facilitate mathematical treatment.

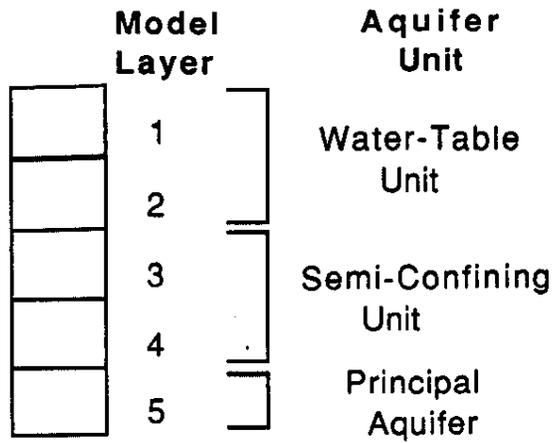
The groundwater system beneath the Raw Materials Fabrication Area was divided into five hydrologic intervals, referred to as layers. This subdivision was chosen to provide a reasonable resolution of the vertical groundwater flow patterns. The selected intervals are shown in Figure 3. The areal extent of the modeled areas is shown in Figure 4 and are described in detail in S. S. Papadopoulos (1986).

The conceptual model of the hydrogeologic system at the Separations Area consisted of seven hydrogeologic (four aquifers and three aquitards) units shown in Figure 5. The areal extent and finite difference grid used in the study area is detailed in Duffield et al. (1986) and shown in Figure 6.

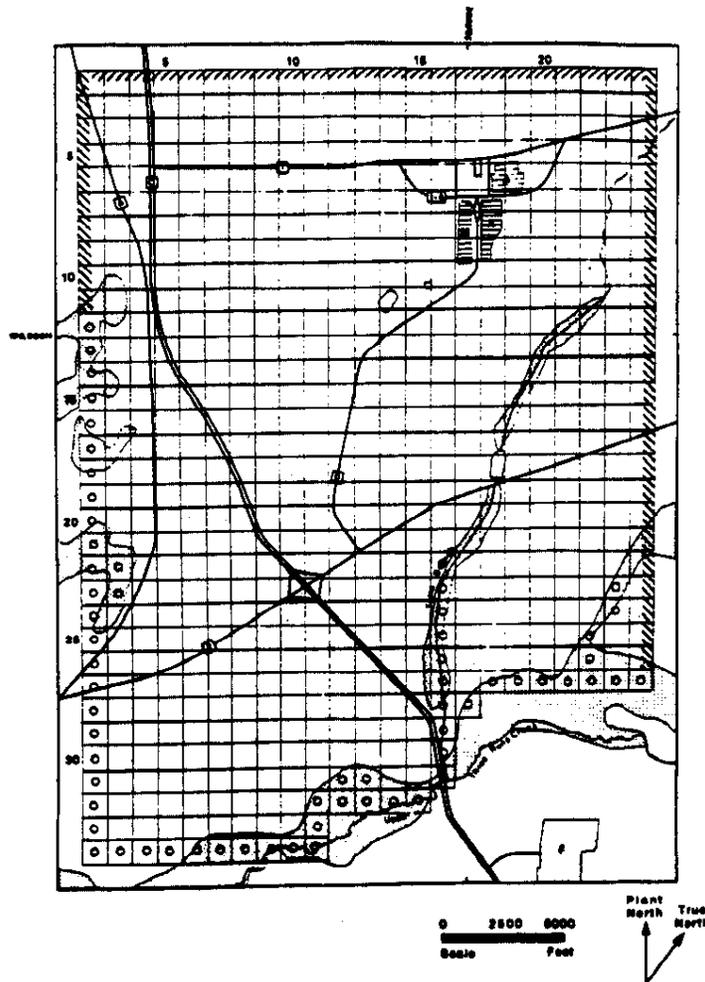
In the conceptual models the confining layers were represented by leakance coefficients accounting for vertical conductivity and saturated thickness in the aquitards. This quasi three-dimensional approach assumes approximately horizontal flow in the aquifers and vertical flow and no storage in the confining beds.

### MODEL CALIBRATION

Calibration of groundwater flow models is the process of obtaining a reasonable match between observed hydrologic data and results calculated by the numerical model. The calibration procedure was carried out by varying estimates of the hydraulic properties from a set of initial values until the best fit of calculated results to observed calibration targets was achieved.



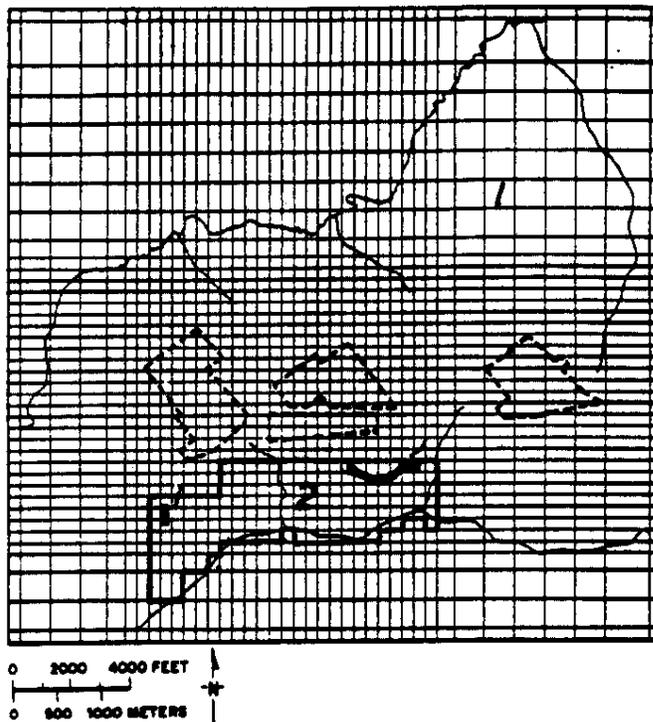
**FIGURE 3. Vertical Discretization in Regional Flow Model at Raw Materials Fabrication Area**



**FIGURE 4. Finite Difference Grid for the Regional Flow Model at Raw Materials Fabrication Area**

	<u>MODEL LAYER</u>	<u>AQUIFER UNIT</u>	<u>UNDERLYING CONFINING UNIT / TYPE</u>
•	1	Barnwell	Ten Clay / aquitard
•	2	McBean	Green Clay / aquitard
•	3	Congaree	Ellenton Clay / aquitard
•	4	Upper Tuscaloosa	Middle Clay / aquiclude

**FIGURE 5. Vertical Discretization in Regional Flow Model at Separations Area**



**FIGURE 6. Finite Difference Grid for the Regional Flow Model at Separations Area**

In this study, observed hydraulic head and stream base flow measurements were used as calibration targets. The hydraulic parameters derived from the calibration process for each layer were used in the final modeling of the flow and transport. The results of the parameter estimation for the two areas are shown in Tables 1 and 2.

## RESULTS

The three-dimensional numerical models were used to determine the flow directions, velocities, and outcrop concentrations in the two specific production areas. The flow path and velocity data obtained provided information for the PATHRAE runs (analytical model use to calculate health risk from groundwater transport). Transport calculations of a few specific species were then run for comparison with the results obtained from PATHRAE.

The comparison runs were made for the two SRP locations, the Raw Materials Fabrication Area and the Separations Area. A brief description of the sites, the model input data, and example output data are described in Looney et al. (1986). The facility input parameters were defined to be common for the modeling approaches.

The results of the model comparison for selected constituents from the two areas are shown in Figure 7. Three groundwater velocities were assessed using PATHRAE to aid in data interpretation; because of the nature of the three-dimensional numerical models, the composite velocity (transport distance/transport time) varies for each receptor. In each case, the slowest velocity ( $V_{\min}$ ) is the velocity to the 1 m well, the highest velocity ( $V_{\max}$ ) is the velocity to the outcrop, and the intermediate velocity ( $V_{\text{nom}}$ ) was the velocity to the 100 m well.

In all cases, PATHRAE predicted higher peak concentrations, however, the PATHRAE predictions decreased more rapidly following the peak. The concentrations were generally one to three orders of magnitude below the peak when the PATHRAE predictions first decreased below those of the numerical models. Based on these data,  $V_{\text{nom}}$  was selected for the analysis, and the outcrop distance was adjusted so that the peak would occur in the correct year. The behavior of the results is entirely consistent with expectations and the model formulations.

## ACKNOWLEDGMENT

The information contained in this article was developed during the course of work under Contract No. DE-AC09-76SR00001 with the U.S. Department of Energy.

**TABLE 1**

**Summary of Final Estimates of Hydraulic Parameters Used in the Flow Model of the Raw Materials Fabrication Area**

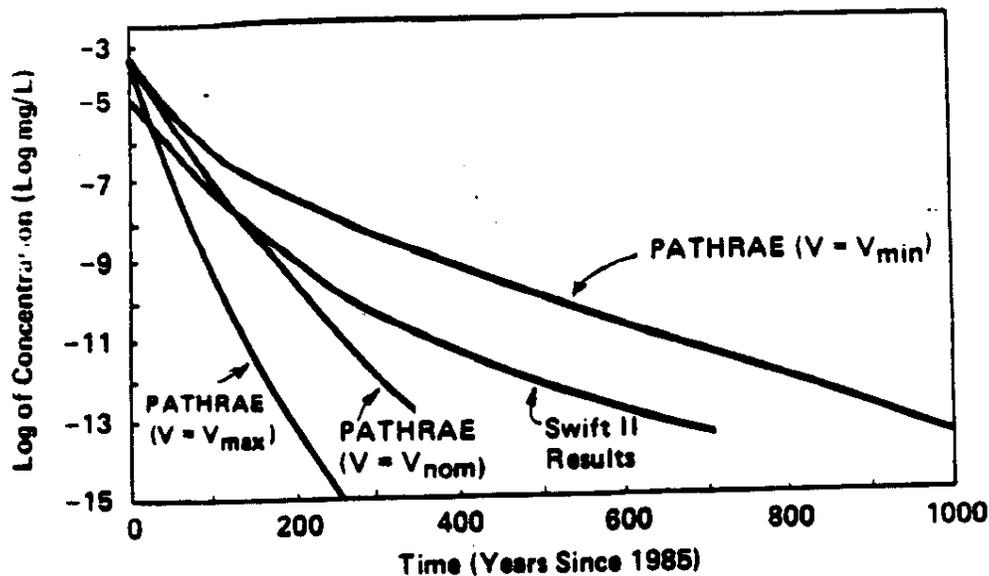
<u>Layer</u>	<u>Transmissivity (ft<sup>2</sup>/day)</u>	<u>Hydraulic Conductivity (ft/day)</u>	<u>Leakance Coefficient (day)<sup>-1</sup></u>
1	175	9	
1-2			3.5 x 10 <sup>-4</sup>
2	2,200	46	
2-3			4.0 x 10 <sup>-4</sup>
3	1,300	35	
3-4			2.7 x 10 <sup>-4</sup>
4	1,600	29	
4-5			6.0 x 10 <sup>-5</sup>
5	12,500	73	

**TABLE 2**

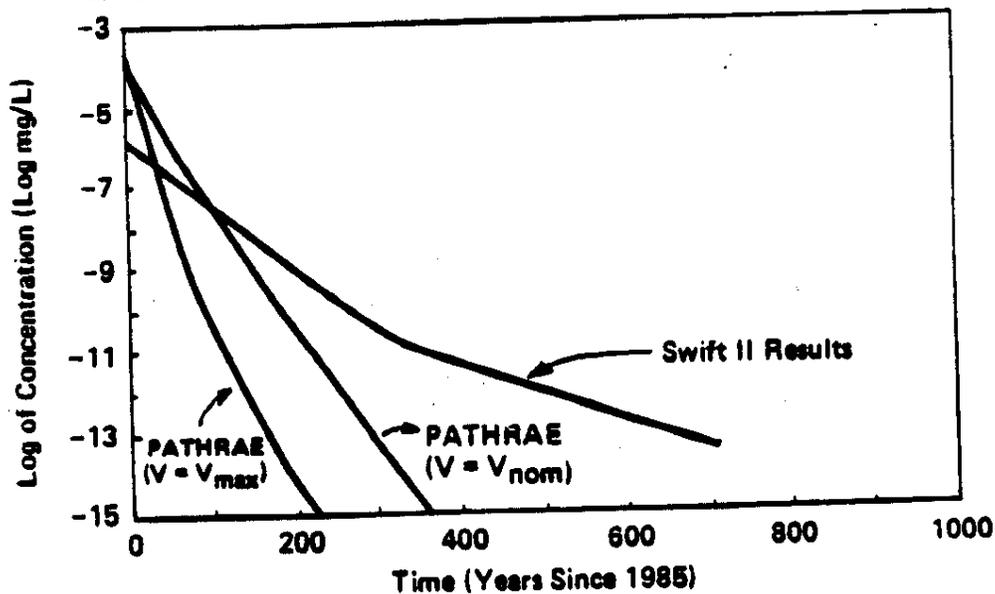
**Summary of Final Estimates of Hydraulic Parameters Used in the Flow Model of the Separations Area**

<u>Layer</u>	<u>Transmissivity (ft<sup>2</sup>/day)</u>	<u>Hydraulic Conductivity (ft/day)</u>	<u>Leakance Coefficient (day)<sup>-1</sup></u>
1		0.8 (Zone 1) 3.6 (Zone 2)	
1-2			5.5 x 10 <sup>-4</sup> (Zone 1) 2.4 x 10 <sup>-4</sup> (Zone 2)
2		4.1	
2-3			4.4 x 10 <sup>-5</sup> (Zone 1) 1.7 x 10 <sup>-5</sup> (Zone 2)
3	3,800		
3-4			4.7 x 10 <sup>-11</sup>
4	9,810		

a) Calculated Nickel Concentrations in the 1 m Well for a Test Waste Site



b) Calculated Nickel Concentrations in the 100 m Well for a Test Waste Site



**FIGURE 7.** Comparison of PATHRAE Results to Multidimensional Model  
 a) at 1 m well, b) at 100 m well. Various flow velocities were tested where  $V_{min} < V_{nom} < V_{max}$ , and  $V_{nom}$  was the nominal value.

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- Duffield, G. M., D. R. Buss, R. W. Root, Jr., S. S. Hughes, and J. W. Mercer, 1986. **Characterization of Groundwater Flow and Transport in the General Separations Area Savannah River Plant, Flow Model Refinement and Particle-Tracking Analysis**, CORR-86-0031, Report by GeoTrans, Inc., for E. I. du Pont de Nemours and Company, Savannah River Laboratory, Aiken, SC.
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- Reeves, M., and R. M. Cranwell, 1981. **User's Manual for the Sandia Waste-Isolation Flow and Transport Model (SWIFT)**, SAND81-2516, Sandia National Laboratories, Albuquerque, NM.



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August 7, 1987

Ms. Marjorie Clearwater  
Low-Level Waste Management Program  
EG&G Idaho, Inc.  
P. O. Box 1625  
Idaho Falls, ID 83415

Dear Ms. Clearwater:

The camera-ready masters and one copy of each of three summary papers for the Denver conference are enclosed. The papers are: "Pathway Analysis Models Used for Assessment of Forty-Five Waste Site Areas at the Savannah River Plant" (DP-MS-87-79) by B. B. Looney, et al., "Three-Dimensional Simulation of Groundwater Flow and Transport of Chemical and Low-Level Radioactive Constituents Within Two Production Areas of the Savannah River Plant" (DP-MS-87-81) by D. E. Stephenson, et al., and "Summary of Environmental Impacts and Costs for Waste site Closure Options at the Savannah River Plant" (DP-MS-87-82) by W. F. Johnson and R. A. Moyer.

If we can be of further assistance, please let me know.

Yours very truly,

L. W. Ice, Process Editor  
Site Services Department

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Enclosures

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J. C. Corey-D. E. Gordon, 773-A  
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File: (DP-MS-87-81)

July 21, 1987

Mr. J. R. Powell, Technical Information Officer  
U. S. Department of Energy  
Savannah River Operations Office  
Aiken, SC 29801

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DP-MS-87-81, "THREE-DIMENSIONAL SIMULATION OF GROUNDWATER FLOW AND TRANSPORT OF CHEMICAL AND LOW LEVEL RADIOACTIVE CONSTITUENTS WITHIN TWO PRODUCTION AREAS OF THE SAVANNAH RIVER PLANT", By D. E. Stephenson, B. B. Looney, C. B. Andrews, and D. R. Buss.

A paper proposed for presentation at the Ninth Annual DOE Low-Level Radioactive Waste Management Conference on August 25-27, 1987 in Denver, Colorado.

Technical questions pertaining to the contents of this document should be addressed to the author(s) or

J. C. Corey, Research Manager  
Environmental Sciences Division  
Savannah River Laboratory

Questions concerning processing of this document should be addressed to the AED Classification Officer & Patent Reviewer at Extension 52606.

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AUTHOR(S) D. E. Stephenson, B. B. Looney, C. B. Andrews, and D. R. BussTITLE "Three-Dimensional Simulation of Groundwater Flow and Transport of Chemical And  
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Author(s): D. E. Stephenson, B. B. Looney, C. B. Andrews, and D. R. Buss

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